EUROPEAN ORGANISATION FOR THE SAFETY OF AIR NAVIGATION



EUROCONTROL EXPERIMENTAL CENTRE

USER MANUAL FOR THE BASE OF AIRCRAFT DATA (BADA) REVISION 3.10

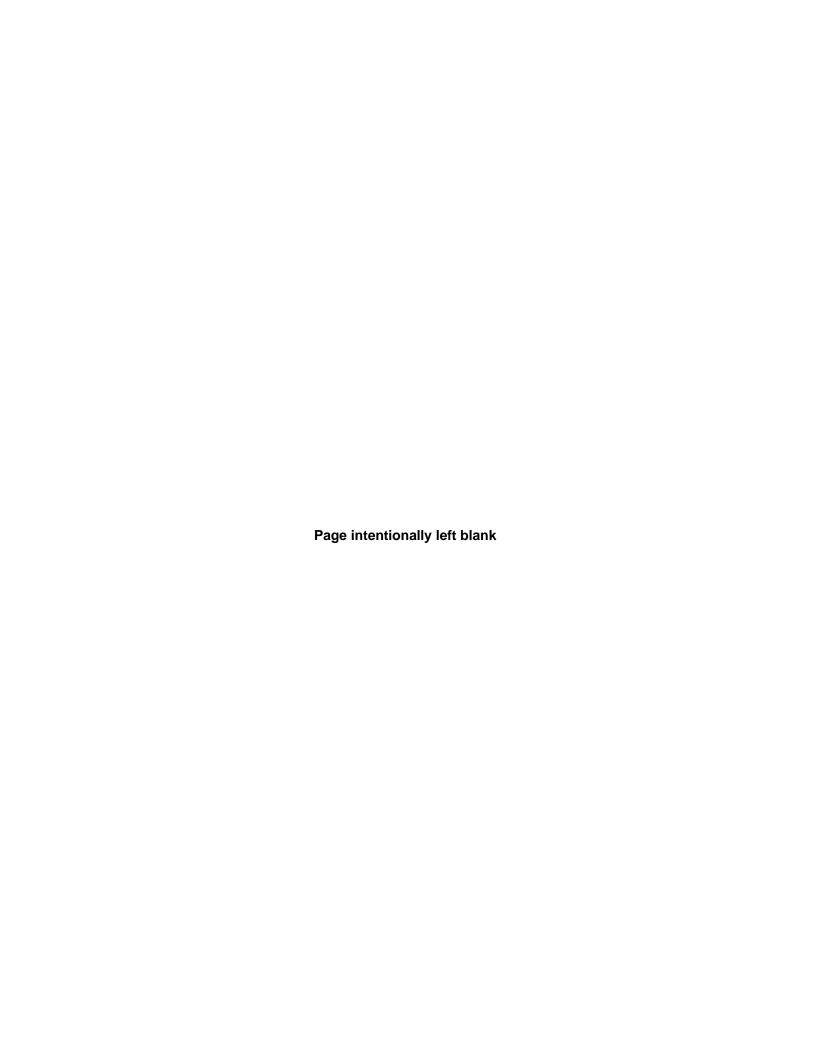
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Abstract:						
The Base of Aircraft Data (BADA procedure coefficients for 399 diff thrust, drag and fuel flow and the Manual for Revision 3.10 of BADA formats. Instructions for remotely a	ferent aircrainuse used to provides def	ft types. Th specify nor finitions of e	e coefficier minal cruise ach of the c	nts include e, climb and coefficients	those used to descent sp	to calculate eeds. User





SUMMARY

The Base of Aircraft Data (BADA) provides a set of ASCII files containing performance and operating procedure coefficients for 399 different aircraft types. The coefficients include those used to calculate thrust, drag and fuel flow and those used to specify nominal cruise, climb and descent speeds. The User Manual for Revision 3.10 of BADA provides definitions of each of the coefficients and then explains the file formats. Instructions for remotely accessing the files via Internet are also given.



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USER MANUAL MODIFICATION HISTORY

Issue Number	Release Date	Comments
Revision 2.1 Issue 1.0	31.05.94	First release of document
Revision 2.2 Issue 1.0	25.01.95	Released with BADA Revision 2.2 - 8 new aircraft models - 2 modified aircraft models - 2 modified equivalences - 6 removed equivalences - 14 new equivalences - modified file formats - additional Synonym File - corrections to formulas in previous version of document - additional description of total-energy and standard atmosphere equations
Revision 2.3 Issue 1.0	08.06.95	Released with BADA Revision 2.3 - document format modified to be consistent with EEC Technical Note standards - new A/C models for B73V and D328 - MD11 changed from equivalence to direct support - generic military fighter model, FGTR, replaces specific fighter models - maximum payload parameter added to all OPF files - Performance Tables Files (*.PTF) introduced - ISA equations used for TAS/CAS conversions instead of approximations (Section 3.2) - use only one formula for correction of speeds at mass values different from reference mass (Section 3.3) - add specification of minimum speed as function of stall speed (Section 3.4) - specification of transition altitude calculated added (Section 4.1) - speed schedules modified for climb (Section 4.1) and descent (Section 4.3) - modify Internet address for remote access and EUROCONTROL contact person (Section 6) - removed Section 7 (General Comments)



Issue Number	Release Date	Comments
Revision 2.4 Issue 1.0	04.01.96	Released with BADA Revision 2.4 - new A/C model for FK70 - C421 changed from equivalence to directly supported - 10 new equivalences - 1 modified equivalence - 3 re-developed models - introduction of dynamic maximum altitude - new temperature correction on thrust - modified max.alt for 4 models - modified minimum weight for 2 models - modified temperature coefficients for 12 models - esf calculation for constant CAS below tropopause changed from binomial approximation to exact formula - cruise Mach numbers changed for 4 models - change in altitude limit for descent speed
Revision 2.5 Issue 1.0	20.01.97	 re-developed models: EA32, B737, B73S, AT42, B767, DC9, BA46, FK10, MD80. new model: CL65, DH83 change of minimum speeds change of climb/descent speed schedules cruise fuel flow correction buffeting speed for jet a/c addition of BADA.GPF file definition of acceleration limits, bank angles and holding speeds 38 new equivalences added (SA4, SA5, SweDen 96) 1 modified equivalence (B74S) modified climb/cruise speeds (BE90, BE99, E120, PA42, FK50, B73F, B767,B747, B727, DA20) Format changes in OPF file Header changes in PTF file Temperature influence on thrust limitation changed Unit of Vstall in OPF file changed to KCAS Correction of typing errors Correction of APF file format explanation
Revision 2.6 Issue 1.0	01.09.97	 - Added non-clean drag and thrust data for: EA32, B73S, MD80, B737, B747, FK10, AT42, B767 and CL65 models - All models mentioned above were re-developed using new clean drag data. - ND16, E120 and FK50 were re-modelled to correct the cruise speed capability. - Change of speed schedule in the take-off / initial climb



Issue Number	Release Date	Comments
		phase and approach / landing phase
		- Change in descent thrust algorithm
		 Use of exact formula for density below tropopause instead of approximation.
		- Addition of formula for pressure above tropopause
		- Change of buffeting limit to 1.2g (was 1.3g)
		- Change of OPF file format
		 Buffeting coefficients for B757 and MD80 were corrected.
		- Hmo for B747 model was corrected to 45,000 ft
		- Low altitude descent behaviour corrected for: SW3, PAYE, DA50, DA10, D328, C421, BE99, BE20 and BE90 models
		- Correction of some minor typing errors
		- dynamic maximum altitude coefficients changed for B747, B74F, C130 and EA30
		- Saab 2000 (SB20) added as equivalent of D328
		- Modified algorithm for lift coefficient
Devision 2.0	04.02.00	Olimb and od law shounded for interrest
Revision 3.0 Issue 1.0	01.03.98	 Climb speed law changed for jet aircraft Descent speed law changed for jet, turbo and piston
		- Reduced power climbs
		- B777, SB20 and B73X models were added
		- DA01 model was removed
		- Use of ICAO doc. 8643/25 standard, which resulted in the removal of 4 additional models
		- B73F and B757 remodelled
		- MD90 added as equivalence model
		- Cruise and descent speeds for several turboprops changed
		- Climb thrust for several a/c changed
		- Removal of C_{m16} from drag expression
Revision 3.1	01.10.98	Released with BADA Revision 3.1
Issue 1.0	3 	Descent & cruise speeds for several jet aircraft changed: DC9, BA46, CL60
		- Descent, cruise & climb speeds for several turboprops changed: D228, SH36
		- Maximum Operating speed for several a/c changed: PA42
		- Stalling speed for several a/c changed: DC8, T154
		- Removed formula for air density calculation above tropopause
		Addition of Appendix D: Solutions for buffeting limit algorithm
		- Removed Section 3.7.2: Maximum Take-Off Thrust
		- Description for Cred parameter added



Issue Number	Release Date	Comments
		 Correction of some minor typing errors Modified PTF File format (Flight Level): Section 6.6 Cruise CAS schedule for jet & turbo aircraft (Section 4.2)
Revision 3.3 Issue 1.0		Released with BADA Revision 3.3 Standard atmosphere explanation added Correction of some typing errors, minor changes in the layout and equations presentation. Several aircraft types have changed ICAO's designator according to the ICAO doc.8643/27. Aircraft types affected by the RD3 are as follows: A300, ATR, B707, B727, B73A, B73B, B73C, B74A, B74B, B757, B767, B777, CARJ, DC8, DHC8, JSTA, JSTB, P31T, PA28, PA42. That resulted in: modification of the name of the OPF and APF files, addition of new models as synonyms, modification of Synonym.NEW and Synonym.LST files. B73A, B757, MD80, B73B, F100, B727, CARJ, FA20, FA50, D228, T154 aircraft models have been remodelled A319, A321, A306, AT72 models have been added Climb, cruise and descent speeds changed for several models. Ground TOL for B73C has been modified. MD80: Cd0 and Cd2 for IC and TO added, maximum altitude at MTOW, ISA weight gradient on maximum altitude Gw and temperature gradient Gt on maximum altitude Have been changed BA46 maximum altitude at MTOW, ISA weight gradient on maximum altitude Gw have been changed BA46 maximum altitude at MTOW, ISA weight gradient on maximum altitude Gw have been changed E145 was added as equivalent of CRJ1 A478 was added as equivalent of AT72
Revision 3.4 Issue 1.0	June 2002	Released with BADA Revision 3.4 - correction of some typing errors - in chapter 3.5 configuration threshold altitude values replaced with H _{max,i} while the corresponding numbers are listed in chapter 5.6 - Appendix B: a new column is added to the table; providing the information on maximum altitude that an aircraft can reach at MTOW (h _{max}) - FGTN aircraft model added - FGTL aircraft model added - FGTR aircraft model removed



Issue Number	Release Date	Comments		
		- DC-9 aircraft model re-modelled		
		- D228 cruise and descent speed modified		
		- SH36 cruise and descent speed modified		
		- B738 maximum operational altitude modified		
		- AT72 cruise speed corrected		
		- PA34 minimum mass modified		
		- B734 aircraft model added		
		- B735 aircraft model added		
		- E145 aircraft model added		
		- B737 aircraft model added		
		- AT45 aircraft model added		
		- B762 aircraft model added		
		- B743 aircraft model added		
		Removal of several existing OPF and APF files due to the change of ICAO aircraft designators according to RD3: A330, A340, BA46, DC9, MD80		
		- Addition of several new OPF and APF files due to the change of ICAO aircraft designators according to RD3: A333, A343, B461, DC94, MD83		
		 Addition of new equivalence aircraft types: A332, A342, A345, A346, B461, B462, B463, DC91, DC92, DC93, DC95, MD81, MD82, MD87, MD88, A124, AC80, AC90, AC95, AJET, AMX, AN72, ATLA, B1, B350, B739, B74D, BDOG, BE10, BE40, BE76, BER4, C17, C72R, C77R, C82R, C210, C212, C337, C526, C56X, CRJ7, E135, EUFI, F1, FT2H, F104, G222, GLF5, HAWK, H25A, H25C, IL96, JS1, JS3, JS20, LJ24, M20T, M20P, K35R, N262, P28T, P28B, PA32, PAY4, P68, PA44, SB05, T204, TBM7 		
		Modification of the value for Maximum bank angles for civil flight during HOLD in BADA.GPF file		
		Configuration Management of BADA files have been changed; files have been migrated from RCS to Continuus Configuration Management System. That resulted in the modification of the "identification" part of all BADA files given in the header.		
Revision 3.5	July 2003	Released with BADA Revision 3.5		
Issue 1.0		 correction of some typing errors 		
		- B712 aircraft model added		
		- LJ45 aircraft model added		
		- C750 aircraft model added		
		- RJ85 aircraft model added		



Issue Number	Release Date	Comments
		- B736 aircraft model added
		- B753 aircraft model added
		- A332 aircraft model added
		- B772 re-modelled
		- B738 re-modelled
		- B763 re-modelled
		- B703 WTC modified
		- JS41 WTC modified
		 Addition of new syn. aircraft types: P180, GLEX, C30J, J328, A7, B52, ETAR, F117, L159
		 Modification of BADA models for existing synonym aircraft types: C17, GLF3, GLF3, GLF4, GLF5
		- SYNONYM_ALL.LST file added.
Revision 3.6	July 2004	Released with BADA Revision 3.6
Issue 1.0		The following models of aircraft added in BADA 3.6: Dash 8-100: DH8A Boeing MD82: MD82 Boeing B767-400: B764 Boeing B777-300: B773 BAE 146-200: B462 The following models of aircraft have been re-modelled in BADA 3.6: Airbus A300B4-203: A30B Airbus A310: A310 Airbus A319: A319 Airbus A320: A320 Airbus A321: A321 Airbus A330-301: A333 Airbus A340-313: A343 Boeing B737-200: B732 Boeing B747-400: B744 Boeing B757-200: B752
		Addition of new synonym aircraft types: A3ST, ASTR, B701, C441, GALX, J728, K35A, K35E, L29B, LJ25, LJ60, NIM, PC12, R135, RJ1H, RJ70, P32R, C208, AA5, S76, DC3, BLAS, AEST, EC35, PAY1, PA18, BE55, C170, B461.
		Correction of syntax errors in BADA files:
		- Boeing B777-200: B772
		- ATR42-500: AT45



Issue Number	Release Date	Comments
D 0.7		D. L. W. BABA B
Revision 3.7 Issue 1.0	March 2009	 Released with BADA Revision 3.7 Modification of the values for constants g and R in Section 3. New description of formula 3.1-8 to match its actual use in some models. Coefficient CVmin, TO is no longer used in climb speed schedule, only in flight envelope determination. Numbering of several equations changed due to reorganisation of related sections. Change of descent thrust computation when CTdes,app and CTdes, Id are null in Section 3.7.3. Clarification of descent fuel flow computation in Section 3.9. Additional information on climb and descent speed schedules in Section 4. Update of some Fortran format descriptions in Section 6. Additional reasons for ROCD discontinuities added in Section 6.6. Introduction of new PTD file format. Update of Section 7 to describe the new means of access to the BADA files. Remodelling of 71 a/c types from BADA 3.6 - more details in [RD8]. Addition of 12 new a/c models for following a/c types: A346, A388, BE58, C510, CRJ2, CRJ9, DA42, DH8D, E135, E170, E190, EA50. All synonym aircraft have been re-evaluated and some reassigned – more details in [RD12] reassigned.
Revision 3.8 Issue 1.0	April 2010	Released with BADA Revision 3.8 - Introduction of new revised atmosphere model and relevant corresponding updates throughout the User Manual document
		 Harmonisation of acronyms for physical constants with the EEC Technical Report No. 2010-001, February 2010 "Revision of Atmosphere Model in BADA Aircraft Performance Model"
		 Clarification of descent fuel flow computation in Section 3.9.
		 Information added on whether some BADA model coefficients may or may not be negative.
		 Missing information about speed schedule in cruise for piston aircraft added (section 4.2)
		 Additional clarifications provided on use of altitudes in Section 4.
		- Additional explanatory note provided on data



Issue Number	Release Date	Comments
		presented in the PTF file.
		 Correction of error in the solution for buffeting limit algorithm.
		- Remodelling of 5 a/c types from BADA 3.7:
		B763, FA50, F900, RJ85, TRIN
		- Addition of 8 new a/c models:
		A318, A3ST, A345, B739, B77L, B77W, F2TH, FA7X.
		 23 new synonym aircraft added – more details in [RD12].
		- Regeneration of all PTF/PTD files
Revision 3.8	August 2010	Clarifications only, no impact on BADA implementations:
Issue 1.1		- Overall review of the document to fix formatting and typography problems.
		- Formula 3.1-19 (approximate value of a constant) removed, formula 3.1-4 added to define T _{ISA,trop} , and some formulas reordered in section 3.1
Revision 3.9	April 2011	Released with BADA Revision 3.9:
Issue 1.0		- Minor updates in the document
		 Clarification about speed calculation in Chapter 4.2. Cruise
		- Remodelling of 4 a/c types from BADA 3.8:
		A320, BE58, DA42, E135
		- Addition of 6 new a/c models:
		AT72, AT75, C56X, E50P, E55P,TBM7
		 17 new synonym aircraft added and 13 existing synonyms have been revised
Revision 3.10	April 2012	Released with BADA Revision 3.10:
Issue 1.0		 Corrected Fortran specification of the PTF file to match actual release files (it would miss the first digit of descent fuel flow in some cases)
		 Clarification about the impact of speed envelope on speed calculation in Chapters 4.1, 4.2 and 4.3
		 Slight change in the description of the buffeting limit algorithm to mention that the discriminant is not "always" but "usually" negative
		 Addition of 10 new a/c models: A342, B463, B748, B788, C172, C182, P180, RJ1H, SR22, TBM8
		 Full remodelling of 9 a/c types: A343, B462, C560, DH8D, F50, PA34, RJ85, SF34, TBM7



Issue Number	Release Date	Comments
		 Partial update of 16 a/c types: A3ST, A318, A345, A388, B722, B735, B739, B743, B763, B772, B77L, B77W, BE20, C56X, E190, F100
		 Addition of 61 new synonym aircraft and revision of 18 existing synonyms



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1. INTRODUCTION

1.1. IDENTIFICATION

This document is the User Manual for the Base of Aircraft Data (BADA) Revision 3.10. This manual replaces the previous User Manual for BADA Revision 3.9 [RD1].

1.2. PURPOSE

BADA is a collection of ASCII files which specifies operation performance parameters, airline procedure parameters and performance summary tables for 399 aircraft types. This information is designed for use in trajectory simulation and prediction algorithms within the domain of Air Traffic Management (ATM). All files are maintained within a configuration management system at the EUROCONTROL Validation Infrastructure Centre of Expertise located at the EUROCONTROL Experimental Centre (EEC) in Brétigny-sur-Orge, France.

This document describes the mathematical models on which the data is based and specifies the format of the files which contain the data. In addition, this document describes how the files can be remotely accessed.

1.3. DOCUMENT ORGANISATION

This document consists of seven sections including Section 1, the Introduction. A list of referenced documents along with a glossary of acronyms and symbols are included in this section.

- **Section 2:** Revision Summary, summarises the differences between BADA Revision 3.10 and the previous BADA Revision 3.9.
- **Section 3:** Operation Performance Models, defines the set of equations, which are used to parameterise aircraft performance. This includes models of aerodynamic drag, engine thrust, and fuel consumption. An atmosphere model is also provided.
- **Section 4:** Airline Procedure Models, defines the set of parameters which is used to characterise standard airline speed procedures for climb, cruise, and descent.
- **Section 5:** Global Aircraft Parameters, defines the set of global aircraft parameters that are valid for all, or a group of, aircraft.
- **Section 6:** File Structure, describes the files in which the BADA aircraft parameters are maintained. Six types of files are identified:
 - Synonym Files listing the supported aircraft types;
 - Operations Performance Files (OPF) containing the performance parameters for a specific aircraft type;
 - Airline Procedures Files (APF) containing speed procedure parameters for a specific aircraft type;
 - Performance Table Files (PTF) containing summary performance tables of true airspeed, climb/descent rates and fuel consumption at various flight levels for a specific aircraft type;
 - Performance Table Data (PTD) containing detailed performance data at various flight levels for a specific aircraft type;



• Global Parameters File (GPF) containing parameters that are valid for all aircraft or a group of aircraft, for instance all turboprops or all military aircraft.

Section 7: Remote File Access to BADA, provides instructions on how to remotely access BADA files from the EUROCONTROL computing facilities over the Internet.

Two appendices are also provided with this document. **Appendix A** provides a list of the aircraft types supported by BADA Revision 3.10 and **Appendix B** gives solutions for a buffeting limit algorithm.

1.4. REFERENCED DOCUMENTS

RD2 Aircraft Type Designators, ICAO Document 8643/40, 2012 edition, http://www.icao.int/publications/DOC8643/ RD3 Aircraft Modelling Standards for Future ATC Systems; EUROCONTROL Division E1 Document No. 872003, July 1987. RD4 Manual of the ICAO Standard Atmosphere; ICAO Document No. 7488, 2nd Edition, 1964. RD5 BADA Product Management Document; EEC Technical Report No. 2009-008, April 2009. RD6 Base of Aircraft Data (BADA) Aircraft Performance Modelling Manual: EEC Technical Report No. 2009-009, April 2009. RD7 Memo on the Calculation of Energy Share Factor; EEC/FAS/BYR/95/50; 22 November 1995. RD8 Revision Summary Document for the Base of Aircraft Data (BADA) Revision 3.10; EEC Technical/Scientific Report No. 12/04/10-46; April 2012. RD9 Aircraft Performance Summary Tables for the Base of Aircraft Data (BADA) Revision 3.10; EEC Technical/Scientific Report No. 12/04/10-47; April 2012. RD10 Aircraft Type Designators, ICAO Document 8643, Versions 24-40. RD11 BADA Support Application – User Guide, revision 1.1, August 2009. RD12 Synonym Aircraft Report for the Base of Aircraft Data (BADA) - Revision 3.10; EEC Technical/Scientific Report No. 12/04/10-49, April 2012. RD13 Model Accuracy Summary Report for the Base of Aircraft Data (BADA) - Revision 3.10; EEC Technical/Scientific Report No. 12/04/10-48, April 2012. RD14 Revision of Atmosphere Model in BADA Aircraft Performance Model: EEC Technical Report No. 2010-001, February 2010. RD15 Mathematical Handbook; M.R. Spiegel; 1968; McGraw-Hill book company.	RD1	User Manual for the Base of Aircraft Data (BADA) Revision 3.9; EEC Technical/Scientific Report No. 11/03/08-08, April 2011.		
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1.5. GLOSSARY OF ACRONYMS

AGL	Above Ground Level		
AGL			
APF	APF Airlines Procedures File		
ASCII American Standard Code for the Interchange of Information			
ATM Air Traffic Management			
BADA Base of Aircraft Data			
CAS	Calibrated Airspeed		
EEC	EUROCONTROL Experimental Centre		
ESF	Energy Share Factor		
ICAO	International Civil Aviation Organisation		
ISA	International Standard Atmosphere		
MLW	Maximum Landing Weight		
MSL	Mean Sea Level		
MTOW	Maximum Take-off Weight		
OPF	Operations Performance File		
PTD	Performance Table Data		
PTF	Performance Table File		
RCS	Revision Control System		
ROCD	Rate of Climb or Descent		
TAS	True Airspeed		
TEM	Total-Energy Model		



1.6. GLOSSARY OF SYMBOLS

A list of the symbols used in equations throughout this document is given below along with a description. Where appropriate, the engineering units typically associated with the symbol are also given.

а	speed of sound	[m/s]
d	distance	[nautical miles]
f	fuel flow	[kg/min]
g ₀	gravitational acceleration	$[m/s^2]$
$\frac{dh}{dt}$	vertical speed	[m/s] or [ft/min]
h	geodetic altitude	[metres] or [ft]
Н	geopotential altitude	[metres] or [ft]
H_{p}	geopotential pressure altitude	[metres] or [ft]
С	general coefficient	
D	drag force	[Newtons]
m	aircraft mass	[tonnes] or [kg]
M	Mach number	[-]
р	Actual pressure	[Pa]
p_0	Standard pressure at MSL	[Pa]
R	real gas constant for air	$[m^2/(K \cdot s^2)]$
ROCD	Rate of Climb or Descent	[m/s] or [ft/min]
S	reference wing surface area	$[m^2]$
T	temperature	[Kelvin]
Thr	thrust	[N]
V	speed	[m/s] or [knots]
ΔΤ	temperature difference	[Kelvin]
W	weight	[N]
η	thrust specific fuel flow	[kg/(min·kN)]
ρ	air density	[kg/m³]



2. REVISION SUMMARY

This section summarises the aircraft types that are supported in BADA Revision 3.10 along with the updates that have been made from the previous release, BADA Revision 3.9.

2.1. SUPPORTED AIRCRAFT

BADA Revision 3.10 provides operations and procedures data for a total of 399 aircraft types. For 127 of these aircraft types, data is provided directly in files. These aircraft types are referred to as being directly supported and referred to as aircraft original models. The way they have been identified is described in [RD6]. For the other 272 aircraft types, the data is specified to be the same as one of the directly supported 127 aircraft types. These aircraft types have been identified as being 'equivalent' to original aircraft models. They are referred to as synonym aircraft. More details on the way they have been identified are given in [RD12].

With three exceptions, each supported aircraft type is identified by a 4-character designation code assigned by the International Civil Aviation Organisation (ICAO) [RD2]. The exceptions are the models representing generic military fighters, which use the designators: FGTH, FGTL, FGTN.

The list of aircraft types supported by BADA Revision 3.10 is given in Appendix A. In this Appendix the supported aircraft types are listed alphabetically by their designation code. For each aircraft type, the aircraft name and type of BADA support (either original or synonym) is specified. Also, for each synonym aircraft, which is supported through equivalence, the corresponding equivalent aircraft type is specified.

2.2. UPDATES FOR BADA REVISION 3.10

Updates made to BADA Revision 3.10 from the previous Revision 3.9 are listed below:

- (a) Updates of existing documentation.
- (b) Addition of 10 new aircraft models.
- (c) Full re-modelling of 9 aircraft models.
- (d) Partial update of 16 aircraft models.
- (e) Addition of new synonym aircraft.
- (f) Implementation of new ICAO aircraft designators according to the ICAO Doc. 8643 [RD2].

A more complete overview of all changes can be found in [RD8].



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3. OPERATIONS PERFORMANCE MODEL

This section defines the various equations and coefficients used by the BADA operations performance model.

The first two subsections describe the equations for atmospheric properties and the Total-Energy Model (TEM) equations respectively.

The remaining eight subsections define the aircraft model in terms of the eight categories listed below:

- aircraft type,
- · mass.
- flight envelope,
- aerodynamics,
- · engine thrust,
- · reduced power,
- · fuel consumption,
- · ground movement.

3.1. ATMOSPHERE MODEL

This section provides expressions for the atmospheric properties (pressure, temperature, density and speed of sound) as a function of altitude which are required for calculation of aircraft performances and movements¹. Conversions from CAS to TAS and Mach number also require the determination of several atmospheric properties as a function of altitude.

The most important equations for atmospheric properties used by BADA and CAS/TAS conversion are summarised in this chapter, while other expressions and more details are provided in [RD14].

3.1.1. Definitions

Mean Sea Level (MSL) Standard atmosphere conditions are those that occur in the International Standard Atmosphere (ISA) at the point where the geopotential pressure altitude H_p^2 is zero. They are denoted as T_0 , p_0 , p_0 and p_0 with the values listed below:

Standard atmospheric temperature at MSL: $T_0 = 288.15$ [K]

Standard atmospheric pressure at MSL: $p_0 = 101325$ [Pa]

Standard atmospheric density at MSL: $\rho_0 = 1.225$ [kg/m³]

Speed of sound: $a_0 = 340.294$ [m/s]

² Geopotential pressure altitude H_p is the geopotential altitude H that occurs in the ISA atmospheric conditions [RD14].

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¹ These equations are based on the International Standard Atmosphere (ISA) [RD4].



<u>Mean Sea Level (MSL)</u> atmosphere conditions are those that occur in a non-ISA atmosphere. They are identified by the sub-index MSL and differ from (T_0, p_0, ρ_0, a_0) in non-ISA conditions.

<u>Non-ISA atmospheres</u> are those that follow the same hypotheses as the ISA atmosphere but differ from it in that one or both of the following parameters is not zero:

- 1. **ΔT**. Temperature differential at MSL. It is the difference in atmospheric temperature at MSL between a given non-standard atmosphere and ISA.
- 2. **Δp**. Pressure differential at MSL. It is the difference in atmospheric pressure at MSL between a given non-standard atmosphere and ISA.

The values of these two parameters uniquely identify any non-ISA atmosphere. Thus, a non-ISA atmosphere provides expressions for the atmospheric pressure, temperature and density as functions of the geopotential altitude H³ and its two differentials. [RD14] provides more details on the corresponding analytical expressions.

3.1.2. Expressions

The relationships linking the atmospheric pressure p, temperature T, geopotential pressure altitude H_p and geopotential altitude H for any ISA⁴ and non-ISA atmosphere are provided below.

Physical constants which are used throughout this chapter are listed below:

Adiabatic index of air: $\kappa = 1.4$

Real gas constant for air: $R = 287.05287 [m^2/(K \cdot s^2)]$

Gravitational acceleration: $g_0 = 9.80665$ [m/s²]

ISA temperature gradient with altitude

below the tropopause: β_{T} = -0.0065 [K/m]

Note that subindex < denotes values below and at the tropopause and subindex > denotes values above the tropopause (as defined by 3.1-11).

Standard Mean Sea Level (subindex $H_p = 0$)

The temperature differential ΔT sets the value of the real temperature T in non-standard atmospheres.

$$H_{p,Hp=0} = 0 (3.1-1)$$

³ Geopotential altitude H is that which under the standard constant gravitational field provides the same differential work performed by the standard acceleration of free fall when displacing the unit of mass a distance dH along the line of force, as that performed by the geopotential acceleration when displacing the unit of mass a geodetic distance dh [RD14].

⁴ By replacing ΔT and Δp parameters with zeros the expressions are made applicable to the case of the standard atmosphere.



$$p_{Hp=0} = p_0 (3.1-2)$$

$$T_{ISA,Hp=0} = T_0$$
 (3.1-3)

$$T_{H_0=0} = T_0 + \Delta T \tag{3.1-4}$$

$$H_{Hp=0} = \frac{1}{\beta_{T,<}} \left[T_0 - T_{ISA,MSL} + \Delta T \cdot Ln \left(\frac{T_0}{T_{ISA,MSL}} \right) \right]$$
(3.1-5)

where T_{ISA} is the standard atmospheric temperature that occurs in the ISA atmosphere. It is a function of the geopotential pressure altitude H_{p} .

Mean Sea Level (subindex MSL)

The pressure differential Δp sets the value of the atmospheric pressure p.

$$H_{MSL}=0$$
 (3.1-6)⁵

$$p_{MSL} = p_0 + \Delta p \tag{3.1-7}$$

$$H_{p,MSL} = \frac{T_0}{\beta_{T,<}} \left[\left(\frac{p_{MSL}}{p_0} \right)^{-\frac{\beta_{T,<}R}{g_0}} - 1 \right]$$
 (3.1-8)

$$T_{ISA,MSL} = T_0 + \beta_{T,<} H_{D,MSL}$$
 (3.1-9)

$$T_{MSI} = T_0 + \Delta T + \beta_{T \le H_{DMSI}}$$
 (3.1-10)

Tropopause

Tropopause is the separation between two different layers: the troposphere, which stands below it, and the stratosphere, which is placed above. Its altitude $H_{p,trop}$ is constant when expressed in terms of geopotential pressure altitude:

$$H_{\text{p.trop}} = 11000 \,[\text{m}]$$
 (3.1-11)

⁵ In order to simplify the expressions, this document assumes that the geopotential altitude at mean sea level is always zero.



a) <u>Determination of Temperature</u>

$$T = f(H_{D}, \Delta T) \tag{3.1-12}$$

$$T_{c} = T_{0} + \Delta T + \beta_{T,c} H_{p,c}$$
 (3.1-13)

$$T_{ISA,trop} = T_0 + \beta_{T,<} H_{p,trop}$$
 (3.1-14)

$$T_{\text{trop}} = T_0 + \Delta T + \beta_{\text{T.<}} H_{\text{p,trop}}$$
(3.1-15)

$$T_{>} = T_{trop} \tag{3.1-16}$$

b) <u>Determination of Air Pressure</u>

$$p = f(T, \Delta T) \tag{3.1-17}$$

$$p_{<} = p_{0} \left(\frac{T_{<} - \Delta T}{T_{0}} \right)^{-\frac{g_{0}}{\beta_{T,<} R}}$$
 (3.1-18)

$$p_{trop} = p_0 \left(\frac{T_{trop} - \Delta T}{T_0} \right)^{-\frac{g_0}{\beta_{T,<} R}}$$
(3.1-19)

 $T_{>} = T_{trop}$, so $p_{>}$ does not directly depend on temperature $T_{>}$. For altitudes above the tropopause, the following formula should be used:

$$p_{>} = p_{trop} \exp \left[-\frac{g_0}{R T_{ISA,trop}} \left(H_{p,>} - H_{p,trop} \right) \right]$$
 (3.1-20)

where altitudes $H_{p,>}$ and $H_{p,trop}$ are expressed in metres.

c) <u>Determination of Air Density</u>

The air density, ρ , in kg/m³, is calculated from the pressure p and the temperature T at altitude using the perfect gas law:

$$\rho = \frac{\mathsf{p}}{\mathsf{R}\,\mathsf{T}}\tag{3.1-21}$$



d) <u>Determination of Speed of Sound</u>

The speed of sound, a, is the speed at which the pressure waves travel through a fluid and it is given by the expression:

$$a = \sqrt{\kappa R T}$$
 (3.1-22)

e) <u>CAS/TAS Conversion</u>

The true airspeed, V_{TAS} , is calculated as a function of the calibrated air speed, V_{CAS} , as follows:

$$V_{TAS} = \left[\frac{2}{\mu} \frac{p}{\rho} \left\{ \left(1 + \frac{p_0}{p} \left[\left(1 + \frac{\mu}{2} \frac{\rho_0}{p_0} V_{CAS}^2 \right)^{\frac{1}{\mu}} - 1 \right] \right)^{\mu} - 1 \right\} \right]^{\frac{1}{2}}$$
(3.1-23)

Similarly, V_{CAS} is calculated as a function of V_{TAS} as follows:

$$V_{CAS} = \left[\frac{2}{\mu} \frac{p_0}{\rho_0} \left\{ \left(1 + \frac{p}{p_0} \left[\left(1 + \frac{\mu}{2} \frac{\rho}{p} V_{TAS}^2 \right)^{\frac{1}{\mu}} - 1 \right] \right)^{\mu} - 1 \right\} \right]^{\frac{1}{2}}$$
 (3.1-24)

where symbols not previously defined are explained below:

$$\mu = \frac{\kappa - 1}{\kappa}$$
 ($\mu = \frac{1}{3.5}$ if $\kappa = 1.4$) (3.1-25)

Note that for these conversion formulas above, the speeds V_{TAS} and V_{CAS} must be specified in m/s.

f) Mach/TAS conversion

The true airspeed, V_{TAS} [m/s], is calculated as a function of the Mach number, M, as follows:

$$V_{TAS} = M \times \sqrt{\kappa R T}$$
 (3.1-26)



g) Mach/CAS transition altitude

The transition altitude (also called crossover altitude), $H_{p,trans}$ [ft], between a given CAS, V_{CAS} [m/s], and a Mach number, M, is defined to be the geopotential pressure altitude at which V_{CAS} and M represent the same TAS value, and can be calculated as follows:

$$H_{p, trans} = \left(\frac{1000}{0.3048 \cdot 6.5}\right) \cdot \left[T_0 \cdot (1 - \theta_{trans})\right]$$
 (3.1-27)

where θ_{trans} is the temperature ratio at the transition altitude,

$$\theta_{\text{trans}} = (\delta_{\text{trans}})^{-\frac{\beta_{\text{T,c}}R}{g_0}}$$
 (3.1-28)

where δ_{trans} is the pressure ratio at the transition altitude,

$$\delta_{\text{trans}} = \frac{\left[1 + \left(\frac{\kappa - 1}{2}\right)\left(\frac{V_{\text{CAS}}}{a_0}\right)^2\right]^{\frac{\kappa}{\kappa - 1}} - 1}{\left[1 + \frac{\kappa - 1}{2}M^2\right]^{\frac{\kappa}{\kappa - 1}} - 1}$$
(3.1-29)



3.2. TOTAL-ENERGY MODEL

The Total-Energy Model equates the rate of work done by forces acting on the aircraft to the rate of increase in potential and kinetic energy, that is:

$$(Thr - D) \cdot V_{TAS} = mg_0 \frac{dh}{dt} + mV_{TAS} \frac{dV_{TAS}}{dt}$$
(3.2-1)

The symbols are defined below with metric units specified:

Thr	-	thrust acting parallel to the aircraft velocity vector	[Newtons]
D	-	aerodynamic drag	[Newtons]
m	-	aircraft mass	[kilograms]
h	-	geodetic altitude	[m]
g_0	-	gravitational acceleration	[9.80665 m/s ²]
V_{TAS}	-	true airspeed	[m/s]
$\frac{d}{dt}$	-	time derivative	[s ⁻¹]

Note that true airspeed is often calculated in knots and altitude calculated in feet thus requiring the appropriate conversion factors.

Without considering the use of devices such as spoilers, leading-edge slats or trailing-edge flaps, there are two independent control inputs available for affecting the aircraft trajectory in the vertical plane. These are the throttle and the elevator.

These inputs allow any two of the three variables of thrust, speed, or rate of climb or descent (ROCD) to be controlled. The other variable is then determined by equation 3.2-1. The three resulting control possibilities are elaborated on below.

- (a) Speed and Throttle Controlled Calculation of Rate of Climb or Descent
 - Assuming that velocity and thrust are independently controlled, then equation 3.2-1 is used to calculate the resulting rate of climb or descent (ROCD). This is a fairly common case for climbs and descents in which the throttle is set to some fixed position (maximum climb thrust or idle for descent) and the speed is maintained at some constant value of calibrated airspeed (CAS) or Mach number.
- (b) ROCD and Throttle Controlled Calculation of Speed
 Assuming that the ROCD and thrust are independently controlled, then equation 3.2-1 is used to calculate the resulting speed.
- (c) Speed and ROCD Controlled Calculation of Thrust

 Assuming that both ROCD and speed are controlled, then equation 3.2-1 can be used to calculate the necessary thrust. This thrust must be within the available limits for the desired ROCD and speed to be maintained.



Case (a), above, is the most common such that equation 3.2-1 is most often used to calculate the rate of climb or descent. To facilitate this calculation, equation 3.2-1 can be rearranged as follows:

$$(Thr - D) \cdot V_{TAS} = mg_0 \frac{dh}{dt} + m V_{TAS} \left(\frac{dV_{TAS}}{dh}\right) \left(\frac{dh}{dt}\right)$$
(3.2-2)

Isolating the vertical speed on the left hand side gives:

$$\frac{dh}{dt} = \frac{(Thr - D) \cdot V_{TAS}}{mg_0} \left[1 + \left(\frac{V_{TAS}}{g_0} \right) \left(\frac{dV_{TAS}}{dh} \right) \right]^{-1}$$
(3.2-3)

Vertical speed is defined as the variation with time of the aircraft geodetic altitude h. The assumption of a standard constant gravity field derives in identical geodetic and geopotential altitudes H [RD14].

The ROCD is defined as the variation with time of the aircraft geopotential pressure altitude H_p . It is the preferred way of presenting the performances of an aircraft as it eliminates possible variations caused by the atmospheric conditions:

$$ROCD = \frac{dH_p}{dt} = \frac{T - \Delta T}{T} \frac{(Thr - D) \cdot V_{TAS}}{mg_0} \left[1 + \left(\frac{V_{TAS}}{g_0} \right) \left(\frac{dV_{TAS}}{dh} \right) \right]^{-1}$$
(3.2-4)

where:

T - atmosphere temperature [K];

 ΔT - temperature differential [K].

It has been shown by Renteux [RD3] that the last term can be replaced by an energy share factor as a function of Mach number, f{M}:

$$f\{M\} = \left[1 + \left(\frac{V_{TAS}}{g_0}\right) \cdot \left(\frac{dV_{TAS}}{dh}\right)\right]^{-1}$$
(3.2-5)

This leads to:

$$\frac{dh}{dt} = \left[\frac{(Thr - D) \cdot V_{TAS}}{mg_0} \right] f\{M\}$$
(3.2-6)

$$ROCD = \frac{dH_{P}}{dt} = \frac{T - \Delta T}{T} \left[\frac{(Thr - D) \cdot V_{TAS}}{mg_{0}} \right] f\{M\}$$
 (3.2-7)

This energy share factor f{M} specifies how much of the available power is allocated to climb as opposed to acceleration while following a selected speed profile during climb.



For several common flight conditions, equation 3.2-5 can be rewritten as is done below. A more comprehensive description of this process can be found in [RD7]:

(a) Constant Mach number in stratosphere (i.e. above tropopause)

$$f\{M\} = 1.0 (3.2-8)$$

Note that above the tropopause the air temperature and the speed of sound are constant. Maintaining a constant Mach number therefore requires no acceleration and all available power can be allocated to a change in altitude.

(b) Constant Mach number below tropopause:

$$f\{M\} = \left[1 + \frac{\kappa R \beta_{T,<}}{2 g_0} M^2 \frac{T - \Delta T}{T}\right]^{-1}$$
 (3.2-9)

In this case, for a typical Mach number of 0.8 the energy share factor allocated to climb is 1.09.

This number is greater than 1 because below the tropopause, the temperature and thus, speed of sound decreases with altitude. Maintaining a constant Mach number during climb thus means that the true airspeed decreases with altitude. Consequently, the rate of climb benefits from not only all the available power but also a transfer of kinetic energy to potential energy.

(c) Constant Calibrated Airspeed (CAS) below tropopause

$$f\{M\} = \left\{1 + \frac{\kappa R \beta_{T,<}}{2 g_0} M^2 \frac{T - \Delta T}{T} + \left(1 + \frac{\kappa - 1}{2} M^2\right)^{\frac{-1}{\kappa - 1}} \left\{ \left(1 + \frac{\kappa - 1}{2} M^2\right)^{\frac{\kappa}{\kappa - 1}} - 1 \right\} \right\}^{-1}$$
(3.2-10)

In this case the energy share factor is less than one. A Mach number of 0.6 for example yields an energy share factor of 0.85.

This number is less than 1 because as density decreases with altitude, maintaining a constant CAS during climb requires maintaining a continual increase in true airspeed. Thus, some of the available power needs to be allocated to acceleration leaving the remainder for climb.

(d) Constant Calibrated Airspeed (CAS) above tropopause.

$$f\{M\} = \left\{1 + \left(1 + \frac{\kappa - 1}{2}M^2\right)^{\frac{-1}{\kappa - 1}} \left\{ \left(1 + \frac{\kappa - 1}{2}M^2\right)^{\frac{\kappa}{\kappa - 1}} - 1 \right\} \right\}^{-1}$$
(3.2-11)

This formula is identical to (3.2-10), except that β_T is now null since we are above the tropopause.

The energy share factors given above apply equally well to descent as to climb. The difference being that the available power is negative for descent.



In cases where neither constant Mach number nor constant CAS is maintained, the following energy share factors are used:

acceleration in climb: f{M} = 0.3
 deceleration in descent: f{M} = 0.3
 deceleration in climb: f{M} = 1.7
 acceleration in descent: f{M} = 1.7

Note that, for the cases of acceleration in climb or deceleration in descent, the majority of the available power is devoted to a change in speed.

For the cases of deceleration in climb or acceleration in descent, the energy share factor is greater than 1 since the change of altitude benefits from a transfer of kinetic energy.



3.3. AIRCRAFT TYPE

Three values are specified for aircraft type, these being the number of engines, n_{eng} , the engine type and the wake category.

The engine type can be one of three values:

- Jet
- Turboprop
- Piston

The wake category can also be one of four values:

J: jumboH: heavyM: mediumL: light

Note that ICAO associates a wake category with each aircraft type designator [RD2].

3.4. MASS

Four mass values are specified for each aircraft in tonnes:

 $\begin{array}{ll} m_{\text{min}} & \text{- minimum mass} \\ m_{\text{max}} & \text{- maximum mass} \\ m_{\text{ref}} & \text{- reference mass} \end{array}$

m_{pvld} - maximum payload mass

Note that the specified mass limits are taken from aircraft performance reference data which is available in the BADA library. In function of specific aircraft certified limitations, a particular aircraft version of a given aircraft type (model) may have different limits. More details on the way the mass limits are selected in BADA are provided in [RD6].

Aircraft operating speeds vary with the aircraft mass. This variation is calculated according to the formula below:

$$V = V_{\text{ref}} \times \sqrt{\frac{m}{m_{\text{ref}}}}$$
 (3.4-1)

In this formula, the aircraft reference speed V_{ref} is given for the reference mass m_{ref} . The speed at another mass, m, is then calculated as V.

An example of an aircraft speed which can be calculated via this formula is the stall speed, V_{stall}.



3.5. FLIGHT ENVELOPE

(a) Maximum Speed and Altitude

The maximum speed and altitude for an aircraft are expressed in terms of the following six parameters:

V_{MO} - maximum operating speed (CAS) [kt]

M_{MO} - maximum operational Mach number

h_{MO} - maximum operating altitude [ft] above standard MSL

h_{max} - maximum altitude [ft] above standard MSL at MTOW under ISA

conditions (allowing about 300 ft/min of residual rate of climb)

G_w - mass gradient on h_{max} [ft/kg]

G_t - temperature gradient on h_{max} [ft/K]

The maximum altitude for any given mass is:

$$h_{\text{max/act}} = \text{MIN} \left[h_{\text{MO}}, h_{\text{max}} + G_{\text{t}} \times (\Delta T - C_{\text{Tc.4}}) + G_{\text{w}} \times (m_{\text{max}} - m_{\text{act}}) \right]$$
(3.5-1)

where: ΔT is the temperature deviation from ISA [K]

mact is the actual aircraft mass [kg]

with: $G_w \ge 0$

 $G_t \leq 0$

if $(\Delta T - C_{T_{C,4}}) < 0$, then: $(\Delta T - C_{T_{C,4}}) = 0$

Formula 3.5-1 should not be executed when the h_{max} value in the OPF file is set to 0 (zero). In that case the maximum altitude is always h_{MO} .

Note that the given speed and altitude limits are taken from available reference data: depending upon specific certifications, a particular aircraft of a given type may present different limits.

(b) Minimum Speed

The minimum speed for the aircraft is in function of aircraft stall speed and specified as follows:

$$V_{min} = C_{Vmin,TO} \times V_{stall}$$
 if in take-off (3.5-2)

$$V_{min} = C_{Vmin} \times V_{stall}$$
 otherwise (3.5-3)

Note: See Section 3.6.2 for minimum speed at high altitude for jet aircraft and Section 5.7 for the values of the minimum speed coefficients.

Here the speeds are specified in terms of CAS. The stall speed depends upon the configuration.



Specifically, five different configurations are specified with a stall speed, $(V_{stall})_{i}$, and configuration threshold altitude, $H_{max,i}$, given for each:

TO - take-off configuration
$$(V_{stall})_{TO}$$

(in climb up to H_{max,TO} AGL)

(in climb between $H_{max,TO}$ and $H_{max,IC}$ AGL)

(in climb above H_{max,IC} AGL,

in descent above H_{max,AP} AGL,

in descent below H_{max.AP} AGL when

$$V \ge V_{\text{min,cruise}} + 10 \text{ kt}$$

AP - approach configuration
$$(V_{stall})_{AP}$$

(in descent between H_{max,AP} AGL and H_{max,LD} AGL when

$$V < V_{min.cruise} + 10 kt$$

in descent below H_{max ID} AGL when

$$V_{min,cruise} + 10 \text{ kt} > V \ge V_{min,approach} + 10 \text{ kt}$$

(in descent below H_{max,LD} AGL when

$$V < V_{min,approach} + 10 \text{ kt}$$

The threshold altitudes are expressed in terms of geopotential pressure altitude. However, when aircraft operations close to the ground are considered, one has to account for airport/runway elevation⁶. The pressure altitude thresholds provided above correspond to geopotential pressure altitude Above Ground Level (AGL).

The stall speeds correspond to a minimum stall speed and not a 1-g stall speed. Also, the BADA model assumes that for any aircraft these stall speeds have the following relationship:

$$(V_{stall})_{CR} \geq (V_{stall})_{IC} \geq (V_{stall})_{TO} \geq (V_{stall})_{AP} \geq (V_{stall})_{LD}$$

The configuration specific values are listed in Section 5.6. The speeds V used during the descent, approach and landing phases are defined in Section 4.3.

⁶ Measured from Mean Sea Level (MSL).



3.6. AERODYNAMICS

3.6.1. Aerodynamic Drag

The lift coefficient, C_L , is determined assuming that the flight path angle is zero. However, a correction for a bank angle ϕ is made.

$$C_{L} = \frac{2 \cdot m \cdot g_{0}}{\rho \cdot V_{TAS}^{2} \cdot S \cdot \cos \phi}$$
 (3.6-1)

Under nominal conditions, the drag coefficient, C_D is specified as a function of the lift coefficient C_L as follows:

$$C_{D} = C_{DOCR} + C_{D2CR} \times (C_{L})^{2}$$
 (3.6-2)

Formula 3.6-2 is valid for all situations except for the approach and landing where other drag coefficients are to be used.

In the approach configuration (as defined in Section 3.5) a different flap setting is used, and formula 3.6-3 should be applied:

$$C_{D} = C_{D0,AP} + C_{D2,AP} \times (C_{L})^{2}$$
 (3.6-3)

In the landing configuration (as defined in Section 3.5) a different flap setting is used, and formula 3.6-4 should be applied:

$$C_{D} = C_{D0,LDG} + C_{D0,\Delta LDG} + C_{D2,LDG} \times (C_{L})^{2}$$
 (3.6-4)

The value of $C_{D0,\Delta LDG}$ represents drag increase due to the landing gear. The values of $C_{D0,LD}$ in the OPF files were all determined for the landing flap setting mentioned in the OPF file.

The drag force [Newtons] is then determined from the drag coefficient in the standard manner:

$$D = \frac{C_D \cdot \rho \cdot V_{TAS}^2 \cdot S}{2}$$
 (3.6-5)

Where:

 ρ is the air density [kg/m³] S is the wing reference area [m²] V_{TAS} is the true airspeed [m/s].

Note that the air density is a function of altitude as described in Section 3.1.



The above equations thus result in eight coefficients for the specification of drag:

 $\begin{array}{lll} S & & & & \\ C_{D0,CR} & & C_{D2,CR} \\ C_{D0,AP} & & C_{D2,AP} \\ C_{D0,LD} & & C_{D2,LD} \\ C_{D0,ALDG} & & & \end{array}$

In case the $C_{D0,AP}$, $C_{D2,AP}$, $C_{D0,LD}$, $C_{D2,LD}$ and $C_{D0,\Delta LDG}$ coefficients (referred to as "non-clean" data in this document) are set to 0 (zero) in the OPF file, expression 3.6-2 will be used in all cases.

3.6.2. Low Speed Buffeting Limit (jet aircraft only)

For jet aircraft a low speed buffeting limit has been introduced. This buffeting limit is expressed as a Mach number and can be determined using the following equation:

$$k \times M^3 - C_{Lbo (M=0)} \times M^2 + \frac{W}{S \cdot p \cdot 0.583} = 0$$
 (3.6-6)

where:

k is lift coefficient gradient

C_{Lbo (M=0)} is initial buffet onset lift coefficient for M=0

p is actual pressure [Pa]

M is Mach number

S is the wing reference area [m²]

W is aircraft weight [N]

Note that the factor of 0.583 gives a 0.2 g margin.

The k and $C_{Lbo\ (M=0)}$ parameters have been determined for nearly all jet aircraft in BADA Revision 3.10. If the k and $C_{Lbo\ (M=0)}$ parameters in the OPF file are set to 0 (zero), the minimum speed is given by expressions 3.5-2 and 3.5-3. Otherwise, the solution for M in Formula 3.6-6 can be obtained using the method given in Appendix B. The buffeting limit should be applied as a minimum speed in the following way:

- If $(H_p \ge 15,000 \text{ ft})$ then: $V_{min} = MAX(V_{min,stall}, M_b)$

- If $(H_p < 15,000 \text{ ft})$ then: $V_{min} = V_{min,stall}$

where: H_D is the geopotential pressure altitude

M_b is the lowest positive solution of expression 3.6-6

 $V_{\text{min.stall}}$ is given by expressions 3.5-2 and 3.5-3

Note that the units of the two values $V_{min,stall}$ and M_b inside the MAX() expression should be the same.



3.7. ENGINE THRUST

The BADA model provides coefficients that allow the calculation of the following thrust levels:

- · maximum climb and take-off,
- maximum cruise,
- · descent.

The thrust is calculated in Newtons and includes the contribution from all engines. The subsections below provide the equations for each of the thrust conditions.

3.7.1. Maximum Climb and Take-Off Thrust

The maximum climb thrust at standard atmosphere conditions, $(Thr_{max\ climb})_{ISA}$, is calculated in Newtons as a function of the following information:

- engine type: either Jet, Turboprop or Piston;
- geopotential pressure altitude, H_p [ft];
- true airspeed, V_{TAS} [kt];
- temperature deviation from standard atmosphere, ΔT [K].

The equations corresponding to the three engine types are given below.

Jet:
$$\left(Thr_{max climb}\right)_{ISA} = C_{Tc,1} \times \left(1 - \frac{H_p}{C_{Tc,2}} + C_{Tc,3} \times H_p^2\right)$$
 (3.7-1)

Turboprop:
$$\left(\text{Thr}_{\text{max climb}}\right)_{\text{ISA}} = \frac{C_{\text{Tc,1}}}{V_{\text{TAS}}} \times \left(1 - \frac{H_p}{C_{\text{Tc,2}}}\right) + C_{\text{Tc,3}}$$
 (3.7-2)

Piston:
$$\left(Thr_{max \, climb}\right)_{ISA} = C_{Tc,1} \times \left(1 - \frac{H_p}{C_{Tc,2}}\right) + \frac{C_{Tc,3}}{V_{TAS}}$$
 (3.7-3)

For all engine types, the maximum climb thrust is corrected for temperature deviations from standard atmosphere, ΔT , in the following manner:

$$Thr_{max climb} = (Thr_{max climb})_{ISA} \times (1 - C_{Tc,5} \cdot \Delta T_{eff})$$
 (3.7-4)

Where:

$$\Delta T_{\text{eff}} = \Delta T - C_{\text{Tc.4}} \tag{3.7-5}$$

with the limits:

$$0.0 \le \Delta T_{\text{eff}} \times C_{\text{Tc.5}} \le 0.4$$
 (3.7-6)

and:

$$C_{Tc.5} \ge 0.0$$
 (3.7-7)

This maximum climb thrust is used for both take-off and climb phases.



3.7.2. Maximum Cruise Thrust

The normal cruise thrust is by definition set equal to drag (Thr = D). However, the maximum amount of thrust available in cruise situation is limited. The maximum cruise thrust is calculated as a ratio of the maximum climb thrust given by expression 3.7-4, that is:

$$(Thr_{cruise})_{MAX} = C_{Tcr} \times Thr_{max climb}$$
 (3.7-8)

The coefficient C_{Tcr} is currently uniformly set for all aircraft (see Section 5.5).

3.7.3. Descent Thrust

Descent thrust is calculated as a ratio of the maximum climb thrust given by expression 3.7-4, with different correction factors used for high and low altitudes, and approach and landing configurations (see Section 3.5), that is:

if
$$H_p > H_{p,des}$$
:
$$Thr_{des,high} = C_{Tdes,high} \times Thr_{max\,climb} \tag{3.7-9}$$

if $H_p \le H_{p,des}$:

Cruise configuration:
$$Thr_{des,low} = C_{Tdes,low} \times Thr_{max climb}$$
 (3.7-10)

Approach configuration:
$$Thr_{des,app} = C_{Tdes,app} \times Thr_{max climb}$$
 (3.7-11)

Landing configuration:
$$Thr_{des,Id} = C_{Tdes,Id} \times Thr_{max climb}$$
 (3.7-12)

Note that for those models where "non-clean" data (see Section 3.6.1) is available, $H_{p,des}$ cannot be below $H_{max,AP}$.



3.8. REDUCED CLIMB POWER

The reduced climb power has been introduced to allow the simulation of climbs using less than the maximum climb setting. In day-to-day operations, many aircraft use a reduced setting during climb in order to extend engine life and save cost. The correction factors that are used to calculate the reduction in power have been obtained in an empirical way and have been validated with the help of air traffic controllers.

In BADA, climbs that are performed using the full climb power will result in profiles that match the reference data that is found in the Flight Manual of the aircraft. Climbs with reduced power will give a realistic profile.

$$C_{pow,red} = 1 - C_{red} \times \frac{m_{max} - m_{act}}{m_{max} - m_{min}}$$
(3.8-1)

The value of C_{red} is a function of the aircraft type and is given in Section 5.11.

Nevertheless:

If
$$H_p < (0.8 \cdot h_{max})$$
:
$$C_{red} = f \; (aircraft \; type) \qquad (see \; Section \; 5.11)$$
 Else
$$C_{red} = 0 \qquad \qquad [dimensionless]$$

where h_{max} is given by expression 3.5-1.

The power reduction $C_{pow,red}$ is to be applied during the climb phase in expression 3.2-7, which becomes:

$$ROCD = \frac{dH_p}{dt} = \frac{T - \Delta T}{T} \frac{(Thr_{max \ climb} - D) \cdot V_{TAS} \cdot C_{pow,red}}{m \cdot g_0} \cdot f\{M\}$$
 (in climb) (3.8-2)



3.9. FUEL CONSUMPTION

3.9.1. Jet and Turboprop Engines

For the jet and turboprop engines, the <u>thrust specific fuel consumption</u>, η [kg/(min·kN)], is specified as a function of the true airspeed, V_{TAS} [kt]:

jet:
$$\eta = C_{f1} \times \left(1 + \frac{V_{TAS}}{C_{f2}}\right)$$
 (3.9-1)

turboprop:
$$\eta = C_{f1} \times \left(1 - \frac{V_{TAS}}{C_{f2}}\right) \times \left(\frac{V_{TAS}}{1000}\right)$$
 (3.9-2)

The nominal fuel flow, fnom [kg/min], can then be calculated using the thrust, Thr:

jet/turboprop:
$$f_{nom} = \eta \times Thr$$
 (3.9-3)

These expressions are used in all flight phases except during idle descent and cruise, where the following expressions are to be used.

The minimum fuel flow, f_{min} [kg/min], corresponding to idle thrust descent conditions for both jet and turboprop engines, is specified as a function of the geopotential pressure altitude, H_p [ft], that is:

jet/turboprop:
$$f_{min} = C_{f3} \left(1 - \frac{H_P}{C_{f4}} \right)$$
 (3.9-4)

Note that for both jet and turboprop engines, the idle thrust part of the descent stops when the aircraft switches to approach and landing configuration (see Section 3.5), at which point thrust is generally increased. Hence, the calculation of fuel flow during approach and landing phases shall be based on the nominal fuel flow (expressions 3.7-11, 3.7-12 and 3.9-3), and limited to the minimum fuel flow (expression 3.9-4) if necessary:

jet/turboprop:
$$f_{ab/d} = MAX (f_{nom}, f_{min})$$
 (3.9-5)

The <u>cruise fuel flow</u>, f_{cr} [kg/min], is calculated using the thrust specific fuel consumption η , the thrust Thr, and a cruise fuel flow factor, C_{fcr} :

jet/turboprop:
$$f_{cr} = \eta \times Thr \times C_{fcr}$$
 (3.9-6)

For the moment the cruise fuel flow correction factor has been established for a number of aircraft types whenever the reference data for cruise fuel consumption is available. This factor has been set to 1 (one) for all the other aircraft models.



3.9.2. Piston Engines

For piston engines, the nominal fuel flow, fnom [kg/min], is specified to be a constant, that is:

$$f_{\text{nom}} = C_{\text{f1}} \tag{3.9-7}$$

This expression is used in all flight phases except during descent and cruise, where the following expressions are to be used.

The $\underline{\text{minimum fuel flow}}$, f_{min} [kg/min], corresponding to descent conditions for piston engines, is specified to be a constant:

$$f_{min} = C_{f3}$$
 (3.9-8)

The <u>cruise fuel flow</u>, f_{cr} [kg/min], is calculated using a cruise fuel flow factor, C_{fcr}:

$$f_{cr} = C_{f1} \times C_{fcr} \tag{3.9-9}$$

For the moment the cruise fuel flow correction factor has been established for a number of aircraft types whenever the reference data for cruise fuel consumption is available. This factor has been set to 1 (one) for all the other aircraft models.

3.10. GROUND MOVEMENT

Four values are specified that can be of use when simulating ground movements. These parameters are:

- TOL: FAR Take-Off Length [m] with MTOW on a dry, hard, level runway under ISA conditions and no wind.
- LDL: FAR Landing Length [m] with MLW on a dry, hard, level runway under ISA conditions and no wind.
- span: aircraft wingspan [m]length: aircraft length [m]

Note that currently the value of the MLW is not provided in BADA. Apart from these model specific parameters, there are also a number of ground speeds defined as general parameters in Section 5.10.



3.11. SUMMARY OF OPERATIONS PERFORMANCE PARAMETERS

A summary of the parameters specified by the BADA operations performance model is supplied in Table 3-1 below. This table excludes those parameters that have been set to zero.

Detailed information on how these parameters have been obtained during the process of BADA aircraft model identification using the aircraft performance reference documents is provided in [RD6].

Important notice: Parameters listed in bold in the Table 3-1 below should not be modified by the user as such modifications may impact the validity of the data provided in [RD13].

Table 3-1: BADA Operations Performance Parameter Summary

Model Category	Symbols	Units	Description
Aircraft type	n _{eng}	dimensionless	number of engines
(3 values)	engine type	string	either Jet, Turboprop or Piston
(5 values)	wake category	string	either J, H, M or L
Mass	m _{ref}	tonnes	reference mass
(4 values)	m _{min}	tonnes	minimum mass
	m _{max}	tonnes	maximum mass
	m _{pyld}	tonnes	maximum payload mass
Flight envelope	V _{MO}	knots (CAS)	maximum operating speed
(6 values)	M _{MO}	dimensionless	maximum operating Mach number
(6 14.465)	h _{MO}	feet	maximum operating altitude
	h _{max}	feet	max. altitude at MTOW and ISA
	G _w	feet/kg	weight gradient on max. altitude
	Gt	feet/K	temperature gradient on max. altitude
Aerodynamics	S	m ²	reference wing surface area
(16 values for jet	C _{D0,CR}	dimensionless	parasitic drag coefficient (cruise)
aircraft, only 14	C _{D2,CR}	dimensionless	induced drag coefficient (cruise)
values for others)	C _{D0,AP}	dimensionless	parasitic drag coefficient (approach)
	C _{D2,AP}	dimensionless	induced drag coefficient (approach)
	C _{D0,LD}	dimensionless	parasitic drag coefficient (landing)
	C _{D2,LD}	dimensionless	induced drag coefficient (landing)
	C _{D0,ALDG}	dimensionless	parasite drag coef. (landing gear)
	(V _{stall}) _i	knots (CAS)	stall speed [TO, IC, CR, AP, LD]
	C _{Lbo (M=0)}	dimensionless	Buffet onset lift coef. (jet only)



Model Category	Symbols	Units	Description
	K	dimensionless	Buffeting gradient (jet only)
Engine thrust	C _{Tc,1}	Newton (jet/piston) knot-Newton (turboprop)	1st max. climb thrust coefficient
(12 values)	C _{Tc,2}	feet	2nd max climb thrust coefficient
	C _{Tc,3}	1/feet ² (jet) Newton (turboprop) knot-Newton (piston)	3rd max. climb thrust coefficient
	C _{Tc,4}	K	1st thrust temperature coefficient
	C _{Tc,5}	1/K	2nd thrust temperature coefficient
	C _{Tdes,low}	dimensionless	low altitude descent thrust coefficient
	C _{Tdes,high}	dimensionless	high altitude descent thrust coefficient
	H _{p,des}	feet	transition altitude for calculation of descent thrust
	C _{Tdes,app}	dimensionless	approach thrust coefficient
	$C_{Tdes,Id}$	dimensionless	landing thrust coefficient
	$V_{des,ref}$	knots	reference descent speed (CAS)
	M _{des,ref}	dimensionless	reference descent Mach number
Fuel flow (5 values)	C _{f1}	kg/(min·kN) (jet) kg/(min·kN·knot) (turboprop) kg/min (piston)	1st thrust specific fuel consumption coefficient
	C _{f2}	knots	2nd thrust specific fuel consumption coefficient
	C _{f3}	kg/min	1st descent fuel flow coefficient
	C _{f4}	feet	2nd descent fuel flow coefficient
	C _{fcr}	dimensionless	cruise fuel flow correction coefficient
Ground	TOL	m	take-off length
movement	LDL	m	landing length
(4 values)	span	m	wingspan
·	length	m	length

Note that the following coefficients can have negative values:

K, G_t , $C_{Tc,2}$, $C_{Tc,3}$, $C_{Tdes,low}$, $C_{Tdes,high}$, C_{f2} , C_{f4} .



4. AIRLINE PROCEDURE MODELS

This section defines the standard airline procedures, which are parameterised by the BADA airline procedure models. Definition of the standard airline procedures in BADA is driven by a requirement to provide means of simulating standard or nominal aircraft operations using different simulation and modelling tools for various ATM applications.

The BADA airline procedure model is provided for three separate flight phases: climb, cruise and descent. For each of these phases and each aircraft model, the BADA airline procedure model requires the following information to determine aircraft speed schedule:

- 1. BADA airline procedure default speeds provided in Airline Procedure File (APF):
 - V₁ standard CAS [knots] below 10,000 ft;
 - V₂ standard CAS [knots] between 10,000 ft and Mach transition altitude;
 - M standard Mach number above Mach transition altitude:

where the Mach transition altitude is defined in Section 3.1 (g).

- Stall speeds for take-off and landing configurations provided in Operations Performance File (OPF)
- 3. Coefficients provided in the Section 5.7 and 5.8

The process of definition of the BADA airline procedure default speeds and choice of aircraft configurations in function of flight phase is described in [RD6]. The airline procedure model below 10,000 ft with corresponding coefficients (mentioned under item 3 above) have been defined taking into account aircraft manufacturer's performance reference data and aircraft operational data available at EUROCONTROL.

The fact that the way aircraft is operated varies significantly in function of specific airspace procedures and operating policies of locally dominant airlines is widely recognised. It is for that reason that the resulting speed schedules of the BADA standard airline procedure model may differ from a geographical location or of an aerospace's specific aircraft operation.

To account for the local aircraft operation characteristics and improve conformance of the simulated aircraft behaviour with real operations, the user of BADA is given a possibility to modify the BADA default speeds (as provided in APF file). The change of speed related APF parameters should be done in accordance with the BADA modelling procedure described in the Chapter 2.2.3 of [RD6].

However, the stall speeds (as provided in OPF file) and coefficients detailed in Section 5.7 and 5.8 are not subject to modification. The BADA User should not modify them.

The altitude levels, used for determination of CAS speed schedules and provided in the following chapters, are expressed in terms of geopotential pressure altitude. However, different reference datums for altitude measurement⁷ may be applied in function of the user application and its functional design choices.

The BADA Airline Procedure Model only identifies the possibility to introduce notion of different altitude altimetry for calculation of the CAS speed schedules in the user application. The implementation decision is left to the application owner.

-

⁷ Such as use of standard operational pressure settings used in aviation: QNH for MSL pressure, QFE for pressure at the airport reference point or QNE corresponding to standard MSL1013 hPa. These can be selected through the altimeter's pressure setting knob in the aircraft.



4.1. CLIMB

The following parameters are defined for each aircraft type to characterise the climb phase:

 $V_{\text{cl,1}}$ - standard climb CAS [knots] between 1,500/6,000 and 10,000 ft

V_{cl,2} - standard climb CAS [knots] between 10,000 ft and Mach transition altitude

M_{cl} - standard climb Mach number above Mach transition altitude

• For jet aircraft the following CAS schedule is assumed, based on the parameters mentioned above and the take-off stall speed:

from 0 to 1,499 ft	$C_{Vmin} \cdot (V_{stall})_{TO} + Vd_{CL,1}$	(4.1-1)
from 1,500 to 2,999 ft	$C_{Vmin} \cdot (V_{stall})_{TO} + Vd_{CL,2}$	(4.1-2)
from 3,000 to 3,999 ft	$C_{Vmin} \cdot (V_{stall})_{TO} + Vd_{CL,3}$	(4.1-3)
from 4,000 to 4,999 ft	$C_{Vmin} \cdot (V_{stall})_{TO} + Vd_{CL,4}$	(4.1-4)
from 5,000 to 5,999 ft	$C_{Vmin} \cdot (V_{stall})_{TO} + Vd_{CL,5}$	(4.1-5)
from 6,000 to 9,999 ft	min (V _{cl,1} , 250 kt)	
from 10,000 ft to Mach transition altitude	$V_{cl,2}$	
above Mach transition altitude	M_{cl}	

For turboprop and piston aircraft the following CAS schedule is assumed:

from 0 to 499 ft	$C_{Vmin} \cdot (V_{stall})_{TO} + Vd_{CL,6}$	(4.1-6)
from 500 to 999 ft	$C_{Vmin} \cdot (V_{stall})_{TO} + Vd_{CL,7}$	(4.1-7)
from 1,000 to 1,499 ft	$C_{Vmin} \cdot (V_{stall})_{TO} + Vd_{CL,8}$	(4.1-8)
from 1,500 to 9,999 ft	min (V _{cl,1} , 250 kt)	
from 10,000 ft to Mach transition altitude	$V_{cl,2}$	
above Mach transition altitude	McI	

Note 1: The take-off stall speed, $(V_{stall})_{TO}$, must be corrected for the difference in aircraft mass from the reference mass using formula 3.4-1. The values for $Vd_{CL,i}$ can be found in Section 5.

Note 2: The climb speed schedule shall determine an increasing speed from take-off to $V_{cl,1}$. To ensure that monotony, it is recommended to determine the speed schedule from the highest altitude to the lowest one, and to use at each step the speed of the higher altitude range as a ceiling value for the lower altitude range.

Note 3: Any speed from the schedule described above that would be lower (resp. higher) than the minimum (resp. maximum) speed determined for the same conditions using Section 3.5 (b) (resp. Section 3.5 (a)) shall be overriden by this minimum (resp. maximum) speed.



4.2. CRUISE

The following parameters are defined for each aircraft type to characterise the cruise phase:

V_{cr.1} - standard cruise CAS [knots] between 3,000 and 10,000 ft

V_{cr,2} - standard cruise CAS [knots] between 10,000 ft and Mach transition altitude

M_{cr} - standard cruise Mach number above Mach transition altitude

• For jet aircraft the following CAS schedule is assumed:

 $\begin{array}{lll} \text{from 0 to 2,999 ft} & & \text{min (V}_{\text{cr,1}}, \, 170 \,\, \text{kt)} \\ \text{from 3,000 to 5,999 ft} & & \text{min (V}_{\text{cr,1}}, \, 220 \,\, \text{kt)} \\ \text{from 6,000 to 13,999 ft} & & \text{min (V}_{\text{cr,1}}, \, 250 \,\, \text{kt)} \end{array}$

from 14,000 ft to Mach transition altitude $V_{cr,2}$ above Mach transition altitude M_{cr}

For turboprop and piston aircraft the following CAS schedule is assumed:

 $\begin{array}{lll} \text{from 0 to 2,999 ft} & & \text{min (V}_{\text{cr,1}}, \, 150 \,\, \text{kt)} \\ \text{from 3,000 to 5,999 ft} & & \text{min (V}_{\text{cr,1}}, \, 180 \,\, \text{kt)} \\ \text{from 6,000 to 9,999 ft} & & \text{min (V}_{\text{cr,1}}, \, 250 \,\, \text{kt)} \\ \end{array}$

from 10,000 ft to Mach transition altitude $V_{cr,2}$ above Mach transition altitude M_{cr}

Note: Any speed from the schedule described above that would be lower (resp. higher) than the minimum (resp. maximum) speed determined for the same conditions using Section 3.5 (b) (resp. Section 3.5 (a)) shall be overriden by this minimum (resp. maximum) speed.



4.3. DESCENT

The following parameters are defined for each aircraft type to characterise the descent phase:

V_{des,1} - standard descent CAS [knots] between 3,000/6,000 and 10,000 ft

V_{des,2} - standard descent CAS [knots] between 10,000 ft and Mach transition altitude

M_{des} - standard descent Mach number above Mach transition altitude

For jet and turboprop aircraft the following CAS schedule is assumed, based on the above parameters and the landing stall speed:

from 0 to 999 ft	$C_{Vmin} \cdot (V_{stall})_{LD} + Vd_{DES,1}$	(4.3-1)
from 1,000 to 1,499 ft	$C_{Vmin} \cdot (V_{stall})_{LD} + Vd_{DES,2}$	(4.3-2)
from 1,500 to 1,999 ft	$C_{Vmin} \cdot (V_{stall})_{LD} + Vd_{DES,3}$	(4.3-3)
from 2,000 to 2,999 ft	$C_{Vmin} \cdot (V_{stall})_{LD} + Vd_{DES,4}$	(4.3-4)
from 3,000 to 5,999 ft	min (V _{des,1} , 220)	
from 6,000 to 9,999 ft	min (V _{des,1} , 250)	
from 10,000 ft to Mach transition altitude	$V_{des,2}$	
above Mach transition altitude	M_{des}	

For piston aircraft the following CAS schedule is assumed:

from 0 to 499 ft	$C_{Vmin} \cdot (V_{stall})_{LD} + Vd_{DES,5}$	(4.3-5)
from 500 to 999 ft	$C_{Vmin} \cdot (V_{stall})_{LD} + Vd_{DES,6}$	(4.3-6)
from 1000 to 1,499 ft	$C_{Vmin} \cdot (V_{stall})_{LD} + Vd_{DES,7}$	(4.3-7)
from 1,500 to 9,999 ft	$V_{des,1}$	
from 10,000 ft to Mach transition altitude	$V_{des,2}$	
above Mach transition altitude	M_{des}	

Note 1: The landing stall speed, $(V_{stall})_{LD}$, must be corrected for the difference in aircraft mass from the reference mass using formula 3.4-1. The values for $Vd_{DES,i}$ can be found in Section 5.

Note 2: The descent speed schedule shall determine a decreasing speed from $V_{des,1}$ to landing. To ensure that monotony, it is recommended to evaluate the speed schedule from the highest altitude to the lowest one, and to use at each step the speed of the higher altitude range as a ceiling value for the lower altitude range.

Note 3: Any speed from the schedule described above that would be lower (resp. higher) than the minimum (resp. maximum) speed determined for the same conditions using Section 3.5 (b) (resp. Section 3.5 (a)) shall be overriden by this minimum (resp. maximum) speed.



5. GLOBAL AIRCRAFT PARAMETERS

5.1. INTRODUCTION

A number of parameters that have been described in Section 3 (Operations Performance Model) and Section 4 (Airline Procedure Model) have values that are independent of the aircraft type or model for which they are used. The values of these and other parameters which have general use, have been put in the Global Parameters File (BADA.GPF). This increases the flexibility and allows an easier evaluation of the values that are used.

The next section gives an overview of the parameters that are defined in the Global Parameters File. If relevant, it also indicates the formula in which the parameter should be used.

5.2. MAXIMUM ACCELERATION

Maximum acceleration parameters are used to limit the increment in TAS (longitudinal) or ROCD (normal). Two parameters are defined:

Name:	Description:	Value [ft/s²]:
a _{I,max (civ)}	maximum longitudinal acceleration for civil flights	2.0
a _{n,max (civ)}	maximum normal acceleration for civil flights	5.0

The two acceleration limits are to be used in the following way:

■ longitudinal acceleration:
$$|V_k - V_{k-1}| \le a_{l,max(civ)} \Delta t$$
 (5.2-1)

• normal acceleration:
$$|\gamma_k - \gamma_{k-1}| \le \frac{a_{n,\max(civ)}}{V} \Delta t$$
 (5.2-2)

where,

$$\gamma = \sin^{-1}\left(\frac{\dot{\mathbf{h}}}{\mathsf{V}}\right) \tag{5.2-3}$$

and,

γ is the climb/descent angle,
 V is the true airspeed [ft/s],
 k, k-1 indicate values at update intervals k and k-1,

 Δt is the time interval between k and k-1 [s]

The values for the maximum longitudinal acceleration for military flights, $a_{l,max (mil)}$, and for the maximum normal acceleration for military flights, $a_{n,max (mil)}$, are currently undefined.



5.3. BANK ANGLES

Nominal and maximum bank angles are defined separately for military and civil flights. These bank angles can be used to calculate nominal and maximum rate of turns.

Name:	Description:	Value [deg]:
$\phi_{hom,civ\;(TO,LD)}$	Nominal bank angles for civil flight during TO and LD	15
$\phi_{ m nom,civ}$ (OTHERS)	Nominal bank angles for civil flight during all other phases	35
$\phi_{nom,mil}$	Nominal bank angles for military flight (all phases)	50
$\phi_{max,civ\;(TO,LD)}$	Maximum bank angles for civil flight during TO and LD	25
$\phi_{max,civ}$ (HOLD)	Maximum bank angles for civil flight during HOLD	35
$\phi_{ m max,civ}$ (OTHERS)	Maximum bank angles for civil flight during all other phase	s 45
$\phi_{max,mil}$	Maximum bank angles for military flight (all phases)	70

The rate of turn, $\dot{\varphi}$, is calculated as a function of the bank angle:

$$\dot{\varphi} = \frac{g_0}{V_{TAS}} \times \tan(\phi) \tag{5.3-1}$$

5.4. EXPEDITED DESCENT

The expedited descent factor is to be used as a drag multiplication factor during expedited descents in order to simulate use of spoilers:

Name:	Description:	Value [-]:
$C_{des,exp}$	Expedited descent factor	1.6

The drag during an expedited descent is calculated using the nominal drag (see Section 3.6.1):

$$D_{\text{des,exp}} = C_{\text{des,exp}} \cdot D_{\text{nom}} \tag{5.4-1}$$

5.5. THRUST FACTORS

Maximum take-off and maximum cruise thrust factors have been specified. The $C_{Th,TO}$ factor is no longer used since BADA 3.0. The C_{Tcr} factor is to be used in expression 3.7-8.

Name:	Description:	Value [-]:
$C_{Th,TO}$	Take-off thrust coefficient	1.2
C_{Tcr}	Maximum cruise thrust coefficient	0.95



5.6. CONFIGURATION ALTITUDE THRESHOLD

For 4 configurations, altitude thresholds have been specified in BADA: take-off (TO), initial climb (IC), approach (AP) and landing (LD). Note that the selection of the take-off and initial climb configurations is defined only with the altitude. The selection of the approach and landing configurations is done through the use of air speed and altitude (see Section 3.5), while the altitudes at which the configuration change takes place should not be higher than the ones given below. The altitude values are expressed in terms of geopotential pressure altitude.

Name:	Description:	Value [ft]:
$H_{\text{max},TO}$	Maximum altitude threshold for take-off	400
$H_{\text{max,IC}}$	Maximum altitude threshold for initial climb	2,000
$H_{max,AP}$	Maximum altitude threshold for approach	8,000
$H_{max,LD}$	Maximum altitude threshold for landing	3,000

5.7. MINIMUM SPEED COEFFICIENTS

Two minimum speed coefficients are specified, which are to be used in expressions 3.5-2 and 3.5-3 and (for C_{Vmin} only) in Section 4.1 and 4.3:

Name:	Description:	Value [-]:
$C_{\text{Vmin},\text{TO}}$	Minimum speed coefficient for take-off	1.2
C_{Vmin}	Minimum speed coefficient (all other phases)	1.3

5.8. SPEED SCHEDULES

The speed schedules applicable below FL100 for climb and descent are based on a factored stall speed plus increment valid for a specified geopotential pressure altitude range.

Name:	Description:	Value [KCAS]:
$Vd_{CL,1}$	Climb speed increment below 1500 ft (jet)	5
$Vd_{CL,2}$	Climb speed increment below 3000 ft (jet)	10
$Vd_{CL,3}$	Climb speed increment below 4000 ft (jet)	30
$Vd_{CL,4}$	Climb speed increment below 5000 ft (jet)	60
$Vd_{CL,5}$	Climb speed increment below 6000 ft (jet)	80
$Vd_{CL,6}$	Climb speed increment below 500 ft (turbo/piston)	20
$Vd_{CL,7}$	Climb speed increment below 1000 ft (turbo/piston)	30
$Vd_{CL,8}$	Climb speed increment below 1500 ft (turbo/piston)	35
$Vd_{DES,1}$	Descent speed increment below 1000 ft (jet/turboprop)	5
$Vd_{DES,2}$	Descent speed increment below 1500 ft (jet/turboprop)	10
$Vd_{DES,3}$	Descent speed increment below 2000 ft (jet/turboprop)	20
$Vd_{DES,4}$	Descent speed increment below 3000 ft (jet/turboprop)	50
$Vd_{DES,5}$	Descent speed increment below 500 ft (piston)	5



$Vd_{DES,6}$	Descent speed increment below 1000 ft (piston)	10
$Vd_{DES,7}$	Descent speed increment below 1500 ft (piston)	20

These values are to be used in the expressions in Section 4.1 and 4.3.

5.9. HOLDING SPEEDS

The holding speeds that are to be used to calculate holding areas are defined according to the ICAO standards:

Name:	Description:	Value [KCAS]:
$V_{\text{hold},1}$	Holding speed below FL140	230
$V_{\text{hold,2}}$	Holding speed between FL140 and FL200	240
$V_{\text{hold,3}}$	Holding speed between FL200 and FL340	265
$V_{\text{hold,4}}$	Holding speed above FL340 [Mach]	0.83

Note that the holding speeds that are used by individual aircraft may vary between types.

5.10. GROUND SPEEDS

A number of ground speeds are defined for the simulation of ground movement. For the moment, no distinction between aircraft type or engine type is made. The following speeds have been defined:

Name:	Description:	Value [KCAS]:
$V_{\text{backtrack}}$	Runway backtrack speed	35
V_{taxi}	Taxi speed	15
V_{apron}	Apron speed	10
V_{date}	Gate speed	5

The runway backtrack speed is the speed the aircraft will maintain when it backtracks across the runway. The taxi speed is used anywhere between the runway and the apron area. The apron speed is used in the apron area while the gate speed is used for all manoeuvring between the gate position and the apron.

5.11. REDUCED POWER COEFFICIENT

The reduced power coefficients are defined for the three different engine types. It is stressed that the values given below were found in an empirical way and have been validated with the help of air traffic controllers:

Name:	Description:	Value [-]:
$C_{red,turbo}$	Maximum reduction in power for turboprops	0.25
$C_{red,piston}$	Maximum reduction in power for pistons	0.0
$C_{red,jet}$	Maximum reduction in power for jets	0.15

The coefficients should be used in Formula 3.8-1.



6. FILE STRUCTURE

6.1. FILE TYPES

All data provided by BADA Revision 3.10 are organised into six types of files:

- · three Synonym Files,
- · a set of Operations Performance Files,
- a set of Airline Procedure Files,
- a set of Performance Table Files.
- a set of Performance Table Data,
- a Global Parameter File.
- Three Synonym Files have the names:

SYNONYM.LST SYNONYM.NEW SYNONYM ALL.LST

The files provide a list of all the aircraft types which are supported by BADA and indicate whether the aircraft type is supported directly (through provision of parameters in other files) or supported by equivalence (through indicating an equivalent aircraft type that is supported directly). In addition to that, SYNONYM_ALL.LST file provides the information on history and evolution of the ICAO aircraft designators over the years. The format of the files is described in Section 6.3.

- There is one Operations Performance File (OPF) provided for each aircraft type which is directly supported. This file specifies parameter values for the mass, flight envelope, drag, engine thrust and fuel consumption that are described in Section 3. Details on the format of the OPF file are given in Section 6.4.
- There is one Airline Procedures File (APF) for each directly supported aircraft type. This file specifies the nominal manoeuvre speeds that are described in Section 4. Details on the format of the APF file are given in Section 6.5.
- There is one Performance Table File (PTF) for each directly supported aircraft type. This file contains a summary table of speeds, climb/descent rates and fuel consumption at various flight levels. Details on the format of the PTF file are given in Section 6.6.
- There is one Performance Table Data (PTD) file for each directly supported aircraft type. This file contains a detailed table of computed performance values at various flight levels. Details on the format of the PTD file are given in Section 6.7.
- Finally there is one Global Parameter File which is named BADA.GPF. This file contains
 parameters that are described in Section 5 and are valid for all aircraft or a group of aircraft (for
 instance all civil flights or all jet aircraft). Details on the format of the GPF file are given in
 Section 6.8.



The names of the OPF, APF, PTF and PTD files are based on the ICAO designation code for the aircraft type. With only the exception of the generic military fighter aircraft types (FGTH, FGTL, FGTN), this code is the same as the International Civil Aviation Organisation (ICAO) designator code for the aircraft type [RD2]. That is:

Note that there are at least two underscore characters between the ICAO code and the file extension such that the length of the file name without the extension is six characters. Most ICAO codes are four characters in length and thus have two underscore characters. Some ICAO codes, however, can be shorter (e.g. F50) and thus require more underscore characters. For example, an Airbus 310 which has the ICAO code of A310 is represented in BADA by the following files:

Operations Performance File:

Ailo_.OPF
Airline Procedures File:

Ailo_.APF
Performance Table File:

Ailo_.PTF
Performance Table Data:

Ailo_.PTD

The Fokker F50, which has the ICAO code of F50, is represented in BADA by the following files:

Operations Performance File: F50____.OPF
Airline Procedures File: F50____.APF
Performance Table File: F50____.PTF
Performance Table Data: F50____.PTD

All files belonging to BADA Revision 3.10, that is the Synonym Files, the GPF file and all APF, OPF, PTF and PTD files, are controlled within a configuration management system. This system is described in Section 6.2.

6.2. FILE CONFIGURATION MANAGEMENT

Starting with the BADA 3.4 release, the BADA Synonym Files, GPF and all APF, OPF, PTF and PTD files are placed and managed under the Change Management Synergy (CM Synergy) tool at EUROCONTROL.

This section briefly describes some of the CM Synergy features that will be used for the management of the BADA files.

CM Synergy provides a complete change management environment in which development and management of the files can be done easily, quickly, and securely. It maintains control of file versions and allows management of project releases with some of the benefits listed below:

- workflow management, which enables easy identification of the files modified to implement the change, and review of the reason for a change,
- project reproducibility by accurately creating baseline configurations,



- role-based security,
- Distributed Change Management (DCM) which allows files sharing among any number of CM Synergy databases. With DCM transfer of an entire database or a subset of a database can be done, either automatically or manually.

The CM Synergy automated migration facilities feature complete version history migration from RCS system archives. This has enabled to bring successfully all the BADA files with their history under the CM Synergy control. A CM Synergy database is created for BADA project. Such a database represents a data repository that stores all controlled data, including data files, their properties and relationships to one another.

The following BADA files are placed in the CM Synergy database:

- the Synonym Files
- the GPF file
- · all APF, OPF, PTF and PTD files

Within the CM Synergy, different methodologies in the way the files are managed are used. For BADA database, the task-based methodology is chosen which enables the tracking of the changes by using tasks, rather than individual files, as the basic unit of work.

The specific procedures used for configuration management are specified in the BADA Configuration Management Manual [RD5].

6.2.1. File Identification

Any file managed in a CM Synergy database is uniquely identified by the following attributes: *name*, *version*, *type*, *and instance*. By default, the four-part name (also called full name) is written like this: *name-version:type:instance*.

A file name can be up to 151 characters long, and the version can be any 32-character combination. The type can be any of the default types (e.g., *csrc*, *ascii*, etc.), or any BADA type that is created (APF, OPF, PTF, PTD, GPF).

The name, version, and type are designated by the user, but the instance is calculated by CM Synergy.

The version of a file corresponds to the evolution of the file in time. By default, CM Synergy creates version numbers, starting with 1, for each file that is created in the CM Synergy database. Each time the object is modified, CM Synergy increments the version.

The instance is used to distinguish between multiple objects with the same name and type, but that are not versions of each other.

It is important to notice that, following the CM Synergy approach of the file identification, no information on the file version is provided in the BADA file itself.

A new layout of the header of BADA files has been developed and it will be described in more details in the following sections.



6.2.2. History

The history of a file shows all the existing versions and the relationships between the versions. By history, CM Synergy means all of the file versions created before the current file version (called predecessors) and all of the file versions created after the current file version (called successors). This functionality allows for the tracking of all modifications to a file.

6.2.3. Release

The release is a label that indicates the version of the project, in this case the release of BADA files. BADA releases are usually identified by a two digit number, e.g. 3.3 or 3.4. However, the name of release in CM Synergy can be made out of any combination of alphabetic and numerical characters.

Like in the case of the file version, no information on the current BADA release is given in the BADA files.

6.2.4. Release Summary file

The ReleaseSummary file provides a list of all files delivered as part of the BADA release. It lists, for each BADA file, the file name and BADA release identification, which is the BADA release in which the file was last modified.



6.3. SYNONYM FILE FORMAT

6.3.1. SYNONYM.LST File

The SYNONYM.LST file is an ASCII file which lists all aircraft types which are supported by the BADA revision. An example of the SYNONYM.LST file is given below (partial listing).

CCC	ccccccc	ccccccccccccccccc	cccccccccc s	SYNONYM.LS	r ccc	cccccc	CCCC/			
CC	C BADA SYNONYM FILE									
CC CC	Fi	le_name: SYNONYM.LST					/			
CC	Creation_date: Mar 26 2002									
CC CC CC	Мо	dification_date: Mar	26 2002				/ /			
	===== A	ircraft List ======	========	:======			:====/			
CC	A/C CODE	NAME OR MODEL	FILE	S	YNONYI	MS	/ /			
		AIRBUS A300B4-600		A	306		/			
-	A30B	AIRBUS A300B4-200	A30B	A	30B	IL76				
-	A310	AIRBUS A310	A310	A	310					
-	A319	AIRBUS A319	A319	A	319					
-	A320	AIRBUS A320	A320	A	320	C17				
-	A321	AIRBUS A321	A321	A	321					
-	A333	AIRBUS A330-300	A333	A	333	A332				
-	A343	AIRBUS A340-300	A343	A	343	A342	A345			
						A346				
-	AT43	ATR ATR 42-300	AT43	A'	Г43	CN35	CVLT			
					Г44					
-	AT45	ATR ATR 42-500	AT45	A'	Г45					
-	AT72	ATR ATR 72	AT72	A'	Г72	A748				
-	ATP	ADVANCED TURBOPROP	ATP	A'	ΓP	G222				
-	B461	BAE 146-100/RJ	B461	B-	461	B462	B463			
				Y	K42					
-	в703	BOEING 707-300	в703	B'	703	B720	K35R			
				E	3TF	E3CF	C135			
				V	C10	IL62				
_	B722	BOEING 727-100	В722	B'	722	B721	BER4			
		BOEING 737-228	B732	B'	732	B731	A124			
		BOEING 737-300	В733		733					
		BOEING 737-400	B734		734					
		BOEING 737-500	B735			В736				
		BOEING 737-700	B737		737					

There are three types of lines in the SYNONYM.LST file with the line type identified by the first two characters in the line. These line types with their associated leading characters are listed below.

- CC comment line
- CD data line
- synonym line

The data is organised into two blocks separated by a comment line consisting of the block name and equal signs "=":

- file identification block
- aircraft list block

Each of these blocks is described in the subsections below.



6.3.1.1. File Identification Block

The file identification block provides information on the file name, creation and modification date. The block consists of 12 comment lines.

The comment lines specify the file name along with the creation and the modification date. The creation date indicates the date when the file was created for the first time. The modification date indicates when the contents of the file were last modified.

6.3.1.2. Aircraft Listing Block

The aircraft listing block consists of 5 comment lines with additional synonym lines for each aircraft supported by the BADA Revision. A partial listing of this block is shown below.

	===== A	ircraft List ======	=======		======/
	A/C CODE	NAME OR MODEL	FILE	SYNONYM	/ / /
- - -	A30B A310 A319 A320	AIRBUS A300B4-600 AIRBUS A300B4-200 AIRBUS A310 AIRBUS A319 AIRBUS A320	A30B A310 A319 A320	A30B A310 A319 A320	
_	A333 A343	AIRBUS A321 AIRBUS A330-300 AIRBUS A340-300 ATR ATR 42-300	A333		
-	AT72 ATP	ATR ATR 42-500 ATR ATR 72 ADVANCED TURBOPROP BAE 146-100/RJ	AT72 ATP	AT45 AT72 ATP B461 YK42	A748 G222 B462 B463
-	В703	BOEING 707-300	в703	B703 E3TF VC10	IL62
- - -	B732 B733 B734 B735	BOEING 727-100 BOEING 737-228 BOEING 737-300 BOEING 737-400 BOEING 737-500 BOEING 737-700	B732 B733 B734 B735	B733 B734	B721 BER4 B731 A124 B736

There is one synonym line for each of the directly supported aircraft within the BADA release. Each such line consists of 4 fields as described below:

(a) Aircraft Code Field

This field identifies the aircraft type. It consists of a three or four-character ICAO code followed by two or more underscore characters.



- (b) Name or Model Field
 - This field identifies the manufacturer and model of the aircraft.
- (c) File Name Field

This field identifies the file name for the APF, OPF, PTF or PTD files associated with the aircraft (minus the file extension). For each aircraft this is the same as the A/C code.

(d) Equivalence Field

This field lists any equivalences associated with the aircraft. By default, each aircraft has at least one equivalence to itself.

Note that in some cases the name or model or equivalence fields may be continued onto the next line as it is the case with the B703 model.

6.3.2. SYNONYM.NEW File

The SYNONYM.NEW file is an ASCII file, which lists all aircraft types, which are supported by the BADA revision. Its format differs from the SYNONYM.LST file in that all supported aircraft are listed alphabetically in the file whether they are supported directly or by equivalence. An example of the SYNONYM.NEW file is given below (partial listing).

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC										
CC	·									
CC	BADA SYNONYM FILE									
CC										
CC										
	e_name: SYNONYM.NEW			/						
CC Cre	eation date: Mar 26 2	2002		/,						
CC CIE	eation_date: Mar 20 2	2002		,						
	lification date: Mar	26 2002		,						
CC	IIIIcacion_date: Mai	20 2002		,						
CC				,						
	rcraft List ======			=====/						
CC	Eloraro Elbo			,						
CC A/C	MANUFACTURER	NAME OR MODEL	FILE	OLD /						
CC CODE				CODE /						
CC				/						
CD * A10	FAIRCHILD	THUNDERBOLT II	FGTN	A10A /						
CD * A124	ANTONOV	ANTONOV AN-124	в732	AN4R /						
CD - A306	AIRBUS	A300B4-600	A306							
CD - A30B	AIRBUS	A300B4-200	A30B	A300 /						
	AIRBUS	A310	A310							
CD - A319	AIRBUS	A319	A319	A319 /						
CD - A320	AIRBUS	A320	A320	EA32 /						
CD - A321	AIRBUS	A321	A321	A321 /						
CD * A332	AIRBUS	A330-200	A333							
	AIRBUS	A330-300	A333							
CD * A342	AIRBUS	A340-200	A343	A342 /						
	AIRBUS	A340-300	A343							
	AIRBUS	A340-500	A343							
CD * A346	AIRBUS	A340-600	A343	A346 /						
CD * A4	MCDONNELL-DOUGLAS	SKYHAWK	FGTN	A4 /						
CD * A6	GRUMMAN	INTRUDER	FGTN	EA6B /						
CD * A748	BAE	BAE 748	AT72							
CD * AC80	ROCKWELL	TURBO COMMANDER	BE20	AC6T /						
CD * AC90	ROCKWELL	TURBO COMMANDER	BE20	AC90 /						
CD * AC95	ROCKWELL	TURBO COMMANDER	BE20	AC95 /						
CD * AJET CD * AMX	DASSAULT EMBRAER	ALPHA JET AMX	FGTN FGTN	AJET / AMX /						
CD * AMA	ANTONOV	AN-12	C130	AMX / AN12 /						
	ANTONOV	AN-124	F27							
CD * AN24	ANTONOV	AN-26	F27 F27	AN24 /						
CD MINZO	AN I ONO V	AN 20	r 2 /	MINZO /						



There are three types of lines in the SYNONYM.NEW file with the line type identified by the first two characters in the line. These line types with their associated two leading characters are listed below.

CC comment line
CD data line
FI end-of-file line

The data is organised into two blocks separated by a comment line consisting of the block name and equal signs "=":

- · file identification block
- aircraft list block

Each of these blocks is described in the subsections below.

6.3.2.1. File Identification Block

The file identification block provides information on the file name, creation and modification date. The block consists of 12 comment lines as shown below.

The comment lines specify the file name along with the creation and last modification date. The creation date indicates the date when the file was created for the first time. The modification date indicates when the contents of the file were last modified.

6.3.2.2. Aircraft Listing Block

The aircraft listing block consists of 5 comment lines and at least one data line for each aircraft supported by the BADA Revision. Some aircraft have more than one data line, see under (f). A partial listing of this block is shown below.

```
CD * A10
           FAIRCHILD
                                                        FGTN___
                               THUNDERBOLT II
                                                                A10A /
CD * A124
           ANTONOV
                               ANTONOV AN-124
                                                        B732
                                                                AN4R /
CD - A306
                                                        A306__
           AIRBUS
                               A300B4-600
                                                                A306 /
CD - A30B
           AIRBUS
                               A300B4-200
                                                        A30B
                                                                A300 /
```

Each data line consists of 6 fields as described below:

(a) Support Type Field

This field is one character in length being one of the following two values:

- "-" to indicate an aircraft type directly supported, and,
- to indicate an aircraft type supported by equivalence with another directly supported aircraft



(b) Aircraft Code Field

This field identifies the aircraft type. It consists of a three or four-character ICAO code.

(c) Manufacturer Field

This field identifies the manufacturer of the aircraft. Examples are Boeing, Airbus or Fokker.

(d) Name or Model Field

This field identifies the name or model for the aircraft type. Examples are the 747-400 series or Learjet 35.

(e) File Field

This field indicates the name of the OPF, APF, PTF or PTD file, which contains the parameters for the aircraft type (minus the file extension).

For an aircraft type which is directly supported this file name will be the same as the ICAO code with an additional two or more underscore characters to form a string of six characters in length. For example, the file name corresponding to the A333 will be A333__. This indicates an OPF file A333__.OPF, an APF file A333__.APF, a PTF file A333__.PTF and a PTD file A333__.PTD. For the Fokker F-27 with an ICAO code of F27, the file names include three underscore characters, that is, F27___.OPF, F27___.APF, F27___.PTF and F27___.PTD.

For an aircraft type which is supported through equivalence the file name will indicate the file for the equivalent aircraft type which should be used. As an example, the Antonov 12 (AN12) is equivalent to the Lockheed C-130 Hercules (C130). Thus the files C130__.OPF, C130__.APF, C130__.PTF and C130__.PTD should be used.

(f) Old Code field

The old code field gives the name of the aircraft that refers to the formerly known aircraft designator as published in one of the previous editions of the ICAO document 8643 [RD10]. This allows the BADA Revision 3.10 user to continue to use the old ICAO standard and to establish a link between the old and the new aircraft designators.

The above fields are specified in the following fixed format (Fortran notation):

'CD', 1X, A1, 1X, A4, 3X, A18, 1X, A25, 1X, A6, 2X, A4



6.3.3. SYNONYM_ALL.LST File

The SYNONYM_ALL.LST file is an ASCII file, which lists all aircraft types, which are supported by the BADA revision. Like in the SYNONYM.NEW file, all supported aircraft are listed alphabetically in the file whether they are supported directly or by equivalence. An example of the SYNONYM_ALL.LST file is given below (partial listing).

CCCC CC CC CC	CCCCCC	CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	CCCCCCCCC SYN	NONYM_ALL.L:	ST CCCCC	ccccccc	!/ / /				
CC CC	Fil	e_name: SYNONYM_A	ALL.LST				/				
CC	Cre	ation_date: May 2	22 2003				/				
CC	Mod	ification_date: N	May 22 2003				/ /				
CC CC							/				
CC==	======	=========				======	/				
CC							/				
CC					ICAO	ICAO	ICAO	ICAO	ICAO	ICAO	ICAO
CC	A/C	NAME OR MODEL	MANUFACTURER	FILE	CODE	CODE	CODE	CODE	CODE	CODE	CODE
CC	, -			BADA 3.5	V24	V25	V26	V27	V28	V29	V30
CC											
CD *	A10	THUNDERBOLT II	FAIRCHILD	FGTN	A10A	A10	A10	A10	A10	A10	A10
CD *	A124	ANTONOV AN-124	ANTONOV	в732	AN4R	A124	A124	A124	A124	A124	A124
CD -	A306	A300B4-600	AIRBUS	A306	A306	A306	A306	A306	A306	A306	A306
CD -	A30B	A300B4-200	AIRBUS	A30B	EA30	A300	A30B	A30B	A30B	A30B	A30B
CD -	A310	A310	AIRBUS	A310		A310	A310	A310	A310	A310	A310
CD *	A318	A318	AIRBUS	A319		A318	A318	A318	A318	A318	A318
	A319	A319	AIRBUS	A319			A319	A319	A319	A319	A319
CD -	A320	A320	AIRBUS	A320		A320	A320	A320	A320	A320	A320
	A321	A321	AIRBUS	A321		A321	A321	A321	A321	A321	A321
		A330-200	AIRBUS	A332	A332	A332	A332	A332	A332	A332	A332
		A330-300	AIRBUS	A333	EA33	EA33	EA33	A330	A333	A333	A333
		A340-200	AIRBUS	A343	A342	A342	A342	A342	A342	A342	A342
		A340-300	AIRBUS	A343	EA34	EA34	EA34	A340	A343	A343	A343
	A345	A340-500	AIRBUS	A343	A345	A345	A345	A345	A345	A345	A345
CD *	A346	A340-600	AIRBUS	A343	A346	A346	A346	A346	A346	A346	A346

There are three types of lines in the SYNONYM_ALL.LST file with the line type identified by the first two characters in the line. These line types with their associated two leading characters are listed below.

CC comment line
CD data line
FI end-of-file line

The data is organised into two blocks separated by a comment line consisting of equal signs "=":

- file identification block
- · aircraft list block

Each of these blocks is described in the subsections below.



6.3.3.1. File Identification Block

The file identification block provides information on the file name, creation and modification date. The block consists of 13 comment lines as shown below.

The comment lines specify the file name along with the creation and last modification date. The creation date indicates the date when the file was created for the first time. The modification date indicates when the contents of the file were last modified.

6.3.3.2. Aircraft Listing Block

The aircraft listing block consists of 7 comment lines and at least one data line for each aircraft supported by the BADA Revision. Some aircraft have more than one data line, see under (f). A partial listing of this block is shown below.

* A10	THUNDERBOLT II	FAIRCHILD	FGTN	A10A	A10	A10	A10	A10	A10	A10
* A124	ANTONOV AN-124	ANTONOV	В732	AN4R	A124	A124	A124	A124	A124	A124
- A306	A300B4-600	AIRBUS	A306							
- A30B	A300B4-200	AIRBUS	A30B	EA30	A300	A30B	A30B	A30B	A30B	A30B

Each data line consists of 5 fields describing the aircraft type and number of additional fields providing the history of ICAO aircraft type designators. Detailed description is given below:

(a) Support Type Field

This field is one character in length being one of the following two values:

- "-" to indicate an aircraft type directly supported, and,
- "*" to indicate an aircraft type supported by equivalence with another directly supported aircraft

(b) Aircraft Code Field

This field identifies the aircraft type. It consists of a three or four-character ICAO code.

(c) Manufacturer Field

This field identifies the manufacturer of the aircraft. Examples are Boeing, Airbus or Fokker.

(d) Name or Model Field

This field identifies the name or model for the aircraft type. Examples are the 747-400 series or Learjet 35.



(e) File Field

This field indicates the name of the OPF, APF, PTF or PTD file, which contains the parameters for the aircraft type (minus the file extension).

For an aircraft type which is directly supported this file name will be the same as the ICAO code with an additional two or more underscore characters to form a string of six characters in length. For example, the file name corresponding to the A333 will be A333__. This indicates an OPF file A333__.OPF, an APF file A333__.APF, a PTF file A333__.PTF and a PTD file A333__.PTD. For the Fokker F-27 with an ICAO code of F27, the file names include three underscore characters, that is, F27___.OPF, F27___.APF, F27___.PTF and F27___.PTD.

For an aircraft type which is supported through equivalence the file name will indicate the file for the equivalent aircraft type which should be used. As an example, the Antonov 12 (AN12) is equivalent to the Lockheed C-130 Hercules (C130). Thus the files C130__.OPF, C130__.APF, C130__.PTF and C130__.PTD should be used.

(f) Old Code fields

The old code fields give the name of the aircraft that refers to the formerly known aircraft designator as published in one of the previous editions (versions, i.e. V24 to V37) of the ICAO document 8643 [RD10]. This allows the BADA Revision 3.10 user to continue to use the old ICAO standard and to establish a link between the old and the new aircraft designators, as well as the corresponding aircraft file name from the most recent BADA release. If the specific aircraft model version did not have an assigned designator in the past editions of the ICAO document or the information was not available to the BADA team, then the most recent designator is used throughout all the versions.



6.4. OPF FILE FORMAT

The Operations Performance File (OPF) is an ASCII file, which for a particular aircraft type specifies the operations performance parameters described in Section 3. An example of an OPF file for the A306 (Airbus 300B4-600) aircraft is shown below.

```
AIRCRAFT PERFORMANCE OPERATIONAL FILE
CC
     File_name: A306__.OPF
     Creation_date: Mar 26 2002
     Modification_date: Mar 26 2002
CC
2 engines
   Airbus A300-B4-622 with PW4158 engines
                                      wake
CC
reference minimum maximum max payload mass grad / .14000E+03 .87000E+02 .17170E+03 .39000E+02 .14100E+00 /
   reference
VMO(KCAS) MMO Max.Alt Hmax
             .82000E+00 .41000E+05 .31600E+05 -.67000E+02 /
    .33500E+03
CC Wing Area and Buffet coefficients (SIM)
           Clbo(M=0)
.15300E+01
CCndrst Surf(m2)
                       k
                                CM16
                      .10290E+01 .00000E+00
    .26000E+03
   Configuration characteristics
CC n Phase Name Vstall(KCAS)
                       CD0
                                CD2
                                       unused
CD 1 CR Clean
            .15100E+03 .19000E-01 .53000E-01
                                      .00000E+00
CD 2 IC
      S15F00
            .11700E+03 .33057E-01 .45362E-01
                                      .00000E+00
            .11700E+03 .33057E-01 .45362E-01
.10900E+03 .38031E-01 .44932E-01
CD 3 TO
      S15F00
                                       .00000E+00
CD 4 AP
      S15F15
                                       .00000E+00
            .97000E+02 .78935E-01
                                       .00000E+00
CD 5 LD
      S30F40
                              .44822E-01
CC
  Spoiler
      RET
CD 1
CD 2
                              .00000E+00
                                       .00000E+00
CC
  Gear
CD 1
      IJΡ
CD 2
      DOWN
                      .22500E-01
                              .00000E+00
                                       .00000E+00
CD 1
      OFF
CD 2
                              .00000E+00 .00000E+00 /
      ON
Max climb thrust coefficients (SIM)
    CC
                                      .36000E+00
CD
    Desc CAS Desc Mach unused .28000E+03 .79000E+00 .00000E+00
CC
                              unused
                                       unused
                     .00000E+00
                              .00000E+00
CC Thrust Specific Fuel Consumption Coefficients
    .88100E+00
            .16900E+05
   Descent Fuel Flow Coefficients
    .26805E+02 .45700E+05
CC
   Cruise Corr.
             unused
                      unused
                              unused
    .10380E+01 .00000E+00 .00000E+00 .00000E+00
length
              LDL
                    span
                                      unused
    .23620E+04 .15550E+04
                     .44840E+02
                              .54080E+02
                                       .00000E+00 /
```

There are three types of lines in the OPF file with the line type identified by the first two characters in the line. These line types with their associated two leading characters are listed below.



CC comment line

CD data line

FI end-of-file line

The comment lines are provided solely for the purpose of improving the readability of the file. All coefficients are contained within the CD lines in a fixed format. The end-of-file line is included as the last line in the file in order to facilitate the reading of the file in certain computing environments.

The data is organised into a total of eight blocks with each block separated by a comment line containing the block name and equal signs "=". These blocks are listed below and are described in further detail in the subsections below.

- file identification block
- aircraft type block
- mass block
- flight envelope block
- aerodynamics block
- · engine thrust block,
- fuel consumption block
- ground movements block

6.4.1. File Identification Block

The file identification block provides information on the file name, creation date and modification date. The block consists of 11 comment lines. An example of the file identification block for the A306__.OPF file is shown below.

The comment lines specify the file name along with the creation date and last modification date. The creation date indicates the date when the file was created for the first time. The modification date indicates when the contents of the file were last modified.

6.4.2. Aircraft Type Block

The OPF aircraft type block consists of 1 data line with 3 comment lines for a total of 4 lines. An example of the aircraft type block is given below.



The data line specifies the following aircraft type parameters:

- ICAO aircraft code (followed by 2 or more underscore characters as required to form a six character string)
- number of engines, n_{eng}
- · engine type
- wake category

The engine type can be one of the following three values: Jet, Turboprop or Piston. The wake category can be one of the four values J (jumbo), H (heavy), M (medium) or L (light).

The four values are specified in the following fixed format (Fortran notation)

The comment lines typically indicate the engine manufacturer's designation and the source of the performance coefficients.

6.4.3. Mass Block

The OPF mass block consists of 1 data line with 2 comment lines for a total of 3 lines.

An example of the mass block is given below.

The data line specifies the following BADA mass model parameters:

```
m_{ref} m_{min} m_{max} m_{pyld} G_w
```

These parameters are specified in the following fixed format (Fortran notation)

6.4.4. Flight Envelope Block

The OPF flight envelope block consists of 1 data line with 2 comment lines for a total of 3 lines. An example of the flight envelope block is given below.

The date line specifies the following BADA speed envelope parameters:

$$V_{MO}$$
 M_{MO} h_{MO} h_{max} G_{i}

Note that all altitudes are expressed in feet.

These parameters are specified in the following fixed format (Fortran notation):



6.4.5. Aerodynamics Block

The OPF aerodynamics block consists of 12 data lines and 8 comment lines for a total of 20 lines. An example of the aerodynamics block is given below.

		CC=====	= Aerodynam	ics ======		=========		=/
		CC Wing		/				
		CCndrst	Surf(m2)	Clbo(M=0)	k	CM16		/
1	->	CD 5	.26000E+03	.15300E+01	.10290E+01	.00000E+00		/
		CC Cc	nfiguration	characterist	ics			/
		CC n Ph	nase Name	Vstall(KCAS)) CD0	CD2	unused	/
2	->	CD 1 CR	Clean	.15100E+03	.19000E-01	.53000E-01	.00000E+00	/
3	->	CD 2 IC	S15F00	.11700E+03	.33057E-01	.45362E-01	.00000E+00	/
4	->	CD 3 TC	S15F00	.11700E+03	.33057E-01	.45362E-01	.00000E+00	/
5	->	CD 4 AF	S15F15	.10900E+03	.38031E-01	.44932E-01	.00000E+00	/
6	->	CD 5 LD	S30F40	.97000E+02	.78935E-01	.44822E-01	.00000E+00	/
		CC Sr	oiler			/		
7	->	CD 1	RET					/
8	->	CD 2	EXT			.00000E+00	.00000E+00	/
		CC Ge	ear					/
9	->	CD 1	UP					/
10) ->	CD 2	DOWN		.2250E-01	.00000E+00	.00000E+00	/
		CC B1	rakes					/
12	2 ->	CD 1	OFF					/
13	3 ->	CD 2	ON			.00000E+00	.00000E+00	/

The first data line specifies the following BADA aerodynamic model parameters:

S C_{M16} $C_{lbo(M=0)}$

These parameters are specified in the following fixed format (Fortran notation):

Note that the "5" under the header "ndrst" stands for the five drag settings. Currently this is not used but is left in for compatibility requirements.

The next line holds besides the stall speed and flap setting for cruise as well as the values for the two drag coefficients for this configuration:

$$(V_{\text{stall}})_{\text{CR}}$$
 C_{D0} C_{D2}

These parameters are specified in the following fixed format (Fortran notation):

The next four data lines have the same format and correspond to the other configurations. The configurations are specified in the following order, corresponding to a semi-monotonically decreasing stall speed:

IC initial climb TO

take-off

AΡ approach

LD landing

The stall speed, $(V_{stall})_{i,i}$ is specified for each configuration, and C_{D0} and C_{D2} are given if available in the following fixed format (Fortran notation):

'CD', 15X, 3 (3X, E10.5)



In case the IC configuration is equal to the CR configuration, the values for C_{D0} and C_{D2} are mentioned only in the CR dataline. Note that C_{D0} and C_{D2} coefficients for IC and TO configurations are not used but are included for the reason of compatibility with previous versions.

The data lines 7 through 9 are not used but are included for the reason of compatibility with previous versions.

Dataline 10 holds the drag increment for landing gear down:

 $C_{D0.\Lambda LDG}$

The format of this line is:

Datalines 11 and 12 are not used but are included for the reason of compatibility with previous versions.

6.4.6. Engine Thrust Block

The OPF engine thrust block consists of 3 data lines with 4 comment lines for a total of 7 lines. An example of the engine thrust block is given below.

```
Max climb thrust coefficients (SIM)
      CC
                     .44800E+05
                                .11600E-09
                                          .67500E+01
           .30400E+06
                                                      .42600E-02
            Desc(low)
                      Desc(high)
                                 Desc level
                                            Desc(app)
                                                       Desc(ld)
           .73000E-02
                      .20600E-01
                                 .80000E+04
                                            .12000E+00
                                                      .36000E+00
     CD
                                                       unused
            Desc CAS
                       Desc Mach
                                 unused
                                            unused
     CC
3 ->
           .28000E+03
                      .79000E+00
                                 .00000E+00
                                            .00000E+00
                                                      .00000E+00 /
```

The first data line specifies the following BADA parameters used to calculate the maximum climb thrust, that is:

$$C_{\text{Tc},1}$$
 $C_{\text{Tc},2}$ $C_{\text{Tc},3}$ $C_{\text{Tc},4}$ $C_{\text{Tc},5}$

These parameters are specified in the following fixed format (Fortran notation):

The second data line specifies the following BADA parameters used to calculate cruise and descent thrust, that is:

$$C_{Tdes,low}$$
 $C_{Tdes,high}$ $H_{p,des}$ $C_{Tdes,app}$ $C_{Tdes,low}$

These parameters are specified in the following fixed format (Fortran notation):

Note that the $C_{Tdes,app}$ and $C_{Tdes,Id}$ coefficients are determined in order to obtain a 3° descent gradient during approach and landing.

The third data line specifies the reference speeds during descent, that is:



These parameters are specified in the following fixed format (Fortran notation):

Note that these two parameters are no longer used in BADA model implementation, but are left in place only to provide information on one of the reference speeds during descent used during the model identification.

The zero values at the end of this data line are not used but are included in the file due to compatibility requirements with previous versions.

6.4.7. Fuel Consumption Block

The OPF fuel consumption block consists of 3 data lines with 4 comment lines for a total of 7 lines. An example of a fuel consumption block is shown below.

```
Thrust Specific Fuel Consumption Coefficients
               .16900E+05
CD
     .88100E+00
CC
   Descent Fuel Flow Coefficients
     .26805E+02 .45700E+05
    Cruise Corr.
                unused
                          unused
                                    unused
                                              unused
     .10380E+01
               .00000E+00
                         .00000E+00
                                   .00000E+00
                                              .00000E+00
```

The first data line specifies the following BADA parameters for thrust specific fuel consumption.

$$C_{f1}$$
 C_{f2}

These parameters are specified in the following fixed format (Fortran notation):

The second data line specifies the following BADA parameters for descent fuel flow.

$$C_{f3}$$
 C_{f4}

These parameters are specified in the following fixed format (Fortran notation):

The third data line specifies the cruise fuel flow correction factor.

 C_{fcr}

The parameter is specified in the following fixed format (Fortran notation):



6.4.8. Ground Movement Block

The OPF ground movement block consists of 1 data line with 3 comment lines for a total of 4 lines. An example of a ground movement block is shown below. The ground movement block is the last block in the OPF file and is thus followed by the end-of-file line as shown below.

The data line specifies the following BADA parameters for ground movements:

TOL LDL span length

These parameters are specified in the following fixed format (Fortran notation):

'CD', 2X, 4 (3X, E10.5)

6.5. APF FILE FORMAT

The Airlines Procedures File (APF) is an ASCII file which, for a particular aircraft type, specifies recommended speed procedures for climb, cruise, and descent conditions. An example of an APF file for the Airbus A306 aircraft is shown below.

```
CC
          AIRLINES PROCEDURES FILE
CC
CC
    File_name: A306___.APF
CC
    Creation_date: Mar 26 2002
CC
    Modification_date: Mar 26 2002
CC
CC
CC
  LO= 087.00 to ---.- / AV= ---.- to ---.- / HI= ---.- to 171.70
CC
CC
Company name -----climb----- --cruise-- ----descent----- --approach- model-
CC COM CO
            mass lo hi
CC
                          lo hi
                                  hi lo
                                             (unused)
CC
   version engines ma cas cas mc xxxx xx cas cas mc mc cas cas xxxx xx xxx xxx xxx opf_
CD *** **
       Default Company
   B4_622 PW4158 LO 250 300 79
B4_622 PW4158 AV 250 300 79
                          250 310 79 79 280 250
                                             0
                                               Ω
CD
                                                 0 A306
                          250 310 79 79 280 250
CD
                                             0
                                               0
                                                 Ω
                                                   A306
                          250 310 79 79 280 250
   B4_622 PW4158C HI 250 300 79
                                             0 0
                                                 0 A306__
CC/////// THE END
```

There are two types of lines in the APF file with the line type identified by the first two characters in the line. These line types with their associated two leading characters are listed below:

CC - comment line
CD - data line

The last line in the file, as shown above, is also a comment line.

The comment lines are provided solely for the purpose of improving the readability of the file. All coefficients are contained within the CD lines in a fixed format.



The data is organised into 2 blocks separated by a comment line containing a string of equal signs, "=":

- file identification block
- speed procedures block

Each of the two blocks is described further in the subsections below.

6.5.1. File Identification Block

The file identification block provides information on the file name, creation date and modification date. The block consists of 14 comment lines. An example of a file identification block is shown below.

```
CC
            ATRITNES PROCEDURES FILE
CC
     File_name: A306__.APF
CC
CC
CC
     Creation_date: Mar 26 2002
CC
CC
     Modification_date: Mar 26 2002
CC
CC
   LO= 087.00 to ---.- / AV= ---.- to ---.- / HI= ---.- to 171.70
CC
```

The comment lines provide background information on the file contents. In addition, the comment lines specify the file name along with the creation and last modification date. The creation date indicates the date when the file was created for the first time. The modification date indicates when the contents of the file were last modified.

The second last comment line in the identification block specifies three mass ranges for the aircraft in tonnes. That is, a low range (LO), average range (AV) and high range (HI). The definition of these ranges is used for interpreting the information presented below in the procedures specification block. In the example given above, all three ranges are assumed equivalent.

6.5.2. Procedures Specification Block

The APF procedures specification block consists of 4 data lines with 7 comment lines for a total of 11 lines. An example of a procedures specification block is shown below.

```
CC COM CO Company name -----climb----- --cruise-- ----descent----- --approach- model- /
        mass lo hi
                 lo hi
                    hi lo
    version engines ma cas cas mc xxxx xx cas cas mc mc cas cas xxxx xx xxx xxx xxx opf_
  CD *** **
1 ->
      Default Company
   2 ->
  CD
3 ->
  CD
```



The first data line specifies the company name for which the next three datalines are valid. The company can be identified by its 3 and 2 letter code plus the company name. The dataline fomat is:

As it is, within BADA all APF files specify procedures for only one "default" company.

The next three data lines specify the following parameters corresponding to climb, cruise and descent:

$$V_{cl,1}$$
 $V_{cl,2}$ M_{cl} $V_{cr,1}$ $V_{cr,2}$ M_{cr} M_{des} $V_{des,2}$ $V_{des,1}$

Note that all Mach number values are also multiplied by a value of 100. For example, the 78 indicated for M_{cl} above corresponds to a Mach number of 0.78.

The three lines specify parameters for mass ranges of Low (LO), Average (AV) and High (HI) respectively. These parameters are specified in the following fixed format (Fortran notation):

Note that approach values are set to zero. These values are not used but are included in the file due to compatibility requirements with previous versions.

Also, each line specifies an aircraft version number, engine, and operational model. The operational model is always the same as the file name. The version number may provide some additional information on the aircraft version covered by the file while the engine states which engine is used by the aircraft.

The file format is designed such that the four data lines can be repeated for the different companies which operate the aircraft and which may have different standard procedures. If data were to be provided for more than one company then the version, engine and operational model fields may be useful since different companies could operate different versions of the aircraft with different engines and thus different associated operational models.



6.6. PTF FILE FORMAT

The Performance Table File (PTF) is an ASCII file, which for a particular aircraft type specifies cruise, climb and descent performance at different flight levels. An example of a PTF file for the Airbus A306 aircraft is shown below.

> BADA PERFORMANCE FILE Apr 23 2002

AC/Type: A306

Source OPF File: Mar 26 2002 Source APF file: Mar 26 2002

Mass Levels [kg] low - 104400 nominal - 140000 high - 171700
 Speeds:
 CAS(LO/HI)
 Mach

 climb
 - 250/300
 0.79

 cruise
 - 250/310
 0.79

 descent
 - 250/280
 0.79
 Temperature: ISA

Max Alt. [ft]: 41000

	cent - 25			79 hig	-	171700						
FL	TAS [kts]	CRUIS [lo	E fuel kg/min nom	ı] hi	TAS [kts]	lo	CLIM ROCD [fpm] nom	MB hi	fuel [kg/min] nom	TAS [kts]	DESCEN ROCD [fpm] nom	TT fuel [kg/min] nom
0	======= 		=====	:=====	====== 157		1990		270.3	131	760	97.2
5					158	2190	1970	1600	267.3	132	780	96.1
10					159	2170	1950	1570	264.3	138	800	95.0
15					166	2290	2030	1650	261.5	149	850	94.0
20					167	2270	2010	1620	258.5	181	1020	31.0
30	230	61.2	81.4	104.3	190	2750	2360	1920	253.0	230	1360	25.0
40	233	61.2	81.4	104.4	225	3350	2780	2270	247.7	233	1380	24.5
60	272	65.9	81.7	99.6	272	4210	3070	2370	236.8	240	1410	23.3
80	280	65.8	81.7	99.7	280	4040	2930	2230	225.7	280	1550	22.1
100	289	65.8	81.7	99.8	289	3860	2780	2090	214.8	289	1590	20.9
120	297	65.7	81.7	99.8	356	3820	2800	2170	204.8	332	1880	19.8
140	306	65.6	81.7	99.9	366	3590	2610	2000	194.3	342	1920	18.6
160	389	82.4	93.1	105.3	377	3360	2410	1820	184.1	353	1960	17.4
180	401	82.1	92.9	105.1	388	3120	2220	1650	174.2	363	2000	16.2
200	413	81.7	92.6	104.9	400	2880	2020	1470	164.5	375	2040	15.1
220	425	81.3	92.3	104.7	412	2630	1810	1290	155.0	386	2080	13.9
240	438	80.9	91.9	104.5	425	2380	1610	1100	145.8	398	2120	12.7
260	452	80.4	91.6	104.3	438	2130	1400	920	136.9	411	2160	11.6
280	466	79.9	91.2	104.1	452	1880	1200	730	128.1	424	2200	10.4
290	468	78.4	90.1	103.4	459	1760	1090	640	123.9	431	2220	9.8
310	464	74.3	87.0	101.5	464	2200	1290	660	115.4	444	2250	8.6
330	459	70.6	84.7	100.6	459	1950	1050	420	107.2	459	2290	7.4
350	455	67.6	83.0	97.9	455	1700	810	170	99.2	455	3150	6.3
370	453	65.1	82.0	90.3	453	1320	510	0	91.6	453	2850	5.1
390	453	63.2	81.9	83.0	453	1080	260	0	84.1	453	2850	3.9
410	453 	61.9	75.9 =====	75.9	453 ======	830	10	0	77.0	453 ======	2880	2.8



The OPF and APF files are generated as a result of a modelling process using MatLab [RD6]. Once these two files are generated, the PTF can be automatically generated. A brief summary of the format of these files is given below.

The header of each PTF file contains information as described below.

file creation date: This is in the first line, at the top-right corner

aircraft type: This is in the third line.

source file dates: The last modification dates of the OPF and APF files which were used to

create the PTF file are given in the 4th and 5th lines respectively.

Speeds: The speed laws for climb, cruise and descent are specified in lines 8, 9 and

10, that is:

 $\begin{array}{ll} \text{climb} & \min(V_{\text{cl,1}},\,250\text{kt})\,/\,V_{\text{cl,2}} & M_{\text{cl}} \\ \text{cruise} & \min(V_{\text{cr,1}},\,250\text{kt})\,/\,V_{\text{cr,2}} & M_{\text{cr}} \\ \text{descent} & \min(V_{\text{des,1}},\,250\text{kt})\,/\,V_{\text{des,2}} & M_{\text{des}} \end{array}$

Mass levels: The performance tables provide data for three different mass levels in lines

8, 9 and 10, that is:

 $\begin{array}{lll} low & 1.2 \; m_{min.} \\ nominal & m_{ref} \\ high & m_{max} \end{array}$

Note that the low mass is not the minimum mass but 1.2 times the

minimum mass.

Temperature: The temperature is mentioned in line 7. All PTF files currently provide data

for ISA conditions only.

Maximum altitude: The maximum altitude as specified in the OPF file, h_{MO}, is given in line 9.

The table of performance data within the file consists of 13 columns. Each of these columns is described below:

Column 1 FL

Column 2 cruise TAS (nominal mass) [knots]

Column 3 cruise fuel consumption (low mass) [kg/min]
Column 4 cruise fuel consumption (nominal mass) [kg/min]
Column 5 cruise fuel consumption (high mass) [kg/min]

Column 6 climb TAS (nominal mass) [knots]

Column 7 rate of climb with reduced power (low mass) [ft/min] rate of climb with reduced power (nominal mass) [ft/min] rate of climb with reduced power (high mass) [ft/min] climb fuel consumption (nominal mass) [kg/min]

Column 11 descent TAS (nominal mass) [knots]

Column 12 rate of descent (nominal mass) [ft/min]

Column 13 descent fuel consumption (nominal mass) [kg/min]

The format for data presented in each line of the table is as follows (Fortran notation):

13, 4X, 13, 2X, 3(1X, F5.1), 5X, 13, 2X, 3(1X, 15), 3X, F5.1, 5X, 13, 2X, 15, 2X, F5.1



Further explanatory notes on the data presented in the performance tables are given below:

- (a) Cruise data is only specified for flight levels greater than or equal to 30.
- (b) Performance data is specified up to a maximum flight level of 510 or to highest level for which a positive rate of climb can be achieved at the low mass.
- (c) True airspeed for climb, cruise and descent is determined based on the speed schedules specified in Sections 4.1, 4.2 and 4.3 respectively.
- (d) Rates of climb are calculated at each flight level assuming the energy share factors associated with constant CAS or constant Mach speed laws and using the reduced power correction as given in Section 3.8.
- (e) The fuel consumption in climb is independent of the aircraft mass and thus only one value is given. There are three different climb rates however corresponding to low, nominal and high mass conditions.
- (f) The rate of descent and fuel consumption in descent is calculated assuming the nominal mass. Values for other mass conditions are not given.
- (g) Discontinuities in climb rate can occur for the following reasons:
 - change in speed between flight levels (e.g. removal of 250 kt restriction above FL100),
 - transition from constant CAS to constant Mach (typically around FL300),
 - transition through the tropopause (FL360 for ISA),
 - end of the application scope for reduced climb power (at 80% of h_{max}).
- (h) Discontinuities in descent rate can occur for the following reasons:
 - transition through tropopause (FL360 for ISA),
 - transition from constant Mach to constant CAS,
 - change in assumed descent thrust (specified by the BADA h_{des} parameter),
 - change to approach or landing aerodynamic configuration,
 - change in speed between flight levels (e.g. application of 250 kt limit below FL100).
- (i) The PTF files are made with "non-clean" configuration data for approach and landing when such data is available (see Section 3.6.1).
- (j) The performance data presented in the table are computed by using 'point type' calculation, that is without performing integration over time: aircraft weight is constant and does not account for consumed fuel, and speed changes take place immediately.
- (k) The flight envelope limitations are not taken into account for calculation of performance parameters⁸.

Note that all PTF files are available in document form in [RD9].

⁸ Example: cruise fuel flow is calculated without checking, for given aircraft weight, speed and FL, that aircraft drag is lower than maximum available cruise thrust.



6.7. PTD FILE FORMAT

In addition to the data provided in the PTF file, more detailed climb and descent performance data are presented in the PTD file. An example of a PTD file for the Airbus A306 aircraft is shown below (partial listing):

Low mass CL ==========	CLIMBS												
FL[-] T[K]	ЫĮБ	rho[kg/m3]	a[m/s]	[kt]	CAS[kt]	M[-] mass[kg]	Thrust[N]	Drag[N] 1	Fuel[kgm]	ESF[-]]	ROC[fpm]	TDC[N]	PWC[-]
N	1013	1.225	340	136.35	136.35	21	297160	85670	215.8	σ.	2452	186284	0.88
N	995	1.207	340	137.34	136.35	0.21 104400	294268	85680	213.9	ο.	2435	183727	0.88
0	σ	1.190	339	138.34	136.35	0.21 104400	38	85691	212.0	0.98	2417	181179	0.88
7	959	1.172	339	144.45	141.35	0.22 104400	288510	82072	211.0	ο.	2527	181833	0.88
0 2	942	1.155	338	145.51	141.35	0.22 104400	285643	82082	209.1	0.97	2509	179299	0.88
30 282	908	1.121	337	168.52	161.35	0.26 104400	279935	72295	209.0	ο.	2937	182892	0.88
7	87	1.088	336	7.	191.35	0.31 104400	274260	67093	210.7	ο.	3470	182476	0.88
0	81	1.024	333	272.30	250.00	0.42 104400	263011	74643	213.7	0.91	4075	165917	0.88
2	7	96.	331	ω.	250.00	0.44 104400	251895	74535	206.0	0.91	3925	156222	0.88
100 268	6968	.90	328	345.37	300.00	0.54 104400	240914	91120	207.0	ω.	3905	131941	0.88
20 2	w	.84	326	355.51	300.00	0.56 104400	230066	90785	199.1	∞.	3703	122681	0.88
40 2	5952	0.796	324	366.04	300.00	0.58 104400	219352	90425	191.3	0.85	3495	113561	0.88
60 2	5491	. 74	321	376.97	300.00		208772	90038	183.6	ω.	3281	104583	0.88
7	50600	σ	319	388.32	300.00	0.63 104400	198326	89622	175.8	0.83	3060	95748	0.88
00 24	46563	•	316	400.10	300.00	0.65 104400	188013	89175	168.1	∞.	2834	87059	0.88
20 2	42791	•	314	412.32	300.00		177835	88694	160.4	0.81	2601	78516	0.88
40 2	27	. 56	311	425.00	300.00	. 07	167790	88179	152.7	∞.	2364	70123	0.88
7	35989	. 53	308	438.16	300.00	0.73 104400	157879	87627	145.0	۲.	2122	61819	0.88
80 2	32932	•	306	451.80	300.00		148102	87036	137.3	0.78	1875	53788	0.88
0	ω	.47	304	458.81	300.00	8	143263	86725	133.4	۲.	1749	49800	0.88
310 227	28745	0.44	302	463.54	293.28	6	133687	83916	124.9	٥.	2184	43839	0.88
7	26201	0.41	299	459.48	280.58	6	124245	79587	115.8	1.09	2205	44658	1.00
0	23842		297	455.37	268.17	0.79 104400	114936	75881	106.8	1.09	1911	39055	1.00
370 217	21663	0.34	295	453.12	256.08	0.79 104400	105761	72808	98.1	1.00	1470	32953	1.00
390 217	19677	0.316	295	453.12	244.46	0.79 104400	96720	70398	89.7	1.00	1174	26322	1.00
410 217	17874	0.287	295	453.12	233.34	0.79 104400	87813	68640	81.5	1.00	855	19173	1.00



The performance values presented in the PTD file are a superset of the climb and descent performance values presented in the PTF file. They are generated in the same conditions as the corresponding PTF file: same aircraft, same source OPF and APF files, same speed laws, same mass levels, same temperature and same flight levels. The purpose of this file is mainly to provide the user with a greater number of computed parameters, especially intermediate parameters used to compute the final TAS and ROCD, which may be useful to validate an implementation of the BADA model.

The files contains performance data consisting of 4 sections:

- low mass climb performance
- nominal mass climb performance
- high mass climb performance
- nominal mass descent performance

Each section contains a table that presents, for several flight levels, a set of performance parameters spread across 16 columns. Each of these columns is described below:

```
Column 1
               Flight level [FL]
Column 2
               Temperature [K]
Column 3
               Pressure [Pa]
               Air density [kg/m<sup>3</sup>]
Column 4
Column 5
               Speed of sound [m/s]
Column 6
               TAS [kt]
Column 7
               CAS [kt]
Column 8
               Mach [dimensionless]
Column 9
               Mass [kg]
Column 10
               Thrust [N]
Column 11
               Drag [N]
Column 12
               Fuel flow [kg/min]
Column 13
               Energy share factor [dimensionless]
Column 14
               Rate of climb/descent [ft/min]
Column 15
               (Thr - D) \cdot C_{pow,red} [kg/min] (see section 3.8)
Column 16
               - climb tables: Power reduction coefficient C<sub>pow,red</sub> [dimensionless]

    descent table: Descent gradient [degree]
```

The format for data presented in each line of the table is as follows (Fortran notation):

Climb tables:

```
16, 1X, I3, 1X, I6, 1X, F7.3, 1X, I7, 2(1X, F8.2), 1X, F7.2, 1X, I6, 2(1X, I9), 1X, F7.1, 1X, F7.2, 1X, I7, 1X, I8, 1X, F7.2
```

Descent tables:

```
I6, 1X, I3, 1X, I6, 1X, F7.3, 1X, I7, 2(1X, F8.2), 1X, F7.2, 1X, I6, 2(1X, I9), 1X, F7.1, 1X, F7.2, 1X, I7, 1X, I8, 1X, F8.2
```



6.8. BADA.GPF FILE FORMAT

The BADA.GPF file is an ASCII file which specifies the values of the global aircraft parameters (see Section 5). The complete BADA.GPF file is shown below:

CC	200000000000000000000000000000000000000	CCCCCCCCC BADA.G	PF CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	cccccccccc/
CC	GLOBAL PA	ARAMETERS FILE		,
CC		·-		,
CC	File_name: BADA.GPF			,
CC	_			/
CC	Creation_date: Mar 2	26 2002		/
CC	Modification_date: N	Mar 26 2002		,
CC				,
CC				,
	Class			.======/
CC.	Ciass			
	Flight = civ,mil			,
				,
	Engine = jet,turbo,pisto		3	/
	Phase = to,ic,cl,cr,des	s,noid,app,ind,gno	1	/
CC				/
	====== Parameters List	===========		:======/
CC				/
	Name Unit			/
CC	Parameter Flight	Engine	Phase	Value /
CC				/
CC	max. long. acc. [fps2]			/
CD	acc_long_max civ	jet,turbo,piston	to,ic,cl,cr,des,hold,app,lnd	.20000E+01 /
CC	max. norm. acc. [fps2]			/
CD	acc_norm_max civ	jet,turbo,piston	to,ic,cl,cr,des,hold,app,lnd	.50000E+01 /
CC	nom. bank angle [deg]			/
CD	ang_bank_nom civ	jet,turbo,piston	to, lnd	.15000E+02 /
CC	nom. bank angle [deg]			/
CD	ang_bank_nom civ	jet, turbo, piston	ic,cl,cr,des,hold,app	.35000E+02 /
CC	nom. bank angle [deg]			/
	ang_bank_nom mil	jet, turbo, piston	to,ic,cl,cr,des,hold,app,lnd	.50000E+02 /
	max. bank angle [deg]	3 , , -	11, 1,1 ,1 ,111, 111, 111,	/
	ang_bank_max civ	jet,turbo,piston	to, lnd	.25000E+02 /
	max. bank angle [deg]	3 , , -		/
	ang_bank_max civ	jet,turbo,piston	hold	.35000E+02 /
	max. bank angle [deg]	500,00000,1000		/
	ang_bank_max civ	iet.turbo.piston	ic,cl,cr,des,app	.45000E+02 /
	max. bank angle [deg]	J,,,	///	/
	ang_bank_max mil	iet.turbo.piston	to,ic,cl,cr,des,hold,app,lnd	.70000E+02 /
	exp. desc. fact. [-]	500,00000,1000		/
		jet,turbo,piston	des	.16000E+01 /
	to thrust factor [-]	500,00000,1000		/
		jet,turbo,piston	to	.12000E+01 /
	cr thrust factor [-]	500,00000,1000		/
		jet,turbo,piston	cr	.95000E+00 /
	max alt for to [ft]	jee, carbo, procon	CI	.550000100 /
		jet,turbo,piston	to	.40000E+03 /
	max alt for ic [ft]	jee, carbo, procon		.100001.03 /
		jet, turbo, piston	ic	.20000E+04 /
	max alt for app [ft]	jee, earbo, pibeon		.200001.01 /
		jet,turbo,piston	ann	.80000E+04 /
	max alt for ld [ft]	jee, earbo, pibeon	ирр	.0000001.01 /
		jet, turbo, piston	lnd	.30000E+04 /
	min speed coef. [-]	jec, carbo, pracon	1110	/ ₽0140006.
		iet turbo piston	cr,ic,cl,des,hold,app,lnd	.13000E+01 /
	min speed coef. [-]	jec,curbo,piscon	ci,ic,ci,des,noid,app,ind	.13000E+01 /
		jet,turbo,piston	+0	.12000E+01 /
	spd incr FL < 15 [KCAS]	jec,curbo,piscon	20	.12000E+01 /
		int	al	.50000E+01 /
	V_cl_1 mil,civ	Jec	cl	.50000E+01 /
	spd incr FL < 30 [KCAS]	dat	a1	1000000000
	V_cl_2 mil,civ	jet	cl	.10000E+02 /
	spd incr FL < 40 [KCAS]	2	-1	200007:00
	V_cl_3 mil,civ	Jet	cl	.30000E+02 /
	spd incr FL < 50 [KCAS]	int	al	60000E+02 /
	V_cl_4 mil,civ	Jet	cl	.60000E+02 /
	<pre>spd incr FL < 60 [KCAS] V_cl_5 mil,civ</pre>	iet	cl	.80000E+02 /
CD	v_C1_3 m11,C1V	ادر	CI	.0000000±702 /



```
CC spd incr FL < 5 [KCAS]
                                                                    .20000E+02
CD V_cl_6
                mil,civ turbo,piston
                                        cl
CC spd incr FL < 10 [KCAS]
CD V_cl_7
                mil,civ turbo,piston
                                        cl
                                                                    .30000E+02
CC spd incr FL < 15 [KCAS]
                                                                    35000E+02
CD V_cl_8
                mil,civ turbo,piston
                                        cl
CC spd incr FL < 10 [KCAS]
CD V_des_1
                mil,civ jet,turbo
                                                                    .50000E+01
CC spd incr FL < 15 [KCAS]
CD V_des_2
                mil,civ jet,turbo
                                        des
                                                                    .10000E+02
CC spd incr FL < 20 [KCAS]
CD V_des_3
                mil,civ jet,turbo
                                        des
                                                                    .20000E+02
CC spd incr FL < 30 [KCAS]
CD V_des_4 mil,civ jet,turbo CC spd incr FL < 5 [KCAS]
                                        des
                                                                    50000E+02
CD V_des_5
                mil,civ piston
                                        des
                                                                    .50000E+01
CC spd incr FL < 10 [KCAS]
CD V_des_6
                                                                    .10000E+02
                                        des
                mil,civ piston
CC spd incr FL < 15 [KCAS]
CD V_des_7
               mil,civ piston
                                        des
                                                                    20000E+02
CC hold. spd FL < 140 [KCAS]
                                                                    .23000E+03
CD V_hold_1
                mil,civ jet,turbo,piston hold
CC hold. spd FL < 200 [KCAS]
                                                                    .24000E+03
CD V_hold_2
               mil,civ jet,turbo,piston hold
CC hold. spd FL < 340 [KCAS]
CD V_hold_3 mil,civ jet,turbo,piston hold
                                                                    .26500E+03
CC hold. spd FL > 340 [M]
                                                                    .83000E+00
CD V_hold_4
                mil,civ jet,turbo,piston hold
CC backtrack spd
                [KCAS]
CD V_backtrack
                mil,civ jet,turbo,piston gnd
                                                                    .35000E+02
CC taxi spd
                 [KCAS]
CD V_taxi
                mil,civ jet,turbo,piston gnd
                                                                    .15000E+02
CC apron spd
                  [KCAS]
CD V_apron
                 mil,civ jet,turbo,piston gnd
                                                                    .10000E+02
CC gate spd
                 [KCAS]
                mil,civ jet,turbo,piston gnd
                                                                   50000E+01
CD V_gate
CC Piston pow. red. [-]
CD C_red_piston mil,civ piston
                                                                    .000000+00
CC Turbo pow. red. [-]
                                                                    .250000+00
CD C_red_turbo
              mil,civ turbo
                                        ic,cl
                [-]
CC Jet power red.
                                                                    .150000+00
CD C_red_jet
                 mil,civ jet
                                        ic,cl
```

There are three types of lines in the BADA.GPF file with the line type identified by the first two characters in the line. These line types with their associated two leading characters are listed below.

CC comment line
CD data line
FI end-of-file line

The data is organised into three blocks separated by a comment line consisting of the block name and equal signs "=":

- file identification block
- class block
- parameter block

Each of these blocks is described in the subsections below.



6.8.1. File Identification Block

The file identification block provides information on the file name, creation and modification date. The block consists of 12 comment lines.

The comment lines specify the file name along with the creation date and last modification date. The creation date indicates the date when the file was created for the first time. The modification date indicates when the contents of the file were last modified.

6.8.2. Class Block

The class block consists of 6 comment lines and defines the three classes (Flight, Engine and Phase) and their instances that are used in the BADA.GPF file.

```
CC
     CC Flight = civ,mil
     CC Engine = jet,turbo,piston
     CC Phase = to,ic,cl,cr,des,hold,app,lnd,gnd
With: civ
                 civil flight
     mil
                 military flight
           =
     jet
                 jet engine
     turbo =
                 turboprop engine
     piston =
                 piston engine
                 take-off
     to
                 initial climb
     ic
                 climb
     cl
                 cruise
     cr
           =
     des
           =
                 descent
     hold
           =
                 holding
                 approach
     app
           =
                 landing
     Ind
           =
                 ground
     gnd
```



6.8.3. Parameter Block

The parameter block contains the values of the global aircraft parameters. This block has 5 comment lines plus a comment line and a dataline for each parameter.

```
CC
                     Unit
     CC Name
     CC Parameter
                     Flight Engine
                                         Phase
                                                                Value
     CC max. long. acc. [fps2]
                           jet,turbo,piston to,ic,cl,cr,des,hold,app,lnd .20000E+01
1 ->
     CD acc_long_max
                    civ
     CC max. norm. acc. [fps2]
                           jet,turbo,piston to,ic,cl,cr,des,hold,app,lnd .50000E+01
2 ->
     CD acc_norm_max
                    civ
     CC nom. bank angle [deg]
     CD ang_bank_nom
                    civ
                           jet, turbo, piston to, lnd
```

The parameter comment line contains the parameter name and its unit.

The parameter data line contains five fields:

(a) Parameter Field: This field identifies the parameter.

(b) Flight Field: This field identifies whether the parameter is valid for a civil flight, a

military flight or both.

(c) Engine Field: This field identifies the engine type (jet, turboprop or piston) for

which the parameter is valid.

(d) Phase Field: This field identifies for which flight phase the parameter is valid. 8

different flight phases are currently defined

(e) Value Field: The value field gives the value of the parameter.

The fields above are specified in the following fixed format (Fortran notation):

The parameter list continues until 'FI' (end of file) is reached.



7. REMOTE FILE ACCESS

The files associated with BADA Revision 3.10 are accessible through the BADA Support Application (BSA). The BSA is a Web application that provides BADA users with the ability to exchange requests, as well as data files and documents, with the BADA team members. It is also used for data repository of the BADA release files and documents.

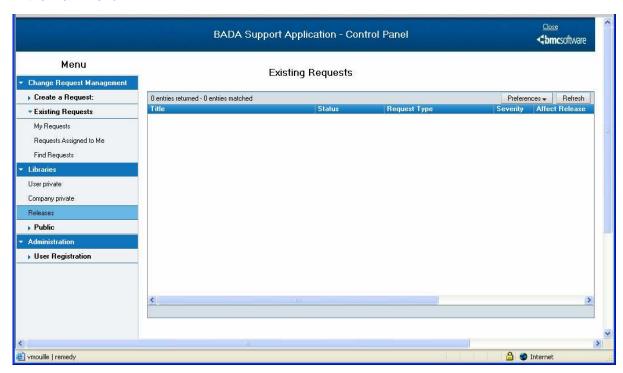
The right to use the BSA is granted to the licensed user of BADA. The application can be accessed by using a dedicated login and password as provided by the BADA team.

Once granted the access right to BSA, the user can access the application at this address:

https://remedyweb.eurocontrol.fr

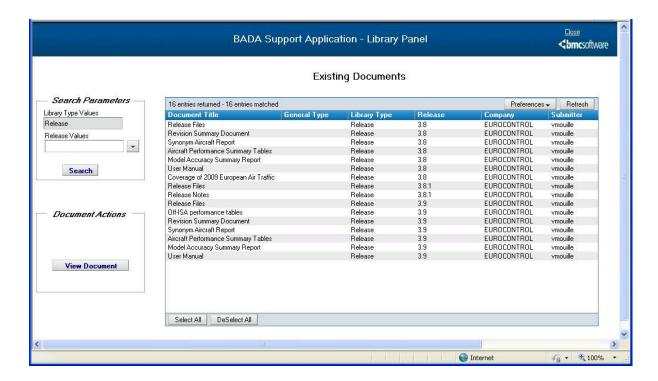
by using the BADA Support Application link and logging in with the provided login/password.

Once logged in, the user can access BADA releases through the Librairies→Releases item located in the main menu:



Then the release library page opens up, from where the user can download the BADA release files:





This process, as well as the general usage of the BSA application, is described in detail in [RD11].

Note that enquiries can be addressed to the following addresses:

E-mail: eec.bada@eurocontrol.int

Fax: + 33 1 69 88 73 33

BADA web page: http://www.eurocontrol.int/eec/public/standard_page/proj_BADA.html



APPENDIX A

BADA REVISION 3.10 - LIST OF AVAILABLE AIRCRAFT MODELS



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Table 7-1: List of Aircraft Types Supported by BADA Revision 3.10

A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
A10	equiv.	FAIRCHILD	THUNDERBOLT II	FGTN	50000		М
A124	equiv.	ANTONOV	AN-124 RUSLAN	A345	41450	32862	Н
A306	direct	AIRBUS	A300B4-600	A306	41000	32378	Н
A30B	direct	AIRBUS	A300B4-200	A30B	39000	31966	Н
A310	direct	AIRBUS	A310	A310	41000	35718	Н
A318	direct	AIRBUS	A318	A318	39800	37606	М
A319	direct	AIRBUS	A319	A319	41000	36365	М
A320	direct	AIRBUS	A320	A320	41000	33295	М
A321	direct	AIRBUS	A321	A321	39100	35396	М
A332	direct	AIRBUS	A330-200	A332	41000	36210	Н
A333	direct	AIRBUS	A330-300	A333	41000	36392	Н
A342	direct	AIRBUS	A340-200	A342	41500	31369	Н
A343	direct	AIRBUS	A340-300	A343	41500	31059	Н
A345	direct	AIRBUS	A340-500	A345	41450	32862	Н
A346	direct	AIRBUS	A340-600	A346	41500	33613	Н
A388	direct	AIRBUS	A380-800	A388	43100	34330	J
A3ST	direct	AIRBUS	A-300ST Beluga	A3ST	35000		Н
A4	equiv.	DOUGLAS	SUPER SKYHAWK	FGTN	50000		М
A400	equiv.	AIRBUS	A-400M	A3ST	35000		Н
A6	equiv.	GRUMMAN	INTRUDER	FGTN	50000		М
A7	equiv.	VOUGHT	CORSAIR II A7	FGTN	50000		М
A748	equiv.	AVRO	AVRO 748	ATP	25000	21628	М
AA5	equiv.	GULFSTREAM	Cheetah AA-5	P28A	12000		L
AC11	equiv.	ROCKWELL	COMMANDER 112	SR22	17500		L
AC90	equiv.	ROCKWELL	TURBO COMMANDER 690B	PAY3	33000		L
AC95	equiv.	GULFSTREAM	Jetprop Commander 980	PAY3	33000		L
AEST	equiv.	TED SMITH	AEROSTAR	MU2	28000		L
AFOX	equiv.	HALLEY	APOLO FOX	P28A	12000		L
AJET	equiv.	DASSAULT	ALPHA JET	FGTN	50000		М
ALSL	equiv.	AIRLONY	SKYLANE	P28A	12000		L



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
AMX	equiv.	EMBRAER	AMX	FGTN	50000		М
AN12	equiv.	ANTONOV	AN-12	C130	32000	21891	М
AN24	equiv.	ANTONOV	AN-24	F27	25000	22777	М
AN26	equiv.	ANTONOV	AN-26	E120	32000		М
AN28	equiv.	ANTONOV	AN-28	D228	28000		L
AN72	equiv.	ANTONOV	AN-72	F28	35000	31000	М
APM4	equiv.	ISSOIRE	APM 40 SIMBA	P28A	12000		L
ASTR	equiv.	IAI	1125 Astra	FA10	45000	38400	М
AT43	direct	ATR	ATR 42-300	AT43	25000	22699	М
AT44	equiv.	ATR	ATR 42-400	AT45	25000	23591	М
AT45	direct	ATR	ATR 42-500	AT45	25000	23591	М
AT46	equiv.	ATR	ATR 42-600	AT45	25000	23591	М
AT72	direct	ATR	ATR 72-200	AT72	25000	20317	М
AT73	direct	ATR	ATR 72-210	AT73	25000	20943	М
AT75	direct	ATR	ATR 72-500	AT75	25000	20779	М
AT76	equiv.	ATR	ATR 72-600	AT75	25000	20779	М
ATLA	equiv.	DASSAULT	1150 ATLANTIC	E120	32000		М
ATP	direct	BAE	ADVANCED TURBOPROP	ATP	25000	21628	М
B1	equiv.	ROCKWELL	B1 LANCER	FGTL	41000		Н
B190	equiv.	BEECH	1900	JS32	25000		L
B350	equiv.	BEECH	SUPER KING AIR 350	BE20	35000		L
B461	equiv.	BAE	146-100/RJ	B462	31000	32716	М
B462	direct	BAE	146-200/RJ	B462	31000	32716	М
B463	direct	BAE	146-300/RJ	B463	31000	29305	М
B52	equiv.	BOEING	B-52 Stratofortress	FGTL	41000		Н
B701	equiv.	BOEING	707-100	B752	42000	35478	М
B703	direct	BOEING	707-300	B703	42000	35000	Н
B712	direct	BOEING	717-200	B712	37000	35187	М
B720	equiv.	BOEING	B720B	B752	42000	35478	М
B721	equiv.	BOEING	727-100	B752	42000	35478	М
B722	direct	BOEING	727-200	B722	37000	33845	М



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
B731	equiv.	BOEING	737-100	T134	39000	34764	М
B732	direct	BOEING	737-200	B732	37000	34508	М
B733	direct	BOEING	737-300	B733	39000	33636	М
B734	direct	BOEING	737-400	B734	37000	33448	М
B735	direct	BOEING	737-500	B735	37000	34768	М
B736	direct	BOEING	737-600	B736	41000	39276	М
B737	direct	BOEING	737-700	B737	41000	37332	М
B738	direct	BOEING	737-800	B738	41000	34982	М
B739	direct	BOEING	737-900	B739	41000	34683	М
B741	equiv.	BOEING	747-100	B743	45000	30943	Н
B742	direct	BOEING	747-200	B742	45000	33180	Н
B743	direct	BOEING	747-300	B743	45000	30943	Н
B744	direct	BOEING	747-400	B744	45000	32726	Н
B748	direct	BOEING	747-8	B748	42100	32973	Н
B74D	equiv.	BOEING	747-400 DOMESTIC	B744	45000	32726	Н
B74R	equiv.	BOEING	747SR	B743	45000	30943	Н
B74S	equiv.	BOEING	747-SP	B742	45000	33180	Н
B752	direct	BOEING	757-200	B752	42000	35478	М
B753	direct	BOEING	757-300	B753	43000	33339	М
B762	direct	BOEING	767-200	B762	43000	35861	Н
B763	direct	BOEING	767-300	B763	43100	36502	Н
B764	direct	BOEING	767-400	B764	45000	33210	Н
B772	direct	BOEING	777-200 ER	B772	43100	34643	Н
B773	direct	BOEING	777-300	B773	43100	31857	Н
B77L	direct	BOEING	777-200 LRF	B77L	43100	35104	Н
B77W	direct	BOEING	777-300 ER	B77W	43100	34314	Н
B788	direct	BOEING	787-8	B788	43100	35901	Н
BA11	direct	BAE	111	BA11	35000	29750	М
BDOG	equiv.	BAE	SA-3 BULLDOG	C182	20000		L
BE10	equiv.	BEECH	KING AIR 100	D228	28000		L
BE20	direct	BEECH	SUPER KING AIR 200	BE20	35000		L



BE30 equiv. BEECH SUPER KING AIR 300 BE20 35000 L L BE33 equiv. BEECH BONANZA 33 C182 20000 L L BE36 equiv. BEECH BONANZA 36 DA42 18000 L BE40 equiv. BEECH BEECHLET 400 C560 45000 41516 M BE55 equiv. BEECH BERCHSTET 400 C560 45000 41516 M BE55 equiv. BEECH BARON 58 BE58 25000 L L BE66 equiv. BEECH DUKE 60 C421 30000 L L BE66 equiv. BEECH DUCHESSE 76 C182 20000 L L BE76 equiv. BEECH TRAVEL AIR 95 TRIN 25000 L L BE99 direct BEECH KING AIR 90 BE91 31000 L L BE91 equiv. <th>A/C Code</th> <th>Model Type</th> <th>Aircraft manufacturer</th> <th>Aircraft model</th> <th>Synonym aircraft</th> <th>h_{MO} [ft]</th> <th>h_{max} [ft]</th> <th>WTC</th>	A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
BE36	BE30	equiv.	BEECH		BE20	35000		L
BE40 equiv. BEECH BEECHJET 400 C560 45000 41516 M BE55 equiv. BEECH BARON 55 PA34 25000 22500 L BE58 direct BEECH BARON 58 BE58 25000 L BE60 equiv. BEECH DUKE 60 C421 30000 L BE65 equiv. BEECH QUEEN AIR 65 PA34 25000 22500 L BE66 equiv. BEECH DUCHESSE 76 C182 20000 L L BE76 equiv. BEECH TRAVEL AIR 95 TRIN 25000 L L BE99 direct BEECH AIRLINER C99 BE99 15000 L L BE91 direct BEECH KING AIR 90 BE9L 31000 L L BMAN equiv. AAK BUSHMAN P28A 12000 L BN2P equiv. BRITTEN-NORMAN B	BE33	equiv.	BEECH	BONANZA 33	C182	20000		L
BE55 equiv. BEECH BARON 55 PA34 25000 22500 L BE58 direct BEECH BARON 58 BE58 25000 L BE60 equiv. BEECH DUKE 60 C421 30000 L BE65 equiv. BEECH QUEEN AIR 65 PA34 25000 22500 L BE76 equiv. BEECH DUCHESSE 76 C182 20000 L L BE95 equiv. BEECH DUCHESSE 76 C182 20000 L L BE95 equiv. BEECH TRAVEL AIR 95 TRIN 25000 L L BE99 direct BEECH KING AIR 90 BE91 31000 L L BMAN equiv. BEECH KING AIR 90 BE91 31000 L L BN2P equiv. BRITTEN-NORMAN PS2A MARITIME DEFENDER PA34 25000 L L BN2T equiv.	BE36	equiv.	BEECH	BONANZA 36	DA42	18000		L
BE58 direct BEECH BARON 58 BE58 25000 L	BE40	equiv.	BEECH	BEECHJET 400	C560	45000	41516	М
BE60 equiv. BEECH DUKE 60 C421 30000 L BE65 equiv. BEECH QUEEN AIR 65 PA34 25000 22500 L BE76 equiv. BEECH DUCHESSE 76 C182 20000 L BE95 equiv. BEECH TRAVEL AIR 95 TRIN 25000 L BE99 direct BEECH AIRLINER C99 BE99 15000 L BE91 direct BEECH KING AIR 90 BE9L 31000 L BE91 equiv. BEECH KING AIR 90 BE9L 31000 L BMAN equiv. AAK BUSHMAN P28A 12000 L BN2P equiv. BRITTEN-NORMAN BN-2A MARITIME DEFENDER PA34 25000 22500 L BN2T equiv. BRITTEN-NORMAN BN-2T Defender 4000 E120 32000 M C10T equiv. ADVANCED AIRCRAFT SPIRIT 750 D228 2800	BE55	equiv.	BEECH	BARON 55	PA34	25000	22500	L
BE65 equiv. BEECH QUEEN AIR 65 PA34 25000 22500 L BE76 equiv. BEECH DUCHESSE 76 C182 20000 L BE95 equiv. BEECH TRAVEL AIR 95 TRIN 25000 L BE99 direct BEECH AIRLINER C99 BE99 15000 L BE91 direct BEECH KING AIR 90 BE9L 31000 L BE91 direct BEECH KING AIR 90 BE9L 31000 L BMAN equiv. AAK BUSHMAN P28A 12000 L BN2P equiv. BRITTEN-NORMAN BN-2T MARITIME PA34 25000 22500 L BN2T equiv. BRITTEN-NORMAN BN-2T Defender 4000 E120 32000 M C10T equiv. ADVANCED AIRCRAFT SPIRIT 750 D228 28000 L C130 direct LOCKHEED HERCULES C130 32000 <td>BE58</td> <td>direct</td> <td>BEECH</td> <td>BARON 58</td> <td>BE58</td> <td>25000</td> <td></td> <td>L</td>	BE58	direct	BEECH	BARON 58	BE58	25000		L
BE76 equiv. BEECH DUCHESSE 76 C182 20000 L BE95 equiv. BEECH TRAVEL AIR 95 TRIN 25000 L BE99 direct BEECH AIRLINER C99 BE99 15000 L BE91 direct BEECH KING AIR 90 BE9L 31000 L BMAN equiv. BEECH KING AIR 90 BE9L 31000 L BMAN equiv. AAK BUSHMAN P28A 12000 L BN2P equiv. BRITTEN-NORMAN BN-2A MARITIME DEFENDER PA34 25000 22500 L BN2T equiv. BRITTEN-NORMAN BN-2T Defender 4000 E120 32000 M C10T equiv. ADVANCED AIRCRAFT SPIRIT 750 D228 28000 L C130 direct LOCKHEED HERCULES C130 32000 21891 M C135 equiv. BOEING STRATOLIFTER C-135 B703	BE60	equiv.	BEECH	DUKE 60	C421	30000		L
BE95 equiv. BEECH TRAVEL AIR 95 TRIN 25000 L	BE65	equiv.	BEECH	QUEEN AIR 65	PA34	25000	22500	L
BE99 direct BEECH AIRLINER C99 BE99 15000 L	BE76	equiv.	BEECH	DUCHESSE 76	C182	20000		L
BE9L direct BEECH KING AIR 90 BE9L 31000 L BE9T equiv. BEECH KING AIR 90 BE9L 31000 L BMAN equiv. AAK BUSHMAN P28A 12000 L BN2P equiv. BRITTEN-NORMAN BN-2A MARITIME DEFENDER PA34 25000 22500 L BN2T equiv. BRITTEN-NORMAN BN-2T Defender 4000 E120 32000 M C10T equiv. ADVANCED AIRCRAFT ANORMAN SPIRIT 750 D228 28000 L C130 direct LOCKHEED HERCULES C130 32000 21891 M C135 equiv. BOEING STRATOLIFTER C-141 A310 42000 35000 H C141 equiv. LOCKHEED STARLIFTER C-141 A310 41000 35718 H C160 direct TRANSALL C160 C160 30000 25500 M C162 equiv.	BE95	equiv.	BEECH	TRAVEL AIR 95	TRIN	25000		L
BE9T equiv. BEECH KING AIR 90 BE9L 31000 L BMAN equiv. AAK BUSHMAN P28A 12000 L BN2P equiv. BRITTEN-NORMAN BN-2A MARITIME DEFENDER PA34 25000 22500 L BN2T equiv. BRITTEN-NORMAN BN-2T Defender 4000 E120 32000 M C10T equiv. ADVANCED AIRCRAFT SPIRIT 750 D228 28000 L C130 direct LOCKHEED HERCULES C130 32000 21891 M C135 equiv. BOEING STRATOLIFTER C-141 A310 42000 35000 H C141 equiv. LOCKHEED STARLIFTER C-141 A310 41000 35718 H C160 direct TRANSALL C160 C160 30000 25500 M C162 equiv. CESSNA SKYCATCHER DA42 18000 L C170 equiv. <	BE99	direct	BEECH	AIRLINER C99	BE99	15000		L
BMAN equiv. AAK BUSHMAN P28A 12000 L BN2P equiv. BRITTEN-NORMAN BN-2A MARITIME DEFENDER PA34 25000 22500 L BN2T equiv. BRITTEN-NORMAN BN-2T Defender 4000 E120 32000 M C10T equiv. ADVANCED AIRCRAFT AIRCRAFT SPIRIT 750 D228 28000 L C130 direct LOCKHEED HERCULES C130 32000 21891 M C135 equiv. BOEING STRATOLIFTER C-141 A310 42000 35000 H C141 equiv. LOCKHEED STARLIFTER C-141 A310 41000 35718 H C160 direct TRANSALL C160 C160 30000 25500 M C162 equiv. CESSNA SKYCATCHER DA42 18000 L C170 equiv. BOEING GLOBEMASTER 3 B764 45000 33210 H C170 <td>BE9L</td> <td>direct</td> <td>BEECH</td> <td>KING AIR 90</td> <td>BE9L</td> <td>31000</td> <td></td> <td>L</td>	BE9L	direct	BEECH	KING AIR 90	BE9L	31000		L
BN2P equiv. BRITTEN-NORMAN NORMAN NORMAN BN-2A MARITIME DEFENDER PA34 25000 22500 L BN2T equiv. BRITTEN-NORMAN NORMAN BN-2T Defender 4000 E120 32000 M C10T equiv. ADVANCED AIRCRAFT AIRCRAFT SPIRIT 750 D228 28000 L C130 direct LOCKHEED HERCULES C130 32000 21891 M C135 equiv. BOEING STRATOLIFTER C-141 A310 42000 35000 H C141 equiv. LOCKHEED STARLIFTER C-141 A310 41000 35718 H C160 direct TRANSALL C160 C160 30000 25500 M C162 equiv. CESSNA SKYCATCHER DA42 18000 L C170 equiv. BOEING GLOBEMASTER 3 B764 45000 33210 H C170 equiv. CESSNA SKYHAWK 172 C172 14000 L	BE9T	equiv.	BEECH	KING AIR 90	BE9L	31000		L
BN2P equiv. NORMAN DEFENDER PA34 25000 22500 L BN2T equiv. BRITTEN-NORMAN BN-2T Defender 4000 E120 32000 M C10T equiv. ADVANCED AIRCRAFT SPIRIT 750 D228 28000 L C130 direct LOCKHEED HERCULES C130 32000 21891 M C135 equiv. BOEING STRATOLIFTER C-141 A310 42000 35000 H C141 equiv. LOCKHEED STARLIFTER C-141 A310 41000 35718 H C160 direct TRANSALL C160 C160 30000 25500 M C162 equiv. CESSNA SKYCATCHER DA42 18000 L C172 equiv. BOEING GLOBEMASTER 3 B764 45000 33210 H C170 equiv. CESSNA 170 C172 14000 L C172 direct	BMAN	equiv.	AAK	BUSHMAN	P28A	12000		L
BN21 equiv. NORMAN BN-21 Defender 4000 E120 32000 M C10T equiv. ADVANCED AIRCRAFT AIRCRAFT SPIRIT 750 D228 28000 L C130 direct LOCKHEED HERCULES C130 32000 21891 M C135 equiv. BOEING STRATOLIFTER C-180 B703 42000 35000 H C141 equiv. LOCKHEED STRATOLIFTER C-141 A310 41000 35718 H C160 direct TRANSALL C160 C160 30000 25500 M C162 equiv. CESSNA SKYCATCHER DA42 18000 L C17 equiv. BOEING GLOBEMASTER 3 B764 45000 33210 H C170 equiv. CESSNA 170 C172 14000 L C172 direct CESSNA SKYHAWK 172 C172 14000 L C182 direct CESSNA	BN2P	equiv.			PA34	25000	22500	L
C101 equiv. AIRCRAFT SPIRIT 750 D228 25000 L C130 direct LOCKHEED HERCULES C130 32000 21891 M C135 equiv. BOEING STRATOLIFTER C- 135C B703 42000 35000 H C141 equiv. LOCKHEED STARLIFTER C-141 A310 41000 35718 H C160 direct TRANSALL C160 C160 30000 25500 M C162 equiv. CESSNA SKYCATCHER DA42 18000 L C17 equiv. BOEING GLOBEMASTER 3 B764 45000 33210 H C170 equiv. CESSNA 170 C172 14000 L C172 direct CESSNA SKYHAWK 172 C172 14000 L C173 equiv. CESSNA CARDINAL 177 C172 14000 L C182 direct CESSNA SKYLANE 182 C182 20000 L C206 equiv. CESSNA TURBO STATIONAIR SR22 17500 L	BN2T	equiv.		BN-2T Defender 4000	E120	32000		М
C135 equiv. BOEING STRATOLIFTER C-135C B703 42000 35000 H C141 equiv. LOCKHEED STARLIFTER C-141 A310 41000 35718 H C160 direct TRANSALL C160 C160 30000 25500 M C162 equiv. CESSNA SKYCATCHER DA42 18000 L C17 equiv. BOEING GLOBEMASTER 3 B764 45000 33210 H C170 equiv. CESSNA 170 C172 14000 L C172 direct CESSNA SKYHAWK 172 C172 14000 L C177 equiv. CESSNA CARDINAL 177 C172 14000 L C182 direct CESSNA SKYLANE 182 C182 20000 L C206 equiv. CESSNA TURBO STATIONAIR SR22 17500 L	C10T	equiv.		SPIRIT 750	D228	28000		L
C135 equiv. BOEING 135C B703 42000 35000 H C141 equiv. LOCKHEED STARLIFTER C-141 A310 41000 35718 H C160 direct TRANSALL C160 C160 30000 25500 M C162 equiv. CESSNA SKYCATCHER DA42 18000 L C17 equiv. BOEING GLOBEMASTER 3 B764 45000 33210 H C170 equiv. CESSNA 170 C172 14000 L C172 direct CESSNA SKYHAWK 172 C172 14000 L C177 equiv. CESSNA CARDINAL 177 C172 14000 L C182 direct CESSNA SKYLANE 182 C182 20000 L C206 equiv. CESSNA TURBO STATIONAIR SR22 17500 L	C130	direct	LOCKHEED	HERCULES	C130	32000	21891	М
C160 direct TRANSALL C160 C160 30000 25500 M C162 equiv. CESSNA SKYCATCHER DA42 18000 L C17 equiv. BOEING GLOBEMASTER 3 B764 45000 33210 H C170 equiv. CESSNA 170 C172 14000 L C172 direct CESSNA SKYHAWK 172 C172 14000 L C177 equiv. CESSNA CARDINAL 177 C172 14000 L C182 direct CESSNA SKYLANE 182 C182 20000 L C206 equiv. CESSNA TURBO STATIONAIR 6 SR22 17500 L	C135	equiv.	BOEING		B703	42000	35000	Н
C162 equiv. CESSNA SKYCATCHER DA42 18000 L C17 equiv. BOEING GLOBEMASTER 3 B764 45000 33210 H C170 equiv. CESSNA 170 C172 14000 L C172 direct CESSNA SKYHAWK 172 C172 14000 L C177 equiv. CESSNA CARDINAL 177 C172 14000 L C182 direct CESSNA SKYLANE 182 C182 20000 L C206 equiv. CESSNA TURBO STATIONAIR 6 SR22 17500 L	C141	equiv.	LOCKHEED	STARLIFTER C-141	A310	41000	35718	Н
C17 equiv. BOEING GLOBEMASTER 3 B764 45000 33210 H C170 equiv. CESSNA 170 C172 14000 L C172 direct CESSNA SKYHAWK 172 C172 14000 L C177 equiv. CESSNA CARDINAL 177 C172 14000 L C182 direct CESSNA SKYLANE 182 C182 20000 L C206 equiv. CESSNA TURBO STATIONAIR 6 SR22 17500 L	C160	direct	TRANSALL	C160	C160	30000	25500	М
C170 equiv. CESSNA 170 C172 14000 L C172 direct CESSNA SKYHAWK 172 C172 14000 L C177 equiv. CESSNA CARDINAL 177 C172 14000 L C182 direct CESSNA SKYLANE 182 C182 20000 L C206 equiv. CESSNA TURBO STATIONAIR 6 SR22 17500 L	C162	equiv.	CESSNA	SKYCATCHER	DA42	18000		L
C172 direct CESSNA SKYHAWK 172 C172 14000 L C177 equiv. CESSNA CARDINAL 177 C172 14000 L C182 direct CESSNA SKYLANE 182 C182 20000 L C206 equiv. CESSNA TURBO STATIONAIR 6 SR22 17500 L	C17	equiv.	BOEING	GLOBEMASTER 3	B764	45000	33210	Н
C177 equiv. CESSNA CARDINAL 177 C172 14000 L C182 direct CESSNA SKYLANE 182 C182 20000 L C206 equiv. CESSNA TURBO STATIONAIR 6 SR22 17500 L	C170	equiv.	CESSNA	170	C172	14000		L
C182 direct CESSNA SKYLANE 182 C182 20000 L C206 equiv. CESSNA TURBO STATIONAIR 6 SR22 17500 L	C172	direct	CESSNA	SKYHAWK 172	C172	14000		L
C206 equiv. CESSNA TURBO STATIONAIR SR22 17500 L	C177	equiv.	CESSNA	CARDINAL 177	C172	14000		L
6 3R22 17500 E	C182	direct	CESSNA	SKYLANE 182	C182	20000		L
C208 equiv. CESSNA CARAVAN PA27 20000 L	C206	equiv.	CESSNA		SR22	17500		L
	C208	equiv.	CESSNA	CARAVAN	PA27	20000		L



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
C210	equiv.	CESSNA	CENTURION	SR22	17500		L
C212	equiv.	CASA	T-12 AVIOCAR	D228	28000		L
C25A	equiv.	CESSNA	525A Citation CJ2	C560	45000	41516	М
C25B	equiv.	CESSNA	525B Citation CJ3	C560	45000	41516	М
C25C	equiv.	CESSNA	525C Citation CJ4	LJ35	45000	40287	М
C27J	equiv.	ALENIA	C-27J Spartan	E120	32000		М
C295	equiv.	CASA	C-295	ATP	25000	21628	М
C303	equiv.	CESSNA	CRUSADER 303	PA31	26300		L
C30J	equiv.	LOCKHEED MARTIN	C130J HERCULES	C130	32000	21891	М
C310	equiv.	CESSNA	310	PA34	25000	22500	L
C337	equiv.	CESSNA	SUPER SKYMASTER	PA27	20000		L
C340	equiv.	CESSNA	C-340/340A	C421	30000		L
C402	equiv.	CESSNA	402	PA34	25000	22500	L
C404	equiv.	CESSNA	TITAN	BE58	25000		L
C414	equiv.	CESSNA	CHANCELLOR 414	PA31	26300		L
C421	direct	CESSNA	GOLDEN EAGLE 421	C421	30000		L
C425	equiv.	CESSNA	CORSAIR	TBM8	31000		L
C441	equiv.	CESSNA	Conquest	PAY3	33000		L
C5	equiv.	LOCKHEED	L-500 GALAXY	A346	41500	33613	Н
C500	equiv.	CESSNA	CITATION 1	C550	43000		L
C501	equiv.	CESSNA	CITATION 1SP	C550	43000		L
C510	direct	CESSNA	CITATION MUSTANG	C510	41000		L
C525	equiv.	CESSNA	CITATION JET	C550	43000		L
C526	equiv.	CESSNA	CITATION JET 526	E50P	41000	40400	L
C550	direct	CESSNA	CITATION II-S2	C550	43000		L
C551	equiv.	CESSNA	CITATION 2SP	C550	43000		L
C560	direct	CESSNA	CITATION V	C560	45000	41516	М
C56X	direct	CESSNA	CITATION Excel	C56X	45000	44523	М
C650	equiv.	CESSNA	CITATION VII	LJ35	45000	40287	М
C680	equiv.	CESSNA	Citation Sovereign	F2TH	47000	41486	М
C72R	equiv.	CESSNA	CUTLASS RG	SR22	17500		L



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
C750	direct	CESSNA	CITATION 10	C750	51000	45180	М
C77R	equiv.	CESSNA	CARDINAL 177RG	P28A	12000		L
C82R	equiv.	CESSNA	SKYLANE R182 RG	C182	20000		L
CA41	equiv.	CORVUS	CA-41 RACER	P28A	12000		L
CE43	equiv.	CERVA	GUEPARD	SR22	17500		L
CL2T	equiv.	CANADAIR	CL-415	SH36	20000		М
CL30	equiv.	BOMBARDIER	Challenger 300	F2TH	47000	41486	М
CL60	direct	CANADAIR	CHALLENGER 600/601	CL60	41000	39223	М
CN35	equiv.	CASA	CN-235	AT43	25000	22699	М
COL4	equiv.	CESSNA	COLUMBIA 400	TRIN	25000		L
CORV	equiv.	WOLFSBERT	CORVUS	DA42	18000		L
CRJ1	direct	CANADAIR	REGIONAL JET CRJ- 100	CRJ1	41000	34333	М
CRJ2	direct	CANADAIR	REGIONAL JET CRJ- 200	CRJ2	41000	36855	М
CRJ7	equiv.	CANADAIR	REGIONAL JET CRJ- 700	CRJ9	41000	36457	М
CRJ9	direct	CANADAIR	REGIONAL JET CRJ- 900	CRJ9	41000	36457	М
CRJX	equiv.	BOMBARDIER	REGIONAL JET CRJ- 1000	CRJ9	41000	36457	М
CVLT	equiv.	CANADAIR	CC-109 COSMOPOLITAN	DH8C	25000	24804	L
D228	direct	DORNIER	228	D228	28000		L
D328	direct	DORNIER	328	D328	32800	29051	М
DA40	equiv.	DIAMOND	DA-40-180 DIAMOND STAR	DA42	18000		L
DA42	direct	DIAMOND	TWIN STAR	DA42	18000		L
DC10	direct	MCDONNELL DOUGLAS	DC-10	DC10	39000	32000	Н
DC3	equiv.	DOUGLAS	DC-3	C421	30000		L
DC85	equiv.	MCDONNELL DOUGLAS	DC-8-50	A310	41000	35718	Н
DC86	equiv.	MCDONNELL DOUGLAS	DC-8-60	DC87	42000	34000	Н
DC87	direct	MCDONNELL DOUGLAS	DC-8-70	DC87	42000	34000	Н



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
DC91	equiv.	MCDONNELL DOUGLAS	DC-9-10	B712	37000	35187	М
DC92	equiv.	MCDONNELL DOUGLAS	DC-9-20	DC94	35000	33500	М
DC93	equiv.	MCDONNELL DOUGLAS	DC-9-30	DC94	35000	33500	М
DC94	direct	MCDONNELL DOUGLAS	DC-9-40	DC94	35000	33500	М
DC95	equiv.	MCDONNELL DOUGLAS	DC-9-50	DC94	35000	33500	М
DH8A	direct	DE HAVILLAND	DASH 8-100	DH8A	25000	25000	М
DH8B	equiv.	DE HAVILLAND	DASH 8-200	DH8C	25000	24804	L
DH8C	direct	DE HAVILLAND	DASH 8-300	DH8C	25000	24804	L
DH8D	direct	DE HAVILLAND	DASH 8-400	DH8D	25000		М
DHC6	equiv.	DE HAVILLAND CANADA	DHC-6 Twin Otter	D228	28000		L
DR30	equiv.	ROBIN	PETIT PRINCE DR- 315	PA27	20000		L
DR40	equiv.	ROBIN	DR-400 DAUPHIN	SR22	17500		L
DV2	equiv.	DOVA	DV-2 INFINITY	DA42	18000		L
E110	equiv.	EMBRAER	BANDEIRANTE	SW4	25000	25000	L
E120	direct	EMBRAER	EMB-120 BRASILIA	E120	32000		М
E121	equiv.	EMBRAER	Xingu	PAY2	29000		L
E135	direct	EMBRAER	EMB-135	E135	41000	38617	М
E145	direct	EMBRAER	EMB-145	E145	37000		М
E170	direct	EMBRAER	EMB-175	E170	41000		М
E190	direct	EMBRAER	EMB-190	E190	41000		М
E2	equiv.	GRUMMAN	E-2 HAWKEYE	E120	32000		М
E3CF	equiv.	BOEING	E-3 SENTRY	B762	43000	35861	Н
E3TF	equiv.	BOEING	E-3A SENTRY	B762	43000	35861	Н
E50P	direct	EMBRAER	Phenom 100	E50P	41000	40400	L
E55P	direct	EMBRAER	Phenom 300	E55P	45000	44923	М
EA50	direct	ECLIPSE	ECLIPSE 500	EA50	41000		L
EPX1	equiv.	EPERVIER	X-1	DA42	18000		L
ETAR	equiv.	DASSAULT	ETENDARD 4	FGTN	50000		М
EUFI	equiv.	EUROFIGHTER	2000	FGTN	50000		М



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
EV97	equiv.	EVEKTOR	SPORTSTAR	P28A	12000		L
F1	equiv.	MITSUBISHI	F1	FGTN	50000		М
F100	direct	FOKKER	100	F100	35000	35000	М
F104	equiv.	LOCKHEED	STARFIGHTER	FGTN	50000		М
F117	equiv.	LOCKHEED	NIGHTHAWK	FGTN	50000		М
F14	equiv.	GRUMMAN	TOMCAT	FGTN	50000		М
F15	equiv.	MCDONNELL DOUGLAS	EAGLE	FGTN	50000		М
F16	equiv.	GENERAL DYNAMICS	FIGHTING FALCON	FGTN	50000		М
F18	equiv.	MCDONNELL DOUGLAS	HORNET	FGTN	50000		М
F1FV	equiv.	AVION	FAVORIT	TRIN	25000		L
F260	equiv.	SIAI- MARCHETTI	SF-260	BE58	25000		L
F27	direct	FOKKER	FRIENDSHIP	F27	25000	22777	М
F28	direct	FOKKER	FOLLOWSHIP	F28	35000	31000	М
F2TH	direct	DASSAULT	FALCON 2000	F2TH	47000	41486	М
F4	equiv.	MCDONNELL DOUGLAS	PHANTOM	FGTN	50000		М
F406	equiv.	CESSNA	F406 Vigilant	PAY3	33000		L
F5	equiv.	NORTHROP	F-5	FGTN	50000		М
F50	direct	FOKKER	50	F50	25000	22108	М
F5SA	equiv.	IRIAF	SAEGHE	FGTN	50000		М
F70	direct	FOKKER	70	F70	37000	36565	М
F900	direct	DASSAULT	FALCON 900	F900	51000	38187	М
FA04	equiv.	FLAMING AIR	PEREGRINE	P28A	12000		L
FA10	direct	DASSAULT	FALCON 10	FA10	45000	38400	М
FA20	direct	DASSAULT	FALCON 20	FA20	42000	38000	М
FA50	direct	DASSAULT	FALCON 50	FA50	49000	41177	М
FA7X	direct	DASSAULT	FALCON 7X	FA7X	51000	39848	М
FGTH	direct	GENERIC	MIL FIGHTER HEAVY	FGTH	50000		М
FGTL	direct	GENERIC	MIL FIGHTER LIGHT	FGTL	41000		Н
FGTN	direct	GENERIC	MIL FIGHTER NORMAL	FGTN	50000		М



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
G120	equiv.	GROB	G-120A	SR22	17500		L
G12T	equiv.	GROB	G-120TP	TBM7	31000		L
G150	equiv.	IAI	Gulfstream G150	F2TH	47000	41486	М
G222	equiv.	ALENIA	SPARTAN C-27A	ATP	25000	21628	М
G250	equiv.	GULFSTREAM	G250	F2TH	47000	41486	М
G280	equiv.	GULFSTREAM AEROSPACE	G280	F2TH	47000	41486	М
GA7	equiv.	GRUMMAN AMERICAN	COUGAR	SR22	17500		L
GALX	equiv.	IAI	1126 GALAXY	F2TH	47000	41486	М
GL5T	equiv.	BOMBARDIER	Global 5000	C750	51000	45180	М
GLAS	equiv.	STODDARD- HAMILTON	GLASAIR	BE58	25000		L
GLEX	equiv.	BOMBARDIER	BD-700 Global Express	C750	51000	45180	М
GLF2	equiv.	GULFSTREAM	GULFSTREAM II	FA7X	51000	39848	М
GLF3	equiv.	GULFSTREAM	GULFSTREAM III	FA7X	51000	39848	М
GLF4	equiv.	GULFSTREAM	GULFSTREAM IV	FA7X	51000	39848	М
GLF5	equiv.	GULFSTREAM	GULFSTREAM V C37	FA7X	51000	39848	М
GLF6	equiv.	GULFSTREAM	G650	FA7X	51000	39848	М
GLST	equiv.	GLASAIR	GlaStar	TRIN	25000		L
GRIZ	equiv.	AERO TEK	TURBO GRIZZLY	PA34	25000	22500	L
H25A	direct	HAWKER SIDDELEY	DOMINE HS 125	H25A	40000		М
H25B	equiv.	HAWKER SIDDELEY	HS 125-700/800	H25A	40000		М
H25C	equiv.	RAYTHEON	HAWKER 1000	FA20	42000	38000	М
HA4T	equiv.	RAYTHEON	HAWKER 4000	F2TH	47000	41486	М
HAR	equiv.	HAWKER SIDDELEY	HARRIER	FGTN	50000		М
HAWK	equiv.	HAWKER SIDDELEY	HAWK	FGTN	50000		М
HELI	equiv.	GENERIC	HELICOPTER	P28A	12000		L
HR10	equiv.	ROBIN	TIARA	TRIN	25000		L
HRNT	equiv.	AAK	HORNET	P28A	12000		L
IL18	equiv.	ILYUSHIN	IL-18	C130	32000	21891	М



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
IL62	equiv.	ILYUSHIN	IL-62 /-62M / MK	A30B	39000	31966	Н
IL76	equiv.	ILYUSHIN	IL-76	B764	45000	33210	Н
IL86	equiv.	ILYUSHIN	IL-86	B763	43100	36502	Н
IL96	equiv.	ILYUSHIN	IL-96	A342	41500	31369	Н
IMPX	equiv.	XTREMAIR	XTREME 3000	BE58	25000		L
J328	equiv.	FAIRCHILD DORNIER	328 Jet	E135	41000	38617	М
JAGR	equiv.	SEPECAT	JAGUAR	FGTN	50000		М
JS1	equiv.	JETSTREAM	JETSTREAM 1	BE20	35000		L
JS20	equiv.	JETSTREAM	JETSTREAM 200	D228	28000		L
JS31	equiv.	BAE	JETSTREAM 31	JS32	25000		L
JS32	direct	JETSTREAM	JETSTREAM Super 31	JS32	25000		L
JS41	direct	JETSTREAM	JETSTREAM 41	JS41	26000	24685	М
K35A	equiv.	BOEING	STRATOTANKER KC-135A	B703	42000	35000	Н
K35E	equiv.	BOEING	STRATOTANKER KC-135D/E	B703	42000	35000	Н
K35R	equiv.	BOEING	STRATOTANKER K35R	B703	42000	35000	Н
KAT3	equiv.	KHRUNICHEV	AT-3	PA31	26300		L
KEST	equiv.	FARNBOROUGH	KESTREL	PAY2	29000		L
L101	direct	LOCKHEED	TRISTAR L-1011	L101	42000	33000	Н
L159	equiv.	AERO (2)	L-159	FGTN	50000		М
L188	equiv.	LOCKHEED	ELECTRA L-188	C160	30000	25500	М
L29A	equiv.	LOCKHEED	JETSTART	CL60	41000	39223	М
L29B	equiv.	LOCKHEED	L1329 JETSTAR	CL60	41000	39223	М
L410	equiv.	LET	TURBOLET 410	D228	28000		L
LJ24	equiv.	LEARJET	24	C560	45000	41516	М
LJ25	equiv.	LEARJET	25	LJ45	51000	44099	М
LJ31	equiv.	LEARJET	31	LJ45	51000	44099	М
LJ35	direct	LEARJET	35	LJ35	45000	40287	М
LJ40	equiv.	LEARJET	40	LJ45	51000	44099	М
LJ45	direct	LEARJET	45	LJ45	51000	44099	М
LJ55	equiv.	LEARJET	55	LJ45	51000	44099	М



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
LJ60	equiv.	LEARJET	60	LJ45	51000	44099	М
M2	equiv.	KUBICEK	M-2 SCOUT	P28A	12000		L
M20P	equiv.	MOONEY	MARK 201	TRIN	25000		L
M20T	equiv.	MOONEY	MARK 20T	TRIN	25000		L
MD11	direct	MCDONNELL DOUGLAS	MD-11	MD11	43000	31837	Н
MD81	equiv.	MCDONNELL DOUGLAS	MD-81	MD82	37000	34448	М
MD82	direct	MCDONNELL DOUGLAS	MD-82	MD82	37000	34448	М
MD83	direct	MCDONNELL DOUGLAS	MD-83	MD83	37000	33513	М
MD87	equiv.	MCDONNELL DOUGLAS	MD-87	MD82	37000	34448	М
MD88	equiv.	MCDONNELL DOUGLAS	MD-88	MD82	37000	34448	М
MD90	equiv.	MCDONNELL DOUGLAS	MD-90	MD83	37000	33513	М
MG21	equiv.	MIKOYAN	MIG-21	FGTN	50000		М
MG23	equiv.	MIKOYAN	MIG-23	FGTN	50000		М
MG25	equiv.	MIKOYAN	MIG-25	FGTN	50000		М
MG29	equiv.	MIKOYAN	MIG-29	FGTN	50000		М
MIR2	equiv.	DASSAULT	MIRAGE 2000	FGTN	50000		М
MIR4	equiv.	DASSAULT	MIRAGE IV	FGTN	50000		М
MRF1	equiv.	DASSAULT	MIRAGE F1	FGTN	50000		М
MU2	direct	MITSUBISHI	MARQUISE / SOLITAIRE	MU2	28000		L
MU30	equiv.	MITSUBISHI	MU-300	C560	45000	41516	М
N262	equiv.	NORD	262	JS41	26000	24685	М
NIM	equiv.	HAWKER SIDDELEY	NIMROD	B738	41000	34982	М
NM5	equiv.	NAL	NM-5	TRIN	25000		L
NNJA	equiv.	BEST OFF	NYNJA	P28A	12000		L
ONEX	equiv.	SONEW	ONEX	DA42	18000		L
P180	direct	PIAGGIO	P180 AVANTI	P180	41000		L
P210	equiv.	CESSNA	P210	BE58	25000		L
P28A	direct	PIPER	PA-28-140 CHEROKEE	P28A	12000		L



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
P28B	equiv.	PIPER	PA-28-236 DAKOTA	SR22	17500		L
P28R	equiv.	PIPER	PA-28R-201 ARROW	DA42	18000		L
P28T	equiv.	PIPER	PA-28RT TURBO ARROW 4	DA42	18000		L
P3	equiv.	LOCKHEED	ORION P-3	C130	32000	21891	М
P32R	equiv.	PIPER	PA-32R-301 SARATOGA SP	C182	20000		L
P32T	equiv.	PIPER	TURBO LANCE 2	TRIN	25000		L
P46T	equiv.	PIPER	Malibu Meridian	BE9L	31000		L
P68	equiv.	PARTENAVIA	P-68 Observer	PA27	20000		L
P68T	equiv.	PARTENAVIA	AP-68-TP-300 SPARTACUS	D228	28000		L
PA18	equiv.	PIPER	PA-18 SUPER CUB	PA34	25000	22500	L
PA23	equiv.	PIPER	APACHE PA23- 150/160	PA27	20000		L
PA27	direct	PIPER	AZTEC PA23- 235/250	PA27	20000		L
PA30	equiv.	PIPER	Twin Comanche	TRIN	25000		L
PA31	direct	PIPER	CHIEFTAIN	PA31	26300		L
PA32	equiv.	PIPER	PA-32 CHEROKEE SIX	TRIN	25000		L
PA34	direct	PIPER	PA-34-220T SENECA III	PA34	25000	22500	L
PA44	equiv.	PIPER	PA-44 SEMINOLE	DA42	18000		L
PA46	equiv.	PIPER	Malibu	BE58	25000		L
PA47	equiv.	PIPER	PA-47	C510	41000		L
PAY1	equiv.	PIPER	PA-A-31T1-500 CHEYENNE I	PAY2	29000		L
PAY2	direct	PIPER	PA-31T-620 CHEYENNE II	PAY2	29000		L
PAY3	direct	PIPER	PA-42-720 CHEYENNE III	PAY3	33000		L
PAY4	equiv.	PIPER	PA-42-1000 CHEYENNE 400	P180	41000		L
PC12	equiv.	PILATUS	PC-12 SPECTRE	BE9L	31000		L
PC6T	equiv.	PILATUS	PC-6C TURBO- PORTER	D228	28000		L
PC9	equiv.	PILATUS	PC-9	BE9L	31000		L



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
PRM1	equiv.	HAWKER BEECHCRAFT	390 Premier 1	C560	45000	41516	М
PRXT	equiv.	PRIVATE EXPLORER	T-EXPLORER	PA34	25000	22500	L
R722	equiv.	BOEING	727-200RE SUPER 27	B722	37000	33845	М
RFAL	equiv.	DASSAULT	RAFALE	FGTN	50000		М
RJ1H	direct	BAE	RJ-100 Avroliner	RJ1H	35000	30949	М
RJ70	equiv.	BAE	RJ-70 Avroliner	RJ85	35000	32166	М
RJ85	direct	BAE	RJ-85 Avroliner	RJ85	35000	32166	М
S601	equiv.	AEROSPATIAL	SB 601 CORVETTE	C550	43000		L
SB05	equiv.	SAAB	SAAB 105	C510	41000		L
SB20	direct	SAAB	SAAB 2000	SB20	31000		М
SB32	equiv.	SAAB	LANSEN	FGTN	50000		М
SB35	equiv.	SAAB	DRAKEN	FGTN	50000		М
SB37	equiv.	SAAB	VIGGEN	FGTN	50000		М
SB39	equiv.	SAAB	GRIPEN	FGTN	50000		М
SBR1	equiv.	ROCKWELL	SABRELINER	FA10	45000	38400	М
SD4	equiv.	TOMARK	VIPER	P28A	12000		L
SF34	direct	SAAB	SF 340	SF34	25000	25000	М
SH33	equiv.	SHORTS	SH3-330	SH36	20000		М
SH36	direct	SHORTS	SH3-360	SH36	20000		М
SHRK	equiv.	SHARK AERO	SHARK	TRIN	25000		L
SLK3	equiv.	SLICK	360	PA27	20000		L
SLK5	equiv.	SLICK	540	TRIN	25000		L
SNTA	equiv.	AIRSPORT	SONATA	P28A	12000		L
SORA	equiv.	ACS	100 SORA	P28A	12000		L
SR01	equiv.	EURODISPLAY	SR-01 MAGIC	DA42	18000		L
SR20	equiv.	CIRRUS	SR-20	SR22	17500		L
SR22	direct	CIRRUS	SR-22	SR22	17500		L
SW18	equiv.	SKYWOOD	TEDDY SW18	P28A	12000		L
SW2	equiv.	SWEARINGEN	MERLIN II	SW4	25000	25000	L
SW3	equiv.	SWEARINGEN	MERLIN III	PAY3	33000		L
SW4	direct	SWEARINGEN	MERLIN IV	SW4	25000	25000	L



A/C Code	Model Type	Aircraft manufacturer	Aircraft model	Synonym aircraft	h _{MO} [ft]	h _{max} [ft]	WTC
T10	equiv.	TNM-AVIA	T10 AVIA TOR	P28A	12000		L
T134	direct	TUPOLEV	TU134A-3	T134	39000	34764	М
T154	direct	TUPOLEV	TU154M	T154	41000	37285	М
T160	equiv.	TUPOLEV	TU160	B742	45000	33180	Н
T204	equiv.	TUPOLEV	TU 204	T154	41000	37285	М
T50S	equiv.	SUKHOI	T-50 PAKFA	FGTN	50000		М
TB30	equiv.	SOCATA	EPSILON TB30	PA27	20000		L
ТВМ7	direct	SOCATA	TBM-700	TBM7	31000		L
TBM8	direct	SOCATA	TBM-850	TBM8	31000		L
TEX2	equiv.	HAWKER BEECHCRAFT	T-6 TEXAN 2	TBM7	31000		L
TOBA	equiv.	SOCATA	TOBAGO TB-10	C172	14000		L
TOR	equiv.	PANAVIA	TORNADO	FGTN	50000		М
TRIN	direct	SOCATA	TRINIDAD TB-20	TRIN	25000		L
TRIS	equiv.	BRITTEN- NORMAN	Trislander	DA42	18000		L
TUCA	equiv.	EMBRAER	TUCANO	BE9L	31000		L
VC10	equiv.	VICKERS	VC10	B762	43000	35861	Н
WSP	equiv.	AAK	WASP	P28A	12000		L
WW24	equiv.	IAI	1124 WESTWIND	FA10	45000	38400	М
YK40	equiv.	YAKOLEV	YAK-40	E120	32000		М
YK42	equiv.	YAKOLEV	YAK-42	DC94	35000	33500	М



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APPENDIX B

SOLUTIONS FOR BUFFETING LIMIT ALGORITHM



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A general solution for finding the roots of a cubic expression can be found in [RD15]. If we take expression 3.6-6, we can rewrite it to:

$$M^{3} - \frac{C_{Lbo(M=0)}}{k} \cdot M^{2} + \frac{\frac{W}{S}}{0.583 \cdot P \cdot k} = 0$$

Let:

$$a_1 = -\frac{C_{Lbo(M=0)}}{k}$$

$$a_2 = 0$$

$$a_3 = \frac{\frac{W}{S}}{0.583 \cdot P \cdot k}$$

Now let:

$$Q = \frac{\left(3 \cdot a_2 - a_1^2\right)}{9}$$

and:

$$R = \frac{\left(9 \cdot a_1 \cdot a_2 - 27 \cdot a_3 - 2 \cdot a_1^3\right)}{54}$$

The discriminant D is equal to: $Q^3 + R^2$. In our case D is usually strictly negative, which means that all roots are unequal and real. A simplified computation method with the help of trigonometry is given below:

$$X_1 = 2 \cdot \sqrt{-Q} \cdot \cos\left(\frac{\theta}{3}\right) - \frac{a_1}{3}$$

$$X_2 = 2 \cdot \sqrt{-Q} \cdot \cos\left(\frac{\theta}{3} + 120^{\circ}\right) - \frac{a_1}{3}$$

$$X_3 = 2 \cdot \sqrt{-Q} \cdot \cos\left(\frac{\theta}{3} + 240^{\circ}\right) - \frac{a_1}{3}$$
With: $\cos\theta = \frac{R}{\sqrt{-Q^3}}$

The solutions X_1 , X_2 and X_3 now give the possible values of M. One solution (in our case usually X_1) is always negative. The others are positive with the lower one (usually X_2) being the low speed buffeting limit we are looking for.



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