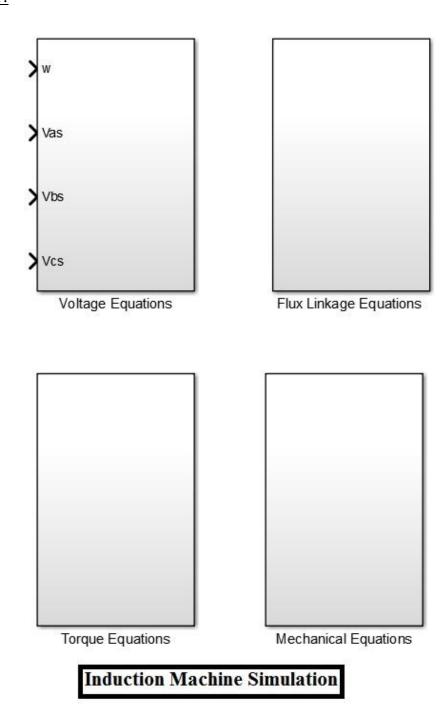
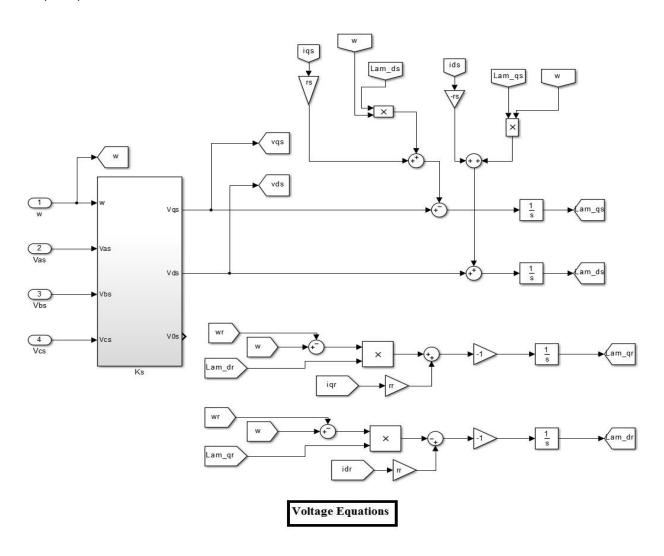
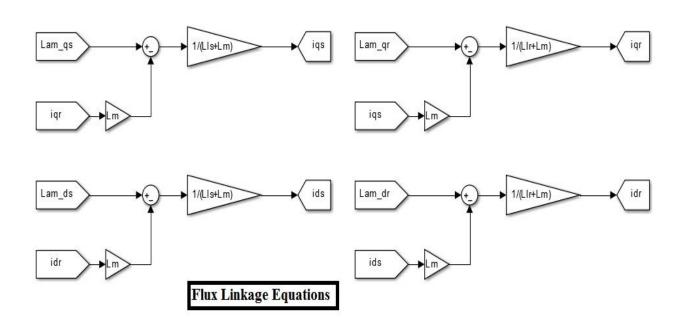
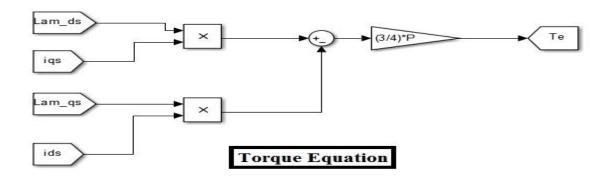
ECE 802, Electric Motor Control, Fall 2013 Exam#2, Induction Machines

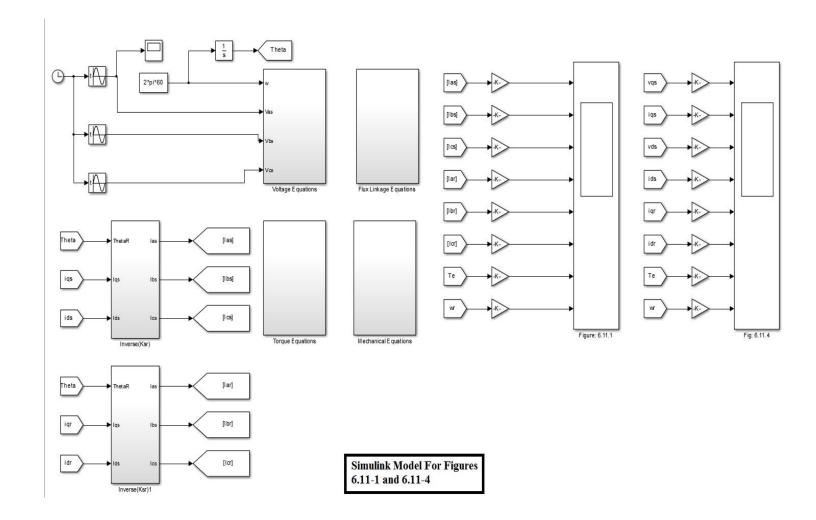
Question 1:







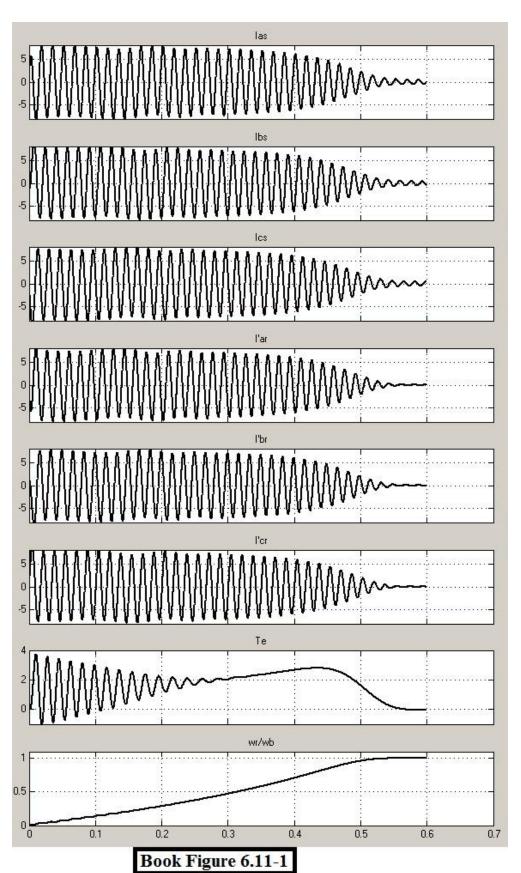


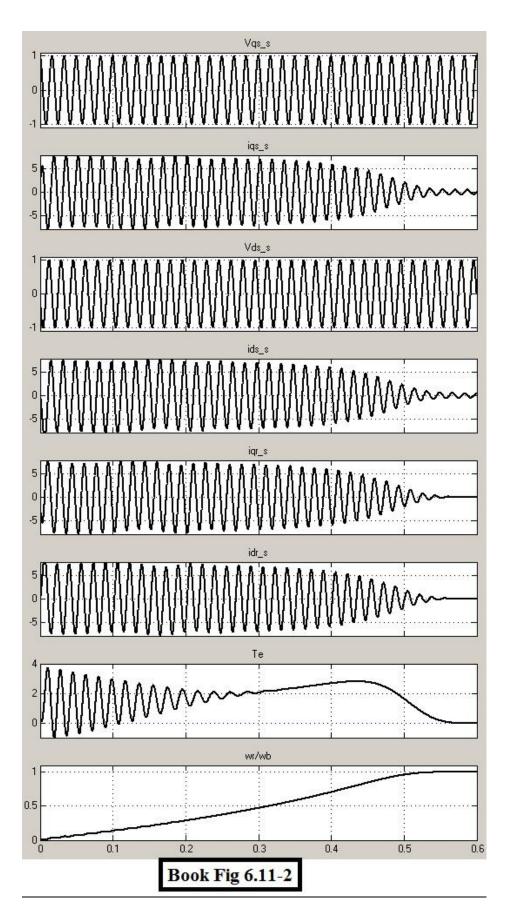


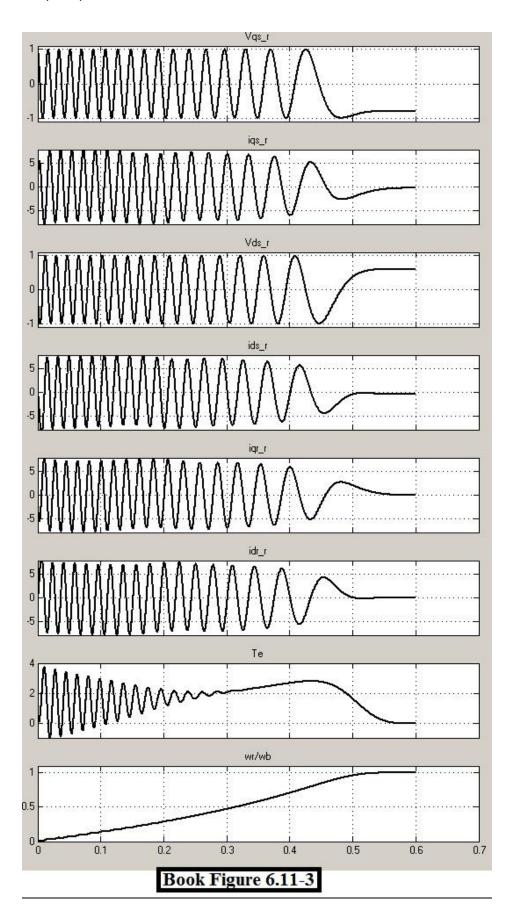
m-file Codes to set up the constants

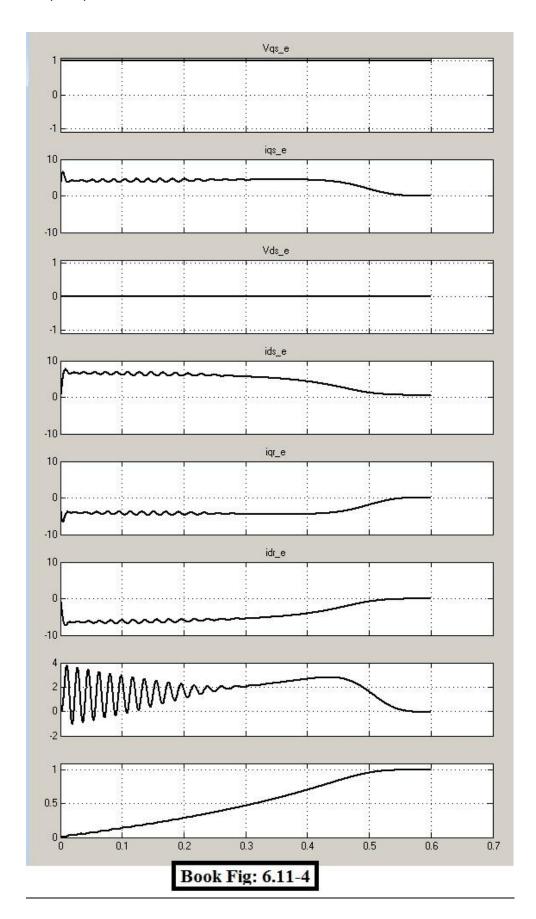
```
clear all;
P = 6;
wb = 2*pi*60;
Vb = sqrt(2)*220/sqrt(3);
Pb = 10*746;
Zb = (3/2)*Vb*Vb/Pb;
Ib = Pb/((3/2)*Vb);
rs = 0.0453*Zb;
rr = 0.0222*Zb;
Lm = 5.41657e-3*Zb;
Lls = 0.205575e-3*Zb;
Llr = 8.541315e-5*Zb;
Tb = Pb/((2/P)*wb);
H = 10;
```

Results









Question 2:

Calculations for steady-state no-load stator flux

Constants:

$$\begin{split} &V_s = 127.017 \ V \\ &r_s = 0.2939 \ \Omega \\ &r_r = 0.1440 \Omega \\ &L_{ls} = 0.0013 \ H \\ &L_{lr} = 5.5416 x 10^{-4} \ H \\ &L_m = 0.0351 \ H \end{split}$$

$$L_{ss} = L_{ls} + L_m = 0.0365 \text{ H}$$

 $L_{rr} = L_{lr} + L_m = 0.0357 \text{ H}$

$$\begin{split} f_e &= 60 Hz \\ w_e &= 2.\pi. f_e = 376.9911 rad/s \end{split}$$

Since for balanced steady-state conditions the q and d axis variables are sinusoidal in all reference frames except the synchronously rotating reference frame, where they are constants, it has been used for calculating the steady state values.

Since the rotor is accelerating with no load torque and because friction and winding losses have been neglected, the machine accelerates to synchronous speed. i.e.

$$w_r = w_e = 376.9911 rad/s$$

In Synchronous reference frame we have,

$$\begin{aligned} V_{qs_e} := \sqrt{2} \cdot V_s & V_{ds_e} := 0 \cdot V & V'_{qr_e} := 0 \cdot V & V'_{dr_e} := 0 \cdot V \\ \begin{bmatrix} I_{qs_e} \\ I_{ds_e} \\ I'_{qr_e} \\ I'_{dr_e} \end{bmatrix} := \begin{bmatrix} r_s & \omega_e \cdot L_{ss} & 0 & \omega_e \cdot L_M \\ -\omega_e \cdot L_{ss} & r_s & -\omega_e \cdot L_M & 0 \\ 0 & (\omega_e - \omega_r) \cdot L_M & r'_r & (\omega_e - \omega_r) \cdot L'_{rr} \\ -(\omega_e - \omega_r) \cdot L_M & 0 & -(\omega_e - \omega_r) \cdot L'_{rr} & r'_r \end{bmatrix}^{-1} \cdot \begin{bmatrix} V_{qs_e} \\ V'_{ds_e} \\ V'_{qr_e} \\ V'_{dr_e} \end{bmatrix}$$

$$[I] = [M] \cdot [V]$$

Then

$$V = \begin{bmatrix} 179.6292 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

$$\mathbf{M} = \begin{bmatrix} 0.2929 & 13.7512 & 0 & 13.2484 \\ -13.7512 & 0.2939 & -13.2484 & 0 \\ 0 & 0 & 0.2939 & 0 \\ 0 & 0 & 0.2939 \end{bmatrix}^{-1}$$

$$= \begin{bmatrix} 0.0016 & -0.0727 & -3.2766 & -0.0700 \\ 0.0727 & 0.0016 & 0.0700 & -3.2766 \\ 0 & 0 & 3.4025 & 0 \\ 0 & 0 & 0 & 3.4025 \end{bmatrix}$$

$$\gg I = \begin{bmatrix} Iqs \\ Ids \\ Iqr \\ Idr \end{bmatrix} = \begin{bmatrix} 0.2791 \\ 13.0569 \\ 0 \\ 0 \end{bmatrix}$$

$$\lambda_{qs} = L_{ss}.Iqs + L_{m}.Iqr = 0.0102$$

$$\lambda_{ds} = L_{ss}.Ids + L_{m}.Idr = 0.4763$$

$$\lambda_{s\,=}\sqrt{\lambda q s^2 + \lambda d s^2}\,=0.4764$$

The steady-state stator flux value calculated by Torque and Flux Observer model $= 0.4763 \approx 0.4764$.

