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# Hydration-based multi-physics modelling of cementitious materials for 3D printing

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### Context and motivation

- Extrusion-based 3D printing with cementitious materials is a growing technology allowing for optimal use of material and freedom of form
- However, there is a lack of simulation tools able to predict stability during printing as well as durability in the service life
- Cementitious materials **involve coupled mechanisms** which cannot be ignored
- Detailed simulation of 3D printing with cement-based materials could help determine key parameters within the process or material mix designs

#### A simulation framework for 3D printing of cement-based materials

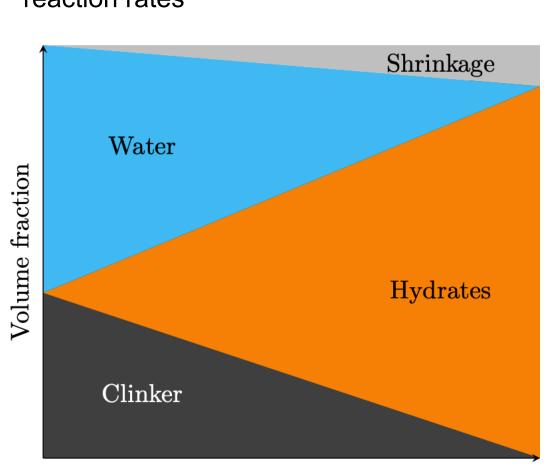
#### **Material Model**

#### Fully coupled thermo-hydro-chemo-mechanics :

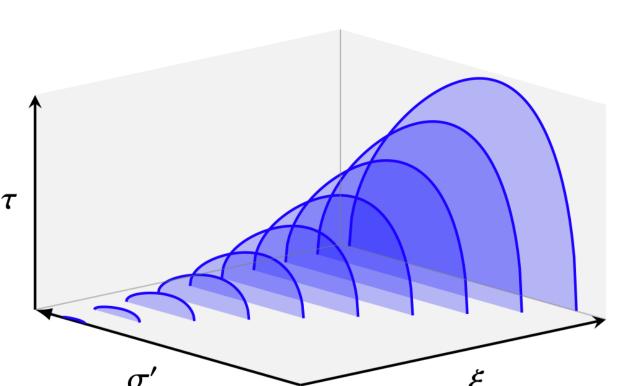
$$(\underline{\underline{\sigma}}, m_f, S, \mathcal{A}_i) = f(\underline{\underline{\varepsilon}}, p_f, T; \xi_i)$$

Driven by **hydration** reactions  $\xi_i$ :

- Hydration-dependent poroelasticity
- Evolving pore structure affecting the retention curve and permeability
- Unsaturated state affecting permeability and hydration reaction rates



 $\begin{array}{c} \alpha \\ \text{Water consumption and shrinkage} \end{array}$ 



Yield surface with chemical hardening
(Asymmetric Cam-Clay model)

0.8

0.6

0.4

0.2

0.2

0.2

0.30°C

-40°C

Time (min)

Hydration kinetics

# External actions

## Mechanical:

Vertical pressure at the printer nozzle from mortar flow

# Thermal:

- Convective heat flux at mortar/air interfaces
   Hydro-thermal:
- Evaporation flux at mortar/air interfaces
   dependent internal and external temperatures,
   relative humidities and wind speed



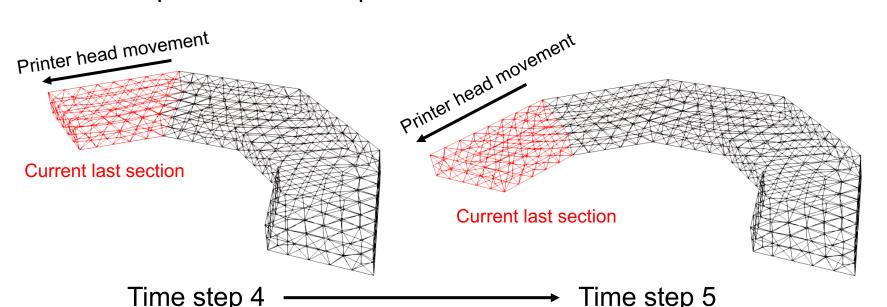
3D simulation of a vase during printing

Magnified displacements

Red colour indicates yielded regions

# Finite element process modelling

- Automated reconstruction of mesh from robot toolpath and lace section
- Mesh-conforming internal boundaries
  for good mesh segmentation at each
  time step
- Both 3D et 2D axisymmetric methods
- Modelling of the printing process through **sequential addition of material**:
- Each time step has a different mesh
- Results of previous time steps are used as initial state for the next



# Conclusions and perspectives

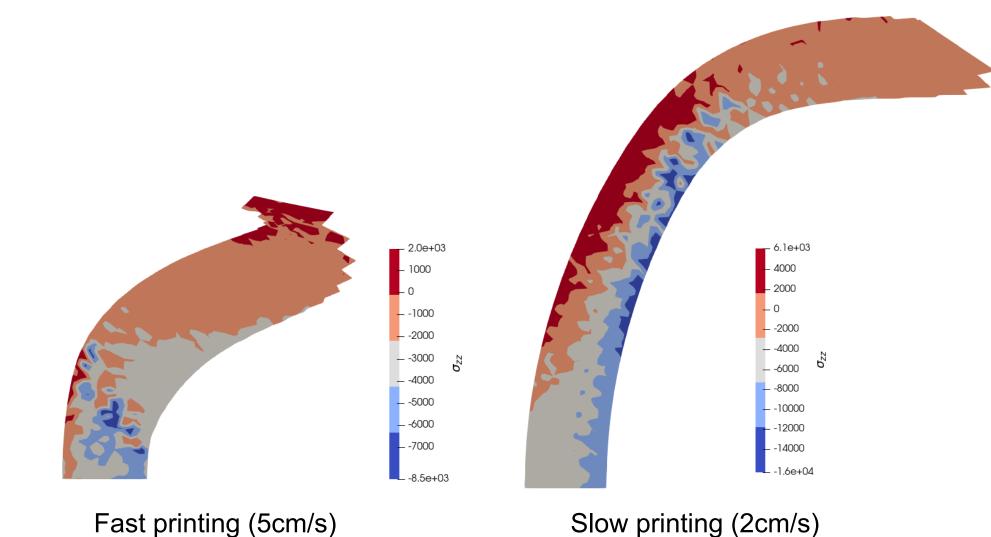
- Showcased is a **new framework for concrete 3D printing simulation** based on a coupled **multiphysics material model** along with a **finite element** tool handling **sequential deposition of the material** as well as external actions during printing
- This framework reveals **several interesting mechanisms** which are worth exploring further, such as the **effect of room temperature** on printing or the **role of the retention curve** in early age stability of 3D printing mortars
- Experimental comparison with imaging methods on live printings could allow for a validation of the framework along with a fine-tuning of certain model parameters

## Plastic failure modes – Printing speed dependence

Printed geometry (axisymmetric corolla)

- 40 Layers height
- Plastic failure does not always occur at the bottommost layer
- It is then hard to use simple
   analytical tools to predict plastic
   collapse of general object, hence the
   need for effective simulation

   frameworks

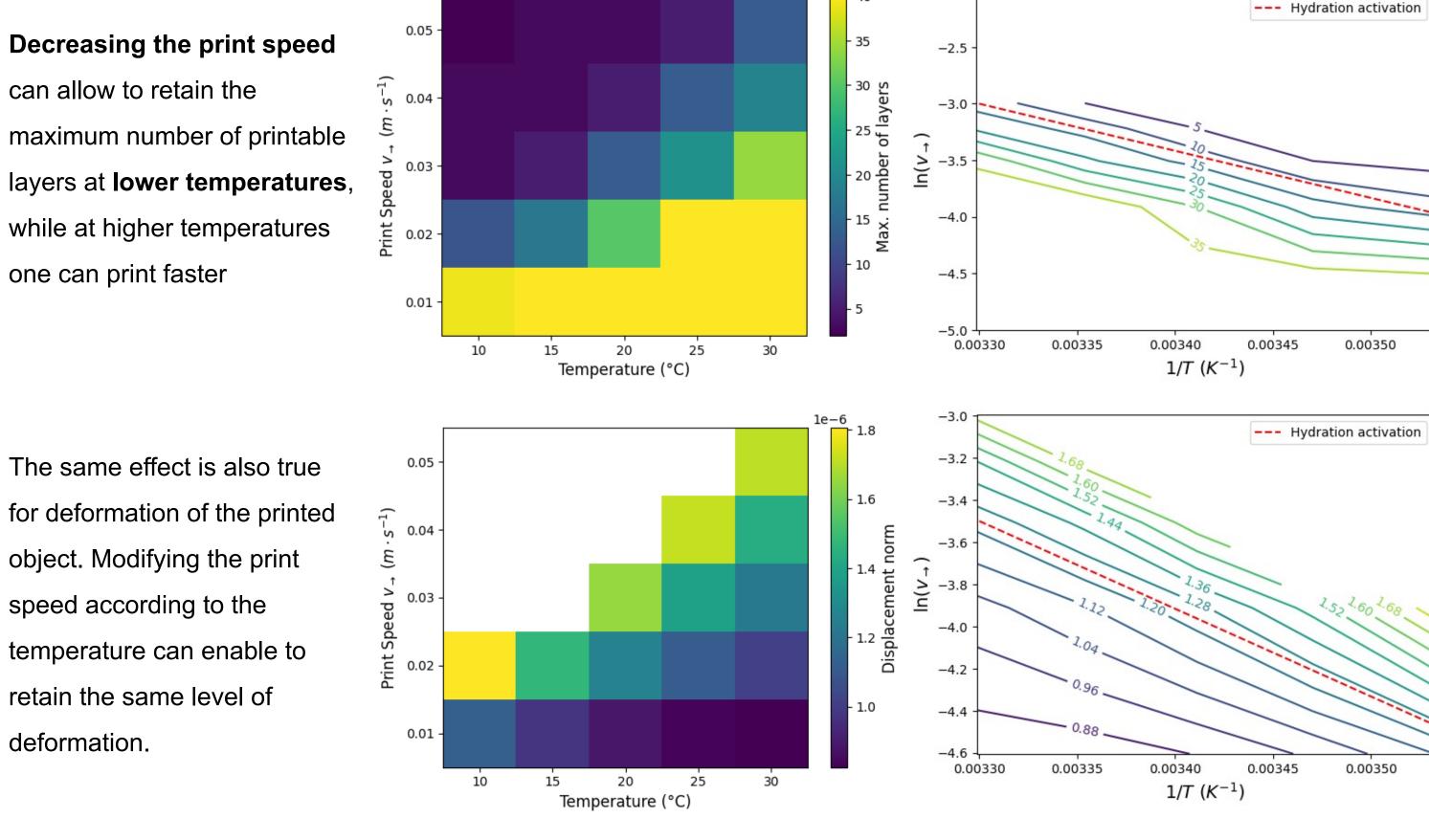


Magnified displacements showing plastic failure mechanisms (Colour is vertical stress)

#### Temperature/print speed effects and trade-off

Printing at different temperatures impacts stability and accuracy of the printing due to modified hydration kinetics:

Can we make up for this impact by adequately modifying the printing speed?



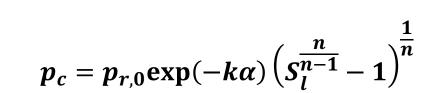
• This effect could be seen as thermo-activated:

$$v_{\rightarrow}(T) \simeq v_{\rightarrow}(T_0) \exp\left(-\frac{E_A}{R(T-T_0)}\right)$$

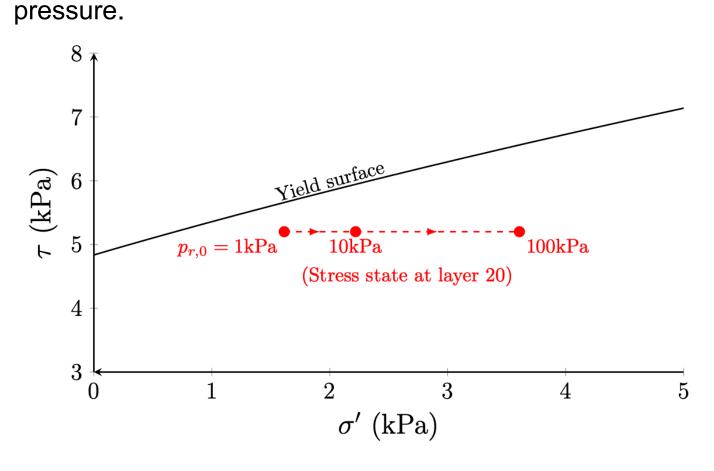
• It has been verified on several geometries that the activation energy  $E_A$  can be taken as that of the hydration reaction (right-side graphs above): it could be used as a rule of thumb for practical applications such as outdoors printing.

#### Retention curve effect on buildability

- Water consumption from hydration and low W/C ratio mixes used in 3D printing lead to a quick desaturation of the medium
- The changing pore structure induces an evolution of the retention curve. Suction is a function of saturation and hydration degree :



Yield is a function of effective stress: it is influenced by the pore



- 0.8 0.6 0.6 0.4 0.2 0.2 0.3 0.4 0.5 0.6 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
- Tailoring of the retention curve through mixes with finer aggregates for instance could improve buildability at a given cement content.
- With the corolla geometry at 2cm/s print speed, simulated printable heights would be:
  - 25 layers for  $p_{r,0} = 1$ kPa
  - 31 layers for  $p_{r,0} = 10$ kPa
  - 40+ layers for  $p_{r,0} = 100$ kPa

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