

## Magnetic hysteresis

Maxwell equations in presence of matter:

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

→ This is always true

→  $\vec{B}$  is the actual magnetic field that exists

→  $\vec{J}$  is the total current that acts as source of  $\vec{B}$ .

When looking at the magnetic response of a material, it is convenient to think of the source term  $\vec{J}$  to be comprising of two parts.

$$\vec{J} = \vec{J}_{\text{free}} + \vec{J}_{\text{bound}}$$

& consequently define two more fields,  $\vec{H}$  &  $\vec{M}$  such that

$$\vec{\nabla} \times \vec{H} = \vec{J}_{\text{free}}$$

$$\vec{\nabla} \times \vec{M} = \vec{J}_{\text{bound}}$$

$\vec{H}$  is thus the field generated by an electromagnet that  $\vec{J}$  can control by turning a knob controlling the current.

$\vec{J}_{\text{free}}$  is the current that goes through wires (or in free space), in principle under our control.

$\vec{M}$ : Magnetization of the material whose source is actually in the magnetic moment associated with electrons  $\oplus$  orbitals & spin. To be able to include it in Maxwell equations (classical), we just treat this as an additional current,  $\vec{J}_{\text{new}}$

$$\Rightarrow \vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

$$\Leftrightarrow \vec{\nabla} \times (\vec{H} + \vec{M}) = \vec{J}_{\text{free}} + \vec{J}_{\text{bound}}$$

with

$$\vec{B} = \mu_0 (\vec{H} + \vec{M})$$

or alternatively, we could trivially define another quantity

$$\vec{J} = \mu_0 \vec{M} \quad [ \text{Sorry about having similar symbols for two very different quantities} ]$$

Note that the above relationship is always valid.

We also usually encounter an additional relationship, that of linear response between the magnetization & the applied field. This is especially true for paramagnetic & diamagnetic materials.

Linear response [not always valid]

$$\vec{M} = \chi \vec{H}$$

$$\Rightarrow \vec{B} = \mu_0 (\vec{H} + \chi \vec{H}) = \mu_0 (1 + \chi) \vec{H}$$

$$\vec{B} = \mu_0 \mu_r \vec{H}$$

$\chi$  - +ve & small for paramagnetic materials

$\chi$  - -ve & very small & diamagnetic materials

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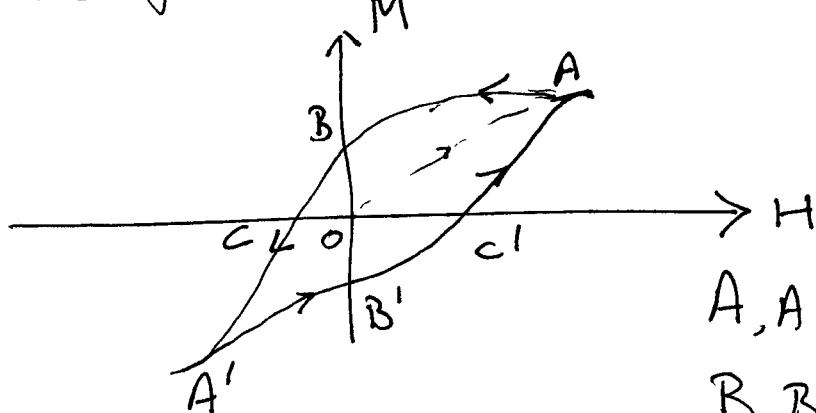
In the statistical mechanics course, we had calculated  $\chi$  for simple systems.

• Paramagnetism — Langevin, Brillouin, Pauli

Diamagnetism — Landau Diamagnetism (free electron orbital diamagnetism (for zero angular momentum states)).

In this experiment, we will be focussing on ferromagnetic materials. These have a spontaneous magnetization below the Curie temperature. Ising model very crudely tries to approximate this phenomenon (not very successfully). [Spin is not a classical variable, components of spin don't commute & obviously spin is not just  $\pm 1$ ].

→ Aim of the experiment: Measure the  $M(H)$  curve for a ferromagnet.



A, A': Saturation

B, B': Remanence

C, C': Coercivity

Hysteresis: History dependent magnetization.

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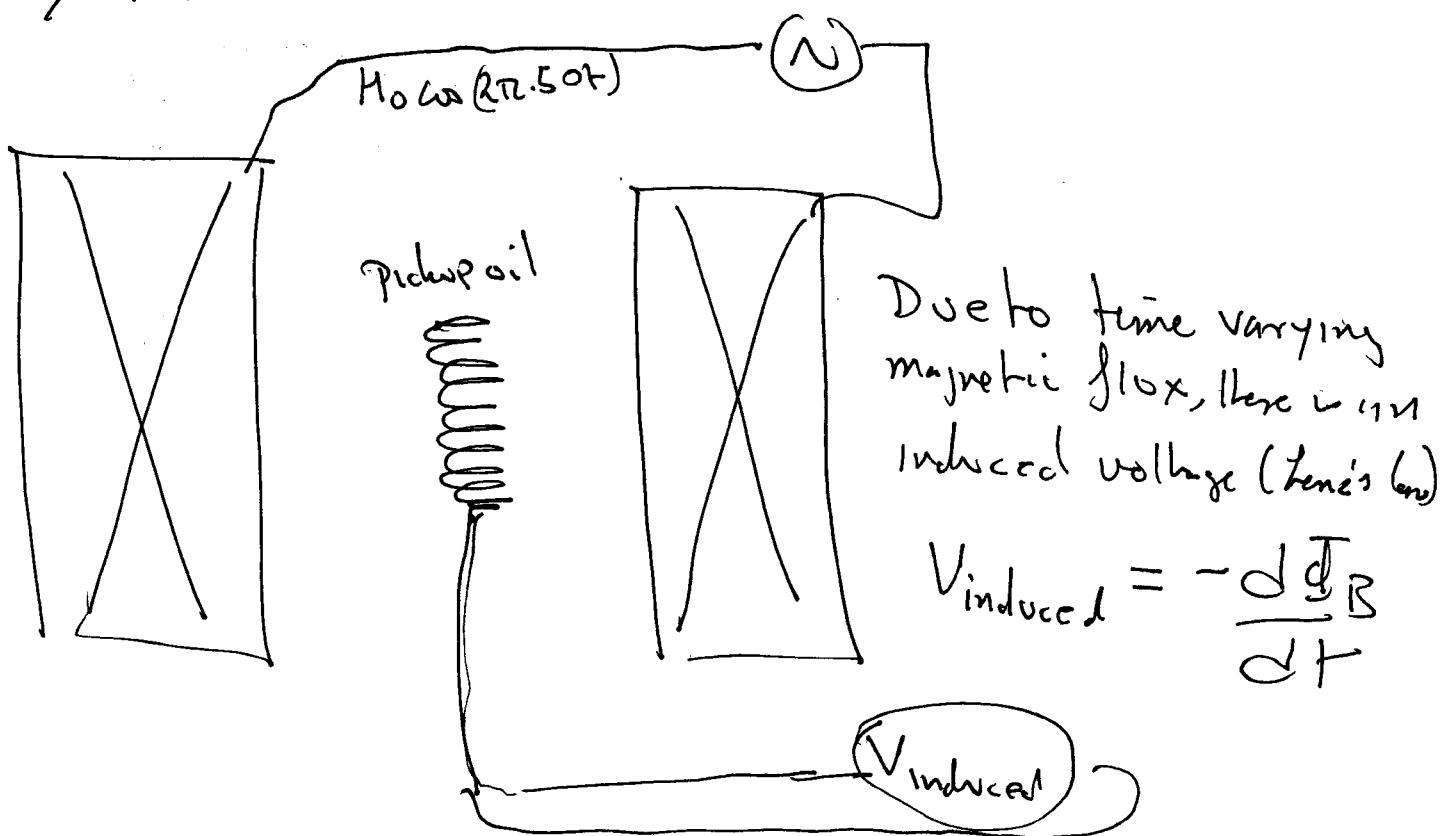
Basic Idea: Using a long solenoid whose current we can control to generate a homogeneous magnetic field that is time varying.

Applied magnetic field,

$$H_a(t) = H_0 \cos(2\pi \cdot 50t)$$

A 50 Hz a.c magnetic field is generated by passing a 50 Hz ac current.

→ Next we have a pickup coil, essentially another very small solenoid such that when inserted within the larger solenoid, the magnetic field it experiences is more or less uniform to the precision required.



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$$\text{Now with } \oint_B = \text{Area} * B \\ = \text{Area} * [\mu_0(H + M)]$$

$\Rightarrow$  By measuring the induced voltage within the pick up coil with a ferromagnetic sample inside the pick up, we can establish the value of magnetization,  $M$ , ~~and~~

$$H_a(t) = H_0 \cos(2\pi \cdot 50 t)$$

$$V_{\text{ind}} = - \text{Area} * \frac{d}{dt} (\mu_0 [H_a(t) + M(t)])$$

Substitute  $e_1$  &  $e_3$   
 $\Rightarrow$

$$\begin{aligned} e_y &= -g_y C_1 H_a + g_y e_3 \\ &= -g_y C_1 H_a + g_y \frac{g_1 A_c}{\omega} \mu_0 H + g_y \frac{g_1 A_s}{\omega} J \end{aligned}$$

Now convert  $H_a$  to  $H$  using ①

$$\begin{aligned} &= -g_y C_1 H - g_y C_1 NM + g_y \frac{g_1 A_c \mu_0}{\omega} H \\ &\quad + g_y \frac{g_1 A_s}{\omega} \mu_0 M \end{aligned}$$

Convert  $H$  to  $H_a$ :  $H = H_a - NM$

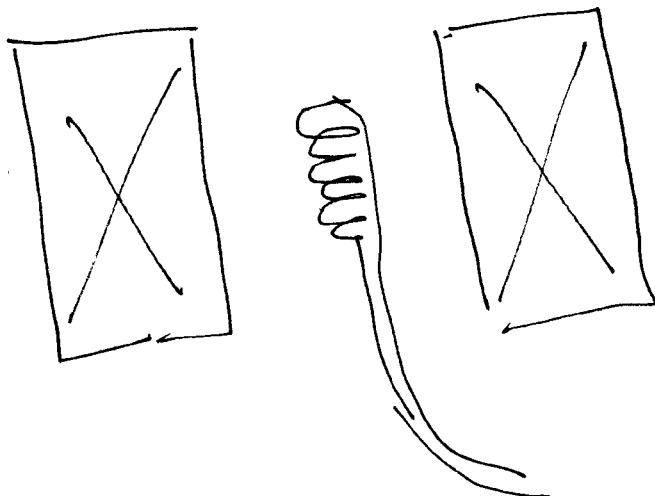
$\Rightarrow$

$$e_y = \left[ -g_y C_1 H_a + g_y \frac{g_1 A_c H_a \mu_0}{\omega} \right] \\ \left[ -NM \frac{g_y g_1 A_c}{\omega} + g_y g_1 A_s \mu_0 M \right]$$

First two terms have  $H_a$  & the other two terms have  $M$

$\rightarrow$  Choose  $C_1$  such that the first two terms cancel.

## Basic Idea



① → A long solenoid generates a time dependent magnetic field,  $H(t) = H_0 \cos \omega t$   
 $\omega = (2\pi \times 50) \frac{\text{rad}}{\text{sec}}$

→ A small pick up coil measures the induced voltage. The sample is placed inside the pick up coil.

Aim: We want to plot  $M$  vs  $H$  for the sample.

→ What is measured is  $H$  vs  $t$  → channel 1  
 $M$  vs  $t$  → channel 2

→ Use "xy mode" to eliminate time & directly plot  $M$  vs  $H$ .

Magnetization is measured using Lenz's law:

Induced voltage ( $e_2$ )

$$e_2 = - \frac{\partial \Phi_B}{\partial t} = - \frac{2}{\partial t} [A_c \mu_0 H(t) + A_s M_0]$$

Signal on the  $y$ -axis (channel 2)

→ This should be the time dependent magnetization of the sample, following the applied magnetic field.

Signal on the  $x$ -axis (channel 1)

→ The magnetic field seen by the sample

= (magnetic field in the solenoid) - demagnetizing

→ Channel 2

Pick up voltage — the signal from empty coil.

① we need to modify  $e_2$  such that the  $H(t)$  part of the  $e_2$  signal is completely eliminated & we only have a signal proportional to  $M(t)$

So ① Integrate  $e_2 \rightarrow e_3 = - \int e_2 dt$

② Phase shift  $e_3$  such that the signal is in phase with the magnetic field.

[Since  $H = H_0 \cos \omega t$

$$\frac{\partial H}{\partial t} \propto \frac{H_0}{\omega} \cos(\omega t + \phi);$$

→ The phase knob brings  $\phi$  to zero

③ ~~Adjust~~ Subtract a fraction of the field signal,  $H_0$  so that only the magnetization part survives in ~~the~~ in  $e_3$ .

④

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$$H = H_a - NM$$

; N: demagnetization factor

H: the field the sample sees is less than what is applied by a constant factor N, called the demagnetization factor.

$$H = H_0 \cos \omega t ; \omega = (2\pi \times 50) \text{ rad/sec}$$

There is a circuit that generates a voltage  $e_1$  proportional to the applied field  $H_a$ .

$$e_1 = C_1 H_a$$

$$B = \mu_0 H + J$$

$$\Phi_B = A_c \mu_0 H + A_s J$$

The induced voltage

$$e_2 = - \frac{\partial \Phi_B}{\partial t}$$

This signal is integrated & phase shifted with an operational amplifier of gain  $g_1$ .

$$e_3 = -g_1 \int e_2 dt$$

$$e_3 = g_1 \frac{A_c H \mu_0}{\omega} + g_1 \frac{A_s J}{\omega} \quad \begin{array}{l} \text{After a phase shift:} \\ H \& J \text{ are periodic signals} \end{array}$$

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Now, there is a differential amplifier with gain  $g_y$

$$e_y = -g_y (e_1 - e_3)$$

$$= -g_y C_1 H_a + e_3 g_y$$

$$e_y = -g_y C_1 H_a + g_y \frac{g_1 A_c H}{\omega} u_o + g_y \frac{g_1 A_s}{\omega} J$$

Write  $H$  as  $H_a$ ;  $H = H_a = NM$

~~too~~ in the second term.

$\Rightarrow$

$$e_y = -g_y C_1 H_a + g_y \frac{g_1 A_c}{\omega} u_o H_a$$

$$- \frac{g_y g_1 A_c}{\omega} u_o NM + g_y \frac{g_1 A_s}{\omega} J$$

$$\left| \begin{array}{l} u_o M \\ = J \end{array} \right.$$

Now adjust  $C_1$  such that the pick up signal cancels. [Note that this will change the x-axis scale also].

i.e. choose  $C_1$  such that

$$g_y C_1 = g_y \frac{g_1 A_c}{\omega} u_o \Rightarrow \boxed{C_1 = g_1 \frac{A_c u_o}{\omega}}$$

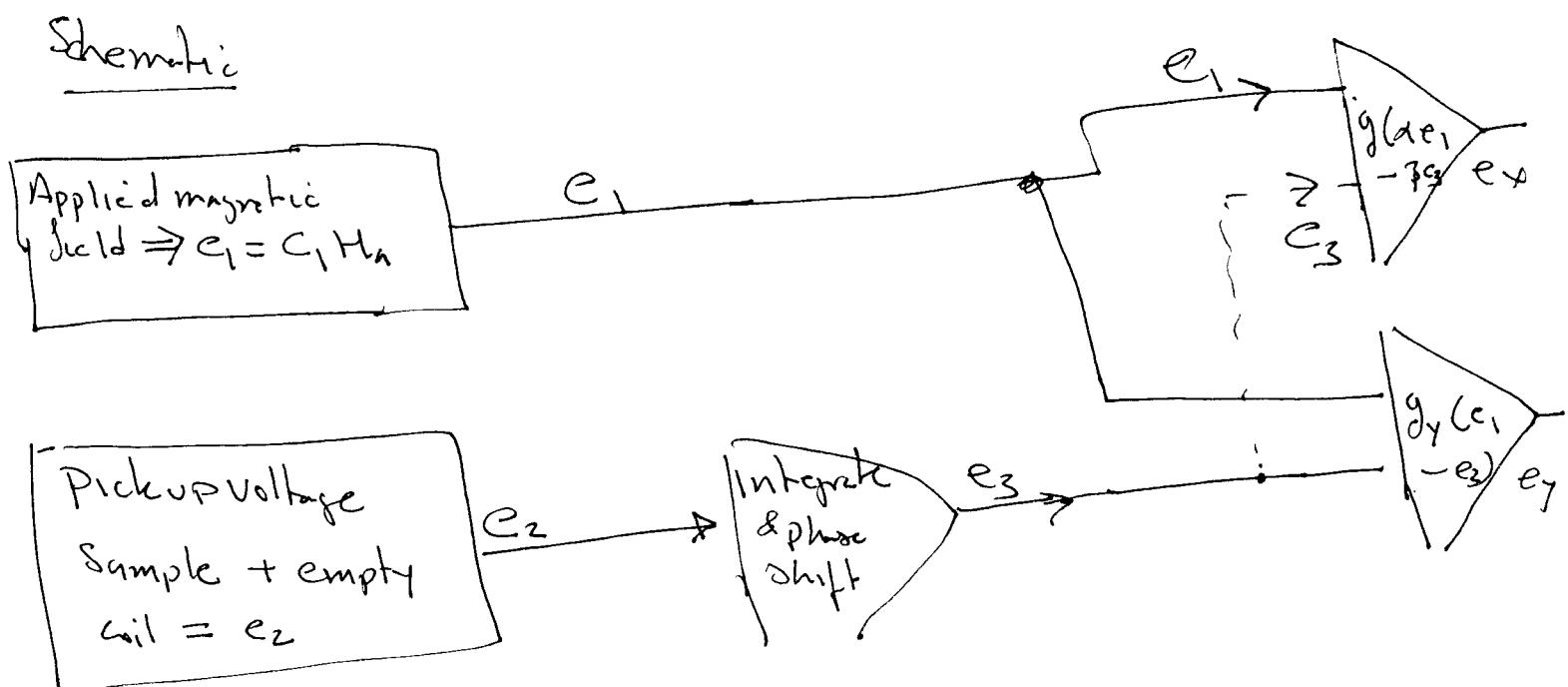
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After appropriately choosing  $C_1$ ,

$$e_y = - \frac{NM\mu_0 g_y g_1 A_c}{\omega} + g_y \frac{g_1}{\omega} A_s \mu_0 M$$

$$e_y = \frac{g_y g_1}{\omega} \mu_0 M (A_s - A_c N)$$

Schematic



Ch 1  $\Rightarrow e_x$  : measures the magnetic field applied by the big solenoid. This field has to be corrected for the demagnetization  
 $\Rightarrow$  subtract part of the magnetic response from applied field.

$$H = H_a - NM$$

Ch 2  $\Rightarrow e_y$  : Measure sample magnetization via a pickup coil. The ~~sample~~ signal has to be corrected for the pick response of empty coil

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The x-axis [channel 1 signal].

We already had

$$e_1 = C_1 H_a$$

with  $C_1$  already chosen ~~to be~~

$$\underline{C_1 = \frac{g_i A c \mu_0}{\omega}}$$

→ This value ensured that the channel 2 signal is only from the sample & the empty coil contribution is subtracted out.

To depict the hysteresis loop in real time, the x axis should be the field seen by the sample & not the applied field, that is we need to correct for the demagnetization factor.

$$H = H_a - NM ; \text{ we want } M(H) \text{ & not}$$

$$M(H_a)$$

$N$ : demagnetization factor.

⇒ take part of the magnetization signal & ~~to be~~ add it to the total signal ~~to be~~ from the signal  $e_1$ .

⇒

$$e_x = g_x (\alpha e_1 - \beta e_3)$$

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 $\Leftrightarrow$ 

$$e_x = g_x (\alpha e_1 - \beta e_3)$$

$$= g_x \alpha \frac{g_1 A_c}{\omega} H_a M_0 - g_x \beta \left( \frac{A_c \mu_0 H g_1}{\omega} + \frac{A_s \mu_0 M_0 g_1}{\omega} \right)$$

$$e_x = \frac{g_x g_1}{\omega} \mu_0 A_c \left[ \alpha H_a - \beta H - \beta M \frac{A_s}{A_c} \right]$$

now  $H = H_a - NM$ , eliminate  $H_a$

$$e_x = K \left[ \alpha H + \alpha NM - \beta H - \beta \frac{A_s}{A_c} M \right]$$

with  $K = \frac{g_x g_1}{\omega} \mu_0 A_c$

or

$$e_x = K \left[ (\alpha - \beta) H + \left( \alpha N - \beta \frac{A_s}{A_c} \right) M \right]$$

Now if we tweak  $\alpha$  &  $\beta$  such that

$\alpha = \frac{A_s}{A_c}$  &  $\beta = N$ , the second term becomes

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zero

$$e_x = K [(\alpha - \beta) H]$$

or

$$H = \frac{e_x}{K(\alpha - \beta)} = \frac{e_x}{K \left( \frac{A_s}{A_c} - N \right)}$$

