

A5) Applying Laplace to linearised System

$$① s \bar{Z}_1(s) = \bar{Z}_2(s)$$

$$② s \bar{Z}_2(s) = \frac{5m}{7} \left[ c(a_1 \bar{Z}_3(s) + a_2 \bar{Z}_1(s)) - k \bar{Z}_1(s) - b \bar{Z}_2(s) \right]$$

$$③ s \bar{Z}_3(s) = a_3 \left[ \bar{V}(s) - R \bar{Z}_3(s) \right] - a_4 \bar{Z}_1(s)$$

$$\Rightarrow ② s^2 \bar{Z}_1(s) = \frac{5m}{7} \left[ ca_1 \bar{Z}_3(s) + ca_2 \bar{Z}_1(s) - k \bar{Z}_1(s) - bs \bar{Z}_1(s) \right]$$

$$\cancel{s^2 \bar{Z}_1} = \frac{5mc a_1 \bar{Z}_3(s)}{7} + \frac{5mc a_2 \bar{Z}_1(s)}{7} - \frac{5mk \bar{Z}_1(s)}{7} - \frac{5mb s \bar{Z}_1(s)}{7}$$

$$\frac{7s^2}{5m} \bar{Z}_1(s) + bs \bar{Z}_1(s) + k \bar{Z}_1(s) - ca_2 \bar{Z}_1(s) = ca_1 \bar{Z}_3(s)$$

$$\bar{Z}_1(s) \left( \frac{7s^2}{5m} + bs + k - ca_2 \right) = ca_1 \bar{Z}_3(s)$$

$$\bar{Z}_3(s) = \frac{\bar{Z}_1(s)}{ca_1} \left( \frac{7s^2}{5m} + bs + k - ca_2 \right)$$

$$③ \Rightarrow s \bar{Z}_3(s) = a_3 \bar{V}(s) - a_3 R \bar{Z}_3(s) - a_4 \bar{Z}_1(s)$$

$$s \bar{Z}_3(s) + a_3 R \bar{Z}_3(s) = a_3 \bar{V}(s) - a_4 \bar{Z}_1(s)$$

$$\bar{Z}_3(s) (s + a_3 R) = a_3 \bar{V}(s) - a_4 \bar{Z}_1(s)$$

$$\frac{\bar{Z}_1(s)}{ca_1} \left( s + a_3 R \right) \left( \frac{7s^2}{5m} + bs + k - ca_2 \right) + a_4 \bar{Z}_1(s) = a_3 \bar{V}(s)$$

$$\bar{Z}_1(s) \left( \frac{ca_1 a_4 + (s + a_3 R)(\frac{7s^2}{5m} + bs + k - ca_2)}{ca_1} \right) = a_3 \bar{V}(s)$$

$$\frac{\bar{Z}_1(s)}{\bar{V}(s)} = \frac{ca_1 a_3}{(s + a_3 R)(\frac{7s^2}{5m} + bs + k - ca_2) + ca_1 a_4}$$

A5) This is a 3<sup>rd</sup>-order transfer function thus has 3 poles. This can be modelled using the product of a first and Second order transfer function for analytical purposes. Furthermore, the System's response can be approximated using the sum of the responses from the decomposed functions.

~~Due to the nature of the summation the slower response would become dominant. For example;~~

~~An oscillatory impulse response would be generated if the Second order function was underdamped~~

Due to the nature of the summation, oscillations present in an impulse response from the Second-order System would become apparent in the overall System's impulse response; ~~therefore, an underdamped Second order system would produce oscillations within~~ These oscillations would be created due the 2<sup>nd</sup> Order System being underdamped.

A Second order transfer function has the form

$$G(s) = \frac{k}{\tau^2 s^2 + 2\zeta\tau s + 1}$$

where  $k, \zeta, \tau > 0$   $k$ -Static gain  $\zeta$ -damping factor  $\tau$ -time constant of sys

<sup>2<sup>nd</sup> order</sup> A underdamped System is categorized by ~~through by~~ ~~the poles being a pair of complex conjugate, non-real poles. which is found by~~ which can be identified by ~~by~~ can be identified by analysing the discriminant of the denominator.

$$\begin{aligned} \Delta \tau^2 s^2 + 2\zeta\tau s + 1 &= (2\zeta\tau)^2 - 4(\tau^2)(1) \\ &= 4\zeta^2\tau^2 - 4\tau^2 \\ &= 4\tau^2(\zeta^2 - 1) \end{aligned}$$

Therefore, if the damping factor,  $\zeta$ , is

A damping factor of  $\zeta < 1$  would create a negative discriminant hence indicating an underdamped sys due to presence of a pair of non-real conjugate poles.

Analysing poles of the transfer function

$$\Theta = (s + a_3 R) \left( \frac{7s^2 + bs - h - ca_2}{5m} \right) + ca_1 a_4$$
$$- ca_1 a_4 = (s + a_3 R) \left( \frac{7s^2 + bs - h - ca_2}{5m} \right)$$

mapping the quadratic's co-efficients to (eqn of gen form)

$$\tau^2 = \frac{7}{5m} \quad 2\zeta\tau = b$$

$$\tau = \sqrt{\frac{7}{5m}} \quad \zeta = \frac{b}{2\tau}$$

$$\zeta = \frac{b}{2} \left( \frac{\sqrt{5m}}{7} \right)$$

$$= \frac{b\sqrt{5m}}{2\sqrt{7}}$$

Thus providing the damping coefficient,  $\zeta = \frac{b\sqrt{5m}}{2\sqrt{7}}$ , is

$\zeta$

The System would present oscillations within an impulse response providing:

$$0 < \frac{b\sqrt{5m}}{7} < 1$$