$$G_{day} = 0 (8.46)$$

where  $G_{day}$  is the daily soil heat flux density, MJ m<sup>-2</sup> d<sup>-1</sup>.

over a monthly period, G for the soil profile can be significant, especially during Over a monunity period, of the soil heat capacity of 2.0 MJ m<sup>-3</sup> °C<sup>-1</sup> and an efspring and fall. Assuming a constant of a monthly periods in MJ m<sup>-2</sup> d<sup>-1</sup> is estimated from the change in mean monthly air temperature as:

$$G_{month,i} = 0.07 (T_{month,i+1} - T_{month,i-1})$$
 (8.47)

or, if  $T_{month,i+1}$  is unknown,

$$G_{month,i} = 0.14 \left( T_{month,i} - T_{month,i-1} \right) \tag{8.48}$$

where  $T_{month,i}$  is mean air temperature of month i,  $T_{month,i-1}$  is mean air temperature of the previous month, and  $T_{month,i+1}$  is the mean air temperature of the next month (all °C).

For application to short-periods, e.g., when hourly data for G are required, other approaches must be used. One method common to research uses heat flux plates installed near the soil surface, usually at a depth of about 0.1 to 0.15 m. The total heat flux density is determined by performing a calorimetric balance of the soil layer above the plate. Because soil heat flux plates are not a common measurement at weather stations, the reader is referred to other references (Tanner, 1960; Brutsaert, 1982; and Allen et al., 1996) for application descriptions.

For hourly or shorter time periods, G, in the standardized calculation is expressed as a function of net radiation for the two reference types. For the standardized short reference  $ET_{os}$ :

$$G_{hr \, daytime} = 0.1 \, R_n \tag{8.49a}$$

$$G_{hr\ nightime} = 0.5\ R_n \tag{8.49b}$$

where G and  $R_n$  have the same measurement units (MJ m<sup>-2</sup> h<sup>-1</sup> for hourly or shorter time periods). For the standardized tall reference  $ET_{rs}$ :

$$G_{hr daytime} = 0.04 R_n ag{8.50a}$$

$$G_{hr\ nightime} = 0.2\ R_n \tag{8.50b}$$

For standardization, nighttime is defined as when measured or calculated hourly net radiation  $R_n$  is < 0 (i.e., negative). The amount of energy consumed by G is subtracted from  $R_n$  when estimating  $ET_{os}$  or  $ET_{rs}$ . The coefficient 0.1 in Equation 8.49a represents the condition of only a small amount of dead thatch underneath the leaf canopy of the short (clipped grass) reference. Large amounts of thatch insulate the soil surface, reducing the daytime coefficient for grass to about 0.05. However, the 0.1 coefficient is part of the EWRI and FAO standardizations.

8.4.5 1985 Hargreaves Grass Reference Equation

The Hargreaves equation (Hargreaves and Samani, 1982, 1985; Hargreaves et al., 1985) is suggested as a means for estimating  $ET_0$  in situations where weather data are limited and only maximum and minimum air temperature data are available. The form of the 1985 Hargreaves equation is:

$$ET_o = 0.0023 \left( T_{max} - T_{min} \right)^{0.5} \left( T_{mean} + 17.8 \right) \left( R_a \right) \tag{8.51}$$

where  $T_{max}$  and  $T_{min}$  = maximum and minimum daily air temperature,  $^{\circ}$ C.

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 $T_{mean}$  = mean daily air temperature,  $(T_{max} + T_{min})/2$ 

 $R_a$  = average daily exoatmospheric radiation (Equation 8.29).

 $R_a$  = average  $R_a$  = avera mm d<sup>-1</sup> by dividing by  $\lambda = 2.45$  MJ kg<sup>-1</sup>.

The Hargreaves equation was the highest-ranked temperature-based method in the The Halgier The Ha ASCE Wands Asce Wands and Allen (2003) reported Equation 8.51 to estimate well over a wide range of greaves and climates for periods of 5 days or longer without significant error, prolatitudes and vind speeds averaged between 1 and 3 m s<sup>-1</sup>. Itenfisu et al. (2003) comvided file and  $ET_o$  by Equation 8.51 and that by the standardized ASCE PM method for 16 states in U.S. and found mean ratios of  $V_o$ pared daily E and E and found mean ratios of Hargreaves  $ET_o$  to ASCE PM with a mean of 1.06 and E are E and E and E are E and E are E are E and E are E are E and E are E and E are E are E and E are E are E and E are E and E are E are E are E and E are E are E and E are E are E and E are E are E are E and E are E and E are E are E are E and E are E are E and E are E and E are E and E are E and E are E are E are E and E are E are E are E are E and E are E are E are E are E and E are E are E are E are E are E and E are E are E are E and E are E are E are E and E are E are E are E are E are E and E are E are E are E and E are E are E are E are E and E are E and E are E are E are E are E are E and E are E are E are E are E are E are E and E are E are 49 sites in 1.43 to 0.79, with a mean of 1.06 and a standard deviation of 0.13. The Hargreaves equation tended to estimate higher than the ASCE PM method when mean daily  $ET_o$  was low, and vice versa.

One advantage of an equation such as the Equation 8.51 relative to more complex equations such as the Penman or PM equation, which is often overlooked, is the reduced data requirement and therefore reduced chance for data error. This is advantageous in regions where solar radiation, humidity, and wind data are lacking or are of low or questionable quality (Droogers and Allen, 2002). Generally, air temperature can be measured with less error, with less sophisticated equipment, and by less trained individuals than can the other three parameters required by combination equations. Equation 8.51 can be calibrated against the PM equation (Equation 8.3) when data are available to produce a regionally calibrated temperature equation. Examples of this type of calibration in Spain include Martinez-Cob and Tejero-Juste (2004), Vanderlinden et al. (2004), and Gavilan et al. (2005). An alternative to using Equation 8.51 when data are lacking is to employ the PM equation using estimates for missing variables.

## 8.4.6 Effect of Timestep Size on Calculations

The Penman and Penman-Monteith equations can be applied to hourly and 24-h timesteps. The 24-h timesteps can use daily, weekly, 10-d, and monthly averages for weather data. Under many climatic conditions, calculating ETo or ETr using hourly timesteps and then summing over 24 hours provides estimates that closely equal  $ET_o$ or ET, calculated using 24-h average data with 24-h calculation timesteps, especially when applying the standardized ASCE-EWRI PM method (Itenfisu et al., 2003; ASCE-EWRI, 2005). Generally, 24-h ET<sub>o</sub> and ET, have potential for higher accuracy when computed using hourly or shorter timesteps and then summed to 24-hour totals. Hourly calculation is better able to consider impacts of abrupt and gradual changes in weather parameters during the course of a day on ET (Irmak et al., 2005; Allen et al., 2006). Examples of this are high wind conditions during afternoons with low humidity are ity, overpass of cloud fronts and rain events, wintertime, and nighttime calm.

## 8.4.7 Limited Data Availability

Many historical weather data sets include only measurements of daily air temperate. When Exp. ture. When  $ET_o$  estimates are desired, one of three approaches is recommended:

1. When approximate calculations of  $ET_o$  are suitable, apply Equation 8.51.
2. When  $T_o$  are suitable, apply Equation 8.51.

2. When more accuracy is required, calibrate Equation 8.51 at a regional station or stations of  $ET_o$  are suitable, apply Equation of  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  and  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  and  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  and  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  and  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  and  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  and  $ET_o$  are suitable, apply Equation 8.51 at a regional station of  $ET_o$  and  $ET_o$  are suitable at a region  $ET_o$  and  $ET_o$  are suitable at stations that have  $R_s$  and  $u_2$  data. If  $T_d$  or other humidity data are not available,  $T_d$  can be a self-stated as  $t_d$  and  $t_d$  and  $t_d$  are the desired standard for the desired standa  $T_d$  can be estimated from  $T_{min}$  as described in Equation 8.16. The desired standard reference dard reference method can be used as the calibration basis (e.g., Equation 8.3) at

8.4.4.9 Exoatmospheric radiation. Exoatmospheric radiation,  $R_a$ , (also known as extraterrestrial radiation) is defined as the short-wave solar radiation in the absence of an atmosphere, and is a well-behaved function of the day of the year, time of day, and an atmosphere.  $R_a$  is needed for calculating  $R_{so}$ , which is in turn used in calculating  $R_n$ . For daily (24-hour) periods,  $R_a$  is estimated from the solar constant, the solar declination, and the day of the year:

$$R_a = \frac{24}{\pi} G_{sc} d_r \left[ \omega_s \sin(\varphi) \sin(\delta) + \cos(\varphi) \cos(\delta) \sin(\omega_s) \right]$$
 (8.29)

where  $R_a$  = exoatmospheric radiation, MJ m<sup>-2</sup> d<sup>-1</sup>

 $G_{sc}$  = solar constant, 4.92 MJ m<sup>-2</sup> h<sup>-1</sup>

 $d_r$  = inverse relative distance factor (squared) for the earth-sun, unitless

 $\omega_s$  = sunset hour angle, radians

 $\varphi$  = station latitude, radians, positive for the northern hemisphere and negative for the southern hemisphere

 $\delta$  = solar declination, radians.

Parameters  $d_r$  and  $\delta$  are calculated as:

$$d_r = 1 + 0.033 \cos\left(\frac{2\pi}{365}J\right) \tag{8.30}$$

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$$\delta = 0.409 \sin\left(\frac{2\pi}{365} J - 1.39\right) \tag{8.31}$$

where J is the number of the day in the year between 1 (1 January) and 365 or 366 (31 December). The constant 365 in Equations 8.23 and 8.24 is held at 365 even during a leap year. J can be calculated as:

$$J = D_M - 32 + \operatorname{Int}\left(275 \frac{M}{9}\right) + 2 \operatorname{Int}\left(\frac{3}{M+1}\right) + \operatorname{Int}\left(\frac{M}{100} - \frac{\operatorname{Mod}(Y, 4)}{4} + 0.975\right)$$
(8.32a)

where  $D_M$  is the day of the month (1-31), M is the number of the month (1-12), and Yis the number of the year (for example 1996 or 96). The "Int" function in Equation 8.32 finds the integer number of the argument in parentheses by rounding downward. The "Mod(Y,4)" function finds the modulus (remainder) of the quotient Y/4.

For monthly periods, the day of the year at the middle of the month  $(J_{month})$  is approximately:

$$J_{month} = Int(30.4 M - 15)$$
 (8.32b)

The sunset hour angle,  $\omega_s$ , is given by:

$$\omega_s = \arccos\left[-\tan(\varphi)\tan(\delta)\right]$$
 (8.33)

The "arccos" function is the arc-cosine function and represents the inverse of the cosine. This function is not available in all computer languages, so that  $\omega_s$  can alternatively. tively be computed using the arc-tangent (inverse tangent) function:

$$\omega_s = \frac{\pi}{2} - \arctan\left[\frac{-\tan(\varphi)\tan(\delta)}{X^{0.5}}\right]$$
 (8.34)

(8.35) $X = 1 - \left[\tan(\varphi)\right]^2 \left[\tan(\delta)\right]^2$ 

Where