

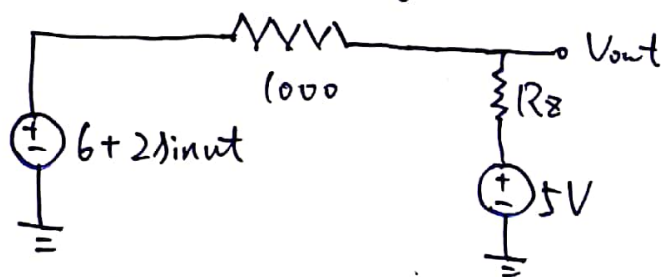
Prob # 1

(1) Circuit # 1

The diode is Zener breakdown when $|V_{in}| > 5$

when $V_{in} \leq 5$; $V_{out} = V_{in}$

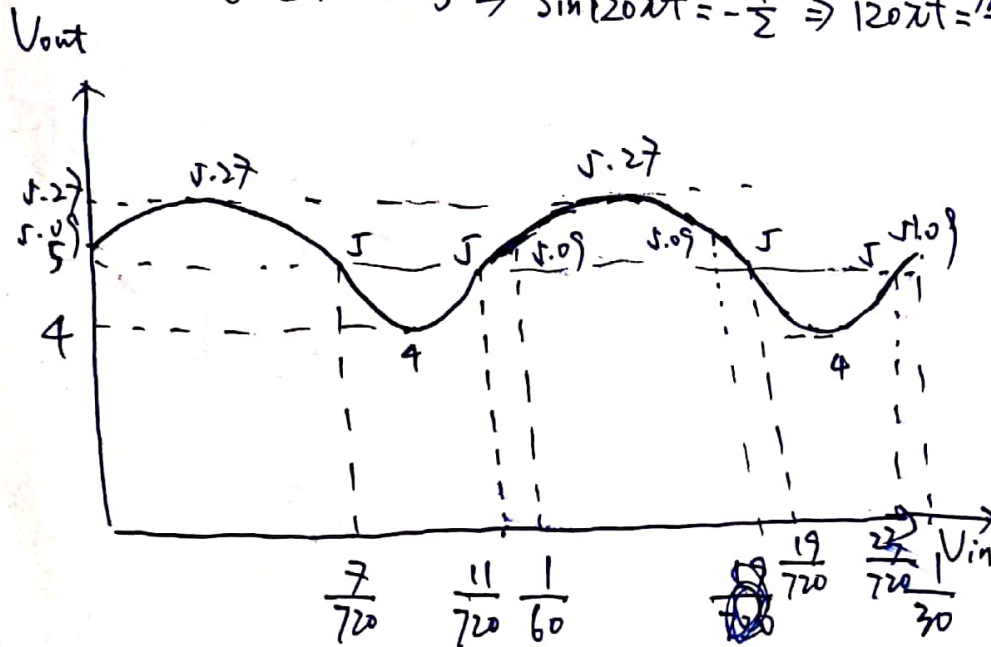
when $V_{in} > 5$; The equivalent circuit



$$R_Z = \frac{1}{k_Z} = 100\Omega \quad V_{out} = \frac{R_Z}{R + R_Z} \cdot (6 + 2\sin\omega t - 5) + 5$$

$$= 5.09 + 0.182\sin\omega t$$

$$6 + 2\sin\omega t = 5 \Rightarrow \sin 120\pi t = -\frac{1}{2} \Rightarrow 120\pi t = \frac{7\pi}{6} \Rightarrow t = \frac{7}{720}$$

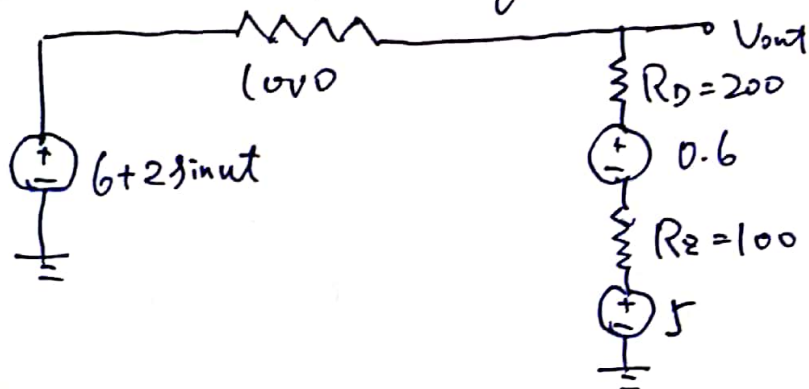


12) Circuit # 2

The ~~two~~ current can pass through the diode when $|V_{in}| > 5.6$

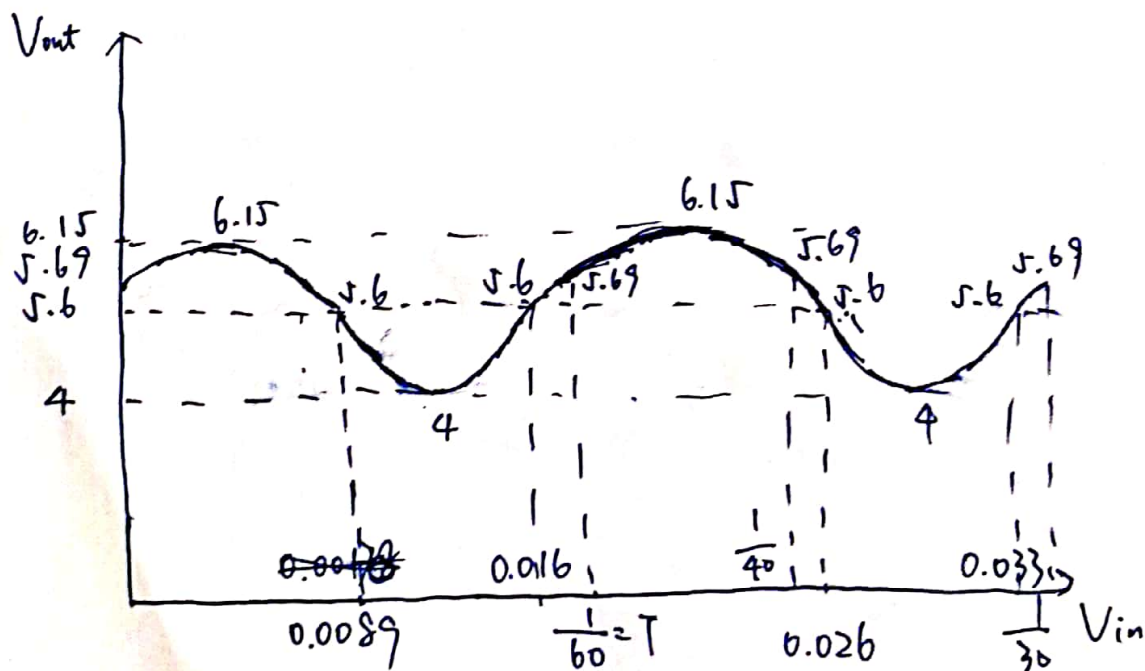
$$\int |V_{in}| \leq 5.6 \Rightarrow V_{out} = 6 + 2\sin 120\pi t$$

$|V_{in}| > 5.6 \Rightarrow$ The equivalent circuit:



$$\begin{aligned} V_{out} &= \frac{R_D + R_Z}{R_D + R_Z + R} \cdot (6 + 2\sin ut - 0.6 - 5) + 0.6 + 5 \\ &= \frac{3}{13} (0.4 + 2\sin ut) + 5.6 \\ &= 5.69 + 0.46 \sin ut \end{aligned}$$

$$6 + 2\sin ut = 5.6 \Rightarrow \sin 120\pi t = -0.2 \Rightarrow t = -$$



Prob (2)

11). $\tilde{V}_{in} = 1 + 0.01 \sin 60\pi t$

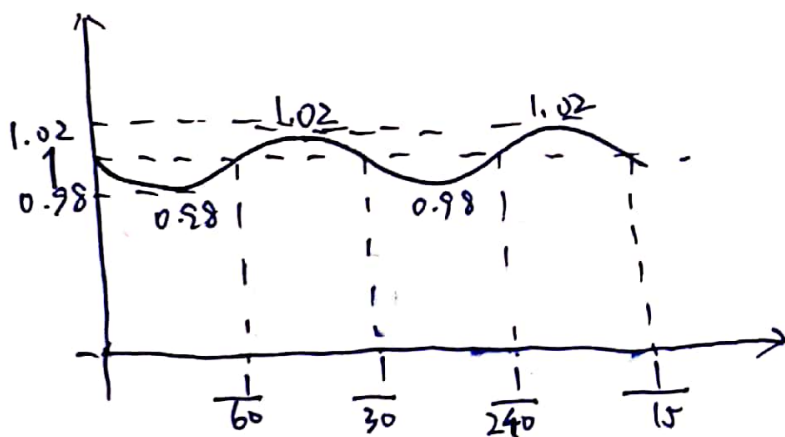
For DC: $\overline{V_{out}} = (\overline{V_{in}} - 2)^2 = 1$

For AC: $\tilde{v}_{out} = \left. \frac{dV_{out}}{dV_{in}} \right|_{\overline{V_{in}}} \cdot \tilde{v}_{in}$
 $= 2(\overline{V_{in}} - 2) \cdot \tilde{v}_{in}$

$= -2 \cdot \tilde{v}_{in}$

$= -0.02 \sin 60\pi t$

$T = \frac{2\pi}{\omega} = \frac{1}{30} \text{ s}$



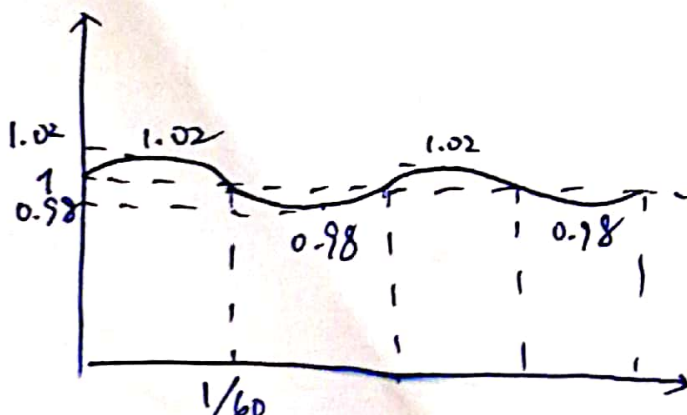
12). $\tilde{V}_{in} = 3 + 0.01 \sin 60\pi t$

For DC: $\overline{V_{out}} = (\overline{V_{in}} - 2)^2 = 1$

For AC: $\tilde{v}_{out} = \left. \frac{dV_{out}}{dV_{in}} \right|_{\overline{V_{in}}} \cdot \tilde{v}_{in}$

$= 2(\overline{V_{in}} - 2) \cdot \tilde{v}_{in}$

$= 0.02 \sin 60\pi t$



Prob #3.

$$(1) I_{dc} = \frac{V_s - 2V_{on} - 2V_{on}}{R \parallel R} = 2 \cdot \frac{V_s - 4V_{on}}{R} = \frac{2V_s - 8V_{on}}{R}$$

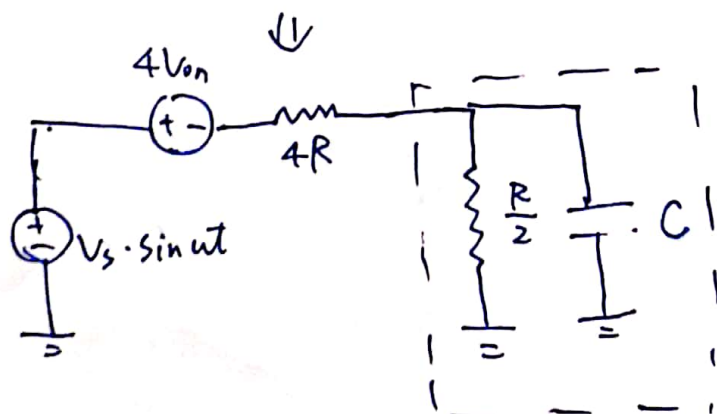
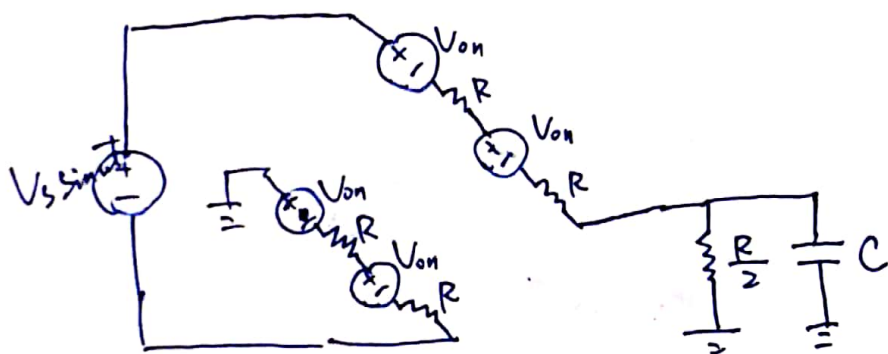
$$\Delta T = \frac{1}{\omega} \cdot \sqrt{\frac{2V_r}{V_s}} \quad V_r = (V_s - 2V_{on} - 2V_{on}) \frac{T}{2RC} = (V_s - 4V_{on}) \frac{T}{2RC} = (V_s - 4V_{on}) \frac{T}{RC}$$

$$\Rightarrow \Delta T = \frac{1}{\omega} \cdot \sqrt{\frac{2(V_s - 4V_{on})T}{V_s RC}} = \sqrt{\frac{2(V_s - 4V_{on})T}{V_s RC}}$$

$$PIV = V_{dc} + 2V_{on} = V_s - 4V_{on} + 2V_{on} = V_s - 2V_{on}$$

(2) The circuit will not work.

if we transform the diodes into ideal models: (Assume first charge)



$$(Z_{load} \ll 4R) \Rightarrow V_{load} = \frac{Z_{load}}{Z_{load} + 4R} \cdot V_s \approx 0.$$

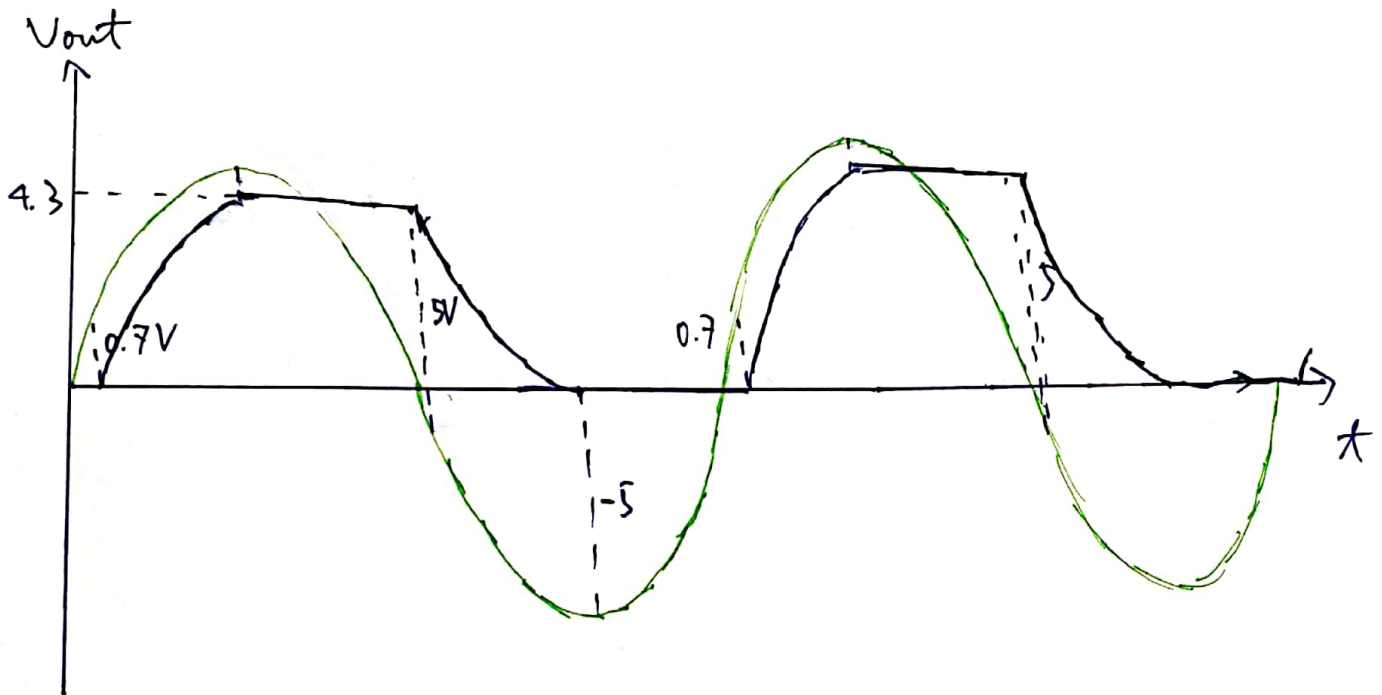
$$Z_{eq}(load) = \left| \frac{1}{j\omega C} \parallel \frac{R}{2} \right| < \left| \frac{1}{j\omega C} \right| = \left| \frac{1}{j \frac{2\pi}{T} C} \right| = \left| \frac{T}{j2\pi C} \right| = \frac{T}{2\pi C}$$

$$\text{Since } RC \gg T \Rightarrow \frac{T}{C} \ll R \Rightarrow \frac{T}{2\pi C} \ll R < 4R$$

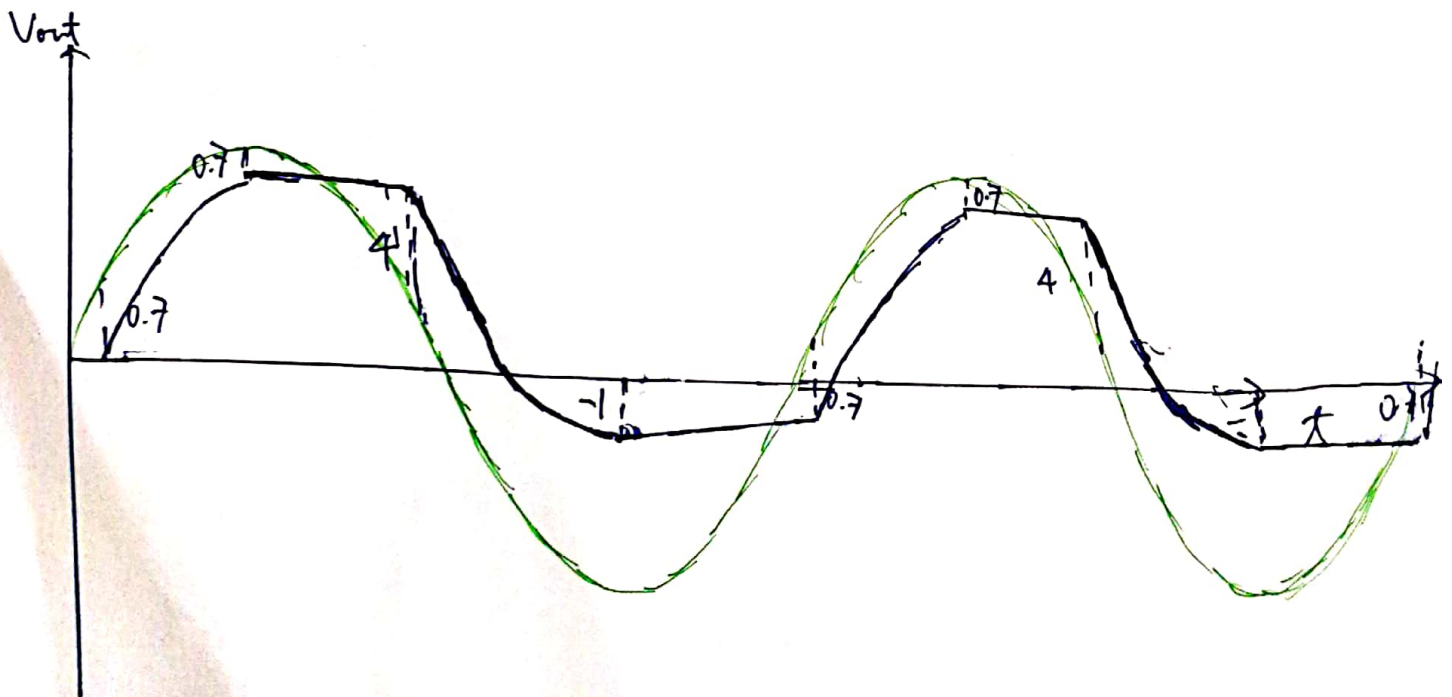
Thus, the load resistance is quite small compared with the diode's inner resistance, so the output voltage is almost equal to zero

Prob #4

- (1). When $V_{in} - V_{out} \geq 0.7$, the diode is turned on.
 When $V_{in} - V_{out} \leq -5$, the diode is Zener breakdown

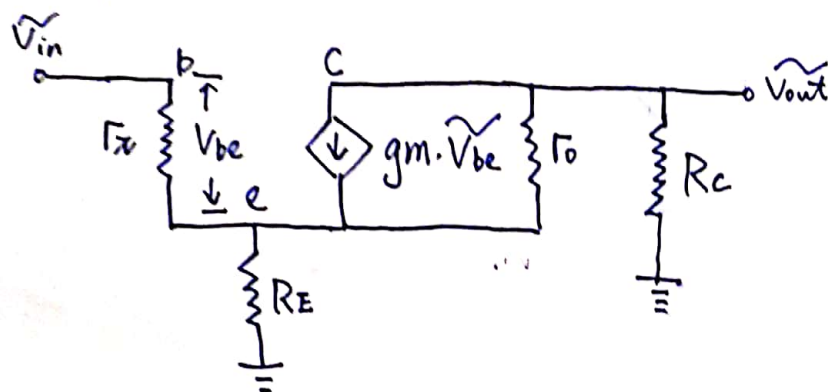


- (2). When $V_{in} - V_{out} \leq 4$, the diode is Zener breakdown.



Prob #5

(1) Plot the small signal model ($r_x, r_o \neq +\infty$)



Suppose in the e port, the small signal voltage is \tilde{V}_e

at node e : using KCL

$$\frac{\tilde{V}_{in} - \tilde{V}_e}{r_x} + g_m \cdot \tilde{V}_{be} + \frac{\tilde{V}_{out} - \tilde{V}_e}{r_o} = \frac{\tilde{V}_e - 0}{R_E} \quad (1)$$

at node c : using KCL :

$$g_m \cdot \tilde{V}_{be} = \frac{\tilde{V}_e - \tilde{V}_{out}}{r_o} + \frac{0 - \tilde{V}_{out}}{R_C} \quad (2)$$

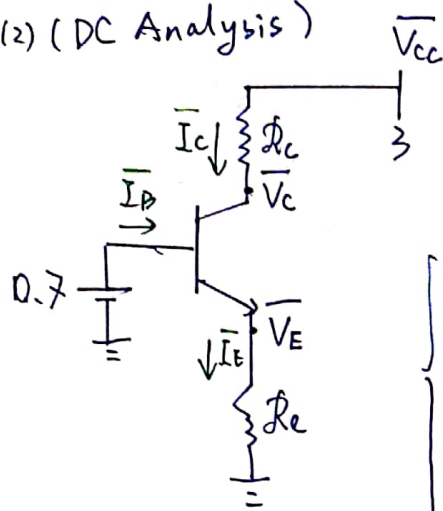
$$\tilde{V}_{be} = \tilde{V}_{in} - \tilde{V}_e \quad (3)$$

combine (1), (2), (3), we get $\tilde{V}_e = \frac{r_o r_C g_m \tilde{V}_{in} + \tilde{V}_{out} r_C + \tilde{V}_{out} r_o}{r_o r_C g_m + r_C}$

$$A_v = \frac{\tilde{V}_{out}}{\tilde{V}_{in}} = \frac{r_C r_o - g_m r_o r_C r_x}{r_o r_x + r_C r_x + r_C r_o + r_o r_C + r_C r_x + g_m r_o r_C r_x}$$

(in your exam, the intermediate calculation process will not count for marks)

(2) (DC Analysis)



DC analysis:

$$\bar{I}_C = \frac{V_{CC} - \bar{V}_C}{R_C}$$

$$\bar{I}_E = \frac{\bar{V}_E - 0}{R_E}$$

$$\bar{I}_C = I_S \left(e^{\frac{q(\bar{V}_{BE} - \bar{V}_E)}{kT}} - 1 \right) \left(1 + \frac{\bar{V}_C - \bar{V}_E}{V_{AF}} \right) *$$

$$\bar{I}_C = \beta \bar{I}_B$$

$$\bar{I}_E = \bar{I}_C + \bar{I}_B$$

$$\begin{cases} \bar{I}_C = \beta \bar{I}_B \\ \bar{I}_E = \bar{I}_C + \bar{I}_B \end{cases} \Rightarrow \bar{I}_E = \frac{\bar{I}_C}{10} + \bar{I}_C \Rightarrow \bar{I}_C = \frac{10}{11} \bar{I}_E ; \bar{I}_E = 1.1 \bar{I}_C$$

Thus, we have $\bar{V}_E = 1.1 \bar{I}_C \cdot R_E = 5500 \bar{I}_C$ ①

$\bar{I}_C = \frac{V_{CC} - \bar{V}_C}{R_C} \Rightarrow \bar{V}_C = V_{CC} - \bar{I}_C R_C = 3 - 5000 \bar{I}_C$ ②

According to *, ①, ②, we have

$$\bar{I}_C = 1 \times 10^{-16} \times \left(e^{\frac{1.6 \times 10^{-19} \times (0.7 - 5500 \bar{I}_C)}{1.38 \times 10^{-23} \times 300}} - 1 \right) \left(1 + \frac{3 - 5000 \bar{I}_C - 5500 \bar{I}_C}{100} \right)$$

Solve the equation, we can get $\bar{I}_C = 8.8 \times 10^{-6} \text{ A}$ (by Casio 991 Calculator)

$$g_m = \frac{d\bar{I}_C}{d\bar{V}_{BE}} \approx \frac{\bar{I}_C}{kT/q} = \frac{8.8 \times 10^{-6} \times 1.6 \times 10^{-19}}{1.38 \times 10^{-23} \times 300} = 3.4 \times 10^{-4} \text{ S}$$

$$r_\pi = 1/d\bar{I}_B/d\bar{V}_{BE} = \frac{\beta}{g_m} = \frac{10}{3.4 \times 10^{-4}} = 2.94 \times 10^4 \Omega$$

$$r_o = 1/d\bar{I}_C/d\bar{V}_{CE} \approx \frac{V_{AF}}{\bar{I}_C} = \frac{100}{8.8 \times 10^{-6}} = 1.14 \times 10^7 \Omega$$

$$R_C = R_E = 5000$$

Thus,

$$A_v = \frac{5000^2 - 3.4 \times 10^{-4} \times 1.14 \times 10^7 \times 2.94 \times 10^4 \times 5000}{2.94 \times 10^4 \times 1.14 \times 10^7 + 5000 \times 2.94 \times 10^4 + 5000^2 + 1.14 \times 10^7 \times 5000 + 2.94 \times 10^4 \times 5000 + 3.4 \times 10^{-4} \times 1.14 \times 10^7 \times 2.94 \times 10^4 \times 5000}$$

$$= -0.592.$$