

A Assignment

Questions Theory & Assignment

For the evaluation, please hand in by 08/11/2024:

- Your response to the theory questions below
- A summary of your solution of the assignment, with some plots
- The source code of your solution

All that on about 2..3 pages only, keep it compact!

Questions Theory:

1. Write down the conservation law for the angular momentum ru_φ . What are the source and sink terms?
2. Choose a control volume containing the rotor disk, and write down the integral form of the conservation equation.
3. Assume a constant angular velocity Ω inside the wake deficit region of the Jensen/Frandsen wake model $0 \leq r \leq D_W(x)$ (no rotation for $r > D_W(x)$), with $u_\varphi = \Omega r$. Derive the formula for $\Omega(x)$ from the integral form using $D_W(x)$ as a radius of the control volume.

Assignment: Aerodynamic forcing of the fore-aft bending of a wind turbine due to turbulence

The total thrust force on a wind turbine rotor moving with velocity $\dot{x}(t)$ can be approximated using the thrust coefficient:

$$\begin{aligned} F_{Thrust}(t) &= C_t \frac{\rho}{2} (u_{Wind} - \dot{x}(t))^2 A_{Rotor} \\ &= C_t \frac{\rho}{2} \int_0^{2\pi} \int_0^R (u_{Wind} - \dot{x}(t))^2 r dr d\varphi \end{aligned}$$

Filling in an environmental model for the wind speed based on a shear profile and a turbulence model with linearized transport

$$u_{Wind}(x, y, z, t) = U_{Shear}(z) + u_{Turb}(x - Ut, y, z)$$

What value should you use for C_t ? According to Blade Element – Momentum Theory, the relationship to the axial induction factor is

$$C_t = 4(1 - a)a$$

Assignment: Aerodynamic forcing of the fore-aft bending of a wind turbine due to turbulence

Thrust coefficient

$$C_t = \frac{F_{Thrust}}{\frac{\rho}{2} U_{\infty}^2 A_{Rotor}}$$

The following terms are obtained:

$$\begin{aligned} F_{Thrust}(t) &= C_t \frac{\rho}{2} \left[\int_0^{2\pi} \int_0^R U_{Shear}^2 r dr d\varphi + \int_0^{2\pi} \int_0^R u_{Turb}^2 r dr d\varphi + \dot{x}^2 A_{Rotor} \right. \\ &\quad - 2\dot{x} \int_0^{2\pi} \int_0^R U_{Shear} r dr d\varphi - 2\dot{x} \int_0^{2\pi} \int_0^R u_{Turb} r dr d\varphi \\ &\quad \left. + 2 \int_0^{2\pi} \int_0^R U_{Shear} u_{Turb} r dr d\varphi \right] \end{aligned}$$

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Analysing the terms:

- $\int_0^{2\pi} \int_0^R u_{Turb} r dr d\varphi = 0$ should average out to zero → to confirm!
- $\dot{x}^2 A_{Rotor}$ is a non-linear term → neglected to linearise the problem, to confirm!
- $C_t \rho \dot{x} \int_0^{2\pi} \int_0^R U_{Shear} r dr d\varphi$ is linear in \dot{x} , therefore

$$\gamma = C_t \rho \int_0^{2\pi} \int_0^R U_{Shear} r dr d\varphi$$

acts as a damping constant to the motion

That leaves for the forcing of the tower vibrations:

$$F_{RHS}(t) = C_t \frac{\rho}{2} \int_0^{2\pi} \int_0^R (U_{Shear} + u_{Turb})^2 r dr d\varphi$$

Assignment: Aerodynamic forcing of the fore-aft bending of a wind turbine due to turbulence

Coordinate transform:

$$x = x$$

$$y = r \cos \varphi$$

$$z = z_{Hub} + r \sin \varphi$$

$$r = \sqrt{y^2 + (z - z_{Hub})^2}$$

$$\varphi = \arctan \frac{z - z_{Hub}}{y}$$

Model parameters:

- Hub height z_{Hub} , in m
- Mass of the RNA M (Rotor-Nacelle Assembly), in kg
- Spring constant of the tower K , in N/m=kg/s²

Eigenfrequency of the tower:

$$f = \sqrt{\frac{M}{K}}$$

2nd order dynamic system of the nacelle motion:

$$M\ddot{x}(t) + \gamma\dot{x}(t) + Kx(t) = F_{RHS}(t)$$

with:

- Damping constant $\gamma = C_t \rho \int_0^{2\pi} \int_0^R U_{Shear} r dr d\varphi$
- Forcing/excitation

$$F_{RHS}(t) = C_t \frac{\rho}{2} \int_0^{2\pi} \int_0^R (U_{Shear} + u_{Turb})^2 r dr d\varphi$$

Assignment: Aerodynamic forcing of the fore-aft bending of a wind turbine due to turbulence

Programming tasks:

- Write a function for $U_{Shear}(z)$ (power law or log law, your choice)
- Implement the isotropic Mann model according to the Matlab example, to compute all three velocity components of $u_{Turb}(x, y, z)$, $v_{Turb}(x, y, z)$ and $w_{Turb}(x, y, z)$
- Write a function that approximates the integral numerically by a sum:

$$\int_0^{2\pi} \int_0^R f(r, \varphi) r dr d\varphi \cong \sum_{n=1}^N w_n f(r_n, \varphi_n)$$

- The quadrature nodes \tilde{r}_n and as well as the quadrature weights \tilde{w}_n are given to you as a table for a unit disk ($R = 1$), the scaled nodes and weights for any rotor radius R are obtained by scaling $r_n = R\tilde{r}_n$ and $w_n = R^2\tilde{w}_n$, also write a function for that and the transform to cartesian coordinates!
- Write a function that interpolates u_{Turb} at arbitrary x, y, z

Assignment: Aerodynamic forcing of the fore-aft bending of a wind turbine due to turbulence

Spatial resolution turbulent velocity component:

$$\Delta x = \frac{6000\text{m}}{8192} = 0.7324\text{m}$$

$$\Delta y = \Delta z = \frac{384\text{m}}{64} = 6\text{m}$$

Preparational tasks:

- Assume a transport velocity of $U = 10 \frac{\text{m}}{\text{s}}$, and generate u_{Turb} for a grid $L_x = 600\text{s} * 10 \frac{\text{m}}{\text{s}} = 6000\text{m}$ long, $L_y = L_z = 384\text{m}$ wide and high; the turbulence field should be centered around $y = 0$ and $z = 192\text{m}$ (shifted $L_z/2$ upwards) to fully cover the rotor disk
- Use an integral length scale of $L = 35.4\text{m}$ as a parameter for the von Kármán spectral tensor
- Use $N_x = 8192$ and $N_y = N_z = 64$ or $N_y = N_z = 128$ (the latter only if the amount of memory in your computer is large enough)

Using this wind field, you now have data for 8192 time steps spaced by $\Delta t = \frac{6000\text{m}}{8192 \cdot 10 \frac{\text{m}}{\text{s}}} = 0.07324\text{s}$, for which you can integrate the forcing term $F_{Thrust}(t)$ per time step, the damping constant γ does not depend on time

Assignment: Aerodynamic forcing of the fore-aft bending of a wind turbine due to turbulence

100m rotor:

- $z_{Hub} = 100\text{m}$
- $M = 1.4 \cdot 10^5 \text{kg}$
- $K = 2.5 \cdot 10^6 \frac{\text{kg}}{\text{s}^2}$

200m rotor:

- $z_{Hub} = 150\text{m}$
- $M = 6.5 \cdot 10^5 \text{kg}$
- $K = 2.0 \cdot 10^6 \frac{\text{kg}}{\text{s}^2}$

300m rotor:

- $z_{Hub} = 200\text{m}$
- $M = 1.9 \cdot 10^6 \text{kg}$
- $K = 1.8 \cdot 10^6 \frac{\text{kg}}{\text{s}^2}$

From previous steps:

- Compute the forcing time series $F_{RHS}(t)$ at all 8192 time steps for a given rotor radius R
- Compute the damping constant γ for a given rotor radius R and hub height z_{Hub}

Solve the 2nd order dynamical system:

- Fourier-transform the equation

$$-\omega^2 M \hat{x}(\omega) + i\omega\gamma \hat{x}(\omega) + K \hat{x}(\omega) = \hat{f}(\omega)$$

- Solve the system in Fourier space

$$\hat{x}(\omega) = \frac{1}{-\omega^2 M + i\omega\gamma + K} \hat{f}(\omega)$$

- Apply the inverse Fourier transform to obtain $x(t)$ for a given set of parameters (you might get very a small imaginary part due to numerical errors in the Fourier transform)
- Check that the two terms that were neglected are indeed small!

Assignment: Aerodynamic forcing of the fore-aft bending of a wind turbine due to turbulence

Try to answer the following questions:

- Plot the three power spectral densities; how does the fore-aft movement change when moving to larger rotors?
- Plot the three motion time series; what can you say about amplitudes and oscillations of the time series?
- Compute the time series of the bending moments at the tower bottom

Quadrature over the Unit Disk, 57 nodes

| weight w | y | z | r | phi |
|-------------------|--------------------|--------------------|-------------------|--------------------|
| 0.114983341799986 | 0 | 0 | 0 | 0 |
| 0.042666281539387 | -0.886967663163937 | 0 | 0.886967663163937 | 3.141592653589793 |
| 0.042666281539387 | 0 | -0.886967663163937 | 0.886967663163937 | -1.570796326794897 |
| 0.042666281539387 | 0 | 0.886967663163937 | 0.886967663163937 | 1.570796326794897 |
| 0.042666281539387 | 0.886967663163937 | 0 | 0.886967663163937 | 0 |
| 0.087938325357146 | -0.424633903743234 | 0 | 0.424633903743234 | 3.141592653589793 |
| 0.087938325357146 | 0 | -0.424633903743234 | 0.424633903743234 | -1.570796326794897 |
| 0.087938325357146 | 0 | 0.424633903743234 | 0.424633903743234 | 1.570796326794897 |
| 0.087938325357146 | 0.424633903743234 | 0 | 0.424633903743234 | 0 |
| 0.076206570461793 | -0.694469023080834 | 0 | 0.694469023080834 | 3.141592653589793 |
| 0.076206570461793 | 0 | -0.694469023080834 | 0.694469023080834 | -1.570796326794897 |
| 0.076206570461793 | 0 | 0.694469023080834 | 0.694469023080834 | 1.570796326794897 |
| 0.076206570461793 | 0.694469023080834 | 0 | 0.694469023080834 | 0 |
| 0.019156522218856 | -0.687853540826993 | -0.687853540826993 | 0.972771806363888 | -2.356194490192345 |
| 0.019156522218856 | -0.687853540826993 | 0.687853540826993 | 0.972771806363888 | 2.356194490192345 |
| 0.019156522218856 | 0.687853540826993 | -0.687853540826993 | 0.972771806363888 | -0.785398163397448 |
| 0.019156522218856 | 0.687853540826993 | 0.687853540826993 | 0.972771806363888 | 0.785398163397448 |
| 0.062085722273139 | -0.596647677814557 | -0.596647677814557 | 0.843787237923759 | -2.356194490192345 |
| 0.062085722273139 | -0.596647677814557 | 0.596647677814557 | 0.843787237923759 | 2.356194490192345 |
| 0.062085722273139 | 0.596647677814557 | -0.596647677814557 | 0.843787237923759 | -0.785398163397448 |
| 0.062085722273139 | 0.596647677814557 | 0.596647677814557 | 0.843787237923759 | 0.785398163397448 |
| 0.095664962820418 | -0.235622520915308 | -0.235622520915308 | 0.333220564678967 | -2.356194490192345 |
| 0.095664962820418 | -0.235622520915308 | 0.235622520915308 | 0.333220564678967 | 2.356194490192345 |
| 0.095664962820418 | 0.235622520915308 | -0.235622520915308 | 0.333220564678967 | -0.785398163397448 |
| 0.095664962820418 | 0.235622520915308 | 0.235622520915308 | 0.333220564678967 | 0.785398163397448 |
| 0.085162533604289 | -0.548940255237015 | -0.312947548883440 | 0.631879396856577 | -2.623453175107159 |
| 0.085162533604289 | -0.548940255237015 | 0.312947548883440 | 0.631879396856577 | 2.623453175107159 |
| 0.085162533604289 | -0.312947548883440 | -0.548940255237015 | 0.631879396856577 | -2.088935805277532 |
| 0.085162533604289 | -0.312947548883440 | 0.548940255237015 | 0.631879396856577 | 2.088935805277532 |
| 0.085162533604289 | 0.312947548883440 | -0.548940255237015 | 0.631879396856577 | -1.052656848312262 |
| 0.085162533604289 | 0.312947548883440 | 0.548940255237015 | 0.631879396856577 | 1.052656848312262 |
| 0.085162533604289 | 0.548940255237015 | -0.312947548883440 | 0.631879396856577 | -0.518139478482635 |
| 0.085162533604289 | 0.548940255237015 | 0.312947548883440 | 0.631879396856577 | 0.518139478482635 |
| 0.020201237989565 | -0.961212285046179 | -0.173857450886836 | 0.976808819653347 | -2.962654139766104 |
| 0.020201237989565 | -0.961212285046179 | 0.173857450886836 | 0.976808819653347 | 2.962654139766104 |
| 0.020201237989565 | -0.173857450886836 | -0.961212285046179 | 0.976808819653347 | -1.749734840618586 |
| 0.020201237989565 | -0.173857450886836 | 0.961212285046179 | 0.976808819653347 | 1.749734840618586 |
| 0.020201237989565 | 0.173857450886836 | -0.961212285046179 | 0.976808819653347 | -1.391857812971208 |
| 0.020201237989565 | 0.173857450886836 | 0.961212285046179 | 0.976808819653347 | 1.391857812971208 |
| 0.020201237989565 | 0.961212285046179 | -0.173857450886836 | 0.976808819653347 | -0.178938513823689 |
| 0.020201237989565 | 0.961212285046179 | 0.173857450886836 | 0.976808819653347 | 0.178938513823689 |
| 0.056834571713157 | -0.790354875311486 | -0.305387322252147 | 0.847302924296247 | -2.772871497753526 |
| 0.056834571713157 | -0.790354875311486 | 0.305387322252147 | 0.847302924296247 | 2.772871497753526 |
| 0.056834571713157 | -0.305387322252147 | -0.790354875311486 | 0.847302924296247 | -1.939517482631164 |
| 0.056834571713157 | -0.305387322252147 | 0.790354875311486 | 0.847302924296247 | 1.939517482631164 |
| 0.056834571713157 | 0.305387322252147 | -0.790354875311486 | 0.847302924296247 | -1.202075170958629 |
| 0.056834571713157 | 0.305387322252147 | 0.790354875311486 | 0.847302924296247 | 1.202075170958629 |
| 0.056834571713157 | 0.790354875311486 | -0.305387322252147 | 0.847302924296247 | -0.368721155836267 |
| 0.056834571713157 | 0.790354875311486 | 0.305387322252147 | 0.847302924296247 | 0.368721155836267 |
| 0.024268628331346 | -0.849372904096328 | -0.462700565982938 | 0.967226004599732 | -2.642784840531044 |
| 0.024268628331346 | -0.849372904096328 | 0.462700565982938 | 0.967226004599732 | 2.642784840531044 |
| 0.024268628331346 | -0.462700565982938 | -0.849372904096328 | 0.967226004599732 | -2.069604139853646 |
| 0.024268628331346 | -0.462700565982938 | 0.849372904096328 | 0.967226004599732 | 2.069604139853646 |
| 0.024268628331346 | 0.462700565982938 | -0.849372904096328 | 0.967226004599732 | -1.071988513736147 |
| 0.024268628331346 | 0.462700565982938 | 0.849372904096328 | 0.967226004599732 | 1.071988513736147 |
| 0.024268628331346 | 0.849372904096328 | -0.462700565982938 | 0.967226004599732 | -0.498807813058749 |
| 0.024268628331346 | 0.849372904096328 | 0.462700565982938 | 0.967226004599732 | 0.498807813058749 |

Quadrature over the Unit Disk, 57 nodes

Cools & Kim: *A survey of known and new cubature formulas for the unit disk*. 2000

<https://www.cs.kuleuven.be/publicaties/rapporten/tw/TW300.pdf>

