Tutorial Robotics IN2067

Exercise Sheet 04

Problem 1

Figure 1 shows a robot with one rotational joint and one prismatic joint. The DH parameters for this robot are

The manipulator is shown for configuration $\Theta_1 = 0, d_2 \neq 0$. Gravitational force applies in negative X_0 -direction, as shown. The inertia tensors are:

$${}^{C_1}I_1 = \begin{pmatrix} I_{xx1} & 0 & 0 \\ 0 & I_{yy1} & 0 \\ 0 & 0 & I_{zz1} \end{pmatrix} \quad {}^{C_2}I_2 = \begin{pmatrix} I_{xx2} & 0 & 0 \\ 0 & I_{yy2} & 0 \\ 0 & 0 & I_{zz2} \end{pmatrix}$$

The masses of the robot's links are m_1 and m_2 , and the centers of mass of the links are located at

$${}^{1}P_{C_{1}} = \left(\frac{l_{1}}{2}, 0, 0\right)^{\mathrm{T}}$$
 ${}^{2}P_{C_{2}} = (0, 0, l_{2})^{\mathrm{T}}.$

- a) Determine the dynamics equations using the Newton-Euler method
- b) Formulate the equations in state space (M-V-G) form

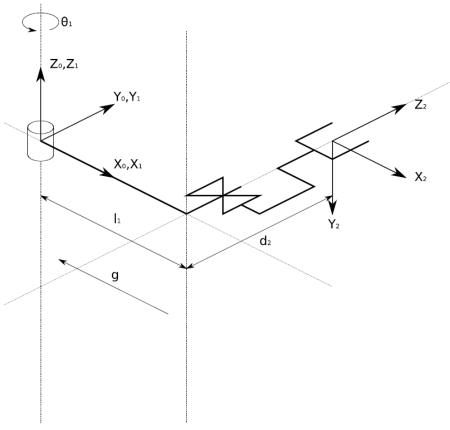


Figure 1: RP Robot (Problem 1)

Newton-Euler Method:

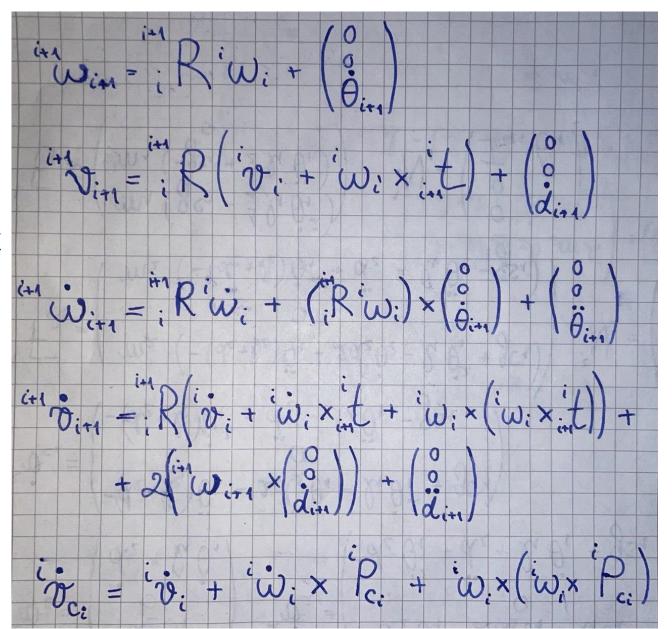
Step 0: Initialization

- Assumption: the robot has N joints, [N+1] is the coordinate frame of the end-effector
- Determine ${}^0\omega_0$, ${}^0\dot{\omega}_0$, 0v_0 , ${}^0\dot{v}_0$, ${}^{N+1}f_{N+1}$, ${}^{N+1}n_{N+1}$
- Consider the direction of gravity g when writing ${}^0\dot{v}_0$

Newton-Euler Method:

Step 1: Compute ${}^i\dot{v}_{c_i}$, ${}^i\omega_i$ and ${}^i\dot{\omega}_i$

- Forward propagation of velocities and accelerations:



Newton-Euler Method:

Step 2: Compute iF_i and iN_i Using the previously computed ${}^i\dot{v}_{c_i}$, ${}^i\omega_i$ and ${}^i\dot{\omega}_i$

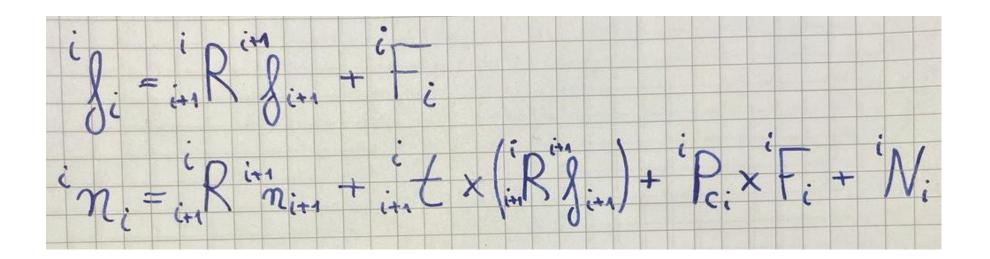
$${}^{i}F_{i} = m_{i} \cdot {}^{i}\dot{v}_{C_{i}}$$

$${}^{i}N_{i} = {}^{C_{i}}I_{i} \cdot {}^{i}\dot{\omega}_{i} + {}^{i}\omega_{i} \times {}^{C_{i}}I_{i} \cdot {}^{i}\omega_{i}$$

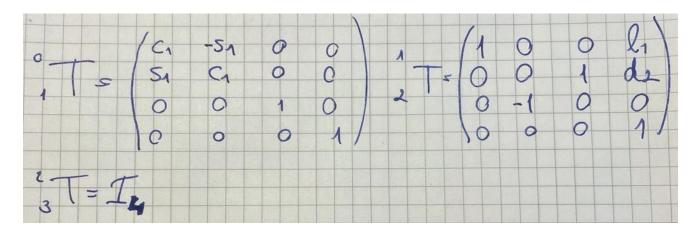
Newton-Euler Method:

Step 3: Compute joint torques vector τ

- Backward propagation of forces and torques:



CF	α	а	d	Θ
1	0°	0	0	$ heta_1$
2	-90°	l_1	d_2	0°
3	0°	0	0	0°



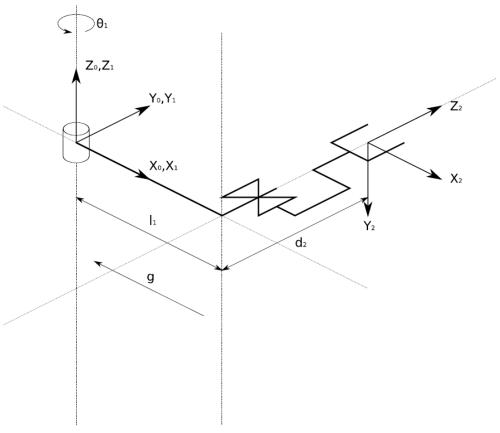


Figure 1: RP Robot (Problem 1)

Newton-Euler Method:

Step 0: Initialization

$$-{}^{0}\omega_{0}, {}^{0}\dot{\omega}_{0}, {}^{0}v_{0}, {}^{3}f_{3}, {}^{3}n_{3} = \begin{pmatrix} 0\\0\\0 \end{pmatrix}$$

- Because not otherwise given in the text

$$- {}^{0}\dot{v}_{0} = \begin{pmatrix} g \\ 0 \\ 0 \end{pmatrix}$$

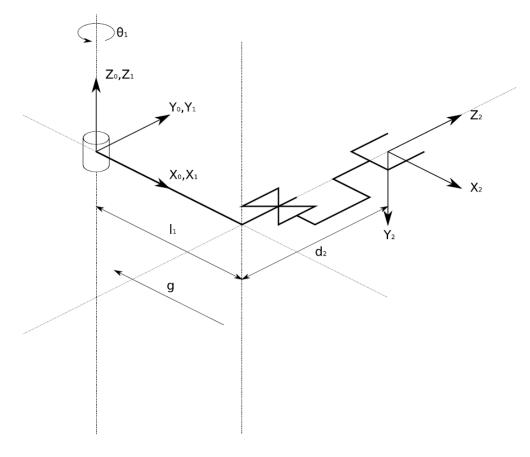
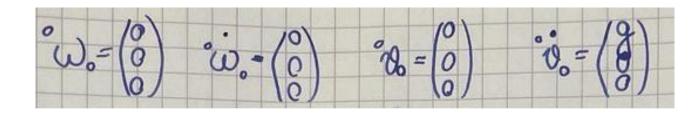


Figure 1: RP Robot (Problem 1)



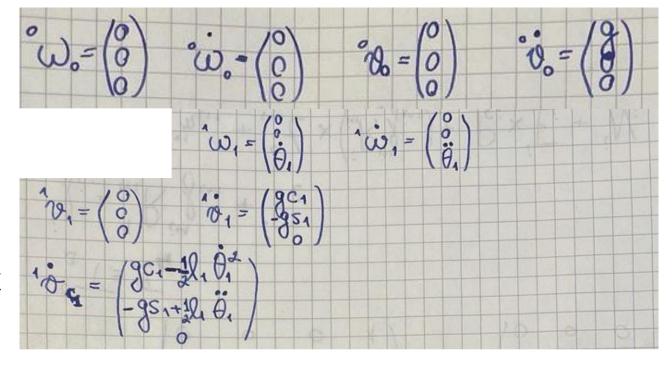


Newton-Euler Method:

Step 1: Compute ${}^i\dot{v}_{c_i}$, ${}^i\omega_i$ and ${}^i\dot{\omega}_i$

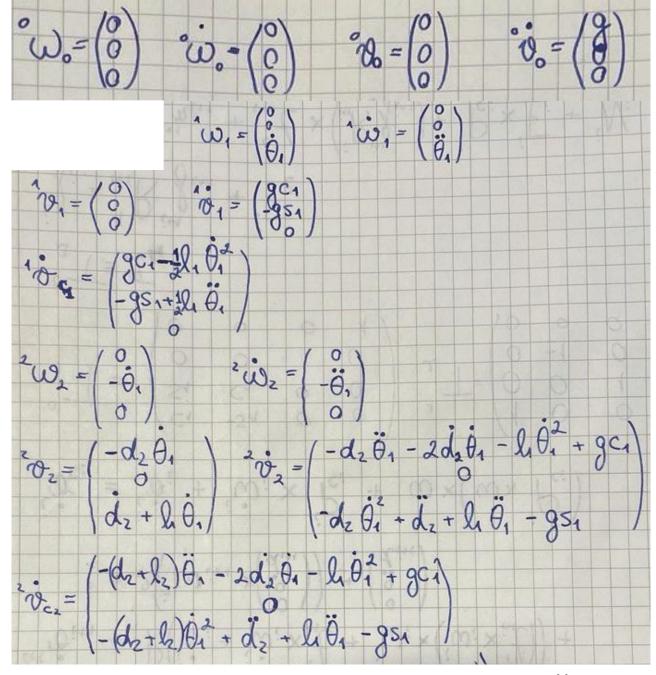
Newton-Euler Method:

Step 1: Compute ${}^i\dot{v}_{c_i}$, ${}^i\omega_i$ and ${}^i\dot{\omega}_i$



Newton-Euler Method:

Step 1: Compute ${}^i\dot{v}_{c_i}$, ${}^i\omega_i$ and ${}^i\dot{\omega}_i$



Newton-Euler Method:

Step 2: Compute ${}^{i}F_{i}$ and ${}^{i}N_{i}$

$${}^{i}F_{i} = m_{i} \cdot {}^{i}\dot{v}_{C_{i}}$$

$${}^{i}N_{i} = {}^{C_{i}}I_{i} \cdot {}^{i}\dot{\omega}_{i} + {}^{i}\omega_{i} \times {}^{C_{i}}I_{i} \cdot {}^{i}\omega_{i}$$

Newton-Euler Method:

Step 2: Compute ${}^{i}F_{i}$ and ${}^{i}N_{i}$

$${}^{i}F_{i} = m_{i} \cdot {}^{i}\dot{v}_{C_{i}}$$

$${}^{i}N_{i} = {}^{C_{i}}I_{i} \cdot {}^{i}\dot{\omega}_{i} + {}^{i}\omega_{i} \times {}^{C_{i}}I_{i} \cdot {}^{i}\omega_{i}$$

$$F_1 = \begin{pmatrix} m_1 \left(g c_1 - \frac{1}{2} l_1 \dot{\theta}_1^2 \right) \\ m_2 \left(-g s_1 + \frac{1}{2} l_1 \dot{\theta}_1 \right) \end{pmatrix} N_1 = \begin{pmatrix} 0 \\ 0 \\ T_{221} \ddot{\theta}_1 \end{pmatrix}$$

Newton-Euler Method:

Step 2: Compute ${}^{i}F_{i}$ and ${}^{i}N_{i}$

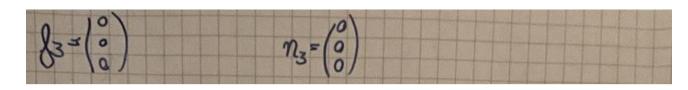
$${}^{i}F_{i} = m_{i} \cdot {}^{i}\dot{v}_{C_{i}}$$

$${}^{i}N_{i} = {}^{C_{i}}I_{i} \cdot {}^{i}\dot{\omega}_{i} + {}^{i}\omega_{i} \times {}^{C_{i}}I_{i} \cdot {}^{i}\omega_{i}$$

$$F_{1} = \begin{pmatrix} m_{1} \left(gc_{1} - \frac{1}{2} l_{1} \dot{\theta}_{1}^{2} \right) \\ m_{1} \left(-gs_{1} + \frac{1}{2} l_{1} \dot{\theta}_{1} \right) \end{pmatrix} N_{1} \begin{pmatrix} 0 \\ 0 \\ T_{221} \dot{\theta}_{1} \end{pmatrix}$$

$$F_{2} = \begin{pmatrix} m_{2} \left(-\left(d_{2} + l_{2} \right) \dot{\theta}_{1} + 2 \dot{d}_{2} \dot{\theta}_{1} - l_{1} \dot{\theta}_{1}^{2} + gc_{1} \right) \end{pmatrix} N_{2} = \begin{pmatrix} 0 \\ -T_{332} \dot{\theta}_{1} \end{pmatrix}$$

$$m_{2} \left(-\left(d_{2} + l_{2} \right) \dot{\theta}_{1}^{2} + \dot{d}_{2} + l_{1} \dot{\theta}_{1} - gs_{1} \right)$$



Newton-Euler Method:

Step 3: Compute joint torques vector τ

Newton-Euler Method:

Step 3: Compute joint torques vector τ

$$\begin{cases} 3^{2} \begin{pmatrix} 0 \\ 0 \end{pmatrix} & n_{3} = \begin{pmatrix} 0 \\ 0 \end{pmatrix} \\ 8^{2} = \begin{pmatrix} m_{2} \left(-(d_{2} + l_{2}) \dot{\theta}_{1} - 2 \dot{d}_{2} \dot{\theta}_{1} - l_{1} \dot{\theta}_{1}^{2} + g c_{1} \right) \\ m_{2} \left(-(d_{2} + l_{2}) \dot{\theta}_{1}^{2} + d_{2} + l_{1} \ddot{\theta}_{1} - g s_{1} \right) \\ n_{2} = \begin{pmatrix} -I_{332} \dot{\theta}_{1} - l_{2} m_{2} \left((d_{2} + l_{2}) \dot{\theta}_{1} + 2 \dot{d}_{2} \dot{\theta}_{1} + l_{1} \dot{\theta}_{1}^{2} - g c_{1} \right) \\ 0 \end{pmatrix}$$

Newton-Euler Method:

Step 3: Compute joint torques vector τ

$$\begin{cases} 3 = \begin{pmatrix} 0 \\ 0 \end{pmatrix} \\ 3 = \begin{pmatrix} 0 \\ 0 \end{pmatrix} \end{cases} \\ R_{3} = \begin{pmatrix} 0 \\ 0 \end{pmatrix} \\ R_{2} = \begin{pmatrix} m_{2} \left(-(d_{2} + l_{2}) \dot{\theta}_{1} - 2 d_{2} \dot{\theta}_{1} - l_{1} \dot{\theta}_{1}^{2} + g_{1} \right) \\ m_{2} = \begin{pmatrix} -(d_{2} + l_{2}) \dot{\theta}_{1}^{2} + d_{2} + l_{1} \ddot{\theta}_{1} - g_{3} \\ 0 \end{pmatrix} \\ R_{2} = \begin{pmatrix} -(d_{2} + l_{2}) \dot{\theta}_{1} - l_{2} m_{2} \left((d_{2} + l_{2}) \ddot{\theta}_{1} + 2 d_{2} \dot{\theta}_{1} + l_{1} \dot{\theta}_{1}^{2} - g_{1} \right) \\ 0 \end{pmatrix} \\ R_{1} = \begin{pmatrix} m_{1} g_{1} - m_{1} \frac{l_{1}}{l_{1}} \dot{\theta}_{1}^{2} - m_{2} \left((d_{2} + l_{2}) \ddot{\theta}_{1} + 2 d_{2} \dot{\theta}_{1} + l_{1} \dot{\theta}_{1}^{2} - g_{1} \right) \\ -m_{1} g_{3} + m_{1} l_{1} \ddot{\theta}_{1} + m_{2} \left((d_{2} + l_{2}) \ddot{\theta}_{1} - d_{2} - l_{1} \ddot{\theta}_{1} + g_{3} \right) \end{pmatrix} \\ m_{4} = \begin{pmatrix} T_{22} + T_{3} g_{2} \ddot{\theta}_{1} - l_{1} m_{1} \left(2 g_{3} - l_{1} \ddot{\theta}_{1} \right) \dot{\theta}_{1}^{2} + l_{2} m_{2} \left((d_{2} + l_{1}) \ddot{\theta}_{1} + l_{2} \dot{\theta}_{1}^{2} - d_{2} - l_{1} \ddot{\theta}_{1} + l_{3} \ddot{\theta}_{1}^{2} - d_{2} - l_{3} \ddot{\theta}_{1} \right) \\ + m_{2} \left(\left(d_{2}^{2} + d_{2} l_{1} + l_{1}^{2} \right) \ddot{\theta}_{1} + 2 d_{2} \dot{\theta}_{2} \dot{\theta}_{1} + \dot{\theta}_{1} l_{1} - l_{1} l_{2} \dot{\theta}_{2}^{2} - d_{2} g_{1} - l_{3} g_{3} \right) \end{pmatrix}$$

Newton-Euler Method:

Step 3: Compute joint torques vector τ

Express τ as a sum of multiple Matrix-Vector products necessary for controlling a robot (future tutorial)

$$T = \begin{pmatrix} \pi_{12} \\ g_{22} \end{pmatrix} = M(\theta) \cdot \ddot{\theta} + V(\theta, \dot{\theta}) + G(\theta)$$

Express τ as a sum of multiple Matrix-Vector products necessary for controlling a robot (future tutorial)

$$T = \binom{n_{12}}{g_{22}} = M(\theta) \cdot \dot{\theta} + V(\theta, \dot{\theta}) + G(\theta)$$

$$\mathcal{M}(\theta) = \begin{pmatrix}
T_{221} + T_{332} + m_{2}(d_{2}^{2} + 2d_{2}l_{2} + l_{2}^{2}) + \frac{m_{3}}{4}l_{3}^{2} \\
l_{1} m_{2}
\end{pmatrix}$$

$$\mathcal{M}(\theta, \dot{\theta}) = \begin{pmatrix}
2 m_{2} \dot{d}_{2} \dot{\theta}_{1} (d_{2} + l_{2}) \\
-m_{2} \dot{\theta}_{3}^{2} (d_{2} + l_{2})
\end{pmatrix}$$

$$G(\theta) = \begin{pmatrix}
3 (-m_{2} c_{3}(d_{2} + l_{2}) - l_{3} c_{3}(\frac{m_{3}}{2} + m_{2})
\end{pmatrix}$$

$$-3 m_{2} c_{3} d_{3} + l_{2} - l_{3} c_{3}(\frac{m_{3}}{2} + m_{2})$$

Problem 2

The manipulator shown in Figure 2 has the following properties:

- Masses of the three links are m_1, m_2, m_3
- Inertia tensors are

$${}^{C_1}I_1 = \begin{pmatrix} I_{xx1} & 0 & 0 \\ 0 & I_{yy1} & 0 \\ 0 & 0 & I_{zz1} \end{pmatrix} \quad {}^{C_2}I_2 = \begin{pmatrix} I_{xx2} & 0 & 0 \\ 0 & I_{yy2} & 0 \\ 0 & 0 & I_{zz2} \end{pmatrix} \quad {}^{C_3}I_3 = \begin{pmatrix} I_{xx3} & 0 & 0 \\ 0 & I_{yy3} & 0 \\ 0 & 0 & I_{zz3} \end{pmatrix}$$

• The positions of the centers of mass for the three links are:

$${}^{0}P_{C_{1}} = \begin{pmatrix} 0 \\ 0 \\ d_{1} - l_{1} \end{pmatrix}, \quad {}^{0}P_{C_{2}} = \begin{pmatrix} \frac{l_{2}}{2}c_{2} \\ \frac{l_{2}}{2}s_{2} \\ d_{1} \end{pmatrix}, \quad {}^{0}P_{C_{3}} = \begin{pmatrix} l_{2}c_{2} + \frac{l_{3}}{2}c_{23} \\ l_{2}s_{2} + \frac{l_{3}}{2}s_{23} \\ d_{1} \end{pmatrix}$$

Furthermore, gravity applies in negative Z_0 -direction, as shown. Using the Lagrangian approach to robot dynamics, determine the manipulator dynamic equations in state space (M-V-G) and configuration space (M-B-C-G) form.

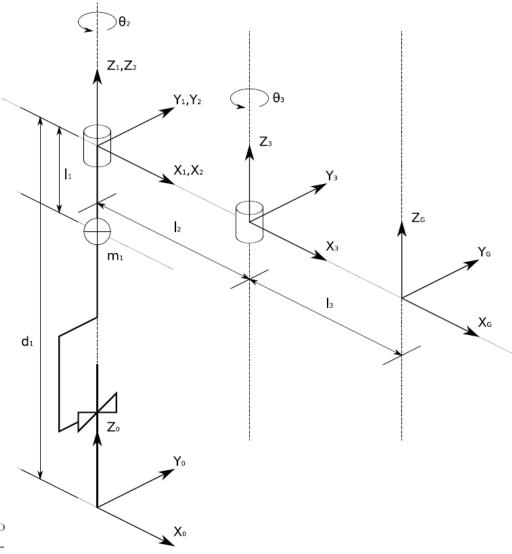


Figure 2: PRR Robot (Problem 2)

Step 1: Compute kinetic and potential energies (for every link)

Lagrange Method:

Step 2: Compute energy derivatives

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ди
\partial \theta_i
  ∂k
\partial \theta_i
  \partial k
\overline{\partial \dot{\theta}_i}
 d \partial k
dt \, \overline{\partial \dot{\theta}_i}
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Pay VERY much attention when computing the time derivative of $\frac{\partial k}{\partial \dot{\theta}_i}$ Besides differentiating the $\dot{ heta}$ terms, you must also differentiate the terms that contain heta! 23

Lagrange Method:

Step 2: Compute energy derivatives

$$\frac{\partial u}{\partial \theta_{i}}$$

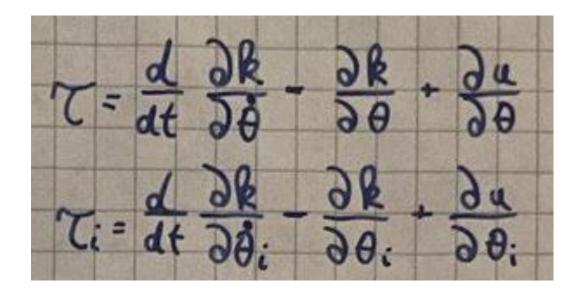
$$\frac{\partial k}{\partial \theta_{i}}$$

$$\frac{\partial k}{\partial \dot{\theta}_{i}}$$

$$\frac{d}{\partial t} \frac{\partial k}{\partial \dot{\theta}_{i}}$$

Pay VERY much attention when computing the time derivative of $\frac{\partial k}{\partial \dot{\theta}_i}$ Besides differentiating the $\dot{ heta}$ terms, you must also differentiate the terms that contain heta! 24

Step 3: Compute joint torques vector τ



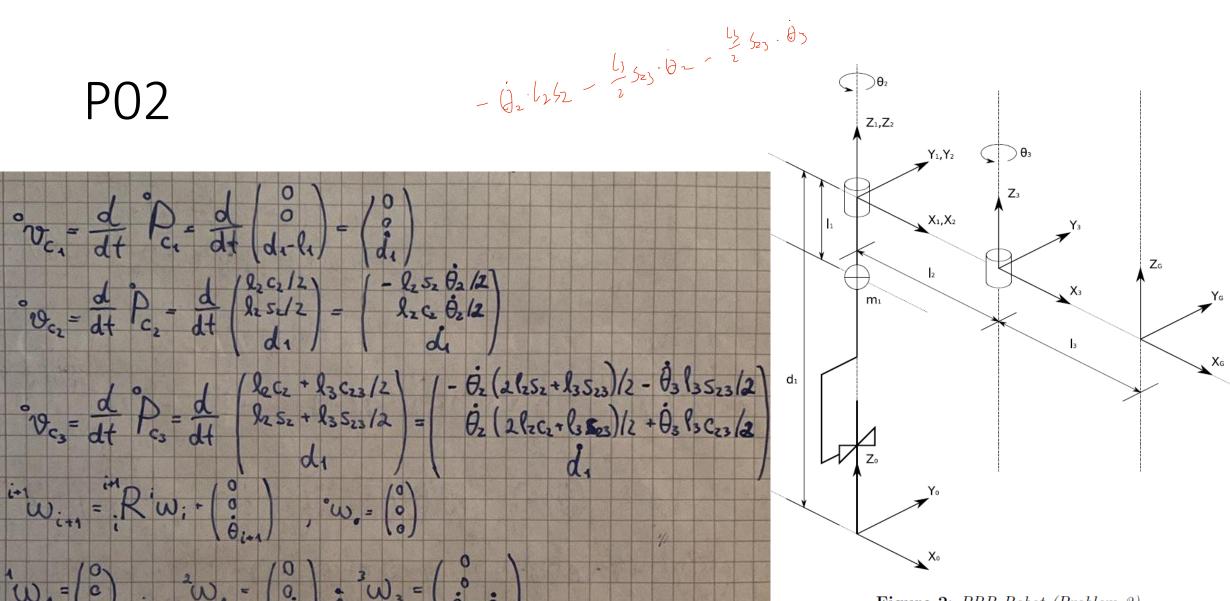


Figure 2: PRR Robot (Problem 2)

ki = \frac{1}{2} mi vot ive + \frac{1}{2} wi \cdot Ti \cdot wi , \frac{1}{2} coordinate frame

\(u_i = -m_i \, \frac{1}{2} \cdot P_{ei} + u_{\text{rej}} \)

Step 1: Compute kinetic and potential energies (for every link)

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Step 1: Compute kinetic and potential energies (for every link)

$$k_1 = \frac{m_1}{2} \frac{\dot{d}^2}{\dot{d}_1} + \frac{m_2}{2} \left(\dot{d}_1^2 + \frac{1}{4} l_2^2 \dot{d}_2^2 \right)$$

$$k_2 = \frac{1}{2} I_{223} \dot{\theta}_2^2 + \frac{m_2}{2} \left(\dot{d}_1^2 + \frac{1}{4} l_2^2 \dot{\theta}_2^2 \right)$$

$$u_1 = m_1 g(d_1 - l_1)$$

$$u_2 = m_2 g d_1$$

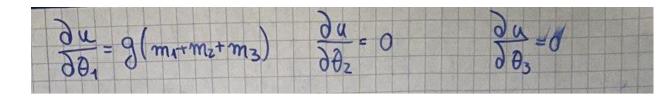
Step 1: Compute kinetic and potential energies (for every link)

$$k_{3} = \frac{1}{2} \frac{1}$$

Lagrange Method:

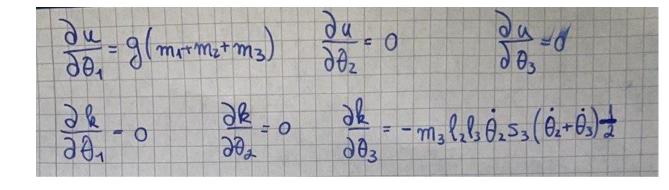
Step 2: Compute energy derivatives

 $\frac{\partial u}{\partial \theta_i}$



Lagrange Method:

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\frac{\partial u}{\partial \theta_i}
\frac{\partial k}{\partial \theta_i}
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Lagrange Method:

ди
$\overline{\partial \theta_i}$
∂k
$\overline{\partial \theta_i}$
∂k
$\overline{\partial \dot{\theta}_i}$

Lagrange Method:

$$\frac{\partial u}{\partial \theta_{i}}$$

$$\frac{\partial k}{\partial \theta_{i}}$$

$$\frac{\partial k}{\partial \dot{\theta}_{i}}$$

$$\frac{d}{dt} \frac{\partial k}{\partial \dot{\theta}_{i}}$$

$$\frac{\partial u}{\partial \theta_{1}} = g(m_{1}+m_{2}+m_{3}) \quad \frac{\partial u}{\partial \theta_{2}} = 0$$

$$\frac{\partial k}{\partial \theta_{3}} = 0$$

$$\frac{\partial k}{\partial \theta_{4}} = 0$$

$$\frac{\partial k}{\partial \theta_{4}} = 0$$

$$\frac{\partial k}{\partial \theta_{3}} = -m_{3}l_{2}l_{3}\dot{\theta}_{2}S_{3}(\dot{\theta}_{2}+\dot{\theta}_{3})\frac{1}{2}$$

$$\frac{\partial k}{\partial \dot{\theta}_{4}} = \dot{d}_{1}(m_{1}+m_{2}+m_{3})$$

$$\frac{\partial k}{\partial \dot{\theta}_{4}} = \dot{\theta}_{2}(T_{222}+T_{223}+\frac{m_{2}l_{2}}{4l_{2}}+m_{3}(l_{2}+l_{3}l_{3}C_{3}+l_{3})+l_{3}(T_{23}+m_{3}(l_{2}+l_{3}l_{3})+l_{3}(T_{23}+m_{3}(l_{2}+l_{3}l_{3}))$$

$$\frac{\partial k}{\partial \dot{\theta}_{3}} = \dot{\theta}_{2}(T_{223}+m_{3}(l_{2}+l_{3}l_{3}C_{3}+l_{3})+\dot{\theta}_{3}(T_{223}+\frac{m_{3}l_{2}}{4l_{3}})$$

$$\frac{\partial k}{\partial \dot{\theta}_{3}} = \dot{\theta}_{2}(T_{223}+m_{3}(l_{2}+l_{3}l_{3}C_{3}+l_{3})+\dot{\theta}_{3}(T_{223}+\frac{m_{3}l_{2}}{4l_{3}})$$

Lagrange Method:

$$\frac{\partial u}{\partial \theta_{i}}$$

$$\frac{\partial k}{\partial \theta_{i}}$$

$$\frac{\partial k}{\partial \dot{\theta}_{i}}$$

$$\frac{d}{dt} \frac{\partial k}{\partial \dot{\theta}_{i}}$$

$$\frac{\partial u}{\partial \theta_{1}} = 9(m_{1} + m_{2} + m_{3}) \quad \frac{\partial u}{\partial \theta_{2}} = 0$$

$$\frac{\partial k}{\partial \theta_{1}} = 0$$

$$\frac{\partial k}{\partial \theta_{3}} = 0$$

$$\frac{\partial k}{\partial \theta_{3}} = -m_{3} l_{2} l_{3} \dot{\theta}_{2} S_{3} (\dot{\theta}_{2} + \dot{\theta}_{3}) \frac{1}{2}$$

$$\frac{\partial k}{\partial \dot{\theta}_{1}} = \dot{d}_{1} (m_{1} + m_{2} + m_{3})$$

$$\frac{\partial k}{\partial \dot{\theta}_{2}} = \dot{\theta}_{2} (T_{222} + T_{222} + \frac{m_{2}}{4} l_{2} + m_{3} (l_{2} + l_{3} l_{3} c_{3} + l_{3}^{2}) + \dot{\theta}_{3} (T_{223} + m_{3} l_{2}^{2} l_{3} l_{3} c_{3} + l_{3}^{2})$$

$$\frac{\partial k}{\partial \dot{\theta}_{2}} = \dot{\theta}_{2} (T_{223} + m_{3} (\frac{1}{2} l_{3} l_{3} c_{3} + \frac{1}{4} l_{3}^{2}) + \dot{\theta}_{3} (T_{223} + \frac{m_{2}}{4} l_{3}^{2})$$

$$\frac{\partial k}{\partial \dot{\theta}_{3}} = \dot{\theta}_{2} (T_{223} + m_{3} (\frac{1}{2} l_{3} l_{3} c_{3} + \frac{1}{4} l_{3}^{2}) + \dot{\theta}_{3} (T_{223} + m_{3} l_{3}^{2} l_{3} l_{3} c_{3} + \frac{1}{4} l_{3}^{2})$$

$$\frac{d}{d l_{3}} \dot{\theta}_{3} = \ddot{\theta}_{2} (T_{223} + m_{3} (\frac{1}{2} l_{3} l_{3} c_{3} + \frac{1}{4} l_{3}^{2}) + \ddot{\theta}_{3} (T_{223} + m_{3} l_{3}^{2} l_{3} l_{3} c_{3} + \frac{1}{4} l_{3}^{2})$$

$$\frac{d}{d l_{3}} \dot{\theta}_{3} = \ddot{\theta}_{2} (T_{223} + m_{3} (\frac{1}{2} l_{3} l_{3} c_{3} + \frac{1}{4} l_{3}^{2}) + \ddot{\theta}_{3} (T_{223} + m_{3} l_{3}^{2} l_{3} c_{3} + \frac{1}{4} l_{3}^{2})$$

$$\frac{d}{d l_{3}} \dot{\theta}_{3} = \ddot{\theta}_{2} (T_{223} + m_{3} (\frac{1}{2} l_{3} l_{3} c_{3} + \frac{1}{4} l_{3}^{2}) + \ddot{\theta}_{3} (T_{223} + m_{3} l_{3}^{2} l_{3} c_{3} + \frac{1}{4} l_{3}^{2})$$

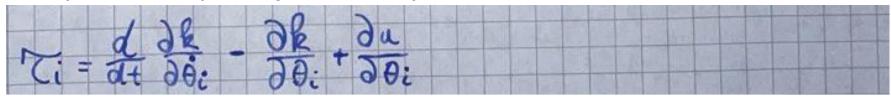
$$\frac{d}{d l_{3}} \dot{\theta}_{3} = \ddot{\theta}_{2} (T_{223} + m_{3} (\frac{1}{2} l_{3} l_{3} c_{3} + \frac{1}{4} l_{3}^{2}) + \ddot{\theta}_{3} (T_{223} + m_{3} l_{3}^{2} l_{3} c_{3} + \frac{1}{4} l_{3}^{2})$$

$$\frac{d}{d l_{3}} \dot{\theta}_{3} = \ddot{\theta}_{2} (T_{223} + m_{3} (\frac{1}{2} l_{3} l_{3} c_{3} + \frac{1}{4} l_{3}^{2}) + \ddot{\theta}_{3} (T_{223} + m_{3} l_{3} l_{3} l_{3} c_{3} + \frac{1}{4} l_{3}^{2})$$

$$\frac{d}{d l_{3}} \dot{\theta}_{3} = \ddot{\theta}_{3} (T_{3} + m_{3} l_{3} l_{3} l_{3} c_{3} + \frac{1}{4} l_{3}^{2} l_{3} + \frac{1}{4}$$

Lagrange Method:

Step 3: Compute joint torques vector τ



Step 3: Compute joint torques vector τ

Express τ as a sum of multiple Matrix-Vector products necessary for controlling a robot (future tutorial)

$$\tau = M(\theta)\ddot{\theta} + V(\theta,\dot{\theta}) + G(\theta)$$

$$\tau = M(\theta)\ddot{\theta} + B(\theta)[\dot{\theta}_i\dot{\theta}_j] + C(\theta)[\dot{\theta}^2] + G(\theta)$$

Express τ as a sum of multiple Matrix-Vector products necessary for controlling a robot (future tutorial)

$$\tau = M(\theta)\ddot{\theta} + V(\theta,\dot{\theta}) + G(\theta)$$

$$\tau = M(\theta)\ddot{\theta} + B(\theta)[\dot{\theta}_i\dot{\theta}_j] + C(\theta)[\dot{\theta}^2] + G(\theta)$$

