Moving Loads Assignment - Part A

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```
In [1]: import numpy as np
    import sympy as sym
    import matplotlib.pyplot as plt
    import matplotlib.animation as animation
    from scipy.integrate import quad
    from matplotlib.ticker import ScalarFormatter
```

Problem 1

First, the wave numbers and their corresponding waves are derived for a beam on elastic foundation. This is to help with interpretation.

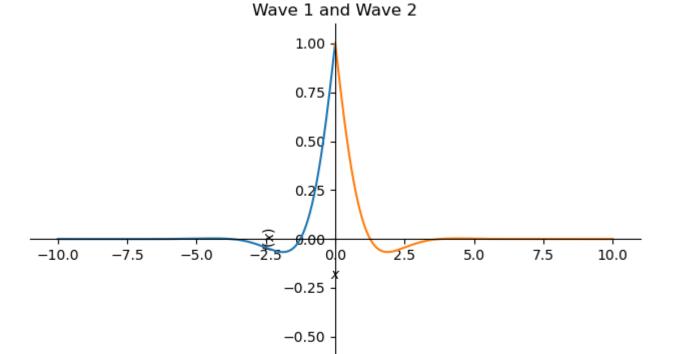
```
In [2]: # define equation parameters
         x, t = sym.symbols('x t', real=True)
         rho, A, EI, ksi = sym.symbols('rho A EI ksi', positive=True)
         # define numerical values (taken from the provided example)
         values = {EI:6.42E6, rho:1, A: 268.33, ksi: 8.333E7}
         omega, k = sym.symbols('omega k')
         w = sym.Function('w')(x, t)
         w = sym.exp(-sym.I * (omega*t - k*x))
         # define the equation of motion
         EQM = sym.Eq(rho*A * sym.diff(w, t, 2) + EI * sym.diff(w, x, 4) + ksi * w, 0)
In [3]: # define the dispersion relation
         display(EQM.simplify())
         disp_eq = EI*k**4 - omega**2 * rho*A + ksi
         display(disp_eq.simplify())
       \left(-A\omega^2\rho + EIk^4 + ksi\right)e^{i(kx-\omega t)} = 0
       -A\omega^2 
ho + EIk^4 + ksi
In [4]: # solve the dispersion relation for k
         k_sol = sym.solve(disp_eq, k)
         for k in k_sol:
             display(k)
         # calculate the cut-off frequency
         wc = np.sqrt(values[ksi]/(values[rho]*values[A]))
         \sqrt[4]{A\omega^2\rho - ksi}
```

$$-rac{\sqrt[4]{A\omega^2
ho-ksi}}{\sqrt[4]{EI}} \ rac{\sqrt[4]{A\omega^2
ho-ksi}}{\sqrt[4]{EI}}$$

```
-rac{i\sqrt[4]{A\omega^2
ho-ksi}}{\sqrt[4]{EI}} \ rac{i\sqrt[4]{A\omega^2
ho-ksi}}{\sqrt[4]{EI}}
```

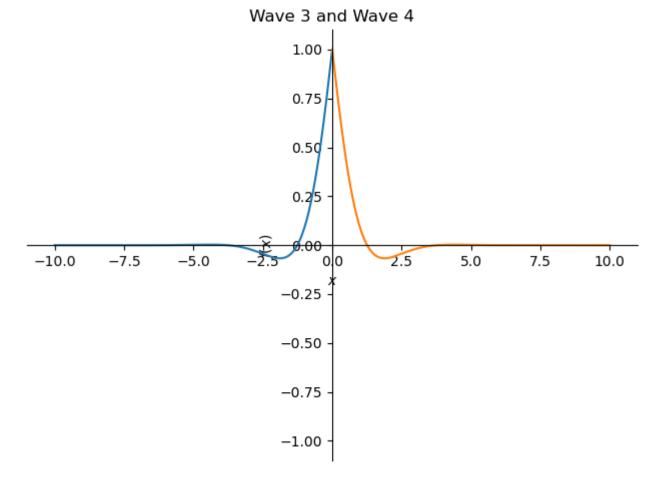
```
In [5]: # Plot the steady state response for relatively low frequency
  omega_val = 0.5*wc # Set a value for omega
  wave1 = sym.exp(sym.I * k_sol[0]*x).subs(values).subs({omega: omega_val})
  wave2 = sym.exp(sym.I * k_sol[1]*x).subs(values).subs({omega: omega_val})
  wave3 = sym.exp(sym.I * k_sol[2]*x).subs(values).subs({omega: omega_val})
  wave4 = sym.exp(sym.I * k_sol[3]*x).subs(values).subs({omega: omega_val})

sym.plot((sym.re(wave1), (x,0,-10)), (sym.re(wave2), (x,10,0)), title='Wave 1 and Wave 2', sho sym.plot((sym.re(wave3), (x,0,-10)), (sym.re(wave4), (x,10,0)), title='Wave 3 and Wave 4', sho
```



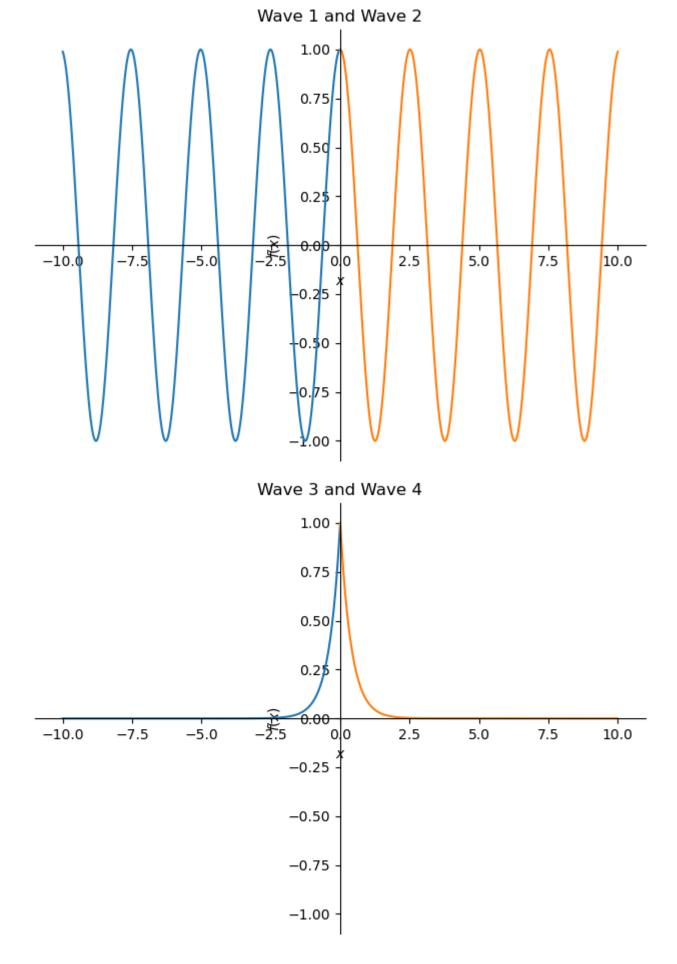
-0.75

-1.00



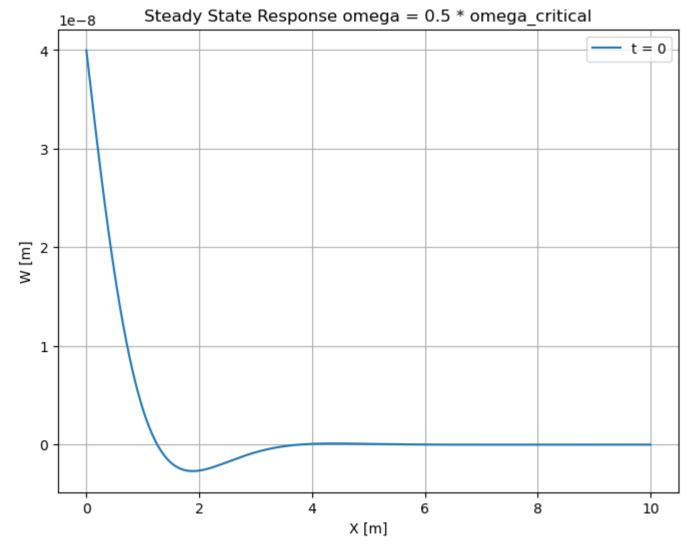
```
In [6]: # Plot the steady state response for relatively low frequency
    omega_val = 2*wc # Set a value for omega
    wave1 = sym.exp(sym.I * k_sol[0]*x).subs(values).subs({omega: omega_val})
    wave2 = sym.exp(sym.I * k_sol[1]*x).subs(values).subs({omega: omega_val})
    wave3 = sym.exp(sym.I * k_sol[2]*x).subs(values).subs({omega: omega_val})
    wave4 = sym.exp(sym.I * k_sol[3]*x).subs(values).subs({omega: omega_val})

sym.plot((sym.re(wave1), (x,0,-10)), (sym.re(wave2), (x,10,0)), title='Wave 1 and Wave 2', she sym.plot((sym.re(wave3), (x,0,-10)), (sym.re(wave4), (x,10,0)), title='Wave 3 and Wave 4', she
```

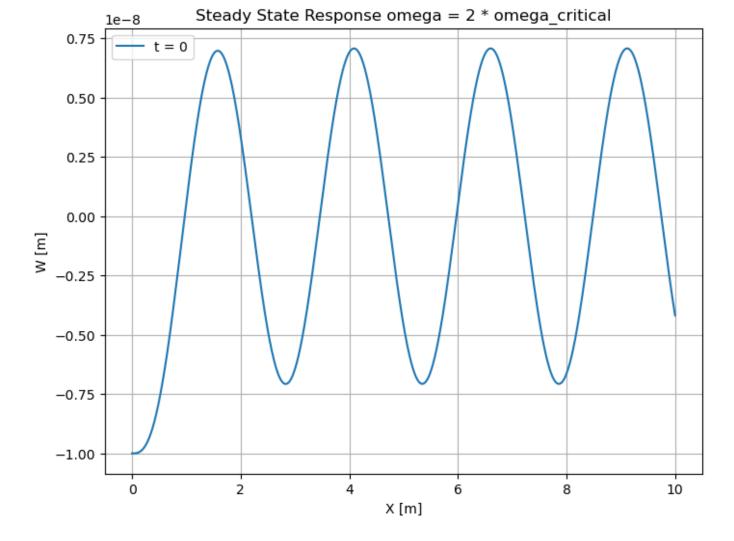


- For frequencies smaller than the cut-off frequency, the steady state response consists of standing waves.
- For frequencies larger than the cut-off frequency, the steady state response consists of two standing waves, and two propagating waves.

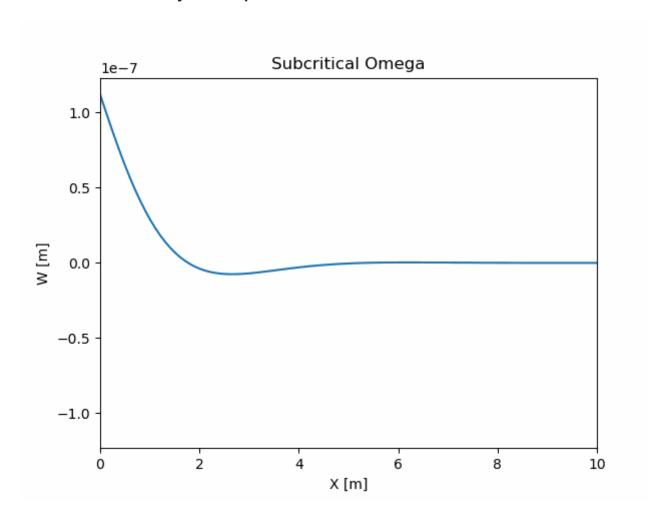
```
In [7]: W = sym.Function('W')(x)
          C1, C2, C3, C4 = sym.symbols('C1 C2 C3 C4')
          F0, wc = sym.symbols('F0 wc')
          W = C1*sym.exp(sym.I*k sol[0]*x) + C2*sym.exp(sym.I*k sol[1]*x) + C3*sym.exp(sym.I*k sol[2]*x)
          display(W)
          # Define boundary conditions
          # No moment at x=0
          eq1 = sym.Eq(W.diff(x,x).subs(x,0),0)
          # Force F0 at x=0
          eq2 = sym.Eq(W.diff(x,x,x).subs(x,0), F0/EI)
          # Radiation conditions at infinity
          eq3 = sym.Eq(C1,0)
          eq4 = sym.Eq(C3,0)
          sol = sym.solve([eq1, eq2, eq3, eq4], (C1, C2, C3, C4))
          sol
                                        x\sqrt[4]{A\omega^2\rho-ksi}
                          ix\sqrt[4]{A\omega^2\rho-ksi}
             ix\sqrt[4]{A\omega^2\rho-ksi}
        C_1e^{-\frac{4\sqrt{EI}}{\sqrt[4]{EI}}}+C_2e^{-\frac{4\sqrt{EI}}{\sqrt[4]{EI}}}+C_3e^{-\frac{4\sqrt{EI}}{\sqrt[4]{EI}}}+C_4e^{-\frac{4\sqrt{EI}}{\sqrt[4]{EI}}}
 Out[7]: {C1: 0,
           C2: -F0*(1 - I)/(2*EI**(1/4)*(A*omega**2*rho - ksi)**(3/4)),
           C4: -F0*(1 - I)/(2*EI**(1/4)*(A*omega**2*rho - ksi)**(3/4))
 In [8]: W = W.subs(sol)
          values = {EI:6.42E6, rho:1, A: 268.33, ksi: 8.333E7, F0: 1}
          wc = np.sqrt(values[ksi]/(values[rho]*values[A]))
 In [9]: omega_val = 0.5*wc
          W_time = sym.re(W.subs(values)*sym.exp(sym.I*omega*t)).subs(omega, omega_val)
In [10]: W_plot = sym.lambdify([x, t], W_time, "numpy")
          # Define a fixed moment in time
          fixed time = 0 # You can change this value to any desired time
          # Generate x values for the plot
          x_{values} = np.linspace(0, 10, 1000)
          # Compute W_plot values at the fixed time
          W values = W plot(x values, fixed time)
          # Plot the results
          plt.figure(figsize=(8, 6))
          plt.plot(x_values, W_values, label=f't = {fixed_time}')
          plt.xlabel('X [m]')
          plt.ylabel('W [m]')
          plt.title('Steady State Response omega = 0.5 * omega critical')
          plt.legend()
          plt.grid(True)
          plt.show()
```

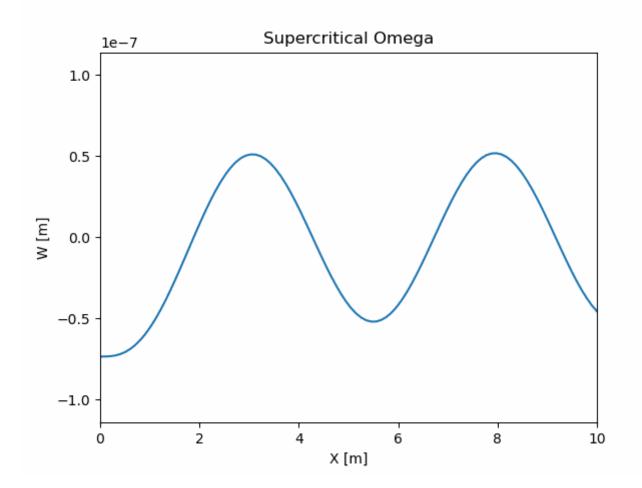


```
In [11]: omega_val = 2.0*wc
         W_time = sym.re(W.subs(values)*sym.exp(sym.I*omega*t)).subs(omega, omega_val)
In [12]: W_plot = sym.lambdify([x, t], W_time, "numpy")
         # Define a fixed moment in time
         fixed_time = 0 # You can change this value to any desired time
         # Generate x values for the plot
         x_{values} = np.linspace(0, 10, 1000)
         # Compute W_plot values at the fixed time
         W_values = W_plot(x_values, fixed_time)
         # Plot the results
         plt.figure(figsize=(8, 6))
         plt.plot(x_values, W_values, label=f't = {fixed_time}')
         plt.xlabel('X [m]')
         plt.ylabel('W [m]')
         plt.title('Steady State Response omega = 2 * omega_critical')
         plt.legend()
         plt.grid(True)
         plt.show()
```



Animations of the steady state response





The steady state response for subcritical omega consists of standing waves only: There is no energy propagting away from the source.

The steady state response for supercritical omega consist of a standing wave and a propagating wave. The standing wave is only of significance close to the source, whilst the propagting wave is visible all the way to infinity.

The standing waves and propagting waves derived in the first part of this problem can be recognized.

```
In [13]: # code for creating animations
# fig, ax = plt.subplots()

# t = np.linspace(0, 2*np.pi/omega_val, 50)
# x = np.linspace(0, 10, 100)

# W_max = np.max(W_plot(0, t))

# line = ax.plot(x, W_plot(x, t[0]))[0]
# ax.set(xlim=[0, 10], ylim=[-1.1*W_max, 1.1*W_max], xlabel='X [m]', ylabel='W [m]', title='Su'

# def update(frame):
# w = W_plot(x, t[frame])

# line.set_ydata(w)
# return (line)

# anim = animation.FuncAnimation(fig=fig, func=update, frames=50, interval=50)
# anim.save(filename="./omega_subcritical.gif", writer="pillow");
# plt.close()
```

Problem 2

The Equation of motion of the system in this problem is:

$$\rho A \frac{\partial^2 w}{\partial t^2} + EI \frac{\partial^4 w}{\partial x^4} + \chi w + \eta \frac{\partial w}{\partial t} = Q_0 \delta(x - Vt)$$
 (1)

In order to obtain the steady-state response of the system, we first apply the Fourier Transform in both space and time to the equation:

$$(-\rho A\omega^2 + EIk^4 + \chi + i\eta)\tilde{w}(k,\omega) = 2\pi Q_0 \delta(\omega - kV)$$
(2)

$$ilde{w}(k,\omega) = rac{2\pi Q_0 \delta(\omega - kV)}{-\rho A \omega^2 + EIk^4 + \chi + i\eta} ag{3}$$

in which

$$ilde{w}(k,\omega) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} w(x,t) \mathrm{e}^{-\mathrm{i}(\omega t - kx)} dx dt$$
 (4)

The solution in the space-frequency domain is:

$$\hat{w}(x,\omega) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} 2\pi \frac{Q_0}{EI} \frac{\delta(\omega - kV)}{\Delta(\omega, k)} e^{-ikx} dk \stackrel{k = \frac{\omega}{V}}{=} \frac{1}{V} \frac{Q_0}{EI} \frac{e^{-i\frac{\omega}{V}x}}{\Delta(\omega, V)}$$
(5)

and in space-time domain, with the moving reference frame substituted:

$$w(\xi) = \frac{1}{2\pi} \frac{1}{V} \frac{Q_0}{EI} \int_{-\infty}^{+\infty} \frac{e^{-i\frac{\omega}{V}\xi}}{\Delta(\omega, V)} d\omega$$
 (6)

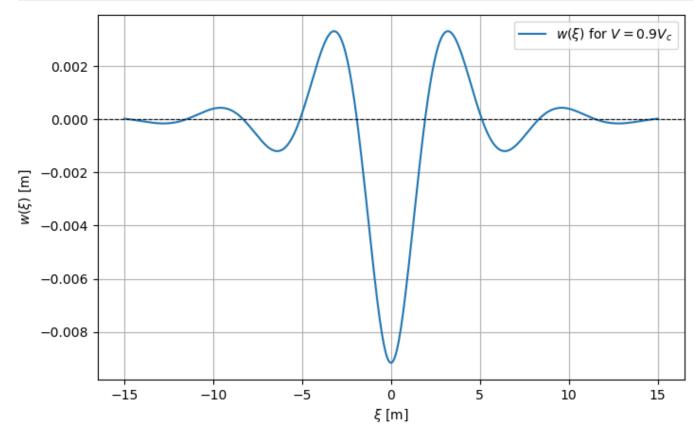
in which:

$$\Delta(\omega, V) = \left(\frac{\omega}{V}\right)^4 - \frac{\rho A}{EI}\omega^2 + i\frac{\eta}{EI}\omega + \frac{\chi}{EI}$$
 (7)

The integration in the solution can be computed numerically, and plots are shown below.

```
In [14]: # Define constants
         rhoA = 268.3
         EI = 6.42e6
         chi = 7.3e6
         eta = 1e2
         Q0 = 80e3
         Vc = (4 * chi * EI / (rhoA**2))**(1/4)
         V = 0.9 * Vc
         # Integrand
         def integrand(omega, xi):
             Delta = (omega / V)**4 - (rhoA / EI) * omega**2 + (chi / EI) + 1j * eta / EI
             return np.exp(-1j * omega * xi / V) / Delta
         # Calculate the w_xi function with numerical integration
         def w xi func(xi):
             result, _ = quad(lambda omega: integrand(omega, xi).real, -1000, 1000)
             return (1 / (2 * np.pi * V * EI)) * Q0 * result
         # Plot
         xi_vals = np.linspace(-15, 15, 500)
         w_xi_vals = np.array([w_xi_func(xi) for xi in xi_vals])
         plt.figure(figsize=(8, 5))
         plt.plot(xi vals, -w xi vals, label=r"$w(\xi)$ for $V = 0.9V c$")
         plt.axhline(0, color='black', linewidth=0.8, linestyle='--')
```

```
plt.xlabel(r"$\xi$ [m]")
plt.ylabel(r"$w(\xi)$ [m]")
plt.legend()
plt.grid()
plt.show()
```



Problem 3

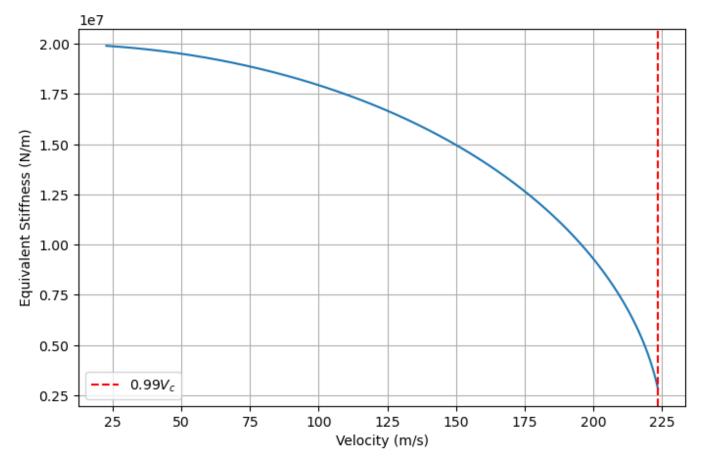
For the same problem considered in the previous question, derive and compute the equivalent stiffness at the loading/contact point and plot it versus velocity. Consider in the plot only the sub-critical velocity range (up to the 99% of the critical velocity) and explain what you observe.

The equivalent stiffness under the moving load is:

$$k_{\rm eq} = \frac{Q_0}{w(\xi = 0)} \tag{8}$$

The deflection under the moving load depends on the speed of the moving load. The result is plotted below. The general trend is obvious, that when the speed approaches critical speed, the equivalent stiffness drops significantly. It does not go to zero as an viscous damping is included in the model. On the other side, when the speed is very small, the equivalent stiffness approaches the static stiffness.

```
plt.xlabel("Velocity (m/s)")
plt.ylabel("Equivalent Stiffness (N/m)")
plt.legend()
plt.grid()
plt.show()
```



Problem 4

Firstly, the material constants are defined as in the assignment.

```
In [16]: Q0 = 80E3
EI = 6.42E6
rhoA = 268.3
L = 100
xi = 7.3E6
zeta = 0.05

V_crit = ((4*xi*EI)/(rhoA)**2)**(1/4)
V = 0.75*V_crit
```

In order to solve the response of simply supported beam, the modal expansion method is used, and solution to problem is:

$$w(x,t) = \sum_{m=1}^{\infty} q_m(t) \sin(\beta_m x)$$
 (9)

in which $\sin(\beta_m x)$ is the mode shapes for m_{th} mode and can be computed easily as follows:

```
In [17]: def beta(n):
    return np.pi * n / L

def mode_shape(x, n):
    return np.sin(beta(n) * x)
```

 $q_m(t)$ is the time-dependant amplitude for each mode. It can be computed using the green's function

method, in which q_m is obtained by:

$$q_m = \int_{\tau=0}^{t} f_m(\tau) g_m(t-\tau) d\tau \tag{10}$$

where the modal forcing f_m and modal green's function g_m are expressed as:

$$f_m(t) = \frac{Q_0 B(t) \varphi_m(Vt)}{\bar{m}_m} \tag{11}$$

$$g_m(t) = \frac{1}{\omega_m} \sin(\omega_m t) H(t)$$
 (12)

Terms mentioned above thus can be defined:

```
In [18]: def omega(n):
    return np.sqrt(beta(n)**4 * EI/rhoA + xi/rhoA)

def omega_b(n):
    return omega(n) * np.sqrt(1 - zeta**2)

def green_function(t, n):
    return 1/omega_b(n) * np.exp(-zeta*omega(n)*t) * np.sin(omega_b(n)*t) * (t >= 0)

def f_n(t, n):
    return 2*Q0/(rhoA*L) * mode_shape(V*t, n)
```

Thus, the expression for the time-dependant magnitude term q_m can be written, and implemented as follows:

$$q_m = \frac{Q_0}{\bar{m}} \begin{cases} \int_{\tau=0}^t \varphi_m(V\tau) g_m(t-\tau) d\tau, & 0 < t < L/V \\ \int_{\tau=0}^{L/V} \varphi_m(V\tau) g_m(t-\tau) d\tau, & t > L/V \end{cases}$$
(13)

Finally, using modal expansion method, the total solution is equal to the contributions from all n modes being considered, and implemented as follows:

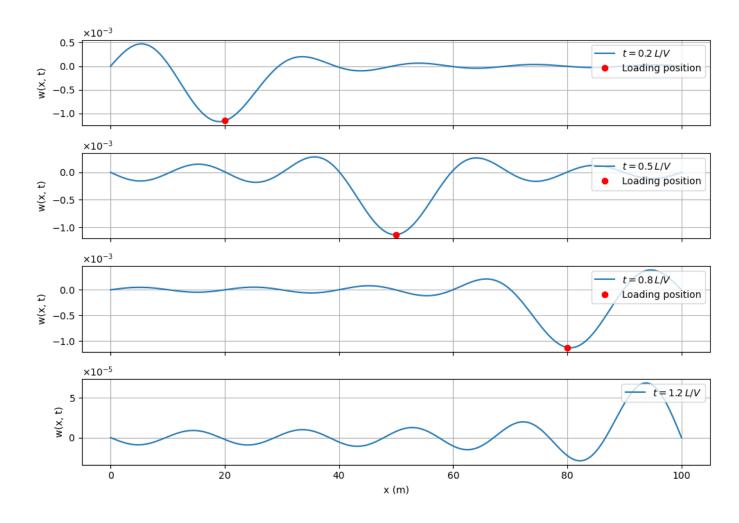
```
In [20]: def w(x,t, N=10):
    total = 0
    for n in range(1, N+1):
        total += q_n(t, n) * mode_shape(x, n)
    return total
```

The response at various time instance are plotted below. It can be seen that: 1) when the load is on the beam, the deflection under the moving load is largest. 2) When load left the beam, in this case, the response is much smaller.

```
In [21]: x_vals = np.linspace(0, L, 200)
t_vals = [0.2*L/V, 0.5*L/V, 0.8*L/V, 1.2 *L/V] # Include t > L/V
```

```
# Plot results
fig, axes = plt.subplots(4, 1, figsize=(10, 8), sharex=True)
for i, t in enumerate(t_vals):
    w_{vals} = [-w(x, t) \text{ for } x \text{ in } x_{vals}]
    n = t / (L / V)
    axes[i].plot(x_vals, w_vals, label=fr'$t = {n:.1f}\,L/V$')
    x load = V * t
    if 0 <= x_load <= L:
        w_load = -w(x_load, t)
        axes[i].plot(x_load, w_load, 'ro', label='Loading position')
    axes[i].set_ylabel('w(x, t)')
    axes[i].legend(loc='upper right')
    axes[i].grid(True)
    axes[i].yaxis.set_major_formatter(ScalarFormatter(useMathText=True))
    axes[i].ticklabel_format(axis='y', style='sci', scilimits=(0,0))
axes[-1].set_xlabel('x (m)')
plt.suptitle('Beam Response Over Time')
plt.tight_layout(rect=[0, 0.03, 1, 0.95])
plt.show()
```

Beam Response Over Time



Problem 5

question A

Deriving the dispersion equation using sympy

```
In [22]: # define the paramters for the ODE
x = sym.symbols('x')
m = sym.symbols('m')
k, omega = sym.symbols('k, omega')
```

```
C1, C2 = sym.symbols('C1 C2')
              kappa, L, k_s, eta_s, T = sym.symbols('kappa L k_s eta_s T')
             W = sym.Function('W')(x)
              # Define the ODE for the beam in terms of kappa
              ODE = sym.Eq(W.diff(x, 2) + kappa**2*W, 0)
              display(ODE)
             W = C1 * sym.sin(kappa*x) + C2 * sym.cos(kappa*x)
           \kappa^2 W(x) + \frac{d^2}{dx^2} W(x) = 0
In [23]: # Define W of the m-th beam element
             W_m = sym.Function('W_m')(x,m)
             W_m = W.subs(x, x-m*L)*sym.exp(-1j*k*m*L)
             display(W_m)
           \left(C_1\sin\left(\kappa\left(-Lm+x
ight)
ight)+C_2\cos\left(\kappa\left(-Lm+x
ight)
ight)e^{-1.0iLkm}
In [24]: # interface conditions
              # Deflection continuity
              eq1 = sym.Eq(W_m.subs(m, m), W_m.subs(m, m+1))
              # Force equilibrium
              eq2 = sym.Eq(-W_m.diff(x).subs(m, m) + W_m.diff(x).subs(m, m+1), k_s/T * W_m.subs(m, m))
              display(eq1)
              display(eq2)
             # Convert the equations to matrix form
              eqns = [eq1.expand(), eq2.expand()]
             M = sym.linear_eq_to_matrix(eqns, [C1, C2])[0]
              display(M)
           \left(C_{1}\sin\left(\kappa\left(-Lm+x
ight)
ight)+C_{2}\cos\left(\kappa\left(-Lm+x
ight)
ight)
ight)e^{-1.0iLkm}=\left(C_{1}\sin\left(\kappa\left(-L\left(m+1
ight)+x
ight)
ight)+C_{2}\cos\left(\kappa\left(-L\left(m+1
ight)
ight)
ight)
            -\left(C_{1}\kappa\cos\left(\kappa\left(-Lm+x
ight)
ight)-C_{2}\kappa\sin\left(\kappa\left(-Lm+x
ight)
ight)
ight)e^{-1.0iLkm}+\left(C_{1}\kappa\cos\left(\kappa\left(-L\left(m+1
ight)+x
ight)
ight)-C_{2}\kappa\sin\left(\kappa\left(-Lm+x
ight)
ight)
ight)
             -e^{-1.0iLkm}\sin\left(L\kappa m-\kappa x
ight)+e^{-1.0iLk}e^{-1.0iLkm}\sin\left(L\kappa m+L\kappa-\kappa x
ight) \qquad e^{-1.0iLkm}e^{-1.0iLkm}\cos\left(L\kappa m-\kappa x
ight)+\kappa e^{-1.0iLkm}\cos\left(L\kappa m+L\kappa-\kappa x
ight)+rac{k_se^{-1.0iLkm}\sin\left(L\kappa m-\kappa x
ight)}{T} \qquad -\kappa e^{-1.0iLkm}\sin\left(L\kappa m-\kappa x
ight)
In [25]: # Compute the determinant of the matrix
              disp_eq = M.det().expand()
              # Substitute xi and K_s to simplify the equation
              disp_eq = disp_eq.subs(k_s/T, K_s).subs(sym.exp(-1j*k*L), xi)
              disp_eq = disp_eq/kappa
              disp_eq = disp_eq/sym.exp(-2j*L*k*m)
In [26]: # Display the derived dispersion equation
```

Dispersion equation provided in the problem:

display(disp_eq.simplify())

 $-rac{K_{s}\xi\sin\left(L\kappa
ight)}{\kappa}-2\xi\cos\left(L\kappa
ight)+\xi^{2.0}+1$

xi, K_s = sym.symbols('xi, K_s')

$$\xi^2 - \left(rac{K_s}{\kappa} \sin(\kappa L) + 2\cos(\kappa L)
ight) \xi + 1 = 0, \quad \xi = \exp(-ikL), \quad K_s = rac{k_s}{T}, \quad \kappa = rac{\omega}{c} = rac{\omega}{\sqrt{T/
ho A}}$$

The provided dispersion equation and the derived dispersion equation are equal.

question B

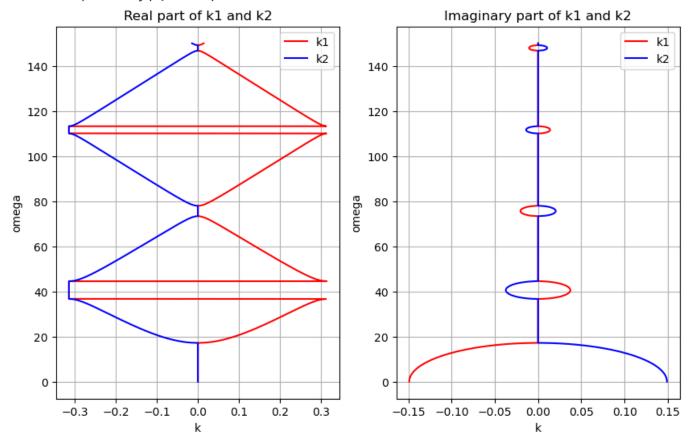
ax[1].legend()

ax[1].set_title('Imaginary part of k1 and k2')

```
In [27]: # Defining numerical values
        values = {L:10, K_s:4E3/15E3}
        # Solve the dispersion equation for xi
        eq = sym.Eq(disp_eq.subs(values), 0)
        sol = sym.solve(eq, xi)
In [28]: xi1 = sol[0]
        xi2 = sol[1]
        k1 = 1j*sym.log(xi1)/(L)
        k2 = 1j*sym.log(xi2)/(L)
        print("Expressions for the wavenumbers k1 and k2:")
        display(k1.simplify())
        display(k2.simplify())
        xi1_lambda = sym.lambdify(kappa, xi1)
        xi2_lambda = sym.lambdify(kappa, xi2)
        k1 lambda = sym.lambdify(kappa, k1.subs(values))
        k2_lambda = sym.lambdify(kappa, k2.subs(values))
       Expressions for the wavenumbers k1 and k2:
               1.0i\log
                                                 L
               1.0i\log
                                                 L
In [29]:
        # Plot the real parts of the dispersion curves
        omega_values = np.linspace(0.001, 150, 10000, dtype=complex)
        kappa_values = omega_values/np.sqrt(15E3/1.1)
        T_val = 15E3
        rhoA = 1.1
        fig, ax = plt.subplots(1, 2, figsize=(10, 6))
        ax[0].plot(np.real(k1_lambda(kappa_values)), omega_values, 'r', label='k1')
        ax[0].plot(np.real(k2_lambda(kappa_values)), omega_values, 'b', label='k2')
        ax[1].plot(np.imag(k1_lambda(kappa_values)), omega_values, 'r', label='k1')
        ax[1].plot(np.imag(k2_lambda(kappa_values)), omega_values, 'b', label='k2')
        ax[0].set_ylabel('omega')
        ax[0].set_xlabel('k')
        ax[0].legend()
        ax[0].set_title('Real part of k1 and k2')
        ax[0].grid();
        ax[1].set_ylabel('omega')
        ax[1].set_xlabel('k')
```

ax[1].grid();

- c:\Users\bart\anaconda3\envs\slender\Lib\site-packages\matplotlib\cbook.py:1762: ComplexWarnin
- g: Casting complex values to real discards the imaginary part return math.isfinite(val)
- c:\Users\bart\anaconda3\envs\slender\Lib\site-packages\matplotlib\cbook.py:1398: ComplexWarnin
- g: Casting complex values to real discards the imaginary part return np.asarray(x, float)



- The real part is nonzero when the imaginary part is zero and the other way around.
- Repeating in k with period of 2pi/L.
- Repeating in omega with 2pi/L * sqrt(T/rhoA)
- Has two stop bands every period in omega.
- The dispersion curve shows a lot of similarities with the periodically supported beam model.

question C

• Equation of Motion in omega, k domain

$$egin{split} &(-
ho A\omega^2+Tk^2) ilde w=2\pi Q_0\delta(\omega-kV)-\hat R(\omega)\sum_{n=-\infty}^\infty e^{-i\left(rac{\omega}{V}-k
ight)nL}\ &(-
ho A\omega^2+Tk^2) ilde w=2\pirac{Q_0}{V}\,\delta\left(rac{\omega}{V}-k
ight)-\hat R(\omega)rac{2\pi}{L}\sum_{n=-\infty}^\infty \delta\left(rac{\omega}{V}-k-rac{2\pi n}{L}
ight) \end{split}$$

• Solution for generic R (omega, k domain)

$$egin{aligned} ilde{w}(\omega,k) &= rac{2\pi}{\Delta_b(\omega,k)} rac{1}{V} rac{1}{T} \Bigg[Q_0 \delta\left(rac{\omega}{V} - k
ight) - \hat{R} rac{V}{L} \sum_{n=-\infty}^{\infty} \delta\left(rac{\omega - \omega_n}{V} - k
ight) \Bigg] \ \Delta_b(\omega,k) &= k^2 - rac{
ho A}{T} \omega^2 \end{aligned}$$

$$\omega_n = n rac{2\pi V}{L}$$

• Solution for generic R (omega, x domain)

$$\hat{w}(x,\omega) = rac{1}{V}rac{1}{T}igg[rac{1}{\Delta_b(\omega,V)}Q_0e^{-irac{\omega}{V}x} - \hat{R}rac{V}{L}\sum_{n=-\infty}^{\infty}rac{1}{\Delta_b(\omega,\omega_n,V)}e^{-irac{(\omega-\omega_n)}{V}x}igg] \ \Delta_b(\omega,V) = igg(rac{\omega}{V}igg)^2 - rac{
ho A}{T}\omega^2 \ \Delta_b(\omega,\omega_n,V) = igg(rac{\omega-\omega_n}{V}igg)^2 - rac{
ho A}{T}\omega^2$$

• Solution for generic R at origin

$$\hat{w}(0,\omega) = rac{1}{V}rac{1}{T}\Bigg[rac{1}{\Delta_b(\omega,V)}Q_0 - \hat{R}rac{V}{L}\sum_{n=-\infty}^{\infty}rac{1}{\Delta_b(\omega,\omega_n,V)}\Bigg]$$

• Use following definition to get rid of infinite sum

$$\sum_{n=-\infty}^{\infty} \frac{1}{\left(\frac{\omega L}{V} - 2\pi n\right)^2 - (\kappa L)^2} = \frac{1}{2\kappa L} \frac{\sin(\kappa L)}{\cos(\kappa L) - \cos\left(\frac{\omega}{V}L\right)}$$

$$\kappa = \frac{\omega}{\sqrt{T/\rho A}}$$

$$\Delta_b(\omega, \omega_n, V) = \left(\frac{\omega - \frac{2\pi nV}{L}}{V}\right)^2 - \kappa^2$$

$$L^2 \Delta_b(\omega, \omega_n, V) = \left(\left(\frac{\omega}{V} - \frac{2\pi n}{L}\right)^2 - \kappa^2\right) L^2$$

$$L^2 \Delta_b(\omega, \omega_n, V) = \left(\frac{\omega L}{V} - 2\pi n\right)^2 - (\kappa L)^2$$

$$\frac{1}{\Delta_b(\omega, \omega_n, V)} = \frac{L^2}{\left(\frac{\omega L}{V} - 2\pi n\right)^2 - (\kappa L)^2}$$

$$\sum_{n=-\infty}^{\infty} \frac{1}{\Delta_b(\omega, \omega_n, V)} = \frac{L^2}{2\kappa L} \frac{\sin(\kappa L)}{\cos(\kappa L) - \cos\left(\frac{\omega}{V}L\right)}$$

• Solution for generic R at origin

$$\hat{w}(0,\omega) = rac{1}{V}rac{1}{T}\left[rac{1}{\Delta_b(\omega,V)}Q_0 - \hat{R}rac{V}{L}rac{L}{2\kappa}rac{\sin(\kappa L)}{\cos(\kappa L) - \cos\left(rac{\omega}{V}L
ight)}
ight]$$

• Specific reaction force

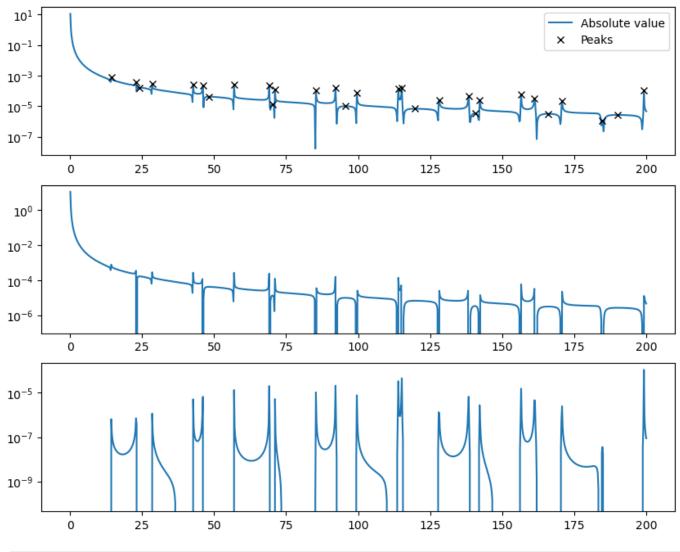
$$\hat{R}=(k_s+i\omega\eta_s)\hat{w}(0,\omega)$$

Now we can solve for $\hat{w}(0,\omega)$ with sympy.

```
In [30]: rhoA, V, T, Q0, L, omega, k_s, eta_s = sym.symbols('rhoA V T Q0 L omega k_s eta_s')
          values = {rhoA:1.1, T:15E3, L:10, k_s:4E3, eta_s:0.5, Q0:55, V:28}
          w_hat = sym.Function('w_hat')(omega)
          delta_b = (omega/V)**2 - rhoA/T * omega**2
          R_hat = (k_s + sym.I*eta_s*omega)*w_hat
          kappa = omega/sym.sqrt(T/rhoA)
          eq1 = sym.Eq(w_hat, 1/V * 1/T * (1/delta_b * Q0 - R_hat * V/2*kappa * sym.sin(kappa*L)/(sym.cc
In [31]: display(eq1.subs(values))
          w_hat = sym.solve(eq1.subs(values), w_hat)[0]
                    2.85449612859225 \cdot 10^{-7} \omega \left(0.5i\omega + 4000.0\right) w_{hat}(\omega) \sin \left(0.0856348838577675\omega\right)
                                                                                             0.10892937980986
        w_{hat}(\omega) = -
                                     \cos{(0.0856348838577675\omega)} - \cos{(\frac{5\omega}{14})}
In [32]: from scipy.signal import find peaks
          w hat lambda = sym.lambdify(omega, w hat)
          omega_values = np.linspace(0.1, 200, 1000)
          fig, ax = plt.subplots(3, 1, figsize=(10, 8))
          ax[0].semilogy(omega_values, np.abs(w_hat_lambda(omega_values)), label='Absolute value')
          ax[1].semilogy(omega values, np.real(w hat lambda(omega values)), label='Real part')
          ax[2].semilogy(omega_values, np.imag(w_hat_lambda(omega_values)), label='Imag part')
          # Find peaks in the absolute value of w_hat
          abs vals = np.abs(w hat lambda(omega values))
          peaks, _ = find_peaks(abs_vals)
          # Plot the peaks on the absolute value plot
          ax[0].plot(omega_values[peaks], abs_vals[peaks], "kx", label='Peaks')
          ax[0].legend()
          print(omega values[peaks])
         [ 14.30710711 22.91141141 24.11201201 28.51421421 42.72132132
          46.12302302 48.32412412 56.92842843 69.13453453 70.33513514
          71.13553554 85.34264264 92.14604605 95.54774775 99.54974975
          113.95695696 115.15755756 119.75985986 128.16406406 138.36916917
```

140.57027027 142.17107107 156.57827828 161.18058058 165.98298298

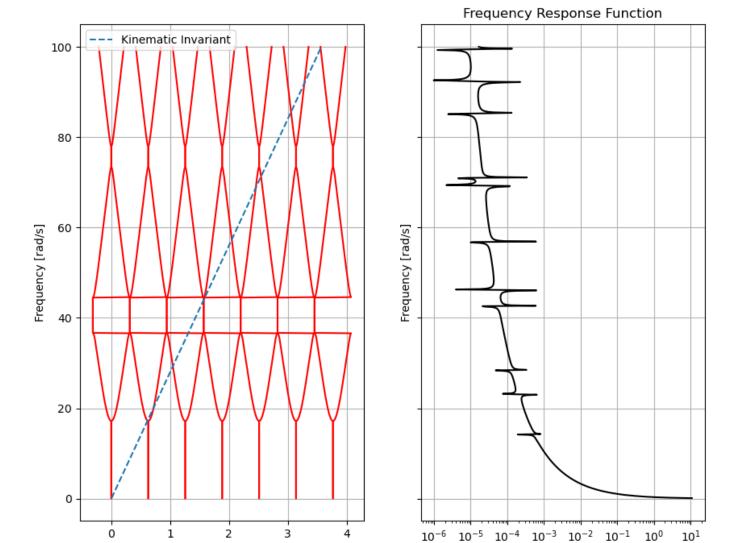
170.78538539 184.79239239 189.99499499 199.1995996]



```
In [41]:
         omega_values = np.linspace(0.1, 100, 1000, dtype=complex)
         kappa_values = omega_values/np.sqrt(15E3/1.1)
         fig, ax = plt.subplots(1,2, figsize=(10, 8), sharey=True)
         for i in range(7):
             ax[0].plot(np.real(k1_lambda(kappa_values))+2*i*np.pi/10, omega_values, 'r')
             ax[0].plot(np.real(k2_lambda(kappa_values))+2*i*np.pi/10, omega_values, 'r')
         ax[0].plot(omega_values/28, omega_values, '--', label='Kinematic Invariant')
         ax[0].set_xlabel('k')
         ax[0].set_ylabel('Frequency [rad/s]')
         ax[0].grid()
         ax[0].legend()
         ax[1].semilogx(np.abs(w_hat_lambda(omega_values)), omega_values, 'black', label='FRF');
         ax[1].set_xlabel('FRF')
         ax[1].set_ylabel('Frequency [rad/s]')
         ax[1].set_title('Frequency Response Function')
         ax[1].grid()
```

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 return np.asarray(x, float)



The obtained FRF is plotted next to the dispersion curve and the kinematic invariant. It is expected that the crossing of the kinematic invariant and the dispersion curve correspond to peaks in the FRF. For higher frequencies they match perfectly, however for lower frequencies this is not the case. We were not able to find the reason why this is the case. When increasing the range to even higher frequencies, the peaks keep on matching with the crossing locations.

FRF

k

question D

Unfortunately, we were not able to anwer question d. We tried using an ifft on the FRF, but the obtained results were not logical at all:

```
In [43]: N = 1000

    fs = 1000
    df = fs/N
    frequency_values = np.linspace(-fs/2, fs/2, N, dtype=complex)
    omega_values = 2 * np.pi * frequency_values

    dt = 1 / fs

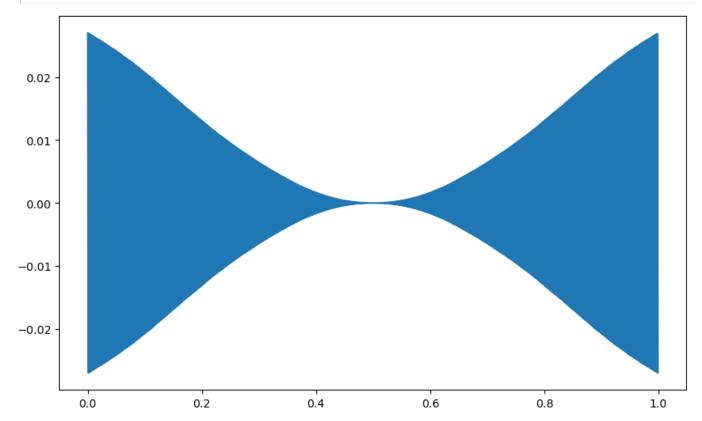
    w_hat = w_hat_lambda(omega_values)

    w_time = np.fft.fft(w_hat)

    time = np.arange(N) * dt

    plt.figure(figsize=(10, 6))
# plt.plot(time, w_time.imag)
```

plt.plot(time, w_time.real);



```
In [ ]:
In [ ]:
```