

PLY-THICKNESS EFFECT ON FIBER-MATRIX INTERFACE CRACK GROWTH

L. Di Stasio^{1,2}, J. Varna¹, Z. Ayadi²

¹Division of Materials Science, Luleå University of Technology, Luleå, Sweden

²EEIGM & IJL, Université de Lorraine, Nancy, France

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Outline

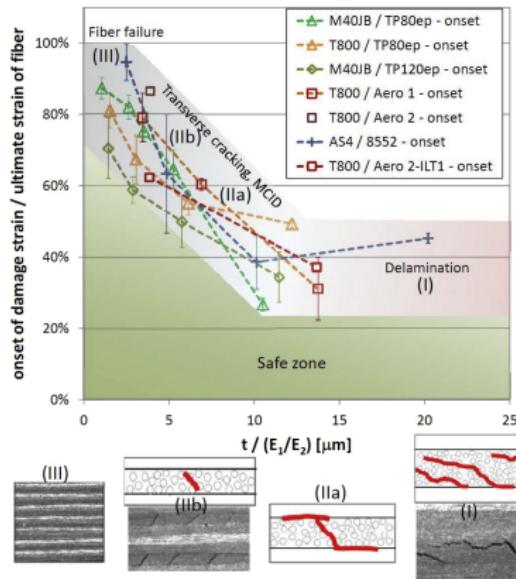
- ➔ Initiation of Transverse Cracks in Thin-plys
- ➔ Modeling the Fiber-Matrix Interface Crack
- ➔ Debond Energy Release Rate
- ➔ Conclusions



INITIATION OF TRANSVERSE CRACKS IN THIN-PLIES

The Thin-ply "Advantage": new material

2018, $[45^\circ, 90^\circ, -45^\circ, 0]$ ns

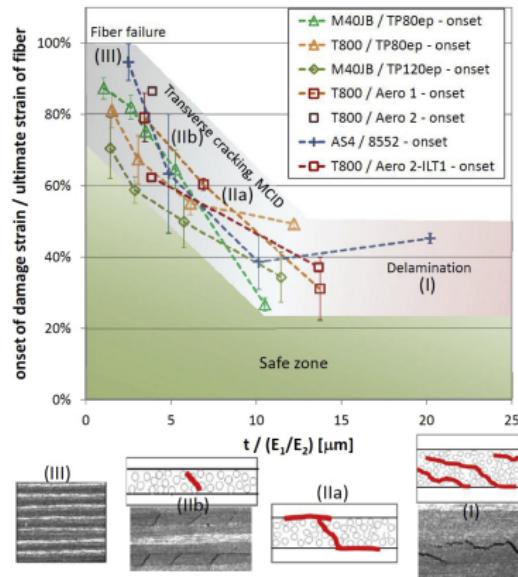


Cugnoni et al., Compos. Sci. Technol. **168**, 2018, p. 467–477.

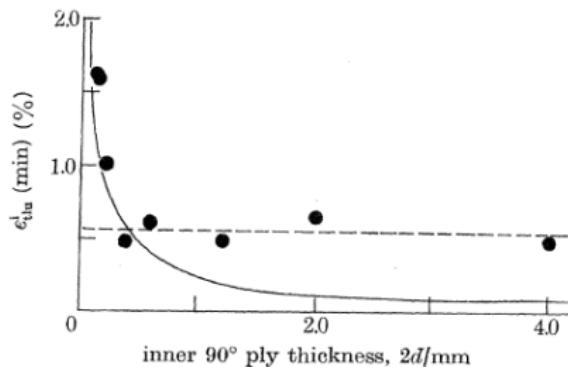
The Thin-ply "Advantage": new material, old result

2018, $[45^\circ, 90^\circ, -45^\circ, 0]_{ns}$

1979, $[0^\circ, 90^\circ]_s$



Cugnoni et al., Compos. Sci. Technol. **168**, 2018, p. 467–477.

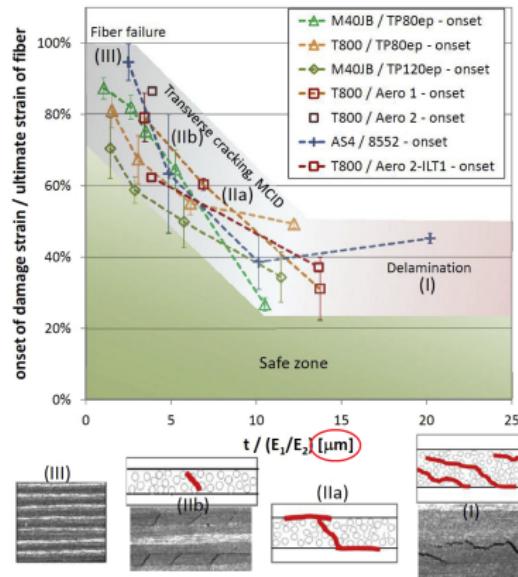


Bailey et al., P. Roy. Soc. A-Math. Phys. **366** (1727), 1979.

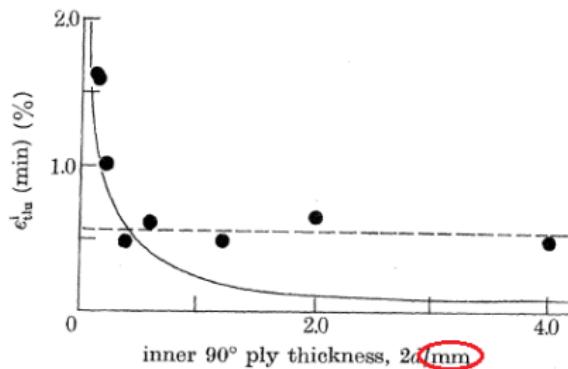
The Thin-ply "Advantage": new material, old result?

2018, $[45^\circ, 90^\circ, -45^\circ, 0^\circ]_{ns}$

1979, $[0^\circ, 90^\circ]_s$

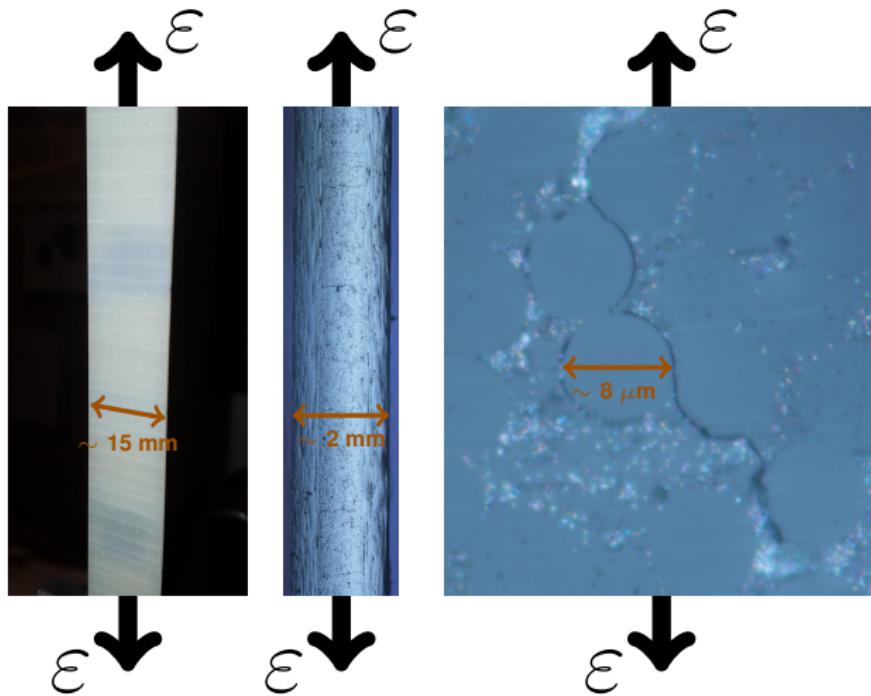


Cugnoni et al., Compos. Sci. Technol. **168**, 2018, p. 467–477.



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Micromechanics of Initiation



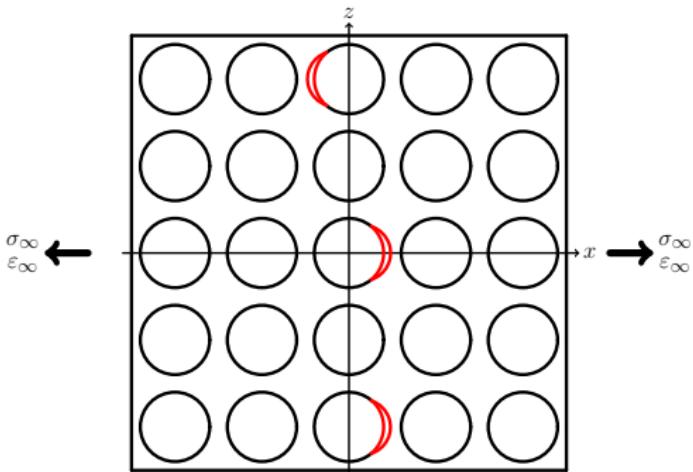
Left:
front view of $[0, 90]_S$,
visual inspection.

Center:
edge view of $[0, 90]_S$,
optical microscope.

Right:
edge view of $[0, 90]_S$,
optical microscope.

Micromechanics of Initiation

Stage 1: isolated debonds



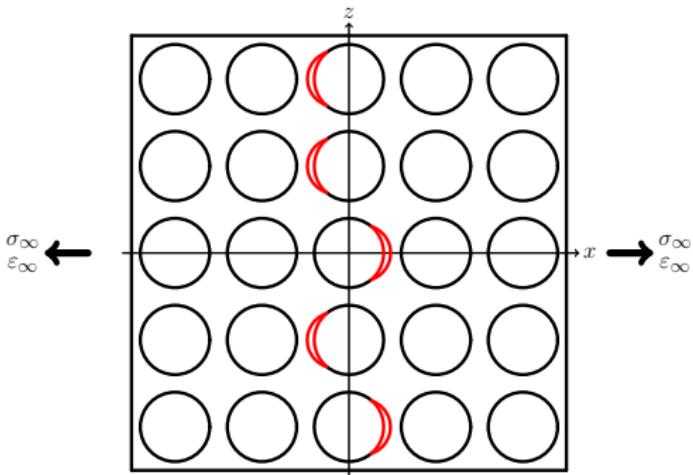
Bailey et al., P. Roy. Soc. A-Math. Phy. **366** (1727), 1979.

Bailey et al., J. Mater. Sci. **16** (3), 1981.

Zhang et al., Compos. Part A-Appl. S. **28** (4), 1997.

Micromechanics of Initiation

Stage 2: consecutive debonds



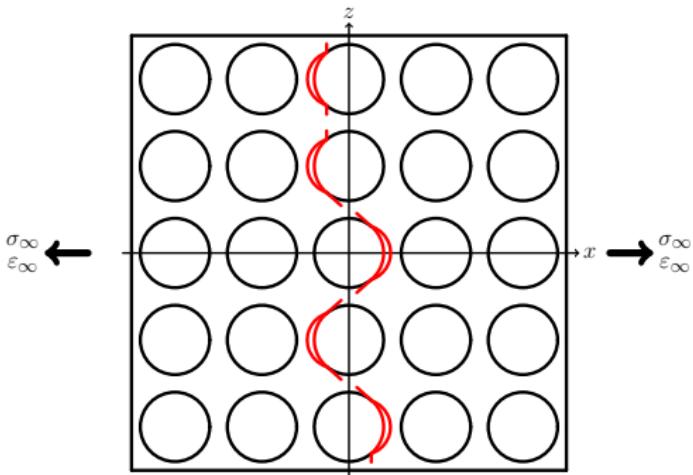
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Micromechanics of Initiation

Stage 3: kinking



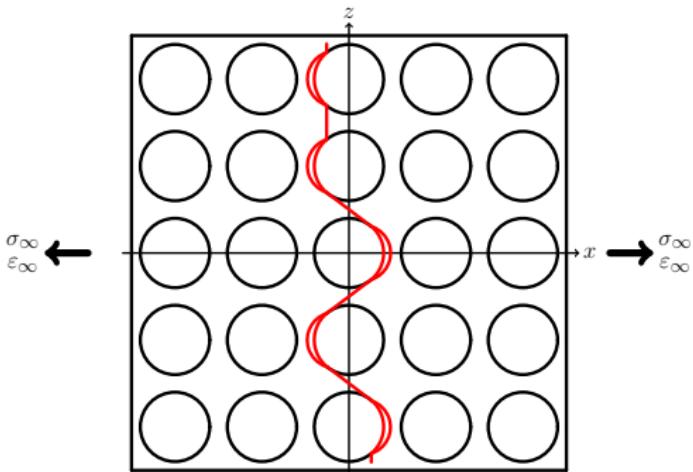
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Zhang et al., Compos. Part A-Appl. S. **28** (4), 1997.

Micromechanics of Initiation

Stage 4: coalescence



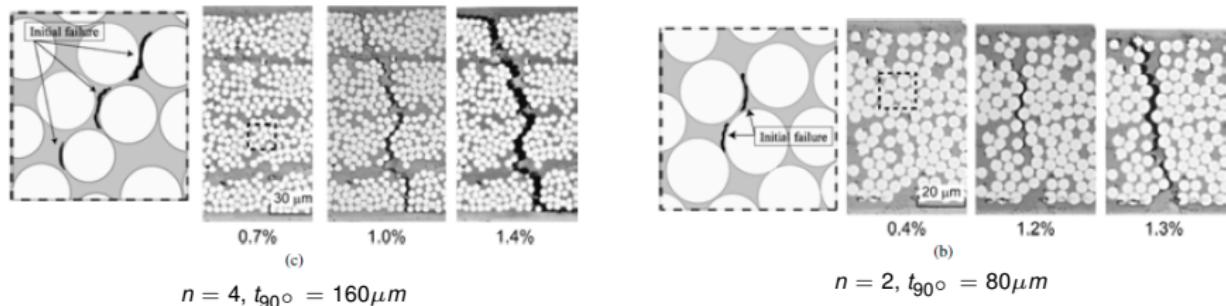
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Zhang et al., Compos. Part A-Appl. S. **28** (4), 1997.

A Counter-intuitive Observation

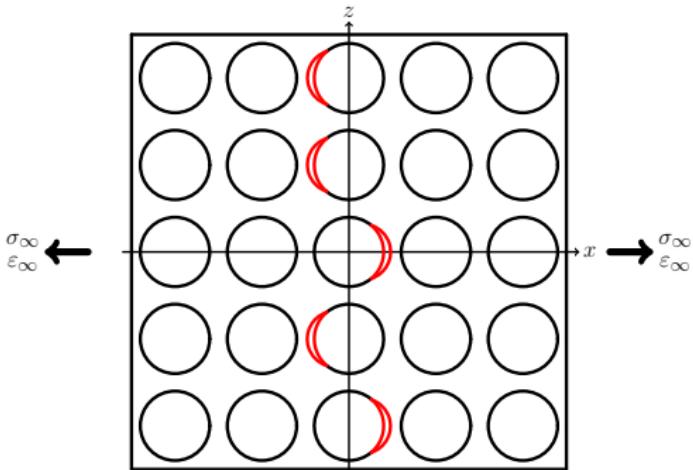
$[0^\circ, 90^\circ_n]_S$



Saito et al., Adv. Compos. Mater. 21 (1), 2012.

Objective of the Study

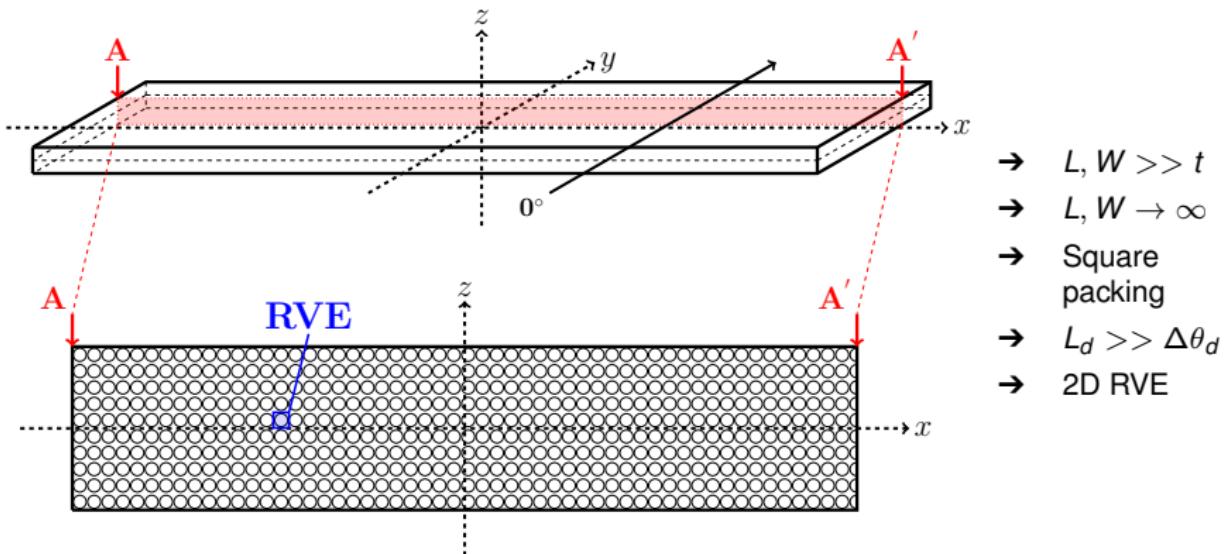
Stage 2: consecutive debonds



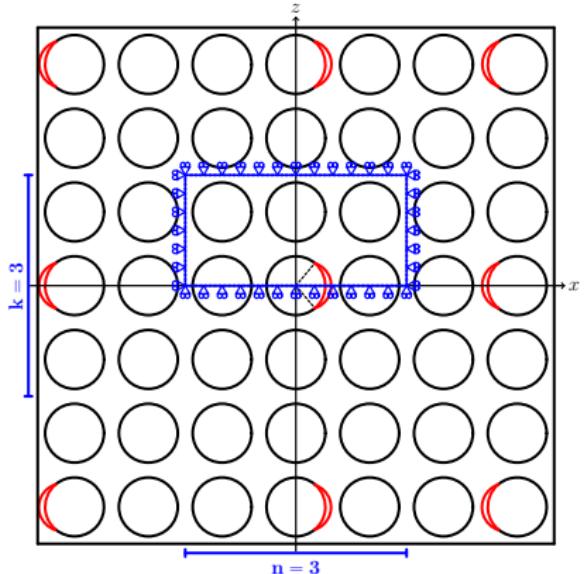
- Effect of debond-fiber interaction?
- Effect of debond-debond interaction?
- Effect of relative debond position on consecutive fibers: same or opposite sides?

MODELING THE FIBER-MATRIX INTERFACE CRACK

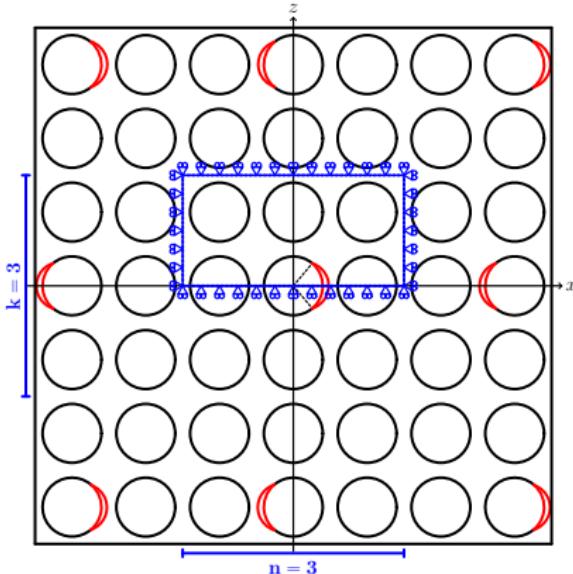
Geometry



Representative Volume Elements

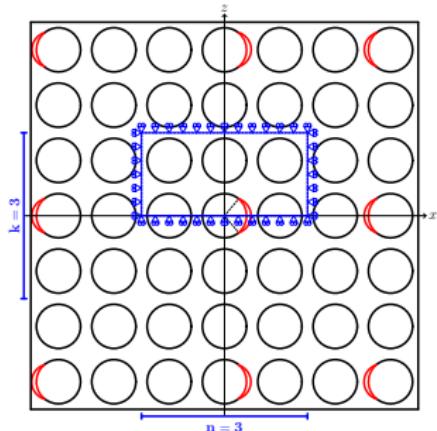


$n \times k - coupling$



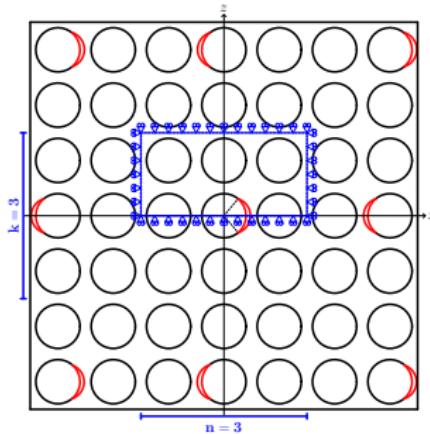
$n \times k - asymm$

Equivalent Boundary Conditions



Symmetric Coupling

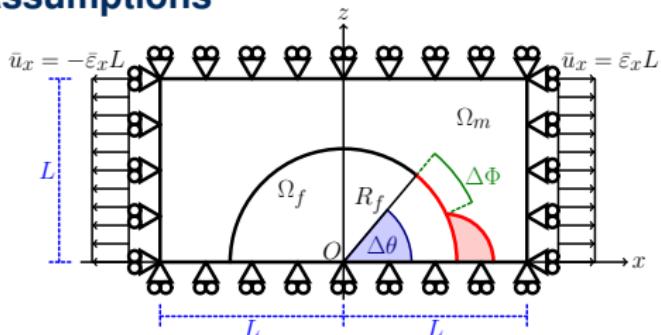
$$u_z(x, h) = u_z^\nu$$



Anti-symmetric Coupling

$$\begin{aligned} u_z(x, h) - u_z(0, h) &= -(u_z(-x, h) - u_z(0, h)) \\ u_x(x, h) &= -u_x(-x, h) \end{aligned}$$

Assumptions

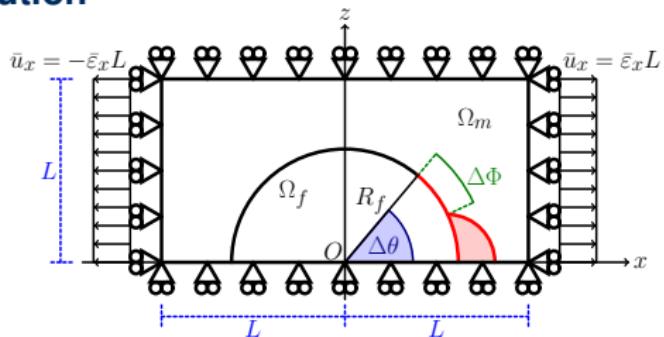


$$R_f = 1 \text{ } [\mu\text{m}] \quad L = \frac{R_f}{2} \sqrt{\frac{\pi}{V_f}}$$

Material	E	ν
glass fiber	70.0	0.2
epoxy	3.5	0.4

- Linear elastic, homogeneous and isotropic materials
- Plane strain
- Frictionless contact interaction
- Symmetric w.r.t. x-axis
- Coupling of x-displacements on left and right side (repeating unit cell)
- Applied uniaxial tensile strain $ε_x = 1\%$
- $V_f = 60\%$

Solution



in Ω_f, Ω_m :

$$\frac{\partial^2 \varepsilon_{xx}}{\partial z^2} + \frac{\partial^2 \varepsilon_{zz}}{\partial x^2} = \frac{\partial^2 \gamma_{zx}}{\partial x \partial z} \quad \text{for } 0^\circ \leq \alpha \leq \Delta\theta : \\ (\vec{U}_m(R_f, \alpha) - \vec{U}_f(R_f, \alpha)) \cdot \vec{n}_\alpha \geq 0$$

$$\varepsilon_y = \gamma_{xy} = \gamma_{yz} = 0 \quad \text{for } \Delta\theta \leq \alpha \leq 180^\circ :$$

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \tau_{zx}}{\partial z} = 0 \quad \vec{U}_m(R_f, \alpha) - \vec{U}_f(R_f, \alpha) = 0$$

$$\frac{\partial \tau_{zx}}{\partial x} + \frac{\partial \sigma_{zz}}{\partial z} = 0 \quad \sigma_{ij} = E_{ijkl} \varepsilon_{kl}$$

$$\sigma_{yy} = \nu (\sigma_{xx} + \sigma_{zz}) + BC$$

→ Oscillating singularity

$$\sigma \sim r^{-\frac{1}{2}} \sin(\varepsilon \log r), \quad V_f \rightarrow 0$$

$$\varepsilon = \frac{1}{2\pi} \log \left(\frac{1-\beta}{1+\beta} \right)$$

$$\beta = \frac{\mu_2(\kappa_1 - 1) - \mu_1(\kappa_2 - 1)}{\mu_2(\kappa_1 + 1) + \mu_1(\kappa_2 + 1)}$$

→ Finite Element Method (FEM) in Abaqus™

→ 2nd order shape functions

→ 6-nodes triangles & 8-nodes quadrilaterals

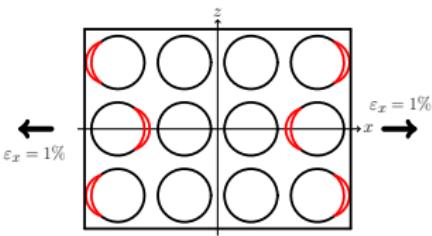
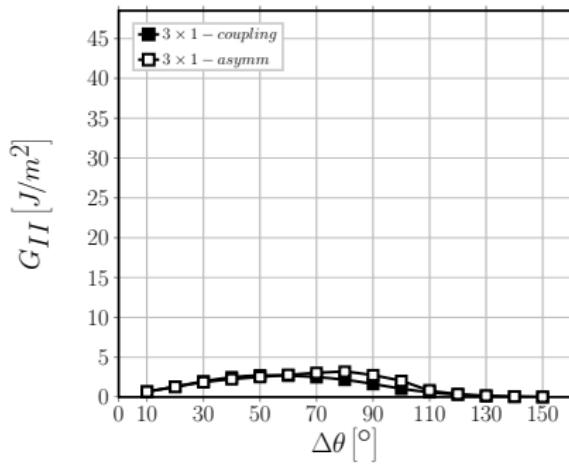
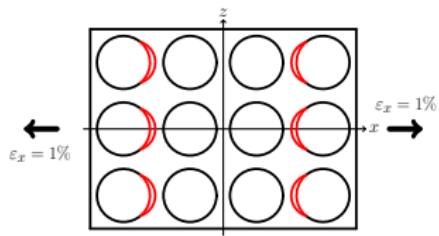
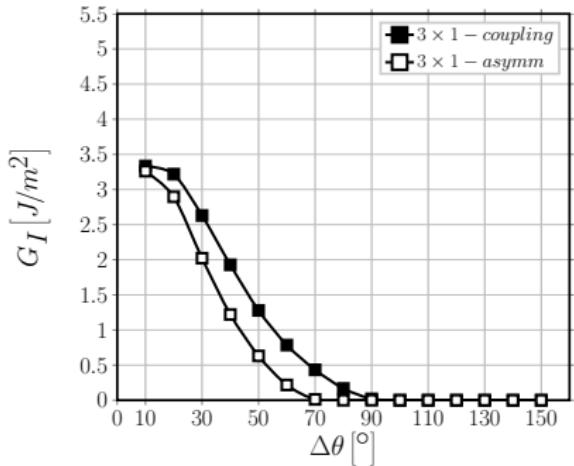
→ regular mesh of quadrilaterals at the crack tip:

- $AR \sim 1$
- $\delta = 0.05^\circ$

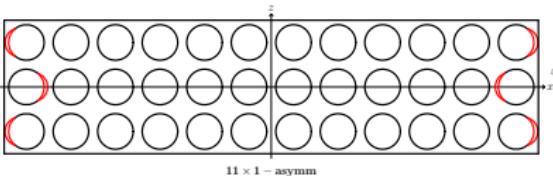
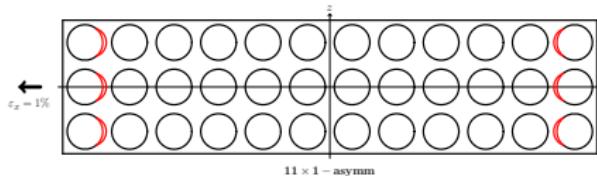
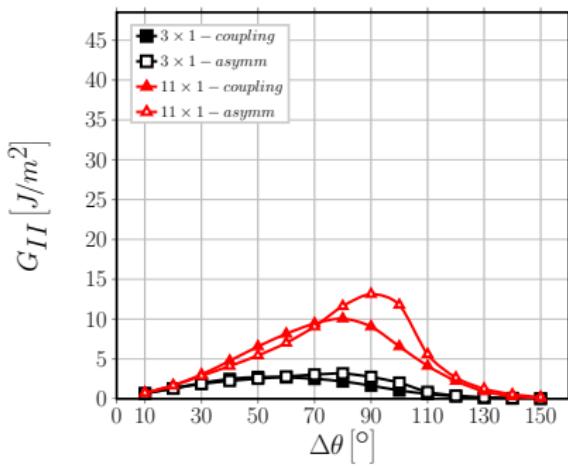
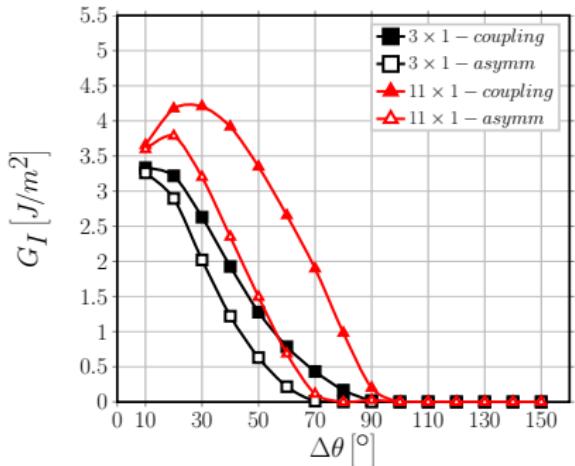
Initiation of Transverse Cracks in Thin-plies Modeling the Fiber-Matrix Interface Crack Debond Energy Release Rate Conclusions
Strain Magnification Crack Shielding Consecutive Debonds: Mode I Consecutive Debonds: Mode II Non-Consecutive Debonds

DEBOND ENERGY RELEASE RATE

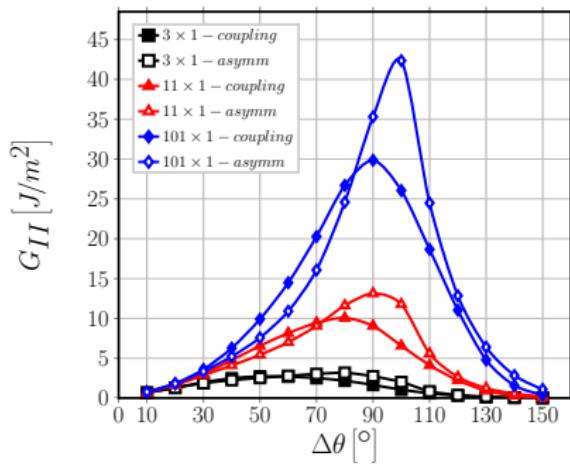
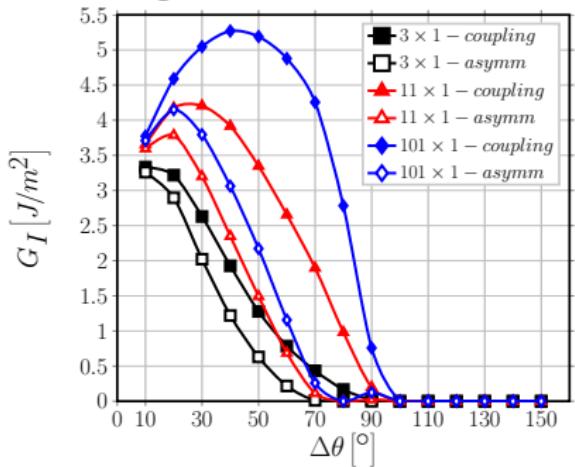
Strain Magnification



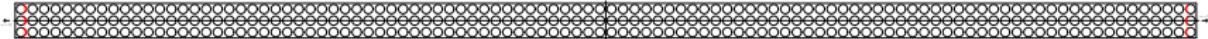
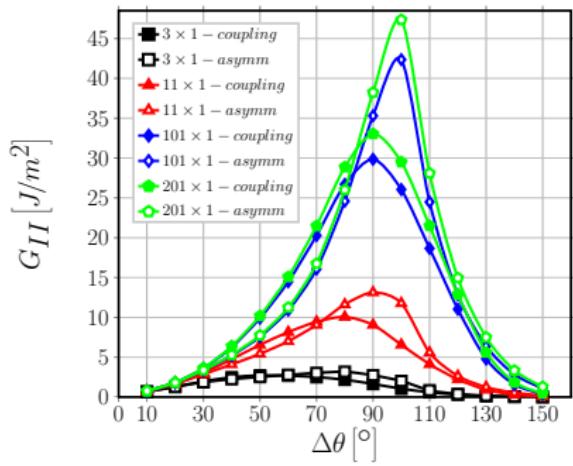
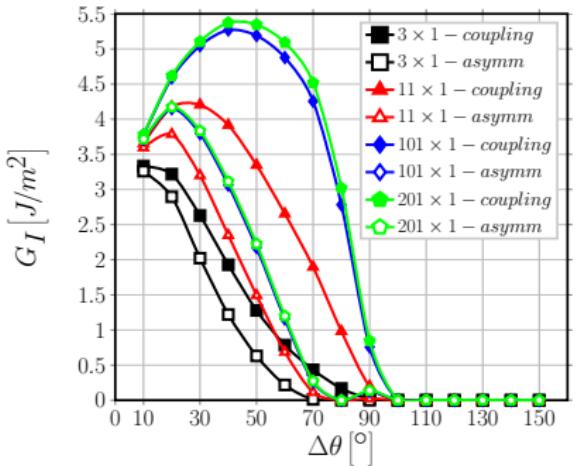
Strain Magnification



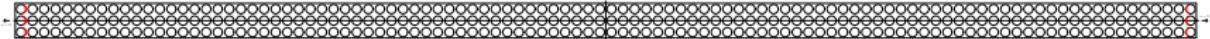
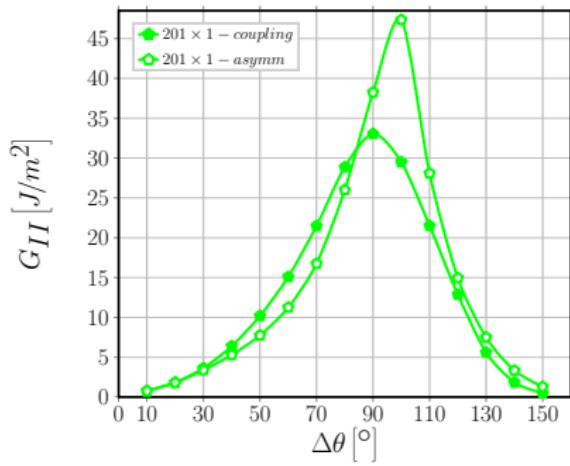
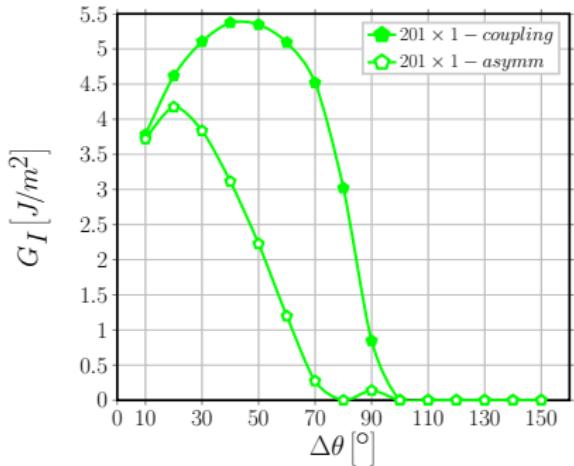
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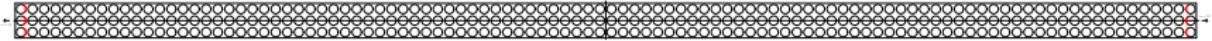
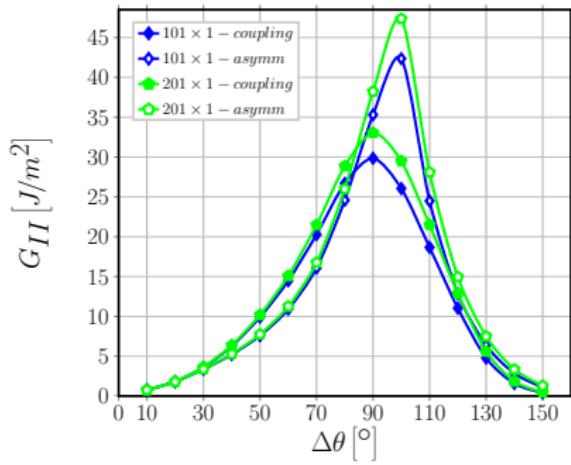
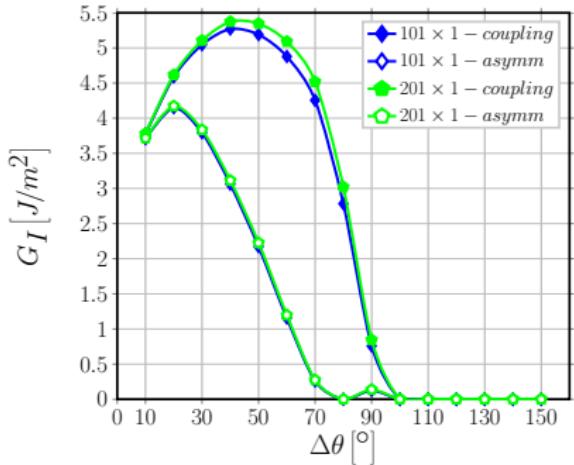
Strain Magnification



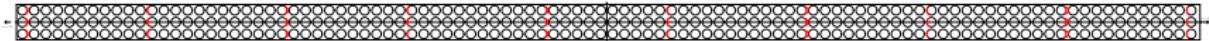
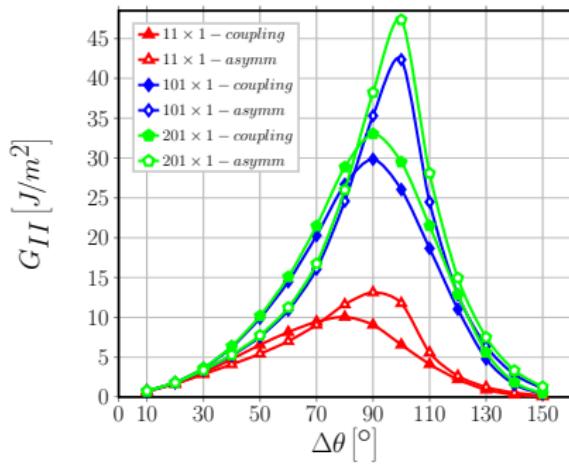
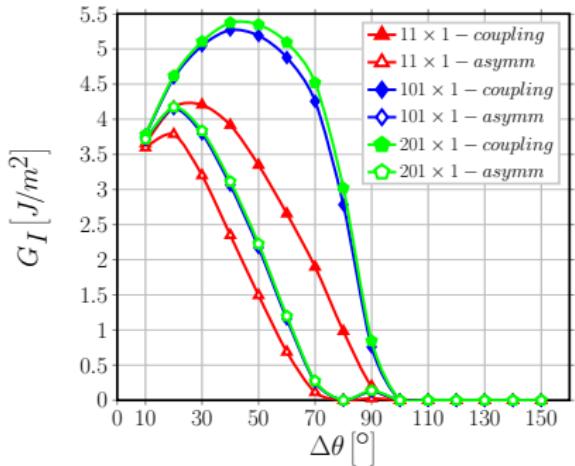
Crack Shielding



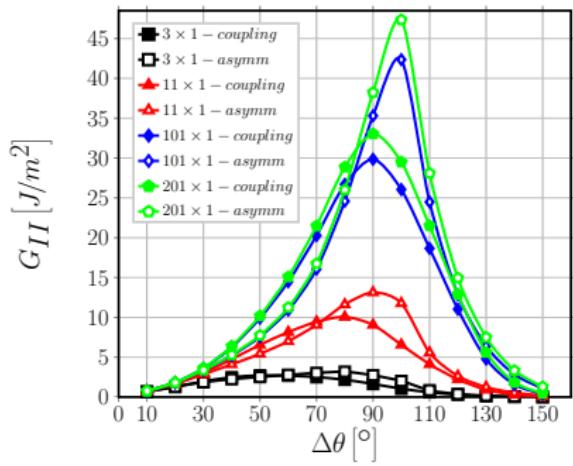
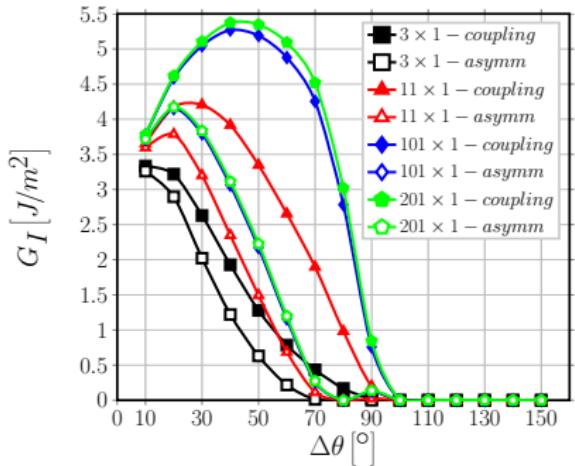
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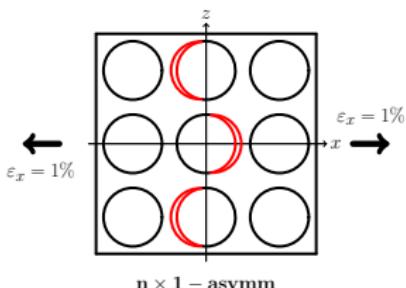
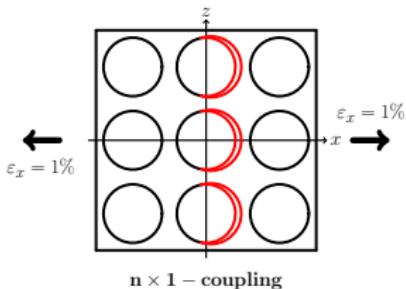
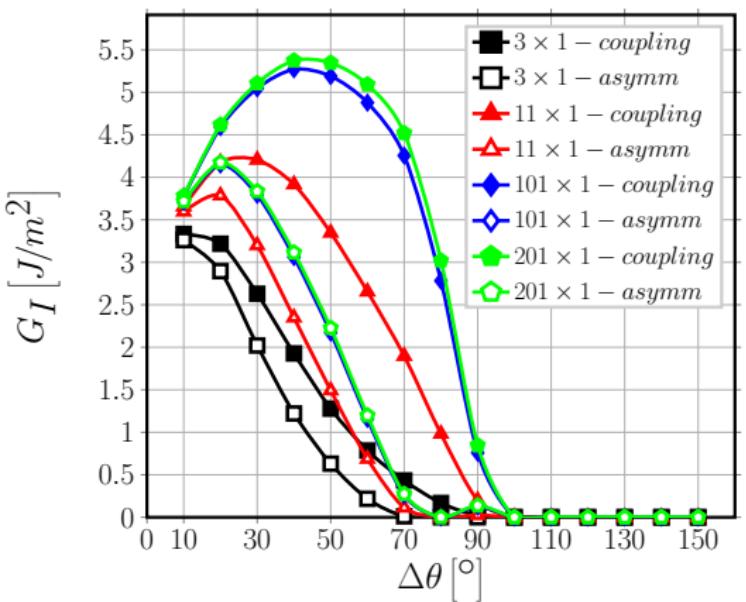
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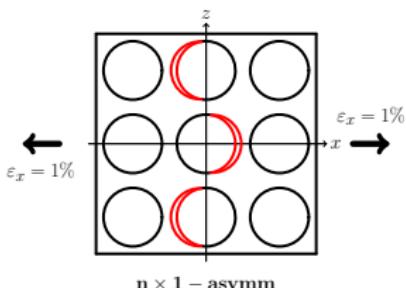
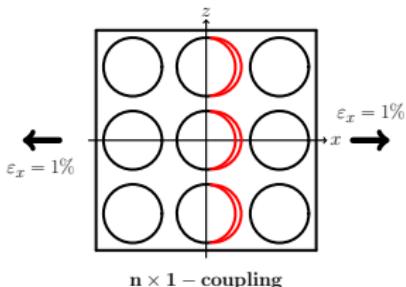
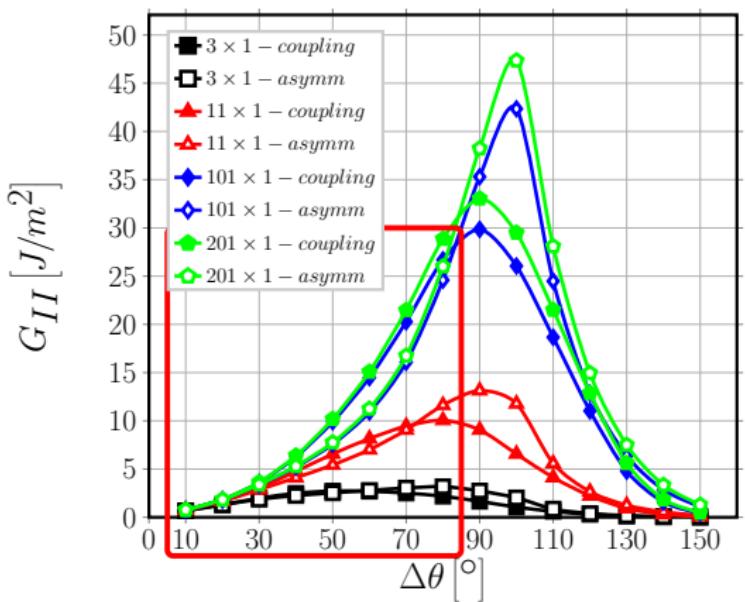
Crack Shielding



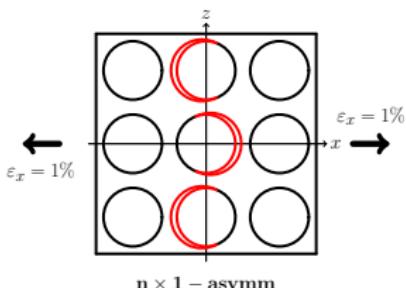
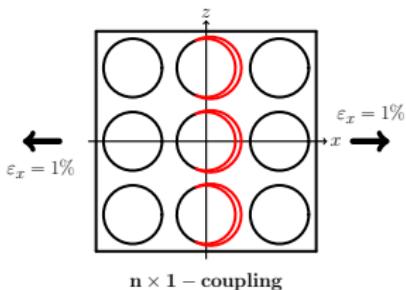
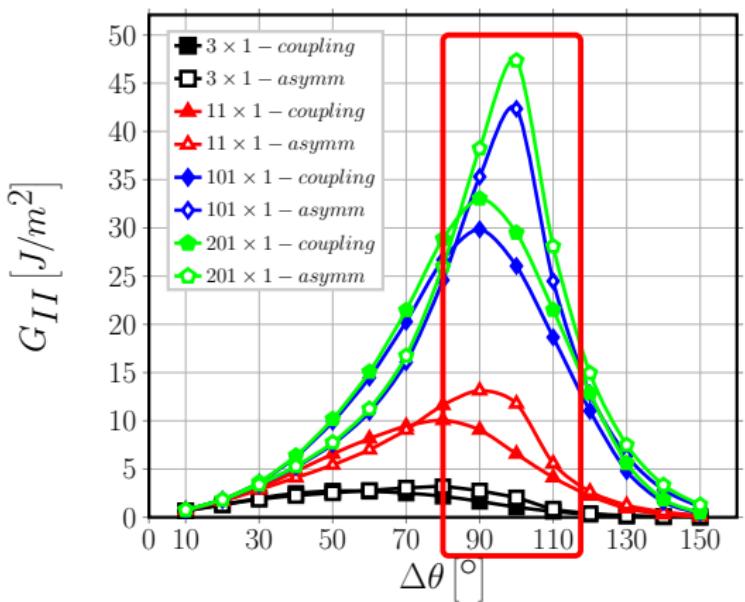
Consecutive Debonds: Mode I



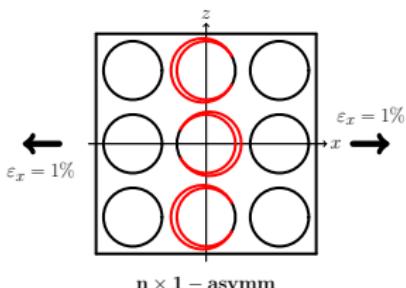
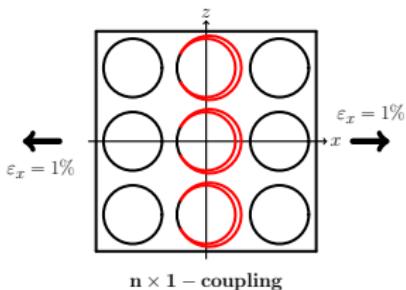
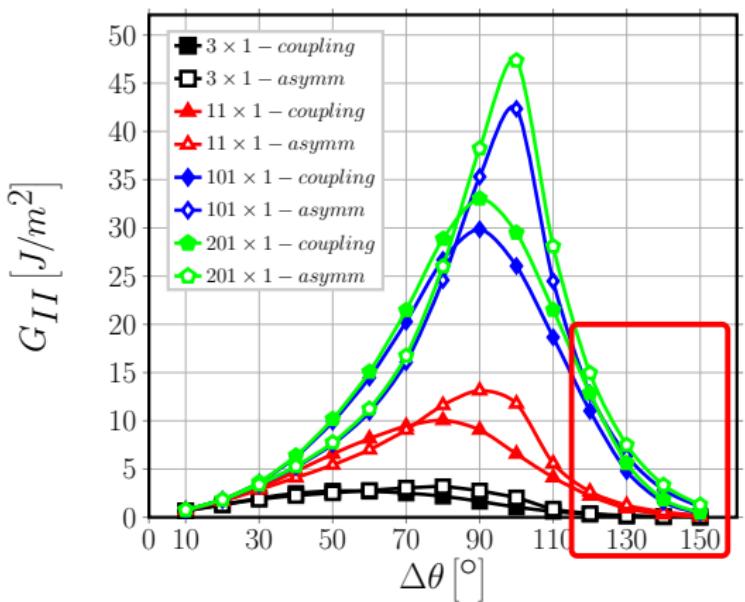
Consecutive Debonds: Mode II



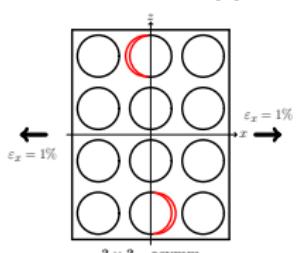
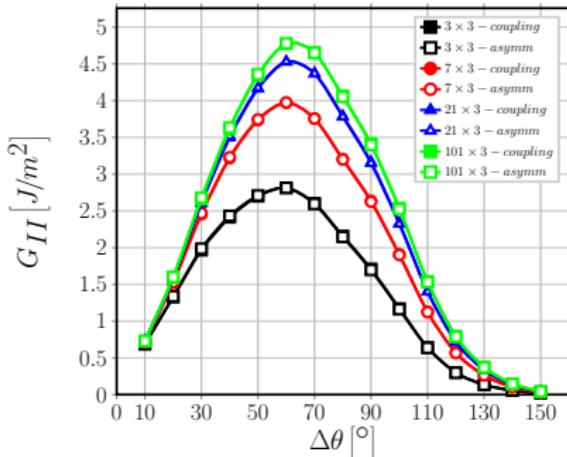
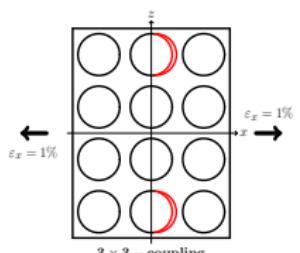
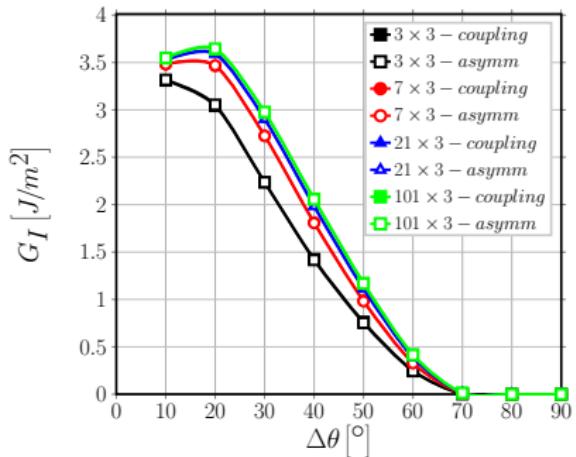
Consecutive Debonds: Mode II



Consecutive Debonds: Mode II



Non-Consecutive Debonds



CONCLUSIONS

Conclusions

- Debond-debond interaction in the through-the-thickness direction is extremely localized: with only a couple of undamaged fibers in between, no effect can be seen!
- For debonds on consecutive vertically-aligned fibers, G_{II} is higher and contact zone onset delayed if debonds are on the same side of their respective fiber.
- No significant difference in G_{II} observed, except in the range $80^\circ - 100^\circ$.
- In the range $80^\circ - 100^\circ$, G_{II} is higher when debonds are located on opposite sides of consecutive vertically-aligned fibers.



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