

Force-Control

$$f_e = k_e x. \quad (11.7)$$

The equation describing this physical system is

$$f = m\ddot{x} + k_e x + f_{\text{dist}}, \quad f_e = k_e x \quad (11.8)$$

or, written in terms of the variable we wish to control, f_e ,

$$f = \cancel{m k_e^{-1} \ddot{f}_e} + \cancel{k_e f_e} + f_{\text{dist}}. \quad (11.9)$$

Using the partitioned-controller concept, as well as

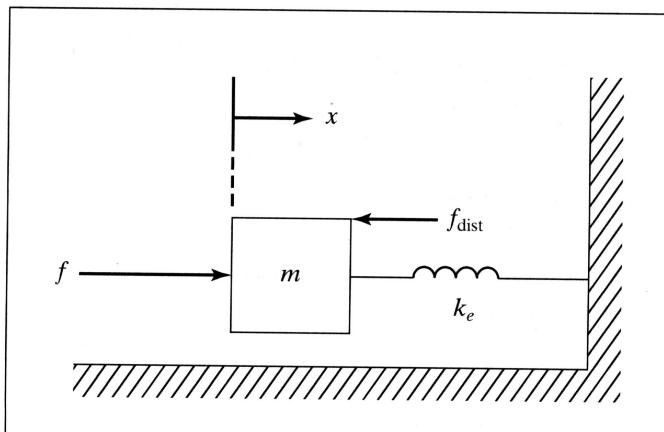
$$\alpha = m k_e^{-1}$$

and

$$\beta = f_e + f_{\text{dist}}$$

we arrive at the control law,

$$f = m k_e^{-1} \left[\ddot{f}_d + k_{vf} \dot{e}_f + k_{pf} e_f \right] + f_e + f_{\text{dist}}, \quad (11.10)$$



$$f = mk_e^{-1} \left[\ddot{f}_d + k_{vf} \dot{e}_f + k_{pf} e_f \right] + f_e + f_{\text{dist}},$$

$$\ddot{e}_f + k_{vf} \dot{e}_f + k_{pf} e_f = 0.$$

If we choose to leave the f_{dist} term out of our control law, equate (11.9) and (11.10), and do a steady-state analysis by setting all time derivatives to zero, we find that

$$e_f = \frac{f_{\text{dist}}}{\alpha}, \quad \alpha = mk_e^{-1} k_{pf}, \quad (11.12)$$

Therefore, we suggest the control law

$$f = mk_e^{-1} \left[\ddot{f}_d + k_{vf} \dot{e}_f + k_{pf} e_f \right] + f_d.$$

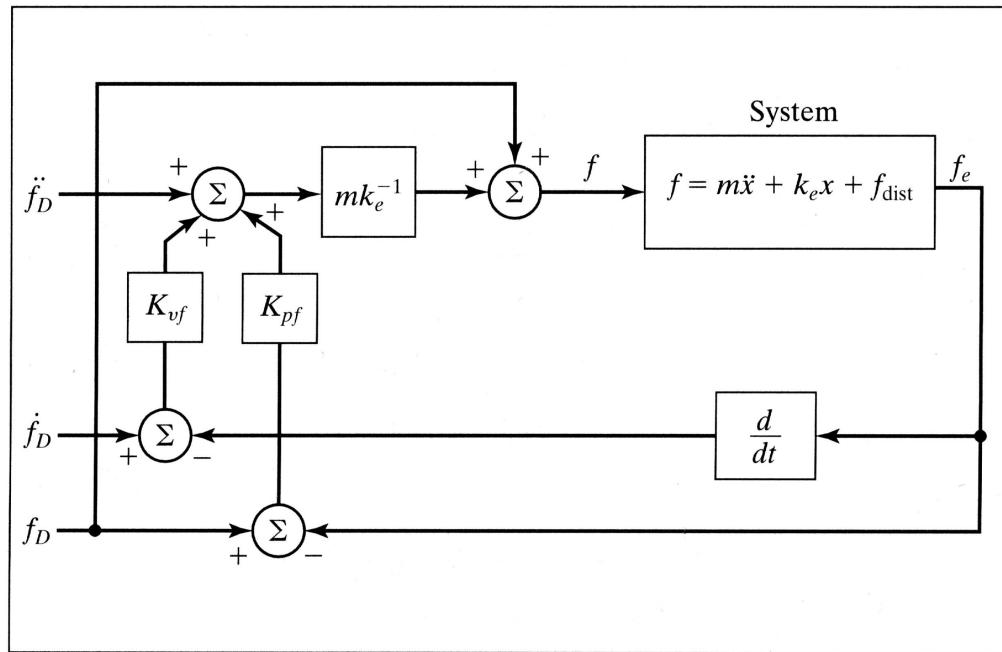
$$e_f = \frac{f_{\text{dist}}}{1 + \alpha}.$$

Closed-Loop Force Control

$$f = m k_e^{-1} \left[\ddot{f}_d + k_{vf} \dot{e}_f + k_{pf} e_f \right] + f_d. \quad (11.14)$$

Figure 11.6 is a block diagram of the closed-loop system using the control law (11.14).

Generally, practical considerations change the implementation of a force-control servo quite a bit from the ideal shown in Fig. 11.6. First, force trajectories are



Practical Force-Control System

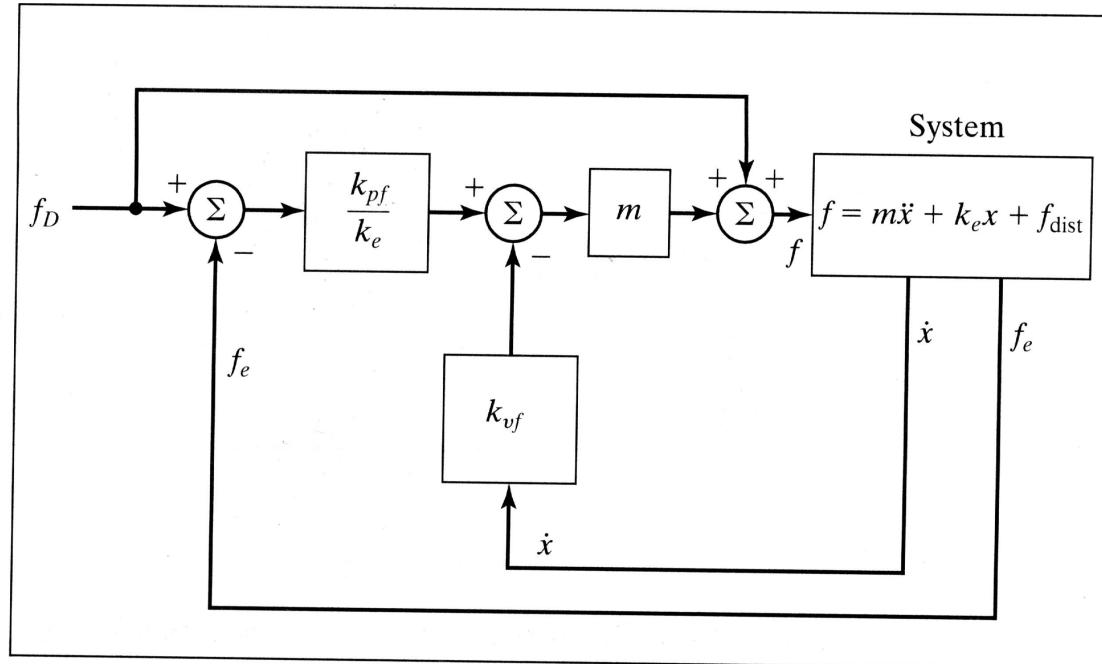
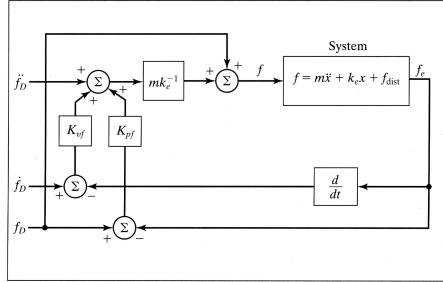


FIGURE 11.7: A practical force-control system for the spring–mass system.

Hybrid-Controller

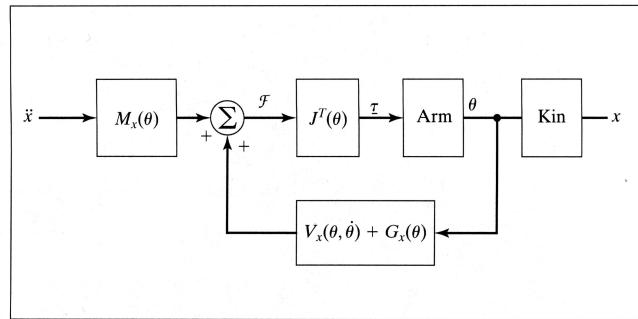


FIGURE 11.11: The Cartesian decoupling scheme introduced in Chapter 10.

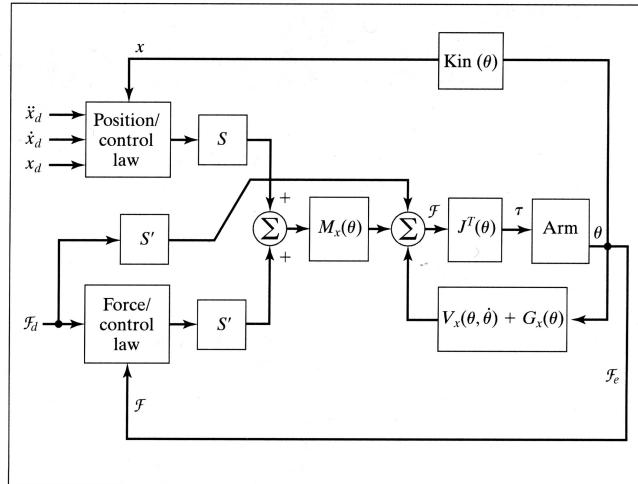


FIGURE 11.12: The hybrid position/force controller for a general manipulator. For simplicity, the velocity-feedback loop has not been shown.

Torque Control

$$\tau_m = k_m i_a.$$

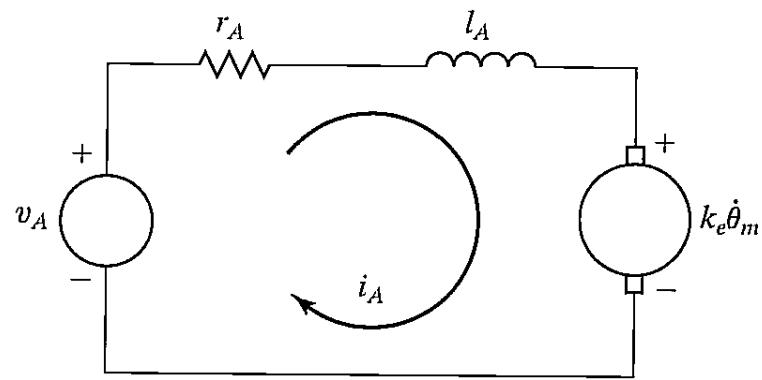
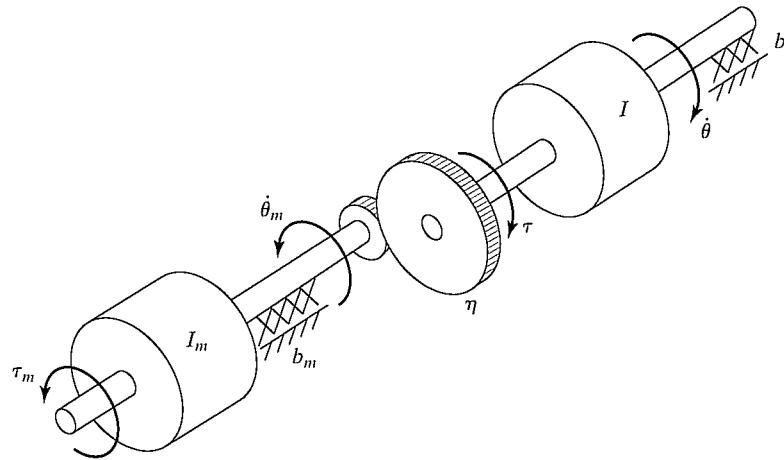


FIGURE 9.11: The armature circuit of a DC torque motor.

$$l_a \ddot{i}_a + r_a i_a = v_a - k_e \dot{\theta}_m.$$

Effective Inertia



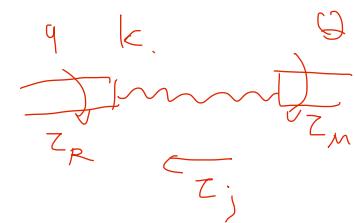
$$\tau = \eta \tau_m,$$

$$\dot{\theta} = (1/\eta) \dot{\theta}_m,$$

$$\tau_m = I_m \ddot{\theta}_m + b_m \dot{\theta}_m + (1/\eta) (I \ddot{\theta} + b \dot{\theta}),$$

$$\tau_m = \left(I_m + \frac{I}{\eta^2} \right) \ddot{\theta}_m + \left(b_m + \frac{b}{\eta^2} \right) \dot{\theta}_m.$$

$$\underline{\tau} = (I + \eta^2 I_m) \ddot{\theta} + (b + \eta^2 b_m) \dot{\theta}.$$



$$z_j = k(\theta - q)$$

Task Requirements

- Robots usually don't fit the ideal of "universally programmable" devices
- Degrees of freedom should match the task
 - Minimizes cost (hardware, computing power, and power consumption)
 - Minimizes size/weight

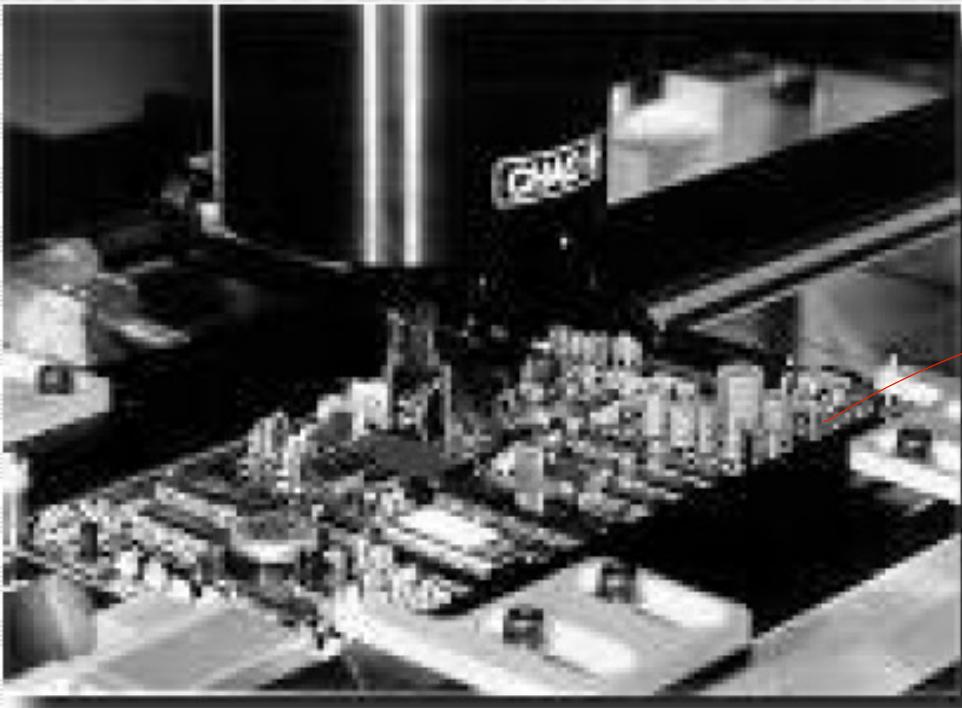
Example: Haptic Device

- 3dof actuation
- Torque not important for many virtual environments
- However, 6dof positioning is important



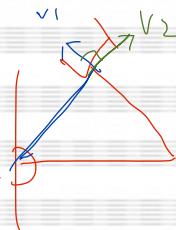
Example: Circuit Assembly

- Placement of components on a circuit board (4 dof)



δ is a topic

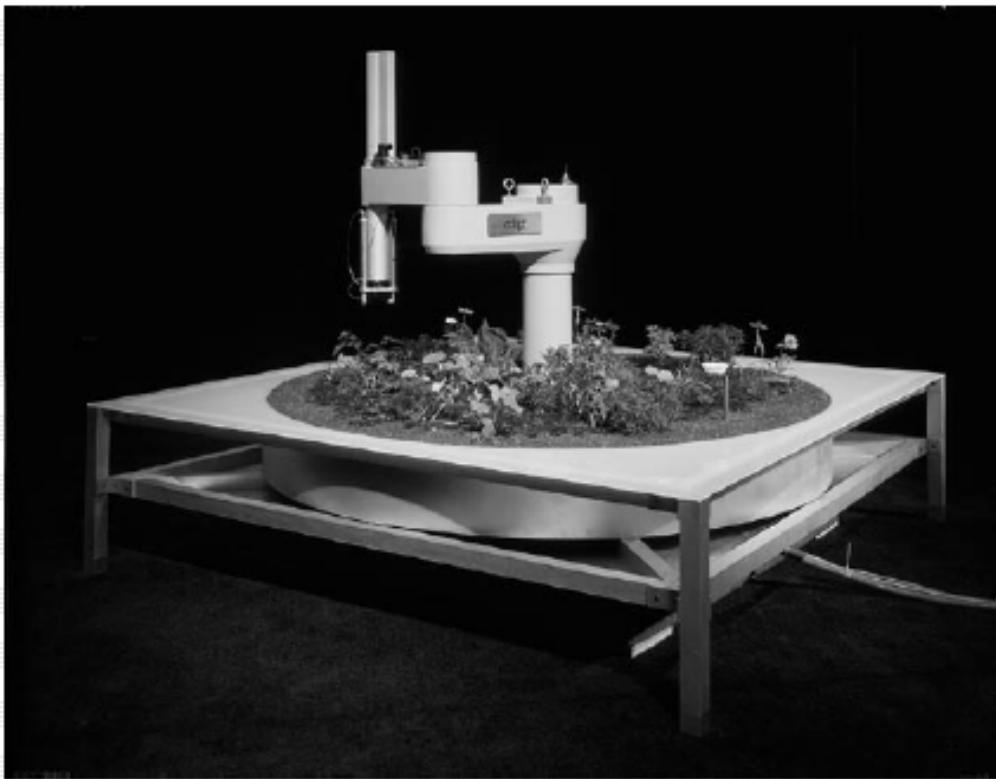
Orientation.



Every velocity response
differ more for dimension

Other Task Requirements

- Workspace
 - Scale and precise shape
- Load Capacity
 - Sizing of structural members
- Speed
- Accuracy and Precision



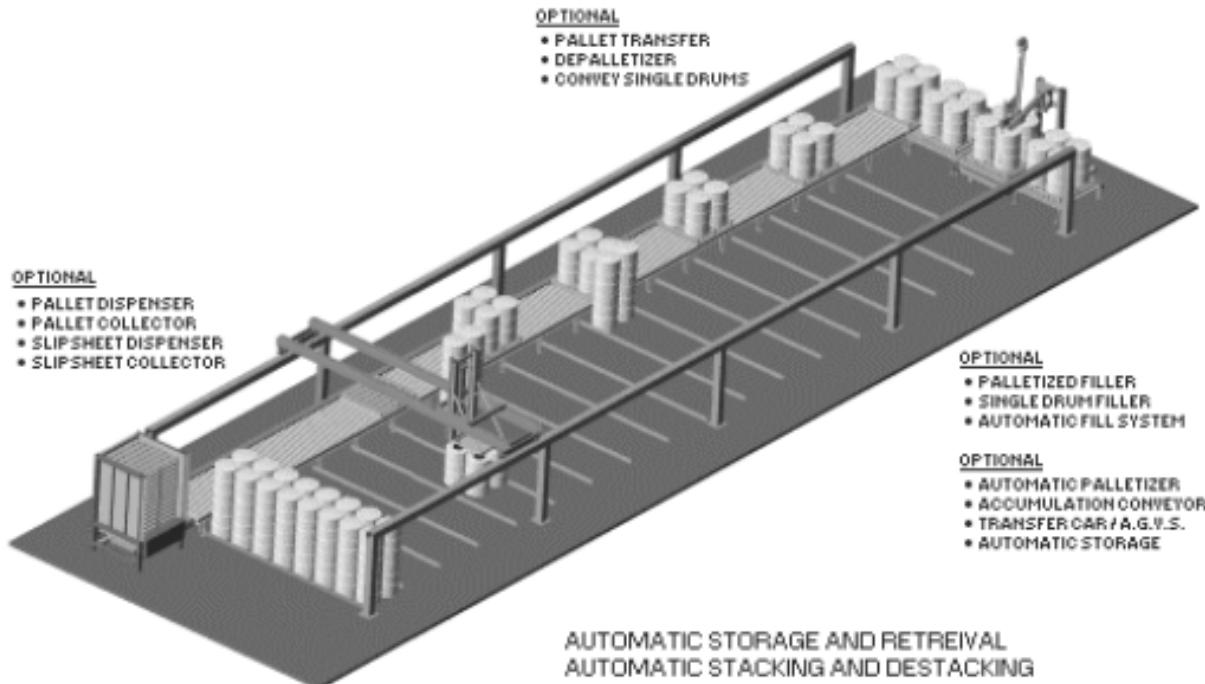
Telegarden (Goldberg, UC Berkeley)

Kinematic Configurations

- Decide degrees of freedom first
- Then choose kinematic configuration to obtain the best
 - Workspace
 - Dynamic properties
 - Use of actuators and sensors
 - Accuracy
- A general, 6dof manipulator is usually classified by the first 3 dof plus a wrist

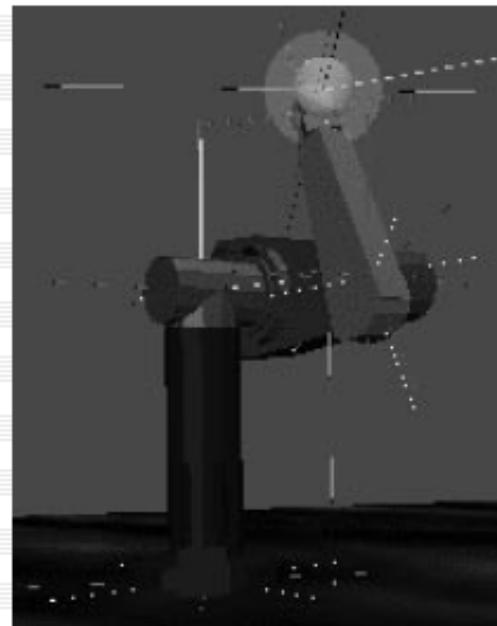
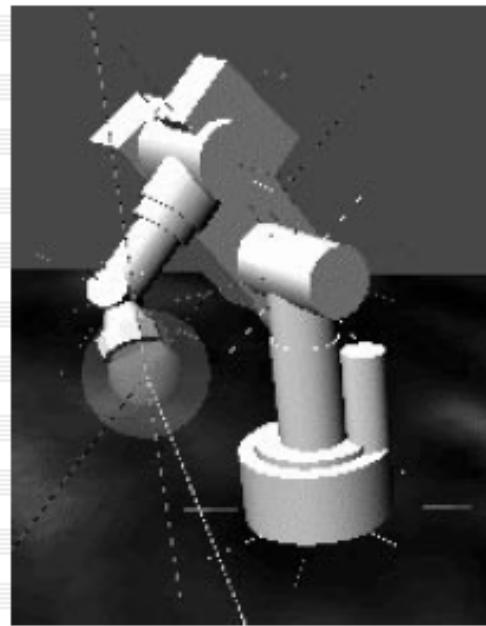
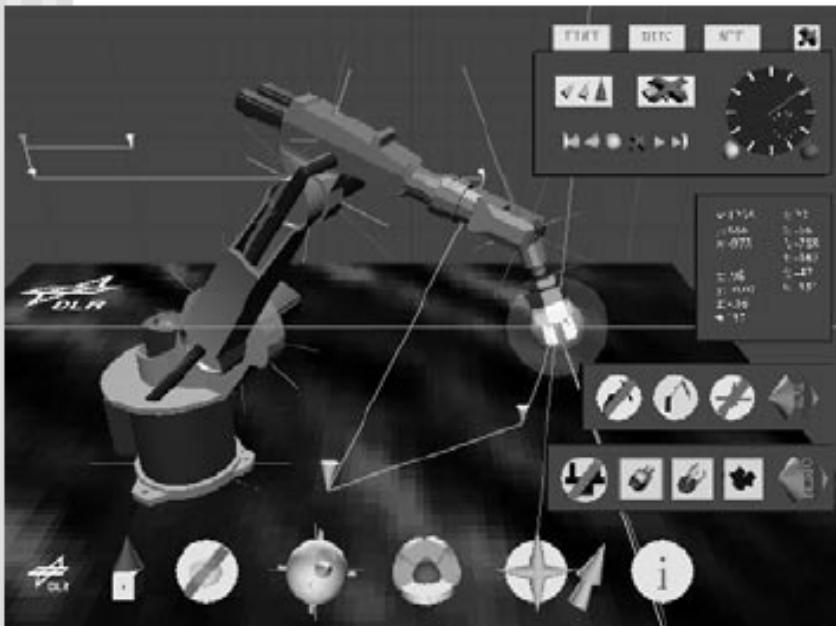
Cartesian Manipulator

- Joints 1, 2, and 3 are prismatic
- Mutually Orthogonal
- Decoupled x, y, and z
- Often used for gantry robots



Articulated Manipulator

- Also called jointed, elbow, or anthropomorphic manipulator
- Least intrusion into the workspace



VRML models from Gerd Hirzinger

Workspace Attributes

■ Design efficiency

- How much material is needed to build different designs with the same workspace?

- Length sum

$$L = \sum_{i=1}^N (a_{i-1} + d_i)$$

- Structural

length
index

$$Q_L = \frac{L}{\sqrt[3]{W}}$$

(W = workspace volume, d_i = distance between joint limits)

Condition of Workspace

- When the manipulator is near a singular point, actions of the manipulator are said to be ***poorly conditioned.***
- Singular conditions are given by

$$\det(J(\theta)) = 0$$

- Thus, use the Jacobian as a measure of manipulator dexterity

Manipulability Measure (vel)

- Yoshikawa defines manipulability as

$$w = \sqrt{\det(J(\theta)J^T(\theta))}$$

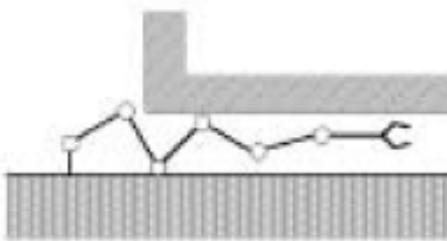
- For a nonredundant manipulator

$$w = |\det(J(\theta))|$$

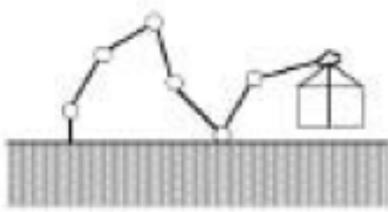
- A good manipulator has a high w over large areas of its workspace

Redundant structures

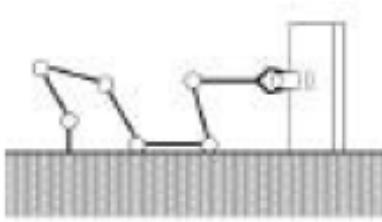
- Can be useful for avoiding collisions while operating in cluttered work environments



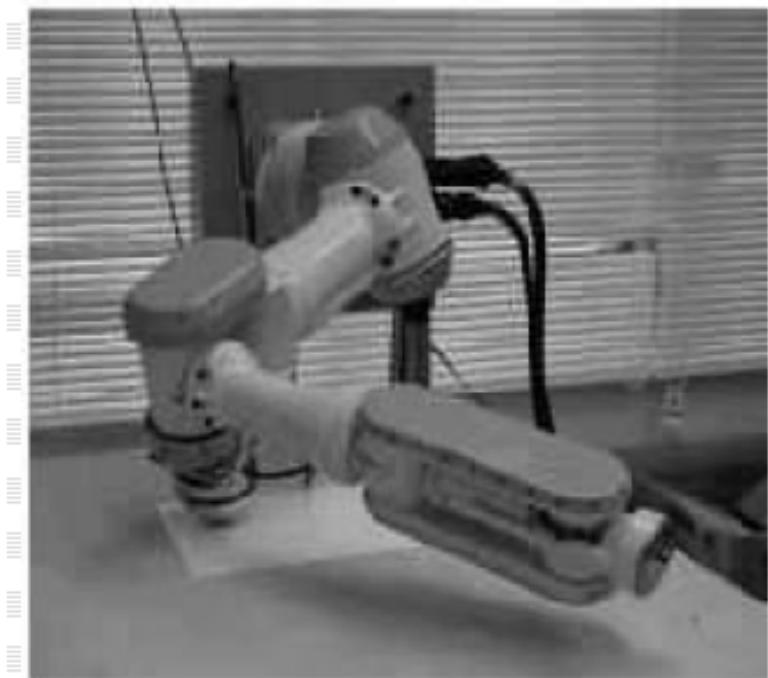
Task A : End point path tracking in narrow space



Task B : Handling heavy load



Task C : Assembling of the precision part



Reduction & Transmission

- **Gears** produce large reductions in a compact configuration

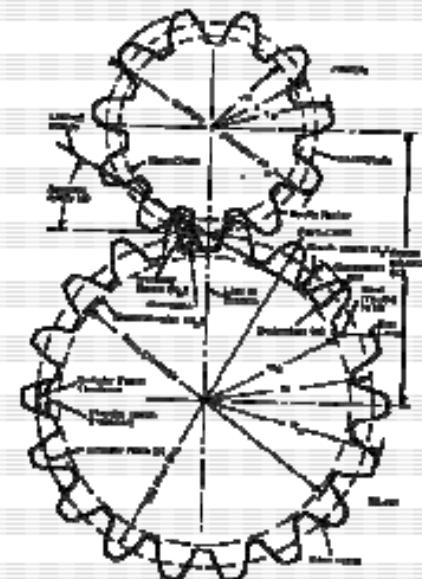
- Disadvantages:
backlash and friction

- Gear ratio: relationship between input and output speeds & torques

$$\eta > 1$$

$$\dot{\theta}_o = \frac{\dot{\theta}_i}{\eta}$$

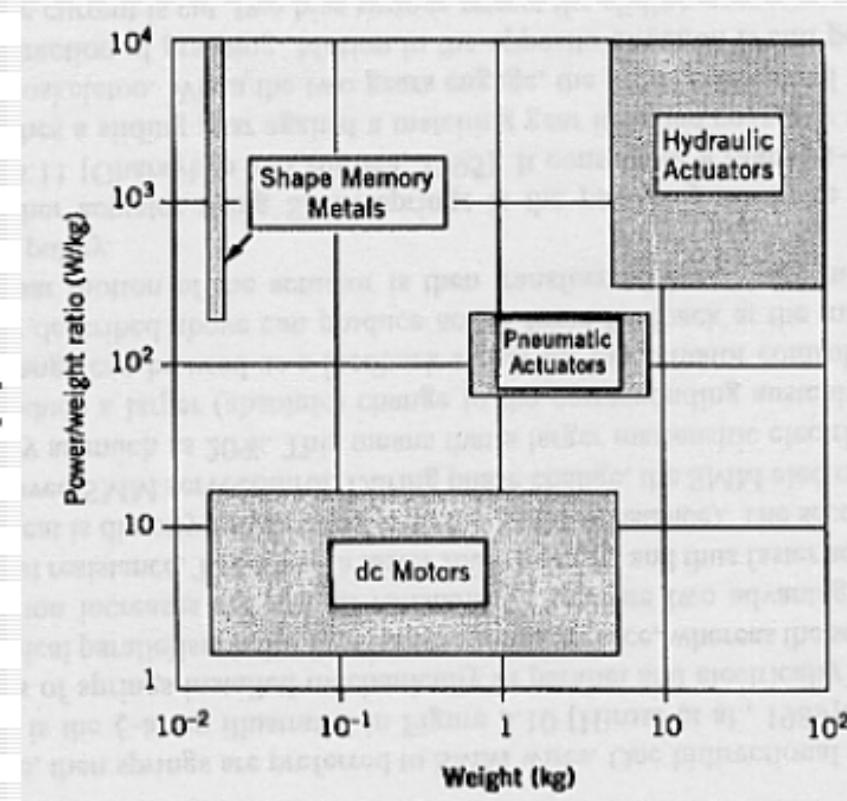
$$\tau_o = \eta \tau_i$$



Frank Buchsbaum

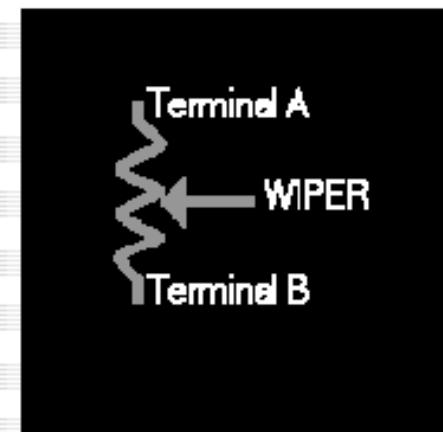
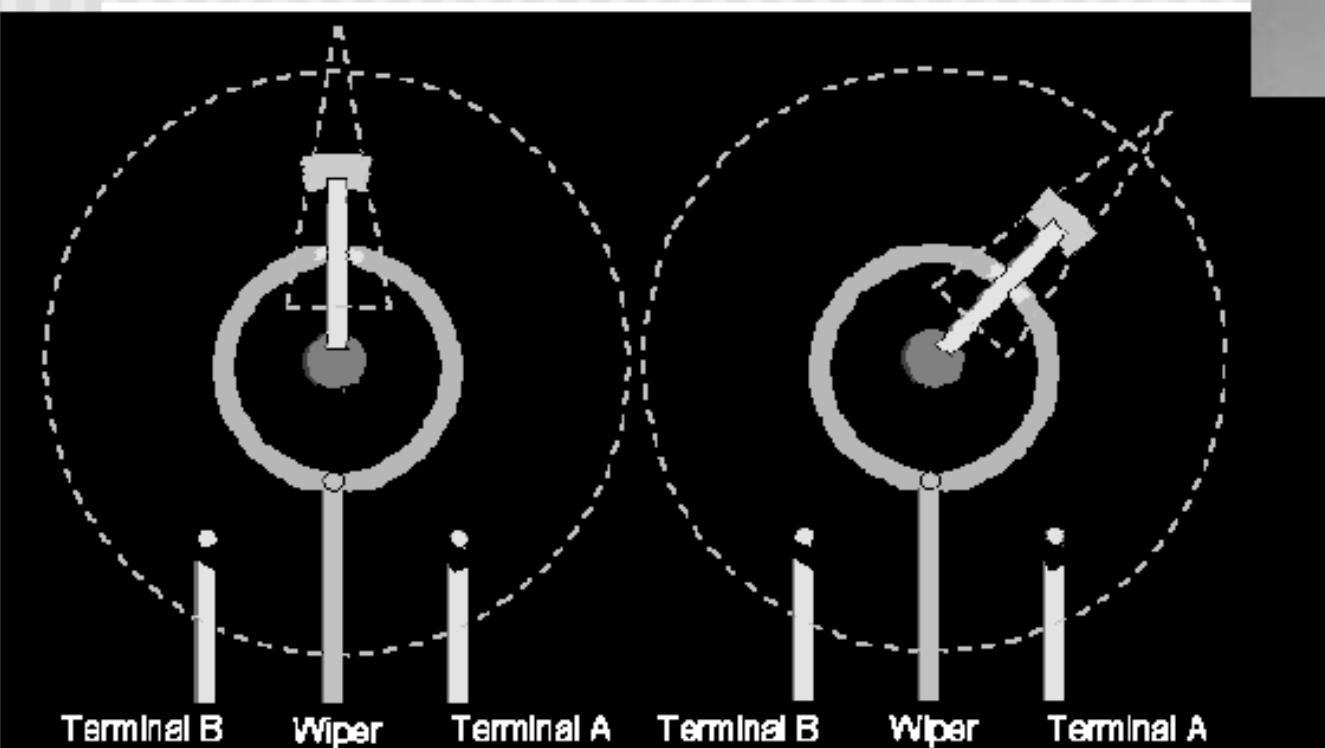
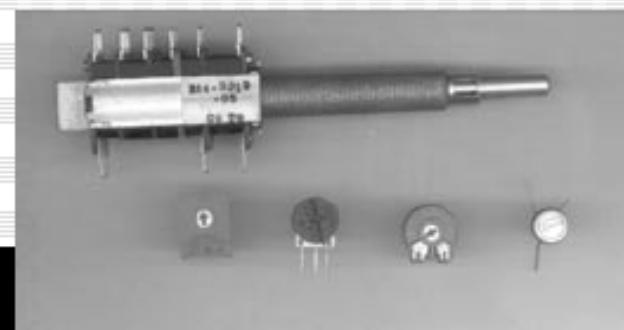
Actuator Types

- Electric motors
 - DC (direct current)
 - Brushed
 - PM (permanent magnet)
- Pneumatic Actuators



Potentiometers

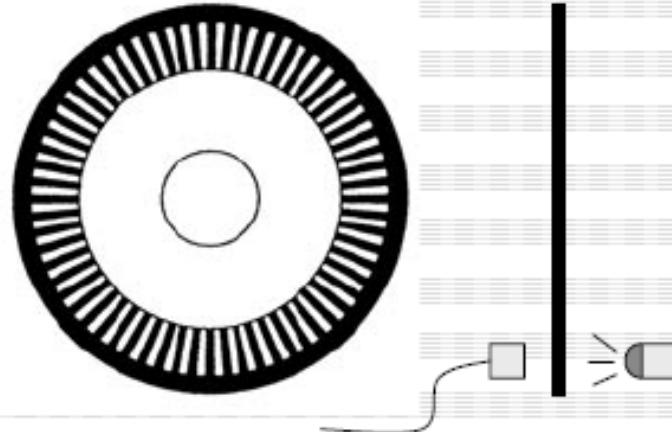
- Produce a voltage proportional to shaft position
- Voltage divider



Potentiometers

- Problems:
 - Friction (for backdriveable systems like haptic devices)
 - Noise
 - Resolution
 - Linearity

Optical Encoders

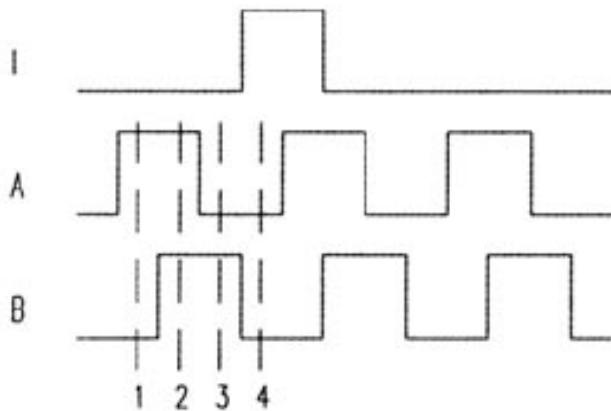
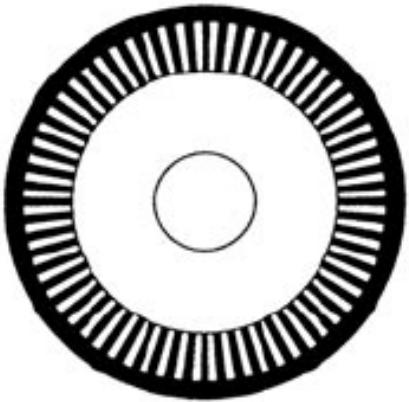


- How do they work?
 - A focused beam of light aimed at a matched photodetector is interrupted periodically by a coded pattern on a disk
 - Produces a number of pulses per revolution (Lots of pulses = high cost)
- Quantization problems at low speeds
- Absolute vs. referential

- (1) * 不同問題， θ 和 $\vec{r} \Rightarrow J$
- (2) 2 章的 chart sheet
- (3) 可能會有 position control 的性質
- (4) Inverse kinematic \Rightarrow how to use J
- (5) no pencil

Optical Encoders

■ Phase-quadrature encoder



State	Ch A	Ch B
S ₁	High	Low
S ₂	High	High
S ₃	Low	High
S ₄	Low	Low

- 2 channels, 90° out of phase
 - allows sensing of direction of rotation
 - 4-fold increase in resolution