

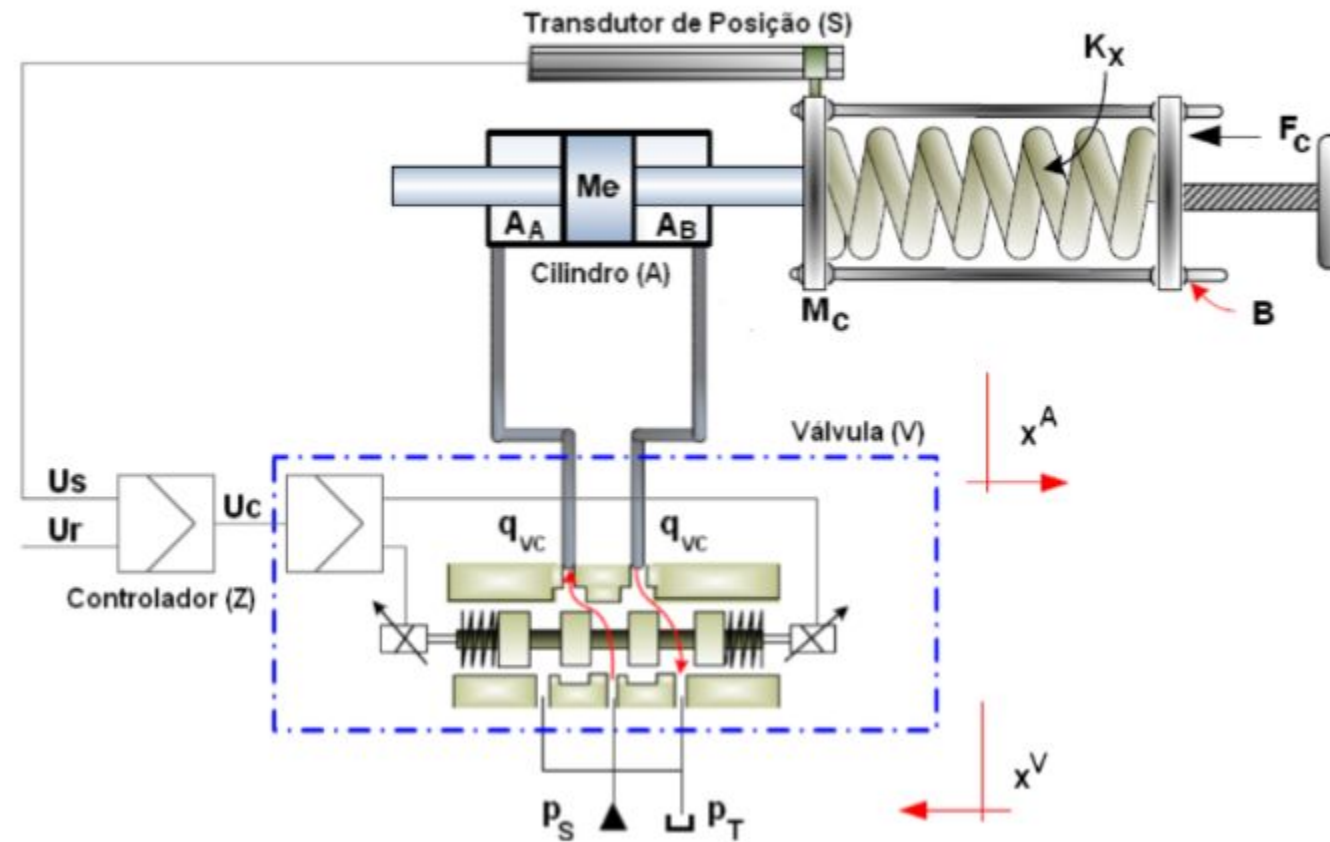


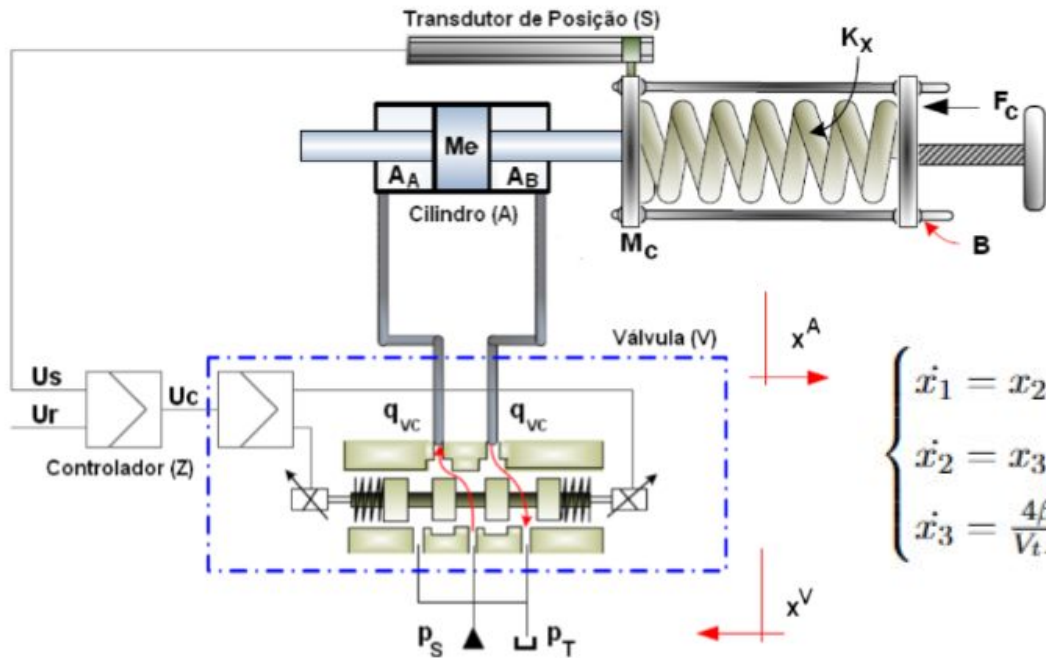
Controle Robusto - DAS410067

Controle de posição de um cilindro hidráulico

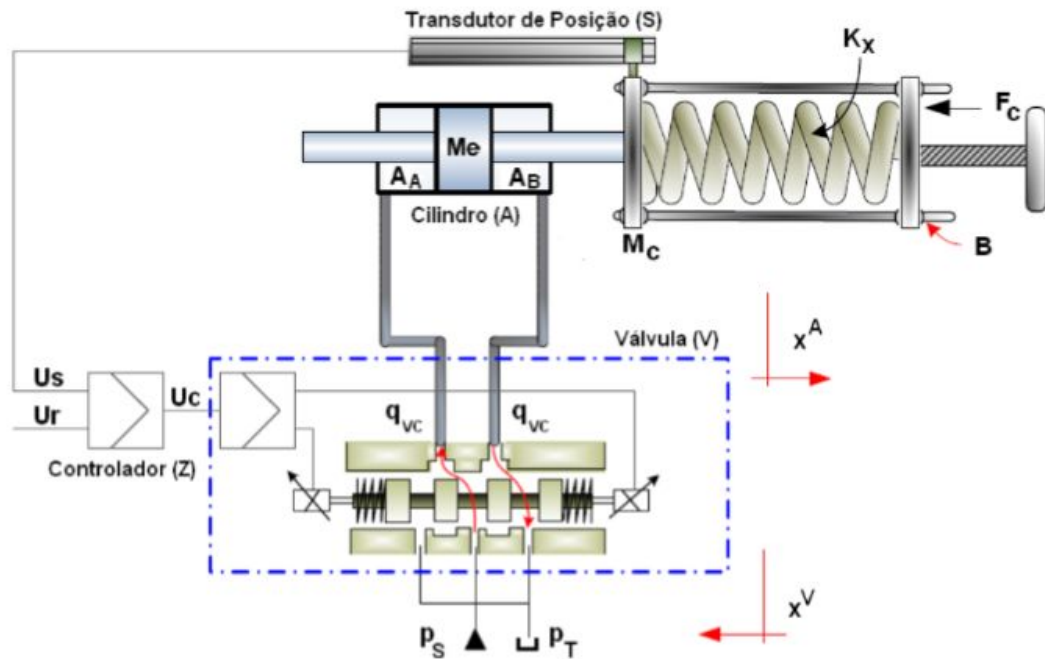
Guilherme Henrique Ludwig

02 de outubro de 2023





$$\begin{cases} \dot{x}_1 = x_2 \\ \dot{x}_2 = x_3 \\ \dot{x}_3 = \frac{4\beta A}{V_t M_e} \left[\left(U_c k_{q0} - \frac{F_C k_{c0}}{A} \right) - x_3 \left(\frac{V_t B}{4\beta A} + \frac{M_e k_{c0}}{A} \right) - x_2 \left(A + \frac{V_t K_x}{4\beta A} + \frac{B k_{c0}}{A} \right) - x_1 \frac{K_x}{A} k_{c0} \right] \end{cases}$$

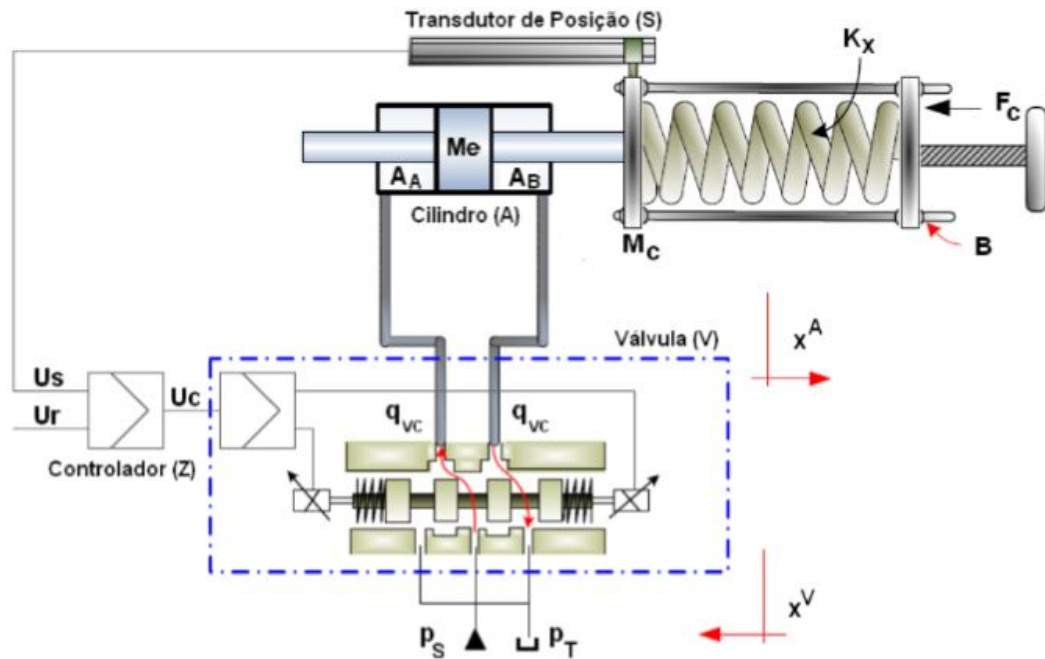


$$A = \begin{pmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -\frac{K_x k_{c0} 4\beta}{V_t M_e} & -\left(\frac{A^2 4\beta}{V_t M_e} + \frac{K_x}{M_e} + \frac{B k_{c0} 4\beta}{V_t M_e}\right) & -\left(\frac{B}{M_e} + \frac{k_{c0} 4\beta}{V_t}\right) \end{pmatrix},$$

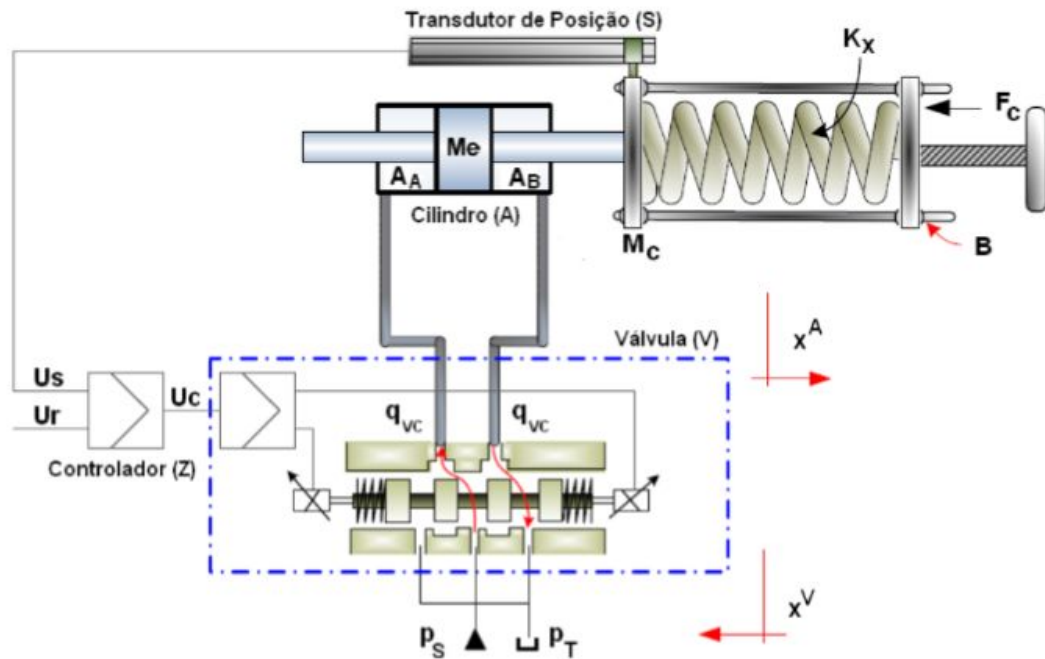
$$B_u = \begin{pmatrix} 0 \\ 0 \\ \frac{4\beta A k_{q0}}{V_t M_e} \end{pmatrix},$$

$$B_w = \begin{pmatrix} 0 \\ 0 \\ -\frac{4\beta k_{c0}}{V_t M_e} \end{pmatrix},$$

$$C = \begin{pmatrix} 1 & 0 & 0 \end{pmatrix},$$



$$\begin{cases} \dot{x} = Ax + B_u u + B_w w \\ y = Cx \end{cases}$$

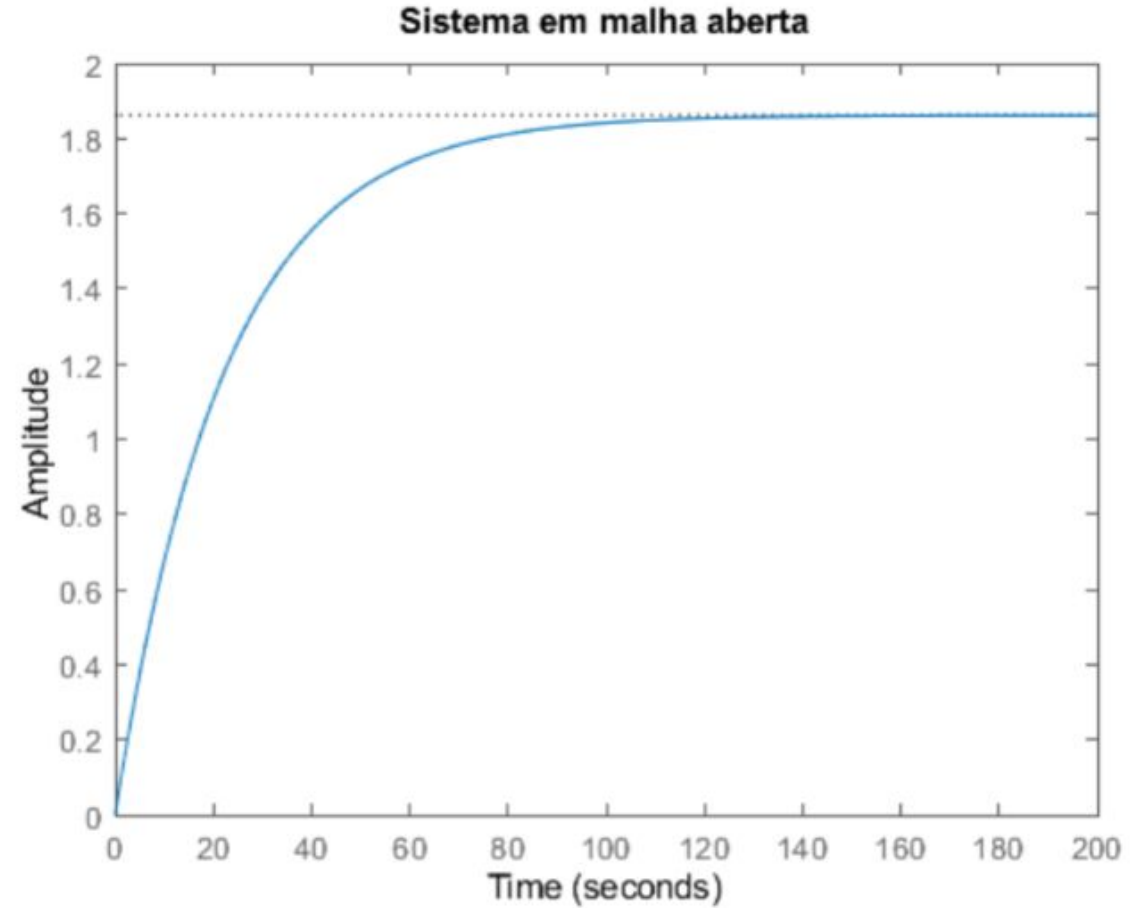
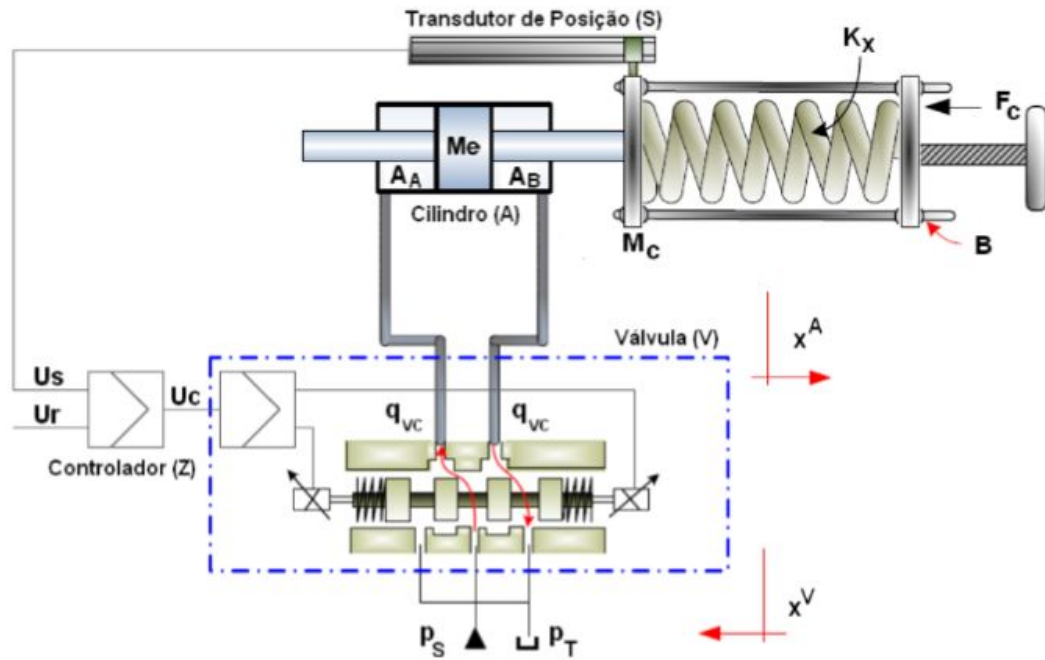


$$AA = \begin{pmatrix} A & \text{zeros}(3, 1) \\ -C & 0 \end{pmatrix}$$

$$B_{uA} = \begin{pmatrix} B_u \\ 0 \end{pmatrix}$$

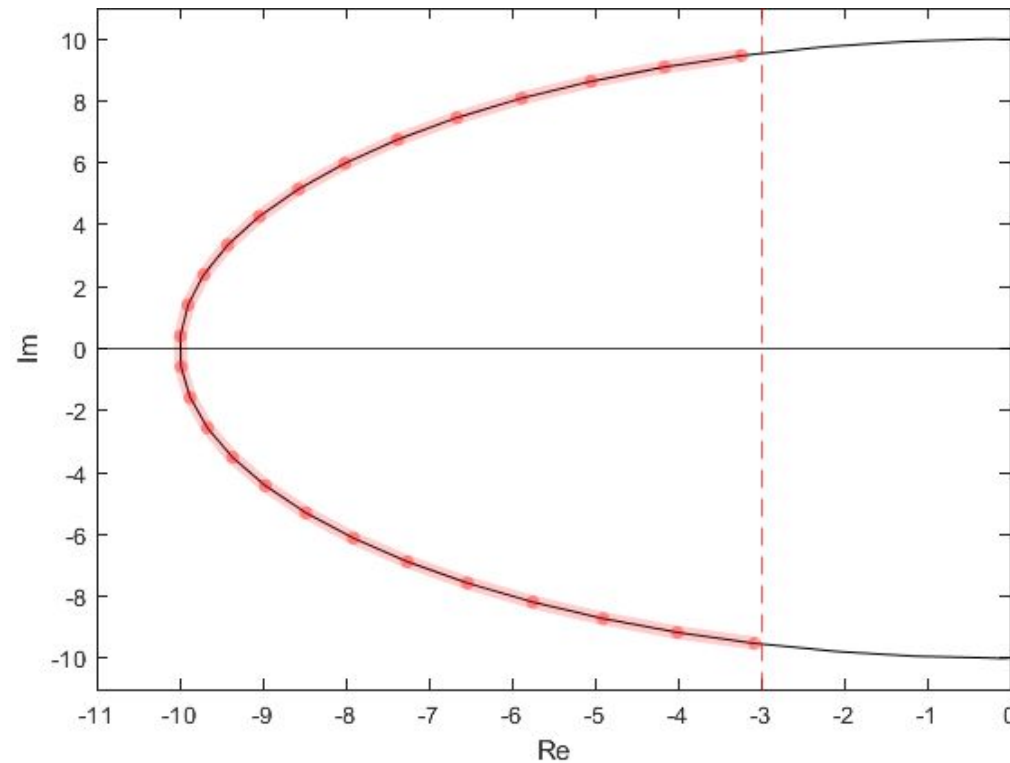
$$B_{wA} = \begin{pmatrix} B_w \\ 0 \end{pmatrix}$$

$$C = \begin{pmatrix} C_A & 0 \end{pmatrix}$$

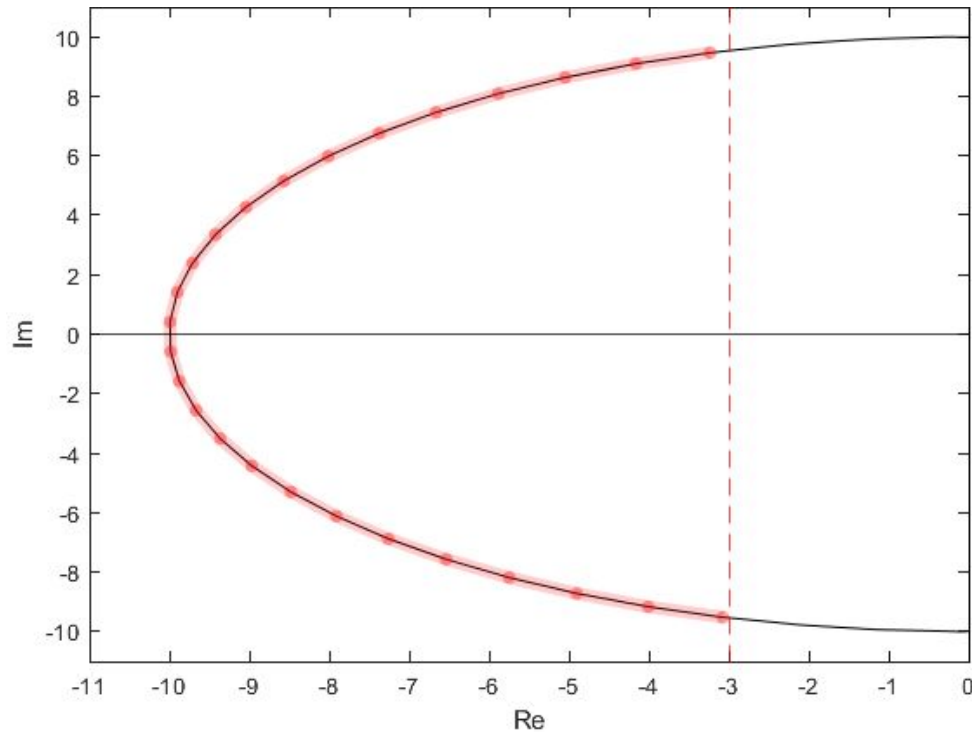


1. Tempo de 5% em malha fechada ≤ 1 segundo
2. Rejeição de perturbações degrau em regime permanente
3. Sobressinal máximo de 5%

Após alguns cenários de simulação e projeto no Matlab, definiu-se que os polos de malha fechada deveriam estar dentro de uma circunferência de raio 10 e ter parte real menor que -3.



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$$L_1 = 6,$$

$$M_1 = 1,$$

$$L_2 = \begin{pmatrix} -10 & 0 \\ 0 & -10 \end{pmatrix},$$

$$M_2 = \begin{pmatrix} 0 & 1 \\ 0 & 0 \end{pmatrix}.$$

Além disso, supôs-se que o sistema pode apresentar incerteza na estimação na constante K_x da mola de retorno de até 2%. Ou seja, definiu-se o vetor PS e matriz A_1 :

$$PS = \begin{pmatrix} 0.02 & -0.02 \end{pmatrix}$$

$$A_1 = \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ -\frac{K_x k_c 0.4 \beta}{V_t M_e} & -\frac{K_x}{M_e} & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

Definiu-se as LMIs:

$$\gamma - \text{trace}(M) \geq 0,$$

$$\begin{pmatrix} M & (C_A P + DW) \\ (C_A P + DW)' & P \end{pmatrix} \geq 0,$$

$$(A_d P + B_{uA} W) + (A_d P + B_{uA} W)' + B_{wA} B_{wA}' \leq 0,$$

$$L_1 \otimes P + M_1 \otimes (A_d P + B_{uA} W) + M_1' \otimes (A_d P + B_{uA} W)' \leq 0,$$

$$L_2 \otimes P + M_2 \otimes (A_d P + B_{uA} W) + M_2' \otimes (A_d P + B_{uA} W)' \leq 0$$

sendo $A_d = A_A + PS(i)A_1$.

