3D1 Geotech Engineering: Soil Classification Lab Report

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Summary

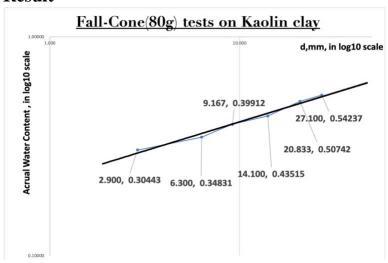
The aim of this experiment is to conduct standardised BS 1377-2:1990 liquid limit and plastic limit on Bentonite clay and Kaolinite clay; and thereby to classify those two types of cohesive soils in terms of the water contents they hold at the limits of their range of plastic behaviour. And from those investigations to determine the basic characteristics of Bentonite and Kaolinite.

Background

Plastic limit W_P , liquid limit W_L (Atterberg limits), are basic measures of the critical water contents of a fine-grained soil (clays and silts). Clays and silts interact with water and thus change sizes and having varying shear strength. And therefore, laboratory tests on W_P and W_L are important in preliminary design stages of any structure to ensure the soil have required engineering properties; such Atterberg limits are also used to distinguish between silt and clay, and between different types of silts and clays.

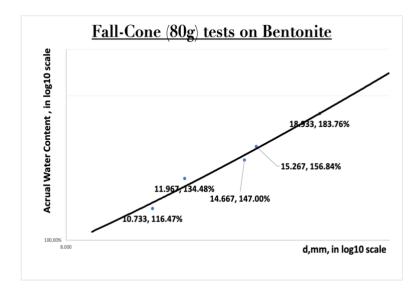
Batches of Bentonite clays of nominal water contents 110,125,140, 155 and 170% and Kaolinite clay of water contents 35, 40, 45, 50 and 55% are tested for liquid limit W_L with BS 1377-2:1990 standardised cone penetrometer; with Kaolinite clay of water contents \boldsymbol{w} of 35, 40 and 45% also tested by non-standard 240g cone.

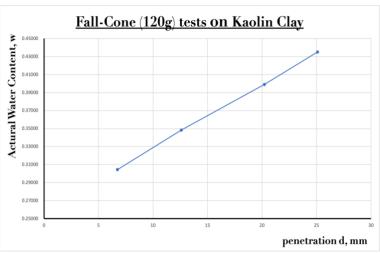
Result



By calculating the corresponding water contents w at penetration d=20mm on the trendline:

 $W_{L,\text{Kaolinite}} = 0.4913$ $W_{L,\text{Bentonite}} = 1.9212$





By averaging actual water contents w of 5 Bentonite samples and 4 Kaolin samples, it resulted:

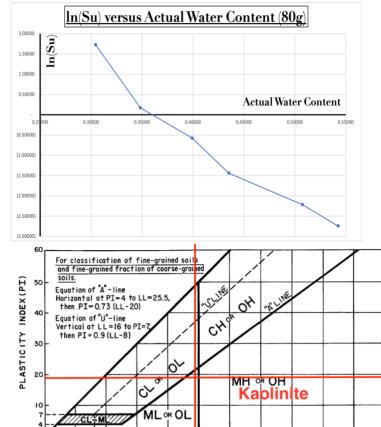
 $W_{P.\text{Kaolinite}} = 29.99\%$

 $W_{P,\text{Bentonite}} = 44.38\%$

Plasticity index, $I_P = W_L - W_P$

 $I_{P,\text{Kaolinite}} = 0.1914$

 $I_{P,\text{Bentonite}} = 1.4774$



LIQUID LIMIT (LL)

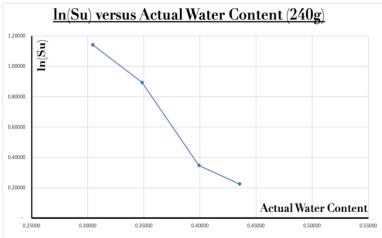
L = Low Plasticity

H = High Plasticity

I = Intermediate Plasticity

V = Very High Plasticity

E = Extremely High Plasticity



It can be plotted on the graph that Kaolinite is below the "A" Line

 $(I_{P,\text{Kaolinite}}19.14 < 21.26)$, and therefore Kaolinite is classified as ML (Low Plasticity Silt).

Bentonite is not within the range of the graph, but it can be calculated (165.71> $I_{P,\text{Bentonite}}$ 147.74>125.65) that, Bentonite is in between the "A" Line and the "U" Line, therefore Bentonite is classified as CH (High Plasticity Clay).

Undrained shear strength Su, of the clay is potentially 1 at the liquid limit.

Discussion

C = Clav

M = Silt

O = Organic

Atterberg limit tests can be used as a guideline to indicate the likelihood of a ground base to consolidate (ground settlement) when under load. For example, if the soil water content is

 $w_{LL} < 35\%$

w_{LL} > 90%

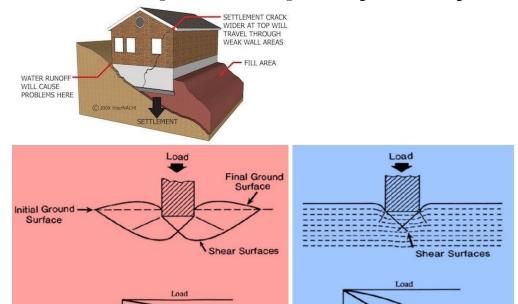
 $35\% \le W_{LL} \le 50\%$

 $50\% \le W_{LL} \le 90\%$

 $70\% \le w_{LL} \le 90\%$

close to its Liquid Limit W_L around an excavated space (such as for tunnels, basements or shafts), a lot of ground settlement (downward movement of the ground) can be expected if a structure is built above; and for soil with water content close to its Plastic Limit W_P the opposite is true.

Therefore, we can recognise a weak bearing soil through the Atterberg limit tests.



A general shear failure (Left, red) occurs for soils that are in a dense or hard state. (e.g., a heavily compacted clay with water content w below plastic limit I_P , therefore is brittle) A punching shear failure (Right, blue) occurs for soils that are in a loose or soft state. (e.g., a highly plastic clay with high water content w close to its liquid limit I_L)

Settlemen

Atterberg limits aren't suitable for natural clayey soils which contain modest proportions of coarse sand and gravel. Because cohesionless (free-running type) coarse soils such as gravel and sands are classified by particle size analysis by using a nest of sieves. (coarse sand and gravel solids do not stick together, whose strength mainly depends on friction between solid particles)

Appendix

Water content	S									Fall cone	80g			Fall cone 240			
Caolin	+						i								-		
nominal wc	Container	Empty weight We	Weight with wet soil	Weight with dry soil	evaporated water weight	Actual Water Content	t In(Su) (80g)	In(Su) (240g)	penetra	penetratio	ation in mm						
Powder									test no	1	1 2	3	avg	1	2	3	avg
309	% b8	2.6	28.78	22.67	6.11	0.30443	1.72788	1.14177		2.7	2.8	3.2	2.900	6.9	6.7	6.6	6.73333
359	% G2	2.61	3.81	3.5	0.31	0.34831	0.17620	0.89451		(6.3	6.6	6.300	12.3	12.5	13	12
405	% G7	2.59	5.78	4.87	0.91	0.39912	(0.57385)	0.34689		9.8	8.2	9.5	9.167	20.2	19.8	20.7	20.2333
455	% C7	2.6	9.46	7.38	2.08	0.43515	(1.43505)	0.22541		15.2	14.3	12.8	14.100	25.2	24.8	25.3	25.
50	% G5	2.61	7.69	5.98	1.71	0.50742	(2.21581)			19.5	20.6	22.4	20.833				
555	% D4	2.59	18.97	13.21	5.76	0.54237	(2.74177			30	26.2	25.1	27.100				
605	%																
655	%																
Bentonite																	
nominal w.c.	Container	Empty weight We	eight with wet soil	Weight with dry soil	actual water content												
Powder																	
	0 B6	2.59	4.43							10.8			10.733				
	5 A8	2.62	4.66							12.2			11.967				
	0 C1	2.59	10.42							14.9		14.7					
	5 H1	2.61	7.49							16.2			15.267				
	0 B4	2.61	8.69		#VALUE!	#VALUE!				17.2			16.933				
18	0 E3	2.6	5.92	3.77	2.15	183.76%				19.6	18.4	18.8	18.933	_		_	
Bentonite PL s	amples																
	1 C8	2.61	5.69	4.74	0.95	44.60%											
	2 G9	2.62	4.52	3.92	0.6	46.15%											
	3 D7	2.66	3.89	3.51	0.38	44.71%				1							
	4 C6	2.6	5.06	4.28	0.78	46.43%											
	5 H7	2.6	5.35	?	#VALUE!	#VALUE!											
	6 A7	2.59	4.13	3.69	0.44	40.00%											
Caolin PL samp	les																
	1 D1	2.58	5.46	4.81	0.65	29.15%											
	2 H9	2.62	4.73	4.24	0.49	30.25%											
	3 E1	2.6	8.33	6.99	1.34	30.52%											
	4 D2	2.67	5.05														