

# Design project - SIE 2025



# Development of a Predictive Tool for the Leaching of Pollutants in Construction Material Deposits

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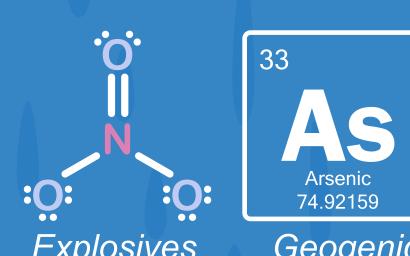
#### Context

Environmental risks associated with the leaching of contaminants from solid excavation waste, particularly from tunnel construction activities, such as the excavation of *Gotthard Road Tunnel*, used as a *theoretical case study*.

• Leaching of pollutants due to water infiltration could lead to contamination of

surface and groundwater,

## **Considered Contaminants**



Precipitation data

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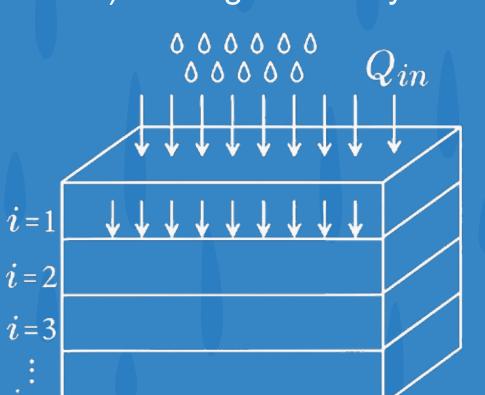
Material properties

#### Regulamentary framework:

- Excavated material must meet ADWO<sup>[1]</sup> limits to be reused, otherwise it goes to Type B-D landfills,
- Landfills must collect, monitor, and treat leachate regularly,
- Leachate discharge is allowed only if it meets legal standards<sup>[2]</sup>.

#### **Goal & Assumptions**

**Goal**: develop a predicitive model for the leaching of inorganic contaminants from excavation material deposits. Particular attention to low solubility contaminants (Arsenic) and high solubility ones (Nitrate).



#### **Assumptions:**

- 1. Water movement within the deposit is considered one-dimensional and vertical,
- 2. The initial concentration of pollutants in the solid phase is assumed to be constant and
- homogeneous throughout the deposit, 3. Pollutants do not undergo any physicochemical transformations

#### Methods

# Infiltration model - Green&Ampt [3]

#### Parameters:

 $K_s$  hydraulic conductivity,  $\psi$  suction,  $\theta_d = \theta_s - \theta_i$  moisture deficit,  $\theta_s$ saturated water content, θ<sub>i</sub> initial water content.

#### **Potential infiltration rate:**

$$f_* = K_s(1+rac{\Psi heta_d}{F})$$
Actual infiltration rate:  $f = min(f^*,R)$ 

 $F(t) = \int_0^t f(t) \; d au \qquad Z = rac{F(t)}{ heta_d} \; .$ 

→ Newton's method to obtain F(t)

**OUTPUTS**: t, f(t),  $f^*(t)$ , F(t) and z(t)



Total deposit Timestep height

#### **Discretization**

 Time-step corresponds to water residence time in one layer

Height of each layer

 Linear interpolation of Green & Ampt outputs

## OUTPUTS:



# of layers

# Diffusion model [4]

Contaminant properties

Release of contaminants governed by diffusion processes, described using Fick's Second Law

Cumulative mass of the costituent released in layer i:

$$M_{ ext{mass}}^{i=1} = 2 \cdot C_0 \cdot rac{S}{V} \cdot \left(rac{D^{ ext{obs}} \cdot t_{i=1}}{\pi}
ight)^{1/2} \left[mg/kg
ight]$$

→ Conversion to aqueous concentration by dividing by WS (water-to-solid ratio)

Linear sorption model to describe equilibrium conditions:

$$C_{aq,eq,i} = rac{(C_0 - M_{\mathrm{mass}}^i)}{k_D} \ [mg/L]$$

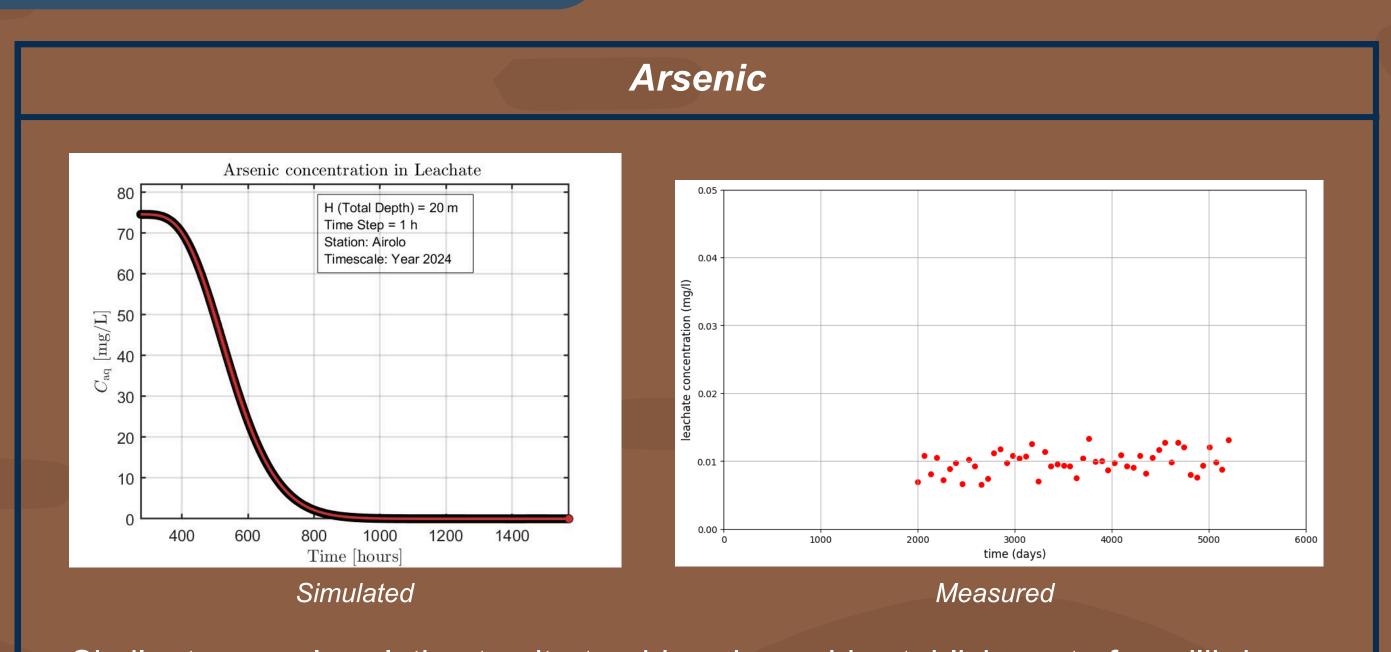
**OUTPUT Concentration of** contaminant in leachate [mg/L]



## **Results and Discussion**

#### **Nitrate** Nitrate concentration in Leachate H (Total Depth) = 20 m Timescale: Year 2024 1500 1000 800 1000 1200 time (days) Time [hours] Simulated Measured

- Concentration decreases over time due to pollutant depletion in the solid phase
  Higher peak concentration observed,
  Simulated results match measured data in magnitude and decline trend,
  Faster simulated decline due to instantaneous sorption model and overestimated
- infiltration depth.



- Similar temporal evolution to nitrate, driven by rapid establishment of equilibrium conditions,
- Significant discrepancies with measured data,
  Improvements include surface complexation modeling and incorporation of pollutant speciation.

## Sensitivity analysis

# Variation of precipitation input (different altitudes): Rapid attainment of thermodynamic equilibrium overrides the influence of precipitation on final concentrations.

 Precipitation affects only the diffusion process, not the time required to reach equilibrium.

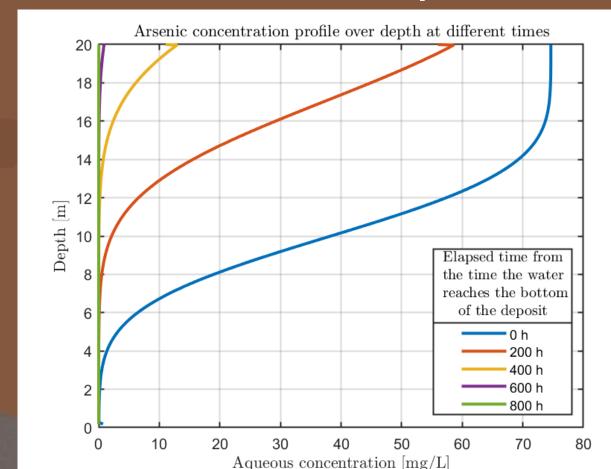
## Variation of time-step (tr):

Larger time-steps result in slower concentration decay and less precise pollutant dynamics,
Smaller tr values yield sharper and more realistic concentration curves.

## Variation of deposit height (H):

Increasing deposit height delays and prolongs contaminant release (slower vertical perticolation),
Peak leachate concentrations remain similar across all heights (rapid solid-liquid equilibrium).

## Vertical concentration profiles



Top layers quickly flush out,Contaminant fronts shift downward with time. Maximal concentrations remain near the bottom until full rinsing (~800 h).

# Conclusion

- The model highlights general trends in contaminant leaching but lacks precision The model highlights general trends in contaminant leaching but lacks precision due to oversimplified starting hypotheses: chemical transformations, kinetic sorption processes and environmental variables were excluded,
  Diffusion is the only controlling mechanism, which leads to a rapid attainment of equilibrium for both pollutants. Major limitation for low solubility contaminants,
  Sensitivity analyses confirm the model's strong dependence on timestep and
- deposit height.
- →The current model is a conceptual prototype and its predictive reliability is low without further refinement,
- →Future development prospectives: Arsenic phisico-chemical parametrisation, time-lagged sorption model, time-scale adjustments, more realistic deposit shape, multidirectional flow.

## References

[1] SR 814.600, Waste Ordinance (2015), [online]

[2] SR 814.201, Waters Protection Ordinance (1998), [online] [3] L. W. Mays, "Water resources engineering", 2nd Edition, 2010.

[4] Kosson et al., Environ. Eng. Sci., 19, 2002. DOI: 10.1089/109287502760079188

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