

UNIT I

FINITE IMPULSE RESPONSE (FIR) FILTER

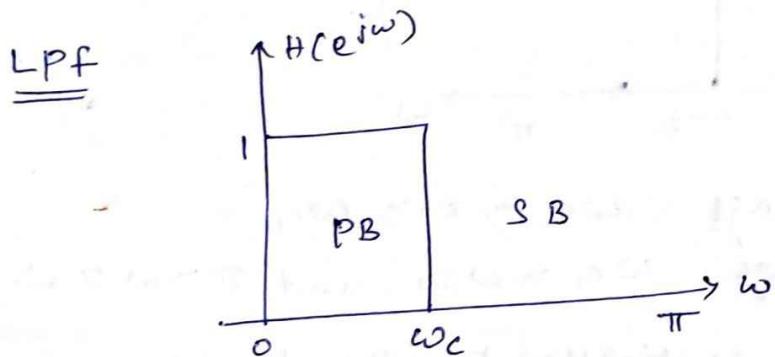
Digital transfer for time domain classification
based on length \rightarrow FIR & IIR.

based on digital transfer for - four types of filter.

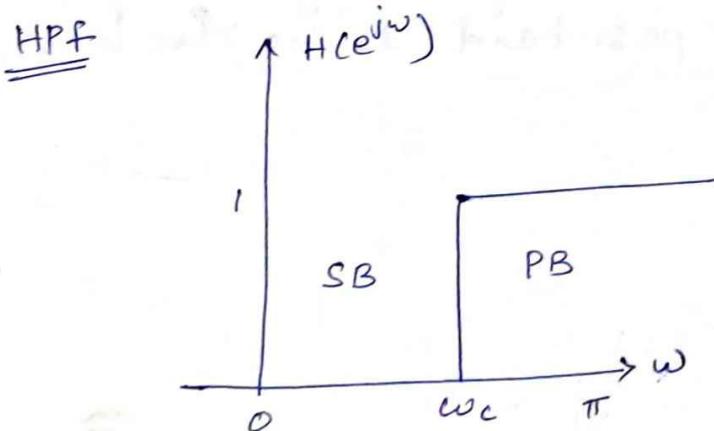
pass band(PB) the range of frequencies where the freq response of the signal takes the value

stop band(SB) the range of frequencies where the freq response of the signal is zero.

- (1) Low pass filter (LPF)
- (2) High pass filter (HPF)
- (3) Band pass filter (BPF)
- (4) band stop filter (BSF)

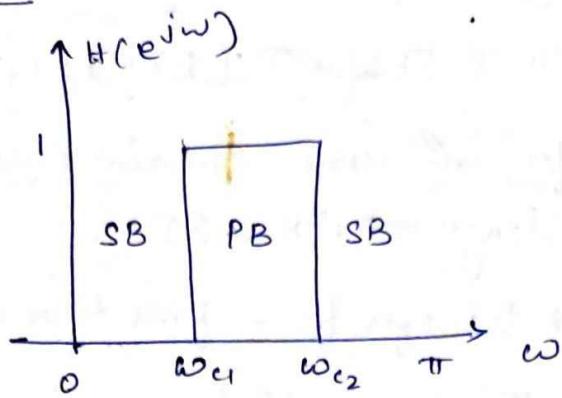


passes low freq $\omega_c > \omega > 0$
blocks high freq $\pi > \omega > \omega_c$



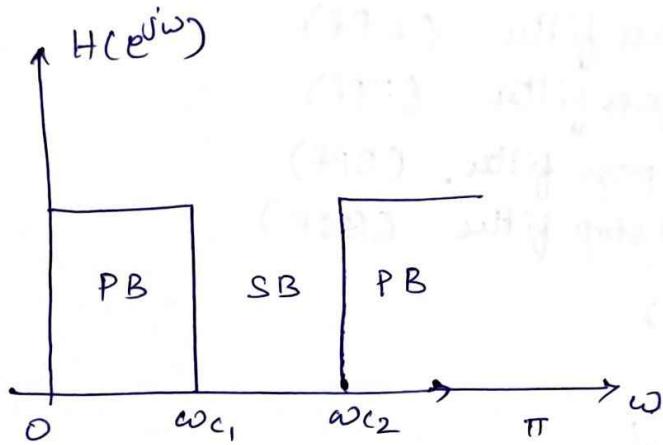
passes high freq $\pi > \omega > \omega_c$
blocks low freq $\omega_c > \omega > 0$

Band pass filter



passes freq in the range $\omega_{c_2} > \omega > \omega_{c_1}$
 blocks freq in the range $\omega_{c_1} > \omega > 0$ & $\pi > \omega > \omega_{c_2}$

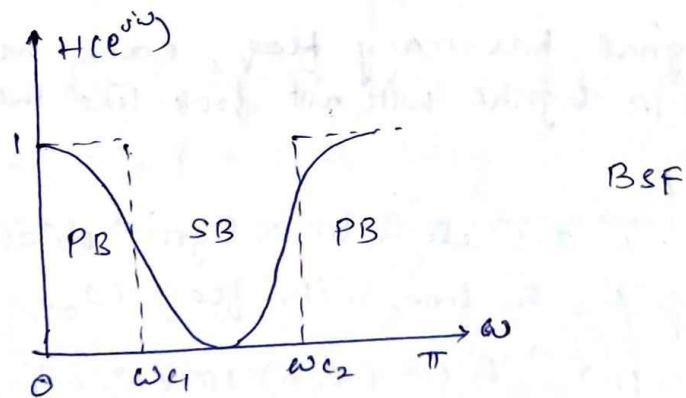
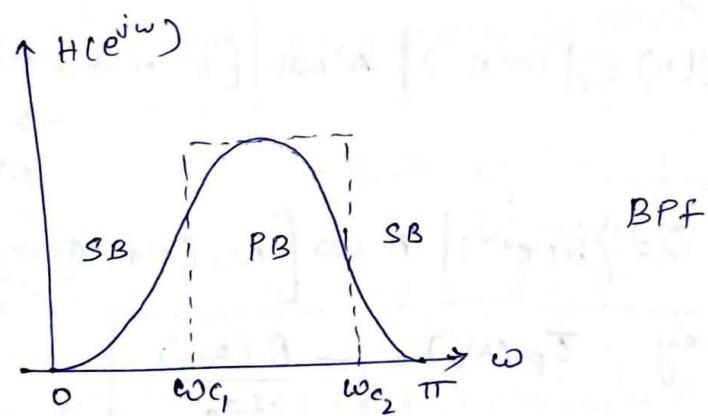
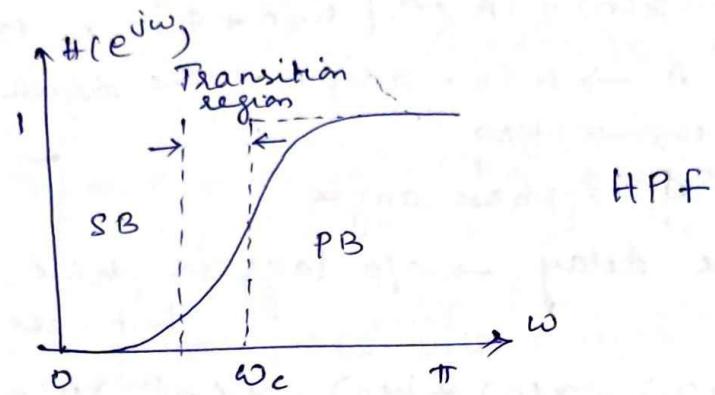
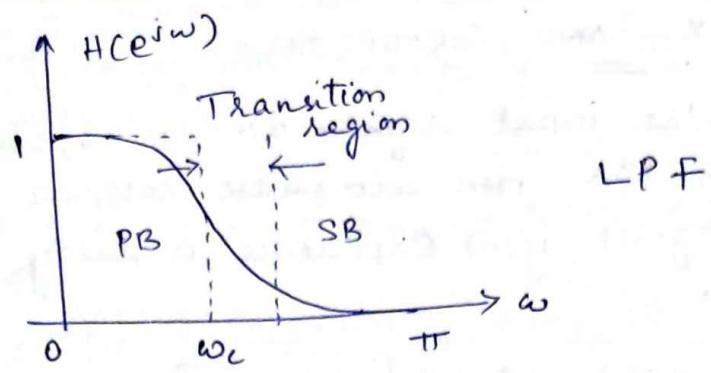
Band stop filter



stops freq in the range $\omega_{c_2} > \omega > \omega_{c_1}$
 pass freq in the range $\omega_{c_1} > \omega > 0$ and $\pi > \omega > \omega_{c_2}$

To develop stable and realizable transfer function, the ideal freq response of the filters are relaxed, by introducing a transition band between the passband and the stop band to permit the mag response to decay more gradually from its maximum value in the pass band to the zero value in the stop band.

(2)



PHASE DELAY AND GROUP DELAY

when the input signal $x(n)$ is applied to a system which has non-zero phase response $\Theta(\omega) = \arg[H(e^{j\omega})]$, the output signal $y(n)$ experience a delay w.r.t the input signal.

$$\text{Let } x(n) = A \cos[\omega_0 n + \phi], \quad +\infty > n > -\infty$$

$A \rightarrow \text{max. amp. of the signal}$

$\omega_0 \rightarrow \text{freq}$

$\phi \rightarrow \text{phase angle}$

due to the delay \rightarrow O/P lags in phase $\Theta(\omega_0)$

but freq remains same.

$$y(n) = x(n) * h(n) = X(e^{j\omega}) H(e^{j\omega})$$

$$y(n) = |H(e^{j\omega})| A \cos [\omega_0 n + \Theta(\omega_0) + \phi]$$

\rightarrow time delayed

phase delay at $\omega = \omega_0$

$$y(n) = |H(e^{j\omega})| A \cos \left[\omega_0 \left(n + \frac{\Theta(\omega_0)}{\omega_0} \right) + \phi \right]$$

$$\boxed{\text{Phase delay } \tau_p(\omega_0) = -\frac{\Theta(\omega_0)}{\omega_0}}$$

when i/p signal has many freq, each with diff phase delay, then O/P signal will not look like the i/p signal.

- group delay

consider an. a discrete-time signal obtained by DSB-SC with carrier freq ω_c & sine with freq ω_0 .

$$x(n) = A \cos(\omega_0 n) \cos(\omega_c n)$$

$$x(n) = \frac{A}{2} \cos(\omega_c - \omega_0)n + \frac{A}{2} \cos(\omega_c + \omega_0)n$$

$$\text{let } \omega_c - \omega_0 = \omega_d$$

$$\omega_c + \omega_0 = \omega_u$$

$$x(n) = \frac{A}{2} \cos \omega_d n + \frac{A}{2} \cos \omega_u n$$

(3)

If the i/p signal is passed thru LTI system whose response is $H(e^{j\omega})$, then o/p is

$$y(n) = \frac{A}{2} |H(e^{j\omega})| \cos [\omega_0 n + \theta(\omega_0)] + \frac{A}{2} \frac{|H(e^{j\omega})|}{|H(e^{j\omega})|} \cos [\omega_u(n) + \theta(\omega_u)]$$

$$y(n) = A |H(e^{j\omega})| \cos \left[\left(\frac{\omega_u + \omega_d}{2} \right) n + \frac{\theta(\omega_u) + \theta(\omega_d)}{2} \right] \\ \cos \left[\left(\frac{\omega_u - \omega_d}{2} \right) n + \frac{\theta(\omega_u) - \theta(\omega_d)}{2} \right]$$

$$y(n) = A \cos \left[\omega_c n + \frac{\theta(\omega_u) + \theta(\omega_d)}{2} \right] * \cos \left[\omega_0 n + \frac{\theta(\omega_u) - \theta(\omega_d)}{2} \right]$$

$$\begin{aligned} \omega_c - \omega_0 &= \omega_d \\ \underline{\omega_c + \omega_0 = \omega_u} \\ \underline{2\omega_c = \omega_d + \omega_u} \\ \therefore \omega_c &= \frac{\omega_d + \omega_u}{2} \end{aligned}$$

$$\begin{aligned} \omega_d - \omega_0 &= \omega_u \\ \underline{\omega_c + \omega_0 = \omega_u} \\ \underline{-2\omega_0 = \omega_u - \omega_d} \\ \frac{\omega_u - \omega_d}{2} &= \omega_0 \end{aligned}$$

Let us Redefine the eqn $x(n) = \frac{A}{2} \cos \omega_0 n + \frac{A}{2} \cos \omega_u n$.

for a narrow band signal wherein ω_d and ω_u are so close to the carrier freq ω_c (ω_0 is very small), then the phase delay due to carrier can be expanded using Taylor's series as

$$\theta_c(\omega) \approx \theta_c(\omega_c) + \left. \frac{d\theta_c(\omega)}{d\omega} \right|_{\omega=\omega_c} (\omega - \omega_c) + \dots$$

 Taylor series
real fn $f(x)$ at a point $x=a$ is

$$f(x) = f(a) + f'(a)(x-a) + \frac{f''(a)}{2!}(x-a)^2 + \frac{f'''(a)}{3!}(x-a)^3 + \dots$$

Let us consider first term in the eqn

$$-\frac{[\theta(\omega_u) + \theta(\omega_l)]}{2\omega_c} \approx -\frac{\theta_c(\omega_c)}{\omega_c}$$

which is same as the phase delay
the sign indicates phase lag.

The second term can be written as

$$-\frac{\theta(\omega_u) + \theta(\omega_l)}{2\omega_0} = -\frac{\theta(\omega_u) + \theta(\omega_l)}{2(\omega_u - \omega_l)} \approx -\frac{d\theta_c(\omega)}{d\omega} \Big|_{\omega=\omega_c}$$

$$\tau_g(\omega_c) = -\frac{d\theta_c(\omega)}{d\omega} \Big|_{\omega=\omega_c}$$

Group delay.

Group delay is differential of phase delay.

The o/p will be distorted if group delay is not constant in LTI systems.

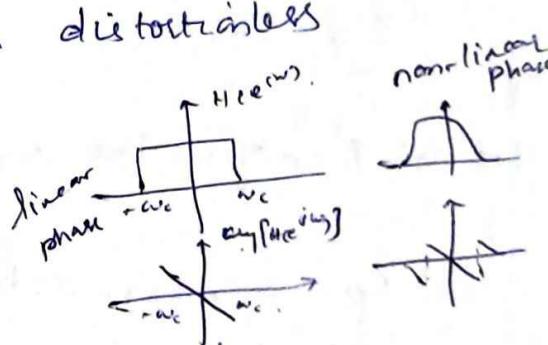
delay equalizer is used to obtain distortionless overall o/p response.

LINEAR PHASE TRANSFER FUNCTION.

Filters with linear or zero phase is required for signal processing applications.

but zero phase are not causal. (made arbitrarily causal)
possible to design FIR filter but impossible to design IIR filter.

The transfer fn has linear phase if its impulse response $h[n]$ is either symmetric or anti-symmetric.



(4)

Let us analyze a causal transfer fn of a FIR filter.

$$H(z) = \sum_{n=0}^{N-1} h(n) z^{-n}$$

F.T of impulse fn $h(n)$ is

$$H(e^{j\omega}) = \sum_{n=0}^{N-1} h(n) e^{-j\omega n}.$$

Polar representation

$$H(e^{j\omega}) = \pm |H(e^{j\omega})| e^{j\phi(\omega)}.$$

where $H(e^{j\omega}) \rightarrow$ mag response

$e^{j\phi(\omega)}$ \rightarrow phase response.

Let us assume the phase of FIR filter transfer fn is linear

i) $\phi(\omega) = -\alpha\omega$, $\pi \geq \omega \geq -\pi$.

$\alpha \rightarrow$ constant delay in phase.

$$\tau_p = -\frac{\phi(\omega)}{\omega} = +\frac{\alpha\omega}{\omega} = \alpha$$

$$\tau_g = -\frac{d\phi(\omega)}{d\omega} = -\frac{d(-\alpha\omega)}{d\omega} = \alpha.$$

Both phase delay and group delay are constant and independent of freq.

The impulse response of FIR filter has linear phase if its impulse response satisfies the following condition

(i) for symmetric impulse response $h(n)$

$$h(n) = h(N-1-n), (N-1) \geq n \geq 0$$

(ii) for antisymmetric impulse response $h(n)$

$$h(n) = -h(N-1-n), (N-1) \geq n \geq 0.$$

The length of the impulse response $h(n)$ can be either even or odd. Based on this, FIR is divided into

- (i) Symmetric impulse response with odd length
- (ii) Symmetric impulse response with even length
- (iii) Antisymmetric impulse response with odd length
- (iv) Antisymmetric impulse response with even length.

(i) Symmetric impulse response with odd length

$$\text{let } N = 9$$

$$H(z) = \sum_{n=0}^8 h(n) z^{-n}$$

$$H(z) = h(0) + h(1)z^{-1} + h(2)z^{-2} + h(3)z^{-3} + h(4)z^{-4} + h(5)z^{-5} \\ + h(6)z^{-6} + h(7)z^{-7} + h(8)z^{-8}$$

using symmetric property

$$h(n) = h(N-1-n)$$

$$h(0) = h(9-1-0) = h(8)$$

$$h(1) = h(7)$$

$$h(2) = h(6)$$

$$h(3) = h(5)$$

$$h(4) = h(4)$$

$$H(z) = h(0)(1+z^{-8}) + h(1)(z^{-1}+z^{-7}) + h(2)(z^{-2}+z^{-6}) \\ + h(3)(z^{-3}+z^{-5}) + h(4)z^{-4}$$

$$H(z) = z^{-4} \left[h(0)(z^4+z^{-4}) + h(1)(z^3+z^{-3}) \right. \\ \left. + h(2)(z^2+z^{-2}) + h(3)(z^1+z^{-1}) + h(4) \right]$$

Freq response is obtained by taking F.T. $z = e^{j\omega}$

$$H(e^{j\omega}) = e^{-j4\omega} \left[h(0)(e^{j4\omega} + e^{-j4\omega}) + h(1)(e^{j3\omega} + e^{-j3\omega}) + h(2)(e^{j2\omega} + e^{-j2\omega}) + h(3)(e^{j\omega} + e^{-j\omega}) + h(4) \right] \quad (5)$$

$$H(e^{j\omega}) = e^{-j4\omega} \left[2h(0)\cos 4\omega + 2h(1)\cos 3\omega + 2h(2)\cos 2\omega + h(3)\cos \omega + h(4) \right]$$

$$\theta(\omega) = -4\omega + \beta$$

$$\beta \rightarrow 0 \text{ at } 2\pi$$

$$\text{phase delay } T_p = 4$$

$$\text{group delay } T_g = 4$$

since both are constant $H(e^{j\omega})$ is a linear fn of ω .

1/3/16
10/10/16
31, 41, 9, 17, 24, 32, 45, 50, 53
36, 37, 38, 45, 50, 53
40, 63, 30, 21

In general case -

$$H(e^{j\omega}) = \sum_{n=0}^8 h(n) e^{-j\omega n}$$

$$H(e^{j\omega}) = \sum_{n=0}^3 h(n) e^{-j\omega n} + h(4)e^{-j4\omega} + \sum_{n=5}^8 h(n) e^{-j\omega n}$$

In general

$$H(e^{j\omega}) = \sum_{n=0}^{\frac{N-3}{2}} h(n) e^{-j\omega n} + h\left(\frac{N-1}{2}\right) e^{-j\omega\left(\frac{N-1}{2}\right)} + \sum_{n=\left(\frac{N+1}{2}\right)}^{N-1} h(n) e^{-j\omega n}$$

Let $n=N-1-m$ be the third term

$$H(e^{j\omega}) = \sum_{n=0}^{\frac{N-3}{2}} h(n) e^{-j\omega n} + h\left(\frac{N-1}{2}\right) e^{-j\omega\left(\frac{N-1}{2}\right)} + \sum_{m=0}^{N-1} h(N-1-m) e^{-j\omega(N-1-m)}$$

using symmetry property

$$h(n) = h(N-1-n)$$

$$\therefore H(e^{j\omega}) = \sum_{n=0}^{\frac{N-3}{2}} h(n) e^{-j\omega n} + h\left(\frac{N-1}{2}\right) e^{-j\omega\left(\frac{N-1}{2}\right)} + \sum_{n=0}^{N-1} h(n) e^{-j\omega(N-1-n)}$$

$$H(e^{j\omega}) = h\left(\frac{N-1}{2}\right)e^{-j\omega\left(\frac{N-1}{2}\right)} + \sum_{n=0}^{\frac{N-3}{2}} h(n) \left[e^{-j\omega n} + e^{j\omega(N-\frac{N-1}{2}-n)} \right]$$

$$H(e^{j\omega}) = e^{j\omega\left(\frac{N-1}{2}\right)} h\left(\frac{N-1}{2}\right) + \sum_{n=0}^{\frac{N-3}{2}} h(n) \left[e^{j\omega\left(\frac{N-1}{2}-n\right)} + e^{-j\omega\left(\frac{N-1}{2}-n\right)} \right]$$

$$H(e^{j\omega}) = e^{-j\omega\left(\frac{N-1}{2}\right)} \left[h\left(\frac{N-1}{2}\right) + \sum_{n=0}^{\frac{N-3}{2}} 2h(n) \cos\omega\left(\frac{N-1}{2}-n\right) \right]$$

Let $\frac{N-1}{2} - n = m$, Then

$$H(e^{j\omega}) = e^{-j\omega\left(\frac{N-1}{2}\right)} \left[h\left(\frac{N-1}{2}\right) + 2 \sum_{m=1}^{\frac{N-1}{2}} h\left(\frac{N-1}{2}-m\right) \cos\omega m \right]$$

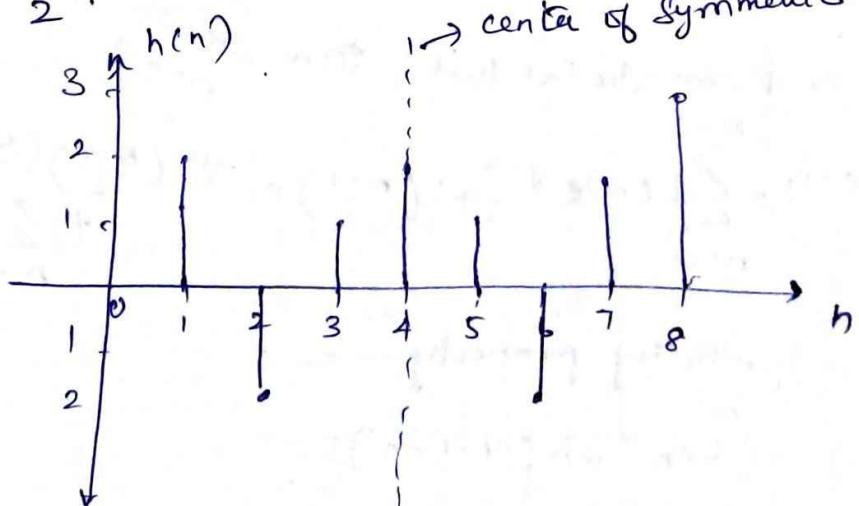
$$H(e^{j\omega}) = e^{-j\omega\left(\frac{N-1}{2}\right)} \left[h\left(\frac{N-1}{2}\right) + 2 \sum_{n=1}^{\frac{N-1}{2}} h\left(\frac{N-1}{2}-n\right) \cos\omega n \right]$$

$$H(e^{j\omega}) = e^{-j\omega\left(\frac{N-1}{2}\right)} \tilde{H}(e^{j\omega})$$

$$\tilde{H}(e^{j\omega}) = h\left(\frac{N-1}{2}\right) + 2 \sum_{n=1}^{\frac{N-1}{2}} h\left(\frac{N-1}{2}-n\right) \cos\omega n$$

$$\phi(\omega) = -\alpha\omega = \left(\frac{N-1}{2}\right)\omega.$$

$$\therefore \alpha = \frac{N-1}{2}.$$



(6)

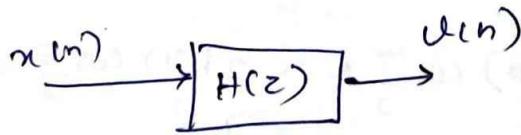
Zero phase filter

To avoid phase distortion the freq response of the filter should not delay the spectral components. Such transfer fn is said to have zero-phase characteristic. A zero-phase TF has no phase component i.e) spectrum is purely real - no img component & non-negative. But it is not possible to design a causal digital filter with a zero phase. Causal real-coefficient filter is used.

All freq are delayed by α sec, \therefore there is no distortion. If the filter does not have linear phase, then diff freq components are delayed by diff amounts, causing significant distortion.

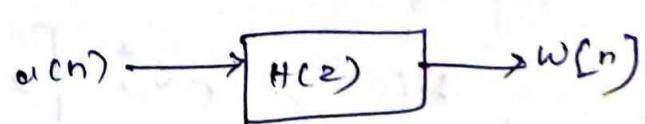
Zero phase-filtering

- (1) process i/p data (finite length) with a causal real-coefficient filter $H(z)$
- (2) Time reverse the o/p of the filter and process by the same filter
- (3) Time reverse once again the o/p of the second filter.



$$u(n) \rightarrow H(z) \rightarrow v(n)$$

$$u(n) = v[-n]$$



$$u(n) \rightarrow H(z) \rightarrow w(n)$$

$$y[n] = w[-n]$$

$$V(\omega) = H(\omega)X(\omega)$$

$$V(\omega) = V^*(\omega)$$

$$Y(\omega) = H^+(\omega)V(\omega) \quad \underline{V(\omega) = H^*(\omega)}$$

$$Y(\omega) = H(\omega)U(\omega)$$

$$Y(\omega) = W^*(\omega) = H^*(\omega)W(\omega)$$

$$Y(\omega) = H^*(\omega) \cdot H(\omega) X(\omega) = |H(\omega)|^2 X(\omega)$$

2. Symmetric Impulse response with Even length.

Consider length of impulse response is even

$$H(z) = \sum_{n=0}^7 h(n) z^{-n}$$

$$H(z) = h(0) + h(1)z^{-1} + h(2)z^{-2} + h(3)z^{-3} + h(4)z^{-4} + h(5)z^{-5} \\ + h(6)z^{-6} + h(7)z^{-7}.$$

Using symmetric property

$$h(n) = h(N-1-n)$$

$$h(0) = h(7)$$

$$h(1) = h(6)$$

$$h(2) = h(5)$$

$$h(3) = h(4).$$

$$H(z) = h(0)(1+z^{-7}) + h(1)(z^{-1}+z^{-6}) + h(2)(z^{-2}+z^{-5}) \\ + h(3)(z^{-3}+z^{-4})$$

$$H(z) = z^{-7/2} \left[h(0) \left(z^{7/2} + z^{-7/2} \right) + h(1) \left(z^{5/2} + z^{-5/2} \right) \right. \\ \left. + h(2) \left(z^{3/2} + z^{-3/2} \right) + h(3) \left(z^{1/2} + z^{-1/2} \right) \right]$$

Free response is obtained by taking f.T (ie) $z = e^{j\omega}$

$$H(e^{j\omega}) = e^{-j\frac{7}{2}\omega} \left[h(0) \left[e^{j\frac{7}{2}\omega} + e^{-j\frac{7}{2}\omega} \right] + h(1) \left[e^{j\frac{5}{2}\omega} + e^{-j\frac{5}{2}\omega} \right] \right. \\ \left. + h(2) \left[e^{j\frac{3}{2}\omega} + e^{-j\frac{3}{2}\omega} \right] + h(3) \left[e^{j\frac{1}{2}\omega} + e^{-j\frac{1}{2}\omega} \right] \right]$$

$$H(e^{j\omega}) = e^{-j\frac{7}{2}\omega} \left[2h(0) \cos \frac{7}{2}\omega + 2h(1) \cos \frac{5}{2}\omega + 2h(2) \cos \frac{3}{2}\omega \right. \\ \left. + 2h(3) \cos \frac{\omega}{2} \right]$$

Comparing this expression with $H(e^{j\omega}) = \pm |H(e^{j\omega})| e^{j\phi(\omega)}$

$$\phi(\omega) = -\alpha\omega = -\frac{7}{2}\omega + \beta$$

(7)

β is either 0 or 2π

$$\text{phase delay } \tau_p = -\alpha = \frac{\pi}{2}$$

$$\text{Groupdelay } \tau_g = -\alpha = \frac{\pi}{2}$$

Since, both delay are constant, it is a linear fn of ω .

In general case.

$$H(e^{j\omega}) = \sum_{n=0}^7 h(n) e^{-j\omega n}$$

$$H(e^{j\omega}) = \sum_{n=0}^3 h(n) e^{-j\omega n} + \sum_{n=4}^7 h(n) e^{-j\omega n}$$

In general

$$H(e^{j\omega}) = \sum_{n=0}^{\frac{N}{2}-1} h(n) e^{-j\omega n} + \sum_{n=\frac{N}{2}}^{N-1} h(n) e^{-j\omega n}$$

Let $n = (N-1-m)$ in the second term

$$H(e^{j\omega}) = \sum_{n=0}^{\frac{N}{2}-1} h(n) e^{-j\omega n} + \sum_{n=0}^{\frac{N}{2}-1} h(N-1-m) e^{-j\omega(N-1-m)}$$

$$\text{using Symmetry} \quad = \sum_{n=0}^{\frac{N}{2}-1} h(n) e^{-j\omega n} + \sum_{n=0}^{\frac{N}{2}-1} h(N-n) e^{-j\omega(N-1-n)}$$

$$h(n) = h(N-1-n)$$

$$H(e^{j\omega}) = \sum_{n=0}^{\frac{N}{2}-1} h(n) e^{-j\omega n} + \sum_{n=0}^{\frac{N}{2}-1} h(n) e^{-j\omega(N-1-n)}$$

$$= \sum_{n=0}^{\frac{N}{2}-1} h(n) \left[e^{-j\omega n} + e^{-j\omega(N-1-n)} \right]$$

$$= e^{-j\omega(\frac{N-1}{2})} \left\{ \sum_{n=0}^{\frac{N}{2}-1} h(n) \left[e^{j\omega(\frac{N-1}{2}-n)} + e^{-j\omega(\frac{N-1}{2}-n)} \right] \right\}$$

$$= e^{-j\omega(\frac{N-1}{2})} \sum_{n=0}^{\frac{N}{2}-1} 2h(n) \cos\omega(\frac{N-1}{2}-n)$$

$$\text{let } \frac{N}{2} - n = m$$

$$H(e^{j\omega}) = e^{-j\omega(\frac{N-1}{2})} \left[\sum_{m=0}^{\frac{N}{2}} 2h\left(\frac{N}{2} - m\right) \cos \omega(m - \frac{1}{2})\omega \right]$$

$$H(e^{j\omega}) = e^{-j\omega(\frac{N-1}{2})} \left[\sum_{n=0}^{\frac{N}{2}} 2h\left(\frac{N}{2} - n\right) \cos \left(n - \frac{1}{2}\right)\omega \right]$$

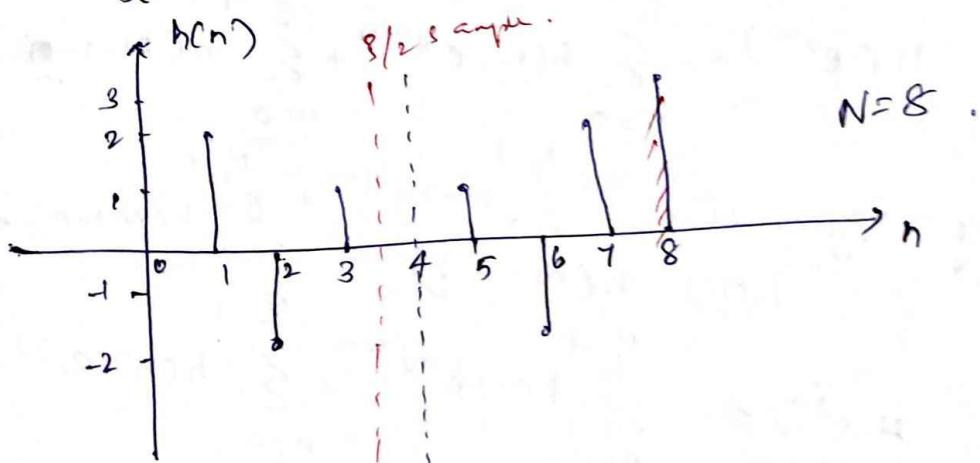
$$H(e^{j\omega}) = e^{-j\omega(\frac{N-1}{2})} \overline{H}(e^{j\omega})$$

$$\overline{H}(e^{j\omega}) = \sum_{n=0}^{\frac{N}{2}} 2h\left(\frac{N}{2} - n\right) \cos \left(n - \frac{1}{2}\right)\omega$$

on comparing $\alpha(\omega) = -\omega = \left(\frac{N-1}{2}\right)\omega$

$$\alpha = \frac{N-1}{2} \rightarrow \text{center of symmetric.}$$

0, 2, -2, 1, 1, -2, 2, 0



(3) Antisymmetric Impulse response with odd length.

Let length $N = 9$

$$h(z) = \sum_{n=0}^8 h(n) z^{-n}$$

$$H(z) = h(0) + h(1)z^{-1} + h(2)z^{-2} + h(3)z^{-3} + h(4)z^{-4} + h(5)z^{-5} \\ + h(6)z^{-6} + h(7)z^{-7} + h(8)z^{-8}$$

using antisymm property

$$h(n) = -h(N-1-n)$$

$$h(0) = -h(8) \quad h(3) = -h(5)$$

$$h(1) = -h(7)$$

$$h(2) = -h(6)$$

~~h(4) = -h(4)~~ does not have center value $h(4) = 0$. $h(\frac{N-1}{2}) = 0$

$$H(z) = h(0)(1-z^{-8}) + h(1)(z^{-1}-z^{-7}) + h(2)(z^{-2}-z^{-6}) \\ + h(3)(z^{-3}-z^{-5})$$

Taking F.T $\Rightarrow z = e^{j\omega}$

$$H(e^{j\omega}) = h(0)(1-e^{-j8\omega}) + h(1)(e^{-j\omega}-e^{-j7\omega}) \\ + h(2)(e^{-j2\omega}-e^{-j6\omega}) + h(3)(e^{j3\omega}-e^{-j5\omega}).$$

$$H(e^{j\omega}) = e^{-j4\omega} [h(0)(e^{j4\omega}-e^{-j4\omega}) + h(1)(e^{j3\omega}-e^{-j3\omega}) \\ + h(2)(e^{j2\omega}-e^{-j2\omega}) + h(3)(e^{j\omega}-e^{-j\omega})]$$

$$= e^{-j4\omega} \left[h(0) \sin 4\omega + h(1) \sin 3\omega + h(2) \sin 2\omega + h(3) \sin \omega \right]$$

$$= e^{-j4\omega} \cdot e^{j\pi/2} \cdot 2 \cdot [h(0) \sin 4\omega + h(1) \sin 3\omega + h(2) \sin 2\omega + h(3) \sin \omega]$$

$$= e^{-j(4\omega-\pi/2)} \cdot 2 \cdot [h(0) \sin 4\omega + h(1) \sin 3\omega + h(2) \sin 2\omega + h(3) \sin \omega]$$

$$\Theta(\omega) = -(\alpha\omega + \beta)$$

$$\Theta(\omega) = -\left(4\omega + \frac{\pi}{2}\right) = -4\omega + \frac{\pi}{2}$$

$$\text{Phase delay } \tau_p = -\alpha = 4 \quad \beta = -\frac{\pi}{2}$$

$$\text{Group delay } \tau_g = -\alpha = 4$$

Since both delay are constant, it is a linear fn of ω .

In general case.

$$H(e^{j\omega}) = \sum_{n=0}^8 h(n)e^{-j\omega n}$$

$$H(e^{j\omega}) = \sum_{n=0}^3 h(n)e^{-j\omega n} + \sum_{n=5}^8 h(n)e^{-j\omega n}$$

$h(4)=0$ for antisymmetric impulse response sequence of odd length.

In general,

$$H(e^{j\omega}) = \sum_{n=0}^{\frac{N-3}{2}} h(n)e^{-j\omega n} + \sum_{n=\frac{N+1}{2}}^{N-1} h(n)e^{-j\omega n}$$

for antisymmetric with odd length $h(\frac{N-1}{2})=0$

$$\forall n \neq N-1-n \quad H(e^{j\omega}) = \sum_{n=0}^{\frac{N-3}{2}} h(n)e^{-j\omega n} + \sum_{n=0}^{\frac{N-3}{2}} h(N-1-n)e^{-j\omega(N-1-n)}$$

using antisymm property

$$h(n) = -h(N-1-n)$$

$$\therefore H(e^{j\omega}) = \sum_{n=0}^{\frac{N-3}{2}} h(n)e^{-j\omega n} - \sum_{n=0}^{\frac{N-3}{2}} h(n)e^{-j\omega(N-1-n)}$$

$$\begin{aligned}
 H(e^{j\omega}) &= \sum_{n=0}^{\frac{N-3}{2}} h(n) \left[e^{-j\omega n} - e^{-j\omega(N-1-n)} \right] \\
 &\quad - e^{-j\omega(\frac{N-1}{2})} \left\{ \sum_{n=0}^{\frac{N-3}{2}} h(n) \left[e^{j\omega(\frac{N-1}{2}-n)} - e^{-j\omega(\frac{N-1}{2}-n)} \right] \right\} \\
 &= e^{-j\omega(\frac{N-1}{2})} \quad (2j) \quad \left\{ \sum_{n=0}^{\frac{N-3}{2}} h(n) \cdot \sin \omega \left(\frac{N-1}{2} - n \right) \right\}
 \end{aligned}$$

$$\text{let } \frac{N-1}{2} - n = m$$

$$H(e^{j\omega}) = e^{-j\omega(\frac{N-1}{2})} \cdot e^{j\pi/2} \left[\sum_{m=1}^{\frac{N-1}{2}} 2h\left(\frac{N-1}{2} - m\right) \sin \omega m \right]$$

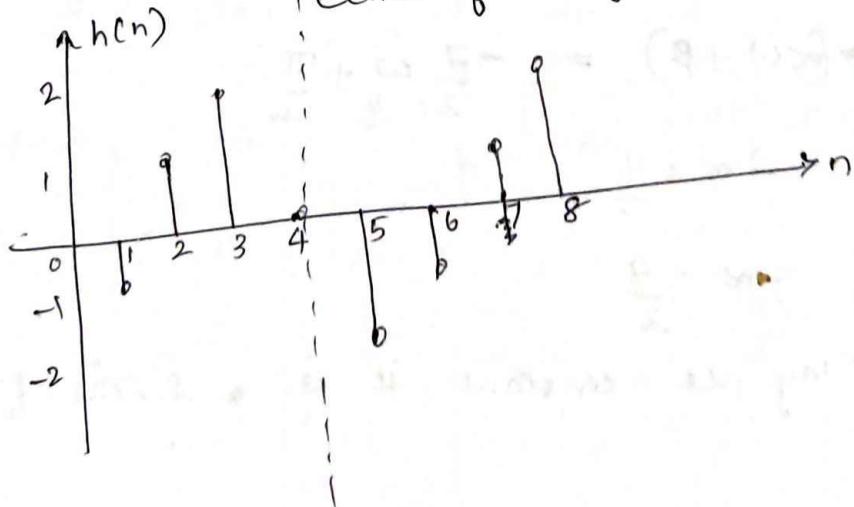
$$H(e^{j\omega}) = e^{-j\left[\omega\left(\frac{N-1}{2}\right) - \frac{\pi}{2}\right]} \overline{H(e^{j\omega})}$$

$$\overline{H(e^{j\omega})} = \sum_{n=1}^{\frac{N-1}{2}} 2h\left(\frac{N-1}{2} - n\right) \sin \omega n.$$

$$\Theta(\omega) = -\alpha\omega + \beta = -\left(\frac{N-1}{2}\right)\omega + \frac{\pi}{2}.$$

$$\alpha = \frac{N-1}{2}, \quad \beta = -\frac{\pi}{2}.$$

center of antisymmetric $\left(\frac{N-1}{2}\right)$.



(A) Antisymmetric impulse response with even length.

Let $N = 8$

$$H(z) = \sum_{n=0}^7 h(n)z^{-n}$$

$$H(z) = h(0) + h(1)z^{-1} + h(2)z^{-2} + h(3)z^{-3} + h(4)z^{-4} + h(5)z^{-5} \\ + h(6)z^{-6} + h(7)z^{-7}.$$

using anti-symm property

$$h(n) = -h(N-1-n).$$

$$h(0) = -h(7) \quad h(2) = -h(5)$$

$$h(1) = -h(6) \quad h(3) = -h(4)$$

$$H(z) = h(0)(1 - z^{-7}) + h(2)(z^{-2} - z^{-5}) + h(3)(z^{-3} + z^{-4}) \\ = z^{-7/2} \left[h(0)(z^{7/2} - z^{-7/2}) + h(1)(z^{5/2} - z^{-5/2}) + h(2)(z^{3/2} - z^{-3/2}) \right. \\ \left. + h(3)(z^{1/2} - z^{-1/2}) \right]$$

Taking F.T $z = e^{j\omega}$

$$H(e^{j\omega}) = e^{-j\frac{7}{2}\omega} \left[h(0) \sin \frac{7}{2}\omega + h(1) \sin \frac{5}{2}\omega + h(2) \sin \frac{3}{2}\omega \right. \\ \left. + h(3) \sin \frac{1}{2}\omega \right] \\ = e^{-j\frac{7}{2}\omega} \cdot e^{\frac{j\pi f}{2}} \left[h(0) \sin \frac{7}{2}\omega + h(1) \sin \frac{5}{2}\omega + h(2) \sin \frac{3}{2}\omega \right. \\ \left. + h(3) \sin \frac{1}{2}\omega \right]$$

$$\Theta(\omega) = -(\alpha\omega + \beta) = -\frac{\pi}{2}\omega + \frac{\pi}{2}$$

$$\tau_p = -\alpha = \frac{7}{2}$$

$$\tau_g = -\alpha = \frac{7}{2}$$

since both delay are constant, it is a linear fn of ω .

(10)

In general

$$H(e^{j\omega}) = \sum_{n=0}^N h(n)e^{-j\omega n}$$

$$H(e^{j\omega}) = \sum_{n=0}^3 h(n)e^{-j\omega n} + \sum_{n=4}^7 h(n)e^{-j\omega n}$$

$$= \sum_{n=0}^{\frac{N}{2}-1} h(n)e^{-j\omega n} + \sum_{n=\frac{N}{2}}^{N-1} h(n)e^{-j\omega n}$$

$$= \sum_{n=0}^{\frac{N}{2}-1} h(n)e^{-j\omega n} + \sum_{n=0}^{\frac{N}{2}-1} h(N-1-n)e^{-j\omega(N-1-n)}$$

using antisymmetry

$$h(n) = -h(N-1-n)$$

$$H(e^{j\omega}) = \sum_{n=0}^{\frac{N}{2}-1} h(n)e^{-j\omega n} - \sum_{n=0}^{\frac{N}{2}-1} h(n)e^{-j\omega(N-1-n)}$$

$$= \sum_{n=0}^{\frac{N}{2}-1} h(n) \left[e^{-j\omega n} - e^{-j\omega(N-1-n)} \right]$$

$$= e^{-j\omega(\frac{N-1}{2})} \sum_{n=0}^{\frac{N}{2}-1} h(n) \left[e^{j\omega(\frac{N-1}{2}-n)} - e^{-j\omega(\frac{N-1}{2}-n)} \right]$$

$$\cdot e^{-j\omega(\frac{N-1}{2})} \cdot 2j \cdot \sum_{n=0}^{\frac{N}{2}-1} h(n) \sin(\omega(\frac{N-1}{2}-n))$$

$$= e^{-j\omega(\frac{N-1}{2})} \cdot e^{j\pi/2} \cdot 2 \sum_{n=0}^{\frac{N}{2}-1} h(n) \sin(\omega(\frac{N-1}{2}-n))$$

$$\text{let } \frac{N}{2} - n = m$$

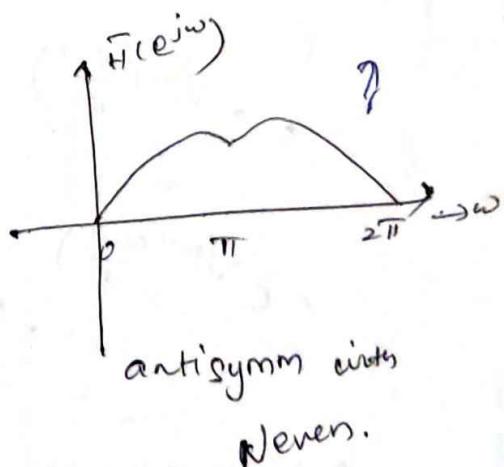
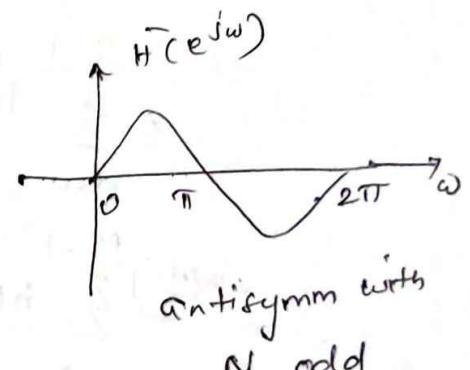
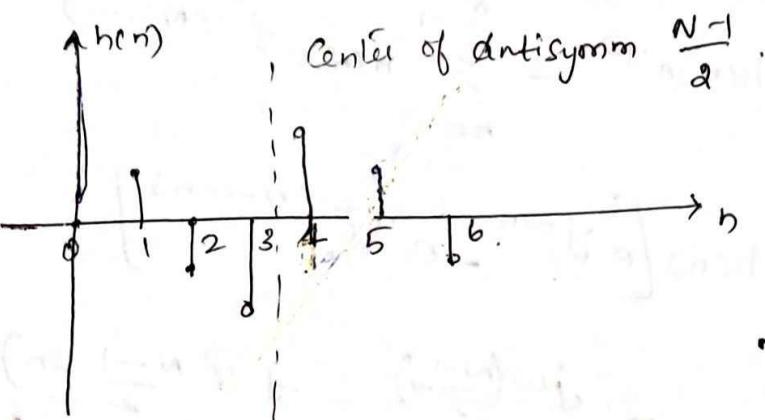
$$H(e^{j\omega}) = e^{-j\omega(\frac{N-1}{2})} e^{j\frac{\pi}{2}} \left[\sum_{m=1}^{\frac{N}{2}} h\left(\frac{N}{2}-m\right) \sin\omega\left(m-\frac{1}{2}\right) \right]$$

$$= e^{-j\left[\left(\frac{N-1}{2}\right)\omega - \frac{\pi}{2}\right]} \left\{ \sum_{n=0}^{\frac{N}{2}} h\left(\frac{N}{2}-n\right) \underbrace{\sin\omega\left(n-\frac{1}{2}\right)}_{H(e^{j\omega})} \right\}$$

$$\begin{aligned} \phi(\omega) &= -\left(\frac{N-1}{2}\omega + \frac{\pi}{2}\right) \\ &= -(\alpha\omega + \beta) \\ &= -\left(\frac{N-1}{2}\omega + \frac{\pi}{2}\right) \end{aligned}$$

$$\tau_p = -\alpha = \frac{N-1}{2} \quad \beta = -\frac{\pi}{2}$$

$$\tau_g = -\alpha = \frac{N-1}{2}$$



DESIGN OF FIR FILTER - FOURIER METHOD

The desired frequency response of a FIR filter can be represented as

$$H_d(e^{j\omega}) = \sum_{n=0}^{\infty} h_d(n) e^{-jn\omega} \quad (1)$$

The freq. response $H(e^{j\omega})$ is periodic with 2π .

The desired impulse response of the filter is given by

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{jnw} d\omega. \quad (2)$$

Z.T

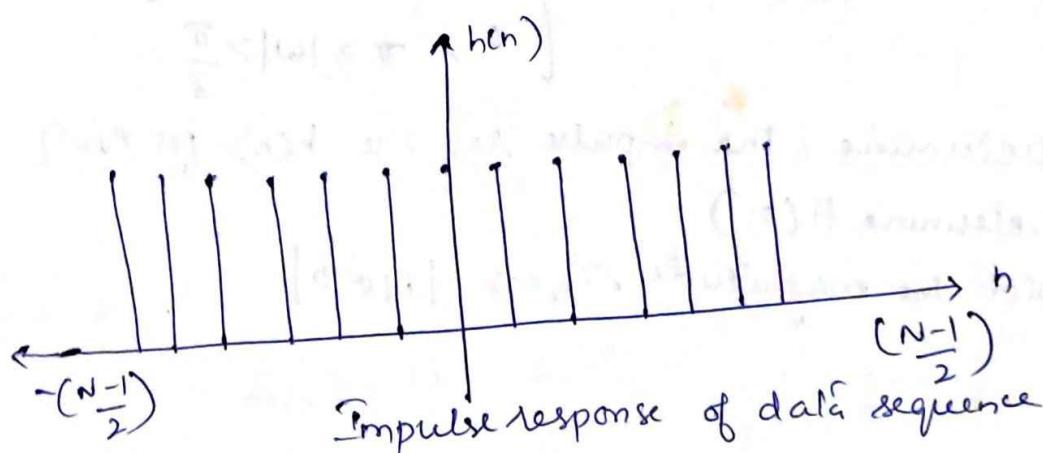
$$H_d(z) = \sum_{n=-\infty}^{\infty} h_d(n) z^n. \rightarrow \text{this is a infinite non-causal system}$$

— (3)

Not realizable.

In order to realize a finite system, the impulse response has to be finitized. This is done by truncating the long sequence as given below

$$h(n) = \begin{cases} h_d(n), & |n| \leq \left(\frac{N-1}{2}\right) \\ 0, & \text{elsewhere} \end{cases} \quad (4)$$



Sub ④ in ③

$$\left(\frac{N-1}{2}\right)$$

$$H(z) = \sum_{n=-\left(\frac{N-1}{2}\right)}^{(N-1)} h(n) z^n = h(0) + \sum_{n=1}^{\frac{N-1}{2}} [h(-n) z^n + h(n) z^{-n}]$$

$$h(n) = h(-n)$$

$$H(z) = h(0) + \sum_{n=1}^{\frac{N-1}{2}} h(n) (z^n + z^{-n})$$

Since impulse response is symmetric at center

$$h(n) = h(-n),$$

$$\therefore H(z) = h(0) + \sum_{n=1}^{\frac{N-1}{2}} h(n) [z^n + z^{-n}]. \rightarrow \text{non-causal}$$

delay unit can be realized using flip flop but advance unit is not realizable.

It can be converted to realizable filter by multiplying entire system with $z^{-\left(\frac{N-1}{2}\right)}$

$$\bar{H}(z) = \left\{ h(0) + \sum_{n=1}^{\frac{N-1}{2}} h(n) [z^n + z^{-n}] \right\} z^{-\left(\frac{N-1}{2}\right)}$$

$$\bar{H}(z) = z^{-\left(\frac{N-1}{2}\right)} H(z)$$

Problems

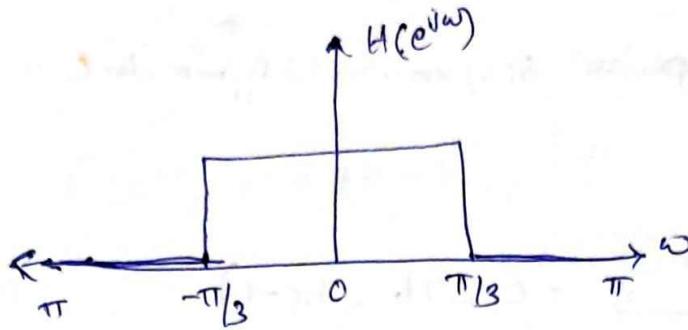
(i) Design an ideal low pass filter whose desired freq response is

$$H_d(e^{j\omega}) = \begin{cases} 1, & \frac{\pi}{3} \geq \omega \geq -\frac{\pi}{3} \\ 0, & \pi \geq |\omega| > \frac{\pi}{3} \end{cases}$$

(i) Determine the impulse response $h(n)$ for $N=9$

(ii) Determine $H(z)$

(iii) Plot the magnitude response $|H(e^{j\omega})|$



desired impulse response

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega$$

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi/3}^{\pi/3} 1 \cdot e^{j\omega n} d\omega$$

$$= \frac{1}{2\pi} \left[\frac{e^{j\omega n}}{jn} \right]_{-\pi/3}^{\pi/3}$$

$$= \frac{1}{2\pi jn} \left[e^{j\pi/3 n} - e^{-j\pi/3 n} \right]$$

$$= \frac{1}{\pi n} \sin \frac{\pi}{3} n, \quad n \geq 0 \geq -n$$

To obtain desired impulse response truncate the infinite sequence of $h_d(n)$ to 9 samples

$$h(n) = \begin{cases} h_d(n) & |n| \leq 4 \\ 0 & \text{otherwise} \end{cases}$$

$$h_d(n) = \underbrace{\frac{\sin \frac{\pi}{3} n}{\pi n}}_{n \neq 0} \quad n = -4, -3, -2, -1, 0, 1, 2, 3, 4$$

For $n=0$

$$h(0) = \lim_{n \rightarrow 0} \frac{\sin \frac{\pi}{3} n}{\pi n}$$

$$\stackrel{n \rightarrow 0}{\sim} \frac{1}{3} \cdot \frac{1}{3} = \frac{1}{9}$$

$$= \lim_{n \rightarrow 0} \frac{1}{3} \cdot \frac{\sin \frac{\pi}{3} n}{\frac{\pi}{3} n} = \frac{1}{3}$$

$$\stackrel{n \rightarrow 0}{\sim} \frac{\sin \alpha}{\alpha} = 1$$

Since impulse response is symmetric

For $4 \geq n \geq 1$

$$h(1) = \frac{\sin \frac{\pi}{3}}{\pi} = 0.276 = h(-1)$$

$$h(2) = \frac{\sin \frac{2\pi}{3}}{2\pi} = 0.138 = h(-2)$$

$$h(3) = \frac{\sin \frac{3\pi}{3}}{3\pi} = 0 = h(-3)$$

$$h(4) = \frac{\sin \frac{4\pi}{3}}{4\pi} = -0.069 = h(-4)$$

(ii) $H(z)$

$$\begin{aligned} H(z) &= h(0) + \sum_{n=1}^{\frac{N-1}{2}} h(n)(z^n + z^{-n}) \\ &= \frac{1}{3} + h(1)(z^1 + z^{-1}) + h(2)(z^2 + z^{-2}) + h(3)(z^3 + z^{-3}) \\ &\quad + h(4)(z^4 + z^{-4}) \\ &= \frac{1}{3} + 0.276(z + z^{-1}) + 0.138(z^2 + z^{-2}) + 0.069(z^4 + z^{-4}) \end{aligned}$$

To obtain realizable filter multiply by $z^{-(\frac{N-1}{2})} = z^{-4}$

$$\begin{aligned} \bar{H}(z) &= \frac{1}{3}z^{-4} + 0.276(z^{-3} + z^{-5}) + 0.138(z^{-2} + z^{-6}) \\ &\quad - 0.069(z^{-4} + z^{-8}) \end{aligned}$$

$$= 0.069$$

$$\begin{aligned} &= -0.069 + 0.138z^{-2} + 0.276z^{-3} + 0.33z^{-4} + 0.276z^{-5} \\ &\quad + 0.138z^{-6} - 0.069z^{-8}. \end{aligned}$$

The impulse response is symm with odd length. (B)

$$\bar{H}(e^{j\omega}) = h\left(\frac{N-1}{2}\right) + 2 \sum_{n=1}^{\frac{N-1}{2}} h\left(\frac{N-1}{2}-n\right) \cos \omega n.$$

N = 9

$$\bar{H}(e^{j\omega}) = h(4) + 2 \sum_{n=1}^4 h(4-n) \cos \omega n.$$

∴ it satisfies the condition

$$h(n) = h(N-1-n)$$

The filter coefficients of causal filter are

$$h(0) = h(8) = -0.069$$

$$h(1) = h(7) = 0$$

$$h(2) = h(6) = 0.138$$

$$h(3) = h(5) = 0.276$$

$$h(4) = 0.333$$

The freq response is

$$\begin{aligned} \bar{H}(e^{j\omega}) &= 0.333 + 2h(3)\cos \omega + 2h(2)\cos 2\omega + 2h(1)\cos 3\omega \\ &\quad + 2h(0)\cos 4\omega \end{aligned}$$

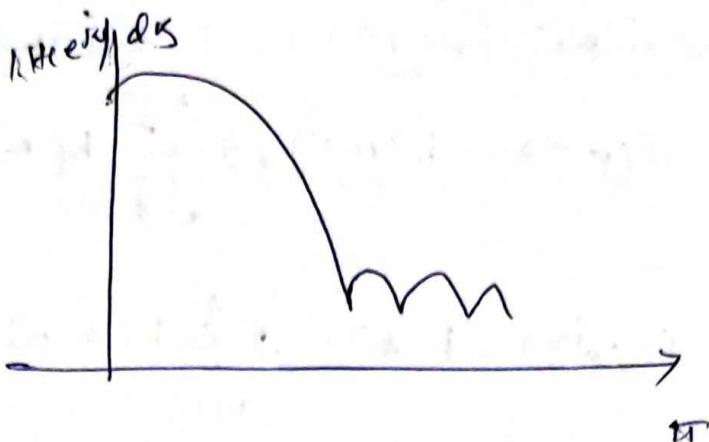
$$\begin{aligned} \bar{H}(e^{j\omega}) &= 0.333 + 2 \times 0.276 \cos \omega + 2 \times 0.138 \cos 2\omega \\ &\quad + 2 \cdot (0.069) \cos 3\omega \\ &\quad + 2(-0.069) \cos 4\omega \\ &= 0.333 + 0.552 \cos \omega + 0.276 \cos 2\omega - 0.138 \cos 4\omega. \end{aligned}$$

$$\text{mag } |H(e^{j\omega})|_{dB} = 20 \lg |\bar{H}(e^{j\omega})|$$

$$\omega (\text{in deg}) \quad 0 \quad 10 \quad 20 \quad 30 \quad 40 \quad 50 \quad 60 \quad 70 \quad 80$$

$$|H(e^{j\omega})|_{dB}$$

$$90 \quad 100 \quad 110 \quad 120 \quad 130 \quad 140 \quad 150 \quad 160 \quad 170 \quad 180$$



Freq response of RPF

FIR filter design

- (1) window method — Rectangular, Hanning, Hamming and Kaiser.
- (2) frequency sampling technique
- (3) optimal filter design methods.

Generalized cosine windows.
(triangular or
Bartlett windows
raised cosine).

34, 25, 27, 49, 51

DESIGN OF FIR FILTER - WINDOWING TECHNIQUES

The frequency response of desired sequence $H_d(e^{j\omega})$ is given by

$$H_d(e^{j\omega}) = \sum_{n=-\infty}^{\infty} h_d(n)e^{-j\omega n}$$

For causal system

$$H_d(e^{j\omega}) = \sum_{n=0}^{\infty} h_d(n)e^{-j\omega n}$$

The $h_d(n)$ is inverse fourier transform of $H_d(e^{j\omega})$, i.e.,

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega.$$

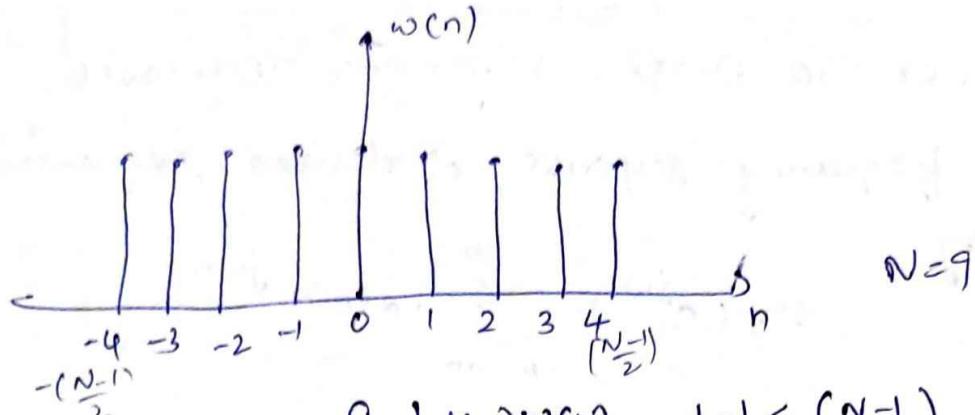
In Fourier method, in order to obtain filter of length N , the infinite length of desired impulse response $h_d(n)$ is truncated at $n = \pm \left(\frac{N-1}{2}\right)$.

Instead of truncating the desired impulse response $h_d(n)$, the same can be obtained by using a 'rectangular window'.

The rectangular window can be defined as

$$w(n) = \begin{cases} 1, & |n| \leq \left(\frac{N-1}{2}\right) \\ 0, & \text{otherwise} \end{cases}$$

The finite duration impulse response is obtained when the desired impulse response (infinite duration) is multiplied with rectangular window $w(n)$.



$$h(n) = \begin{cases} h_d(n)w(n), & |n| \leq \left(\frac{N-1}{2}\right) \\ 0, & \text{otherwise.} \end{cases}$$

$$h_d(n) \times w(n) \xleftrightarrow{\text{F.T.}} H_d(e^{j\omega}) * W(e^{j\omega}).$$

\therefore Frequency of finite data is given by

$$H(e^{j\omega}) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) W(e^{j(\omega-\Omega)}) d\Omega.$$

F.T of rectangular window is

$$W(e^{j\omega}) = \sum_{n=-\frac{N-1}{2}}^{\frac{N-1}{2}} 1 \cdot e^{-j\omega n}$$

$$n = -\frac{N-1}{2}$$

$$= \sum_{n=0}^{N-1} e^{-j\omega n} = e^{j\omega \frac{N-1}{2}} \left(\frac{1 - e^{-j\omega N}}{1 - e^{-j\omega}} \right)$$

$$= e^{j\omega \frac{N-1}{2}} \frac{e^{-j\omega \left(\frac{N-1}{2}\right)}}{e^{-j\omega/2}} \left[\frac{e^{j\omega N/2} - e^{-j\omega N/2}}{e^{j\omega/2} - e^{-j\omega/2}} \right] = e^{j\omega \frac{N-1}{2}} \frac{e^{j\omega N}}{e^{j\omega/2}} \left[\frac{1 - e^{-j\omega N}}{1 - e^{-j\omega}} \right]$$

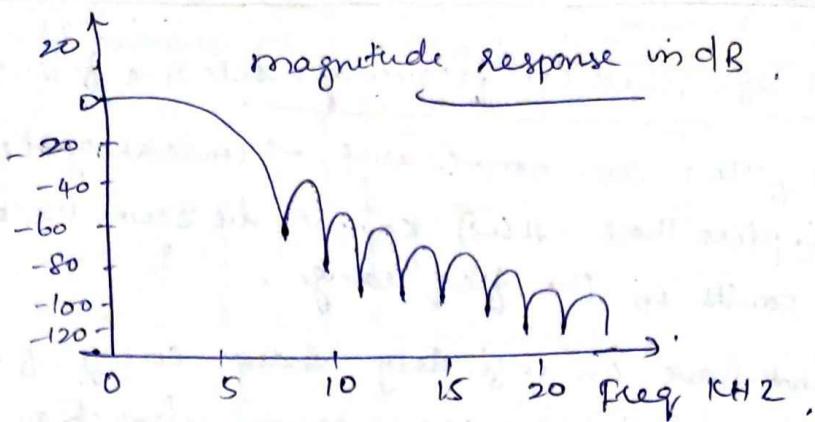
$$= e^{-j\omega \left(\frac{N-1}{2}\right)} \frac{\sin \omega N/2}{\sin \omega/2}$$

$$= e^{j\omega \frac{N-1}{2}} e^{-j\omega \left(\frac{N-1}{2}\right)} \frac{\sin \omega N/2}{\sin \omega/2}$$

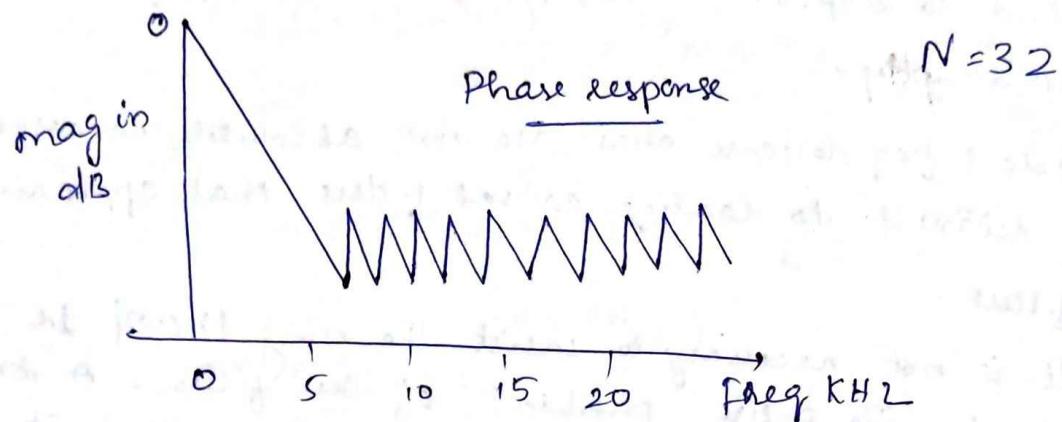
magnitude response

$$|W(\omega)| = \frac{|\sin(\omega N/2)|}{|\sin(\omega/2)|}$$

$$-\pi \leq \omega \leq \pi, \boxed{|W(\omega)| = \frac{|\sin \omega N/2|}{|\sin \omega/2|}}$$



(15)



The freq response of rect. window consists of main lobe and side lobes. The height and width of the main lobe is large compared to side lobes.

Main lobe - central part has energy fr. $\frac{2\pi}{N}$ to $\frac{2\pi}{N}$
 Side lobes - ~~has~~ spectral leakage (Should be ~~ringing effect~~)
 convolution of $H_d(\omega)$ with $W(\omega)$ has smoothing effect (negligible)

as $N \uparrow$ s, main lobe becomes narrower and side lobe width also decreases. But height \uparrow s and effective area remains same. Smoothing effect reduces, but reduces spectral leakage.

Characteristics of Practical frequency-selective filters

ideal filters are non-causal \rightarrow unrealizable

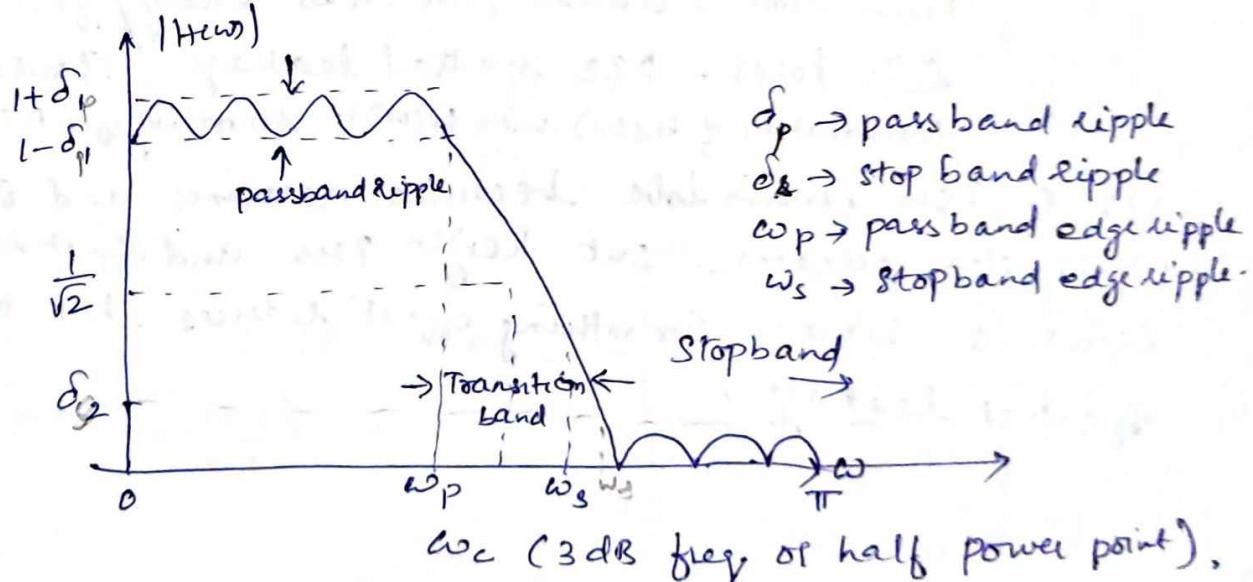
Causality implies that $H(\omega)$ cannot be zero, except at a finite set of points in the freq range.

$H(\omega)$ cannot have an infinitely sharp cutoff from passband to stopband i.e.) $H(\omega)$ cannot drop from unity to zero abruptly.

ideal freq response char are not absolutely necessary. It is relaxed to realize causal filters that approximate ideal filters.

It is not necessary to insist the mag $|H(\omega)|$ be constant in the entire passband of the filter. A small amount of ripple in the passband is tolerable. Also, it is not necessary that $|H(\omega)|$ to be zero in the stopband.

transition of freq response from passband to stopband defines the transition band.



The approximation of $H(\omega)$ depends on the filter co-efficients as well the length of samples.

Passband $0 \leq \omega \leq \omega_p$

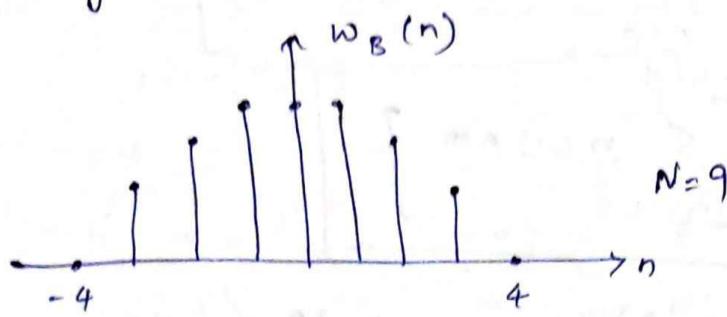
$$1 - \delta_p \leq H(e^{j\omega}) \leq 1 + \delta_p \quad |\omega| \leq \omega_p$$

Stopband $\omega_s \leq \omega \leq \infty$

$$H(e^{j\omega}) \leq \delta_s \quad \omega_s \leq |\omega| < \infty$$

(2) Triangular window (Barlett window).

(16)



Gibbs phenomenon is reduced by choosing a window which has smooth transition in the filter.

$$w_B(n) = 1 - \frac{2|n|}{N-1} \quad , \quad \left(\frac{N-1}{2}\right) \geq n \geq -\left(\frac{N-1}{2}\right)$$

F.T

$$w_B(e^{j\omega}) = \sum_{n=-\left(\frac{N-1}{2}\right)}^{\frac{N-1}{2}} \left(1 - \frac{2|n|}{N-1}\right) e^{j\omega n}$$

$$= \sum_{n=-\left(\frac{N-1}{2}\right)}^{\frac{N-1}{2}} e^{j\omega n} - \frac{2}{N-1} \sum_{n=-\left(\frac{N-1}{2}\right)}^{\frac{N-1}{2}} \ln 1 e^{j\omega n}$$

First term

$$w_B(e^{j\omega}) = \sum_{n=0}^{\frac{N-1}{2}} e^{-j\omega n} = \frac{\sin \frac{\omega N}{2}}{\frac{\sin \frac{\omega}{2}}{2}}$$

$$\begin{aligned} & e^{j\omega\left(\frac{N-1}{2}\right)} + \dots + e^{-j\omega\left(\frac{N-1}{2}\right)} \\ & [1 + e^{j\omega\left(\frac{N-1}{2}\right)} + \dots + e^{-j\omega\left(\frac{N-1}{2}\right)}] \\ & = e^{j\omega\left(\frac{N-1}{2}\right)} \sum_{n=0}^{\frac{N-1}{2}} e^{j\omega n} \\ & = e^{j\omega\left(\frac{N-1}{2}\right)} \frac{(1 - e^{j\omega\frac{N-1}{2}})}{1 - e^{-j\omega}} \end{aligned}$$

Second term

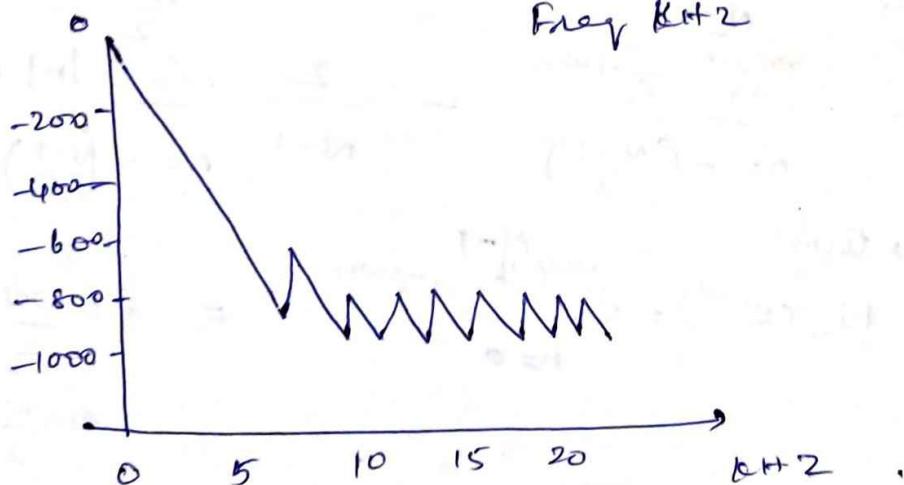
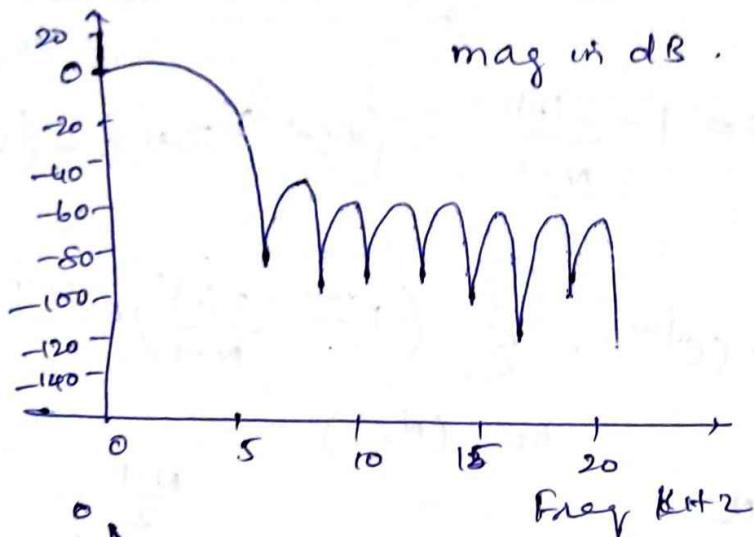
$$\frac{2}{N-1} \sum_{n=-\left(\frac{N-1}{2}\right)}^{\frac{N-1}{2}} \ln 1 e^{-j\omega n} = \frac{2}{N-1} \left[\sum_{n=-\left(\frac{N-1}{2}\right)}^{-1} -n e^{j\omega n} + \sum_{n=0}^{\frac{N-1}{2}} n e^{-j\omega n} \right]$$

$$= \frac{2}{N-1} \left[\sum_{n=1}^{\frac{N-1}{2}} n e^{-j\omega n} + \sum_{n=0}^{\frac{N-1}{2}} n e^{-j\omega n} \right]$$

$$= \frac{2}{N-1} \left[\sum_{n=0}^{\frac{N-1}{2}} n e^{j\omega n} + \sum_{n=0}^{\frac{N-1}{2}} n e^{-j\omega n} \right]$$

$$= \frac{2}{N-1} \left[\sum_{n=0}^{\frac{N-1}{2}} n (e^{j\omega n} + e^{-j\omega n}) \right]$$

$$W_B(e^{j\omega}) = \frac{4}{N-1} \left[\sum_{n=0}^{\frac{N-1}{2}} n \cos \omega n \right]$$



Raised cosine window.

$$W_\alpha(n) = \alpha + (1-\alpha) \cos \left(\frac{2\pi n}{N-1} \right), \quad \frac{N-1}{2} \geq n \geq -\left(\frac{N-1}{2}\right)$$

Taking F-T

$$W_\alpha(e^{j\omega}) = \sum_{n=-\left(\frac{N-1}{2}\right)}^{\frac{N-1}{2}} \left[\alpha + (1-\alpha) \cos \left(\frac{2\pi n}{N-1} \right) \right] e^{-j\omega n}$$

$$w_\alpha(e^{j\omega}) = \sum_{n=-\left(\frac{N-1}{2}\right)}^{\frac{N-1}{2}} \alpha e^{-j\omega n} + (1-\alpha) \sum_{n=-\left(\frac{N-1}{2}\right)}^{\frac{N-1}{2}} \left[\frac{e^{j\frac{2\pi}{N-1}n} + e^{-j\frac{2\pi}{N-1}n}}{2} \right] e^{-j\omega n}$$

$$= \sum_{n=-\left(\frac{N-1}{2}\right)}^{\frac{N-1}{2}} \alpha e^{-j\omega n} + \frac{(1-\alpha)}{2} \sum_{n=-\left(\frac{N-1}{2}\right)}^{\frac{N-1}{2}} e^{+j\left(\omega - \frac{2\pi}{N-1}\right)n} + \frac{(1-\alpha)}{2} \sum_{n=-\left(\frac{N-1}{2}\right)}^{\frac{N-1}{2}} e^{-j\left(\omega + \frac{2\pi}{N-1}\right)n}$$

first term

$$\sum_{n=-\frac{N-1}{2}}^{\frac{N-1}{2}} \alpha e^{-j\omega n} = e^{j\omega\left(\frac{N-1}{2}\right)} \sum_{n=0}^{N-1} \alpha e^{-j\omega n}$$

$$= e^{j\omega\left(\frac{N-1}{2}\right)} \alpha \left[\frac{1 - e^{-j\omega N}}{1 - e^{-j\omega}} \right]$$

$$= e^{j\omega\left(\frac{N-1}{2}\right)} \alpha e^{-j\omega N/2} \frac{\left[e^{j\omega N/2} - e^{-j\omega N/2} \right]}{e^{-j\omega/2} \overline{\left[e^{j\omega/2} - e^{-j\omega/2} \right]}}$$

$$= e^{j\omega\left(\frac{N-1}{2}\right)} \cdot e^{-j\omega\left(\frac{N-1}{2}\right)} \alpha \frac{\sin \omega N/2}{\sin \omega/2}$$

$$= \alpha \frac{\sin \omega N/2}{\sin \omega/2}$$

Second term

$$\frac{1-\alpha}{2} \sum_{n=-\frac{N-1}{2}}^{\frac{N-1}{2}} e^{+j\left(\omega - \frac{2\pi}{N-1}\right)n} = \frac{(1-\alpha)}{2} \cdot e^{j\left(\omega - \frac{2\pi}{N-1}\right)\left(\frac{N-1}{2}\right)} \sum_{n=0}^{N-1} e^{-j\omega n}$$

$$= e^{j(\omega - \frac{2\pi}{N-1})(\frac{N-1}{2})(\frac{1-\alpha}{2})} \left[\frac{1 - e^{-j(\omega - \frac{2\pi}{N-1})N}}{1 - e^{-j(\omega - \frac{2\pi}{N-1})}} \right]$$

$$= e^{j(\omega - \frac{2\pi}{N-1})(\frac{N-1}{2})(\frac{1-\alpha}{2})} \left\{ \frac{e^{-j(\omega - \frac{2\pi}{N-1})\frac{N}{2}}}{e^{-j(\omega - \frac{2\pi}{N-1})\frac{1}{2}}} \left[\frac{\left(e^{j(\omega - \frac{2\pi}{N-1})\frac{N}{2}} - e^{-j(\omega - \frac{2\pi}{N-1})\frac{N}{2}} \right)}{\left(e^{j(\omega - \frac{2\pi}{N-1})\frac{1}{2}} - e^{-j(\omega - \frac{2\pi}{N-1})\frac{1}{2}} \right)} \right] \right\}$$

$$= \frac{1-\alpha}{2} \frac{\sin(\omega - \frac{2\pi}{N-1})\frac{N}{2}}{\sin(\omega - \frac{2\pi}{N-1})\frac{1}{2}}$$

Third term

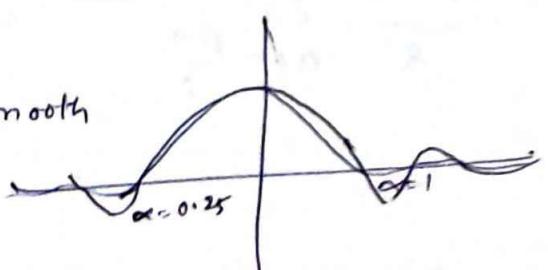
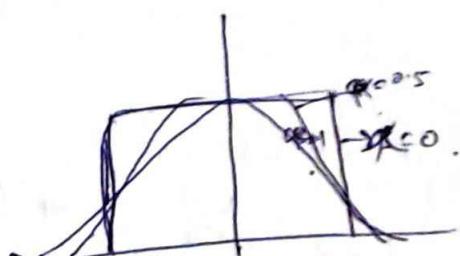
$$\left(\frac{1-\alpha}{2} \right) \sum_{n=-\frac{N-1}{2}}^{\frac{N-1}{2}} e^{-j(\omega + \frac{2\pi}{N-1})n} = \frac{1-\alpha}{2} \left[\frac{\sin(\omega + \frac{2\pi}{N-1})\frac{N}{2}}{\sin(\omega + \frac{2\pi}{N-1})\frac{1}{2}} \right]$$

$$W_\alpha(e^{j\omega})_c \propto \frac{\sin \omega N/2}{\sin \omega/2} + \left(\frac{1-\alpha}{2} \right) \left\{ \frac{\sin(\omega - \frac{2\pi}{N-1})\frac{N}{2}}{\sin(\omega - \frac{2\pi}{N-1})\frac{1}{2}} + \frac{\sin(\omega + \frac{2\pi}{N-1})\frac{N}{2}}{\sin(\omega + \frac{2\pi}{N-1})\frac{1}{2}} \right\}$$

Raised cosine filter has a cosine for 'raised up' at non-zero portion of the freq spectrum.

$\alpha \rightarrow$ roll off factor
measure of excess Bandwidth.
ripple increases as α decreases.

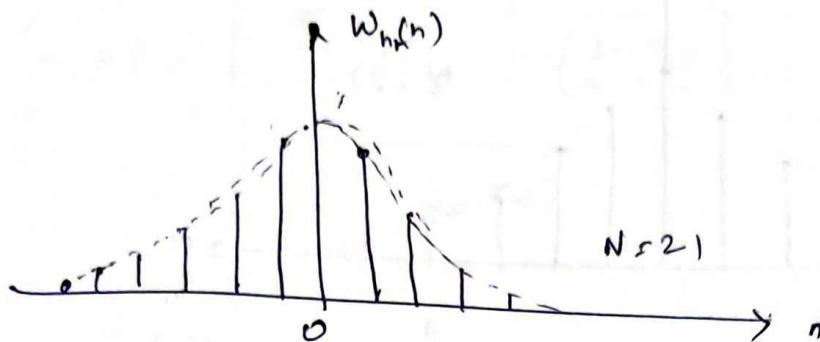
avoids spectral leakage and has smooth envelope.



Hanning Window.

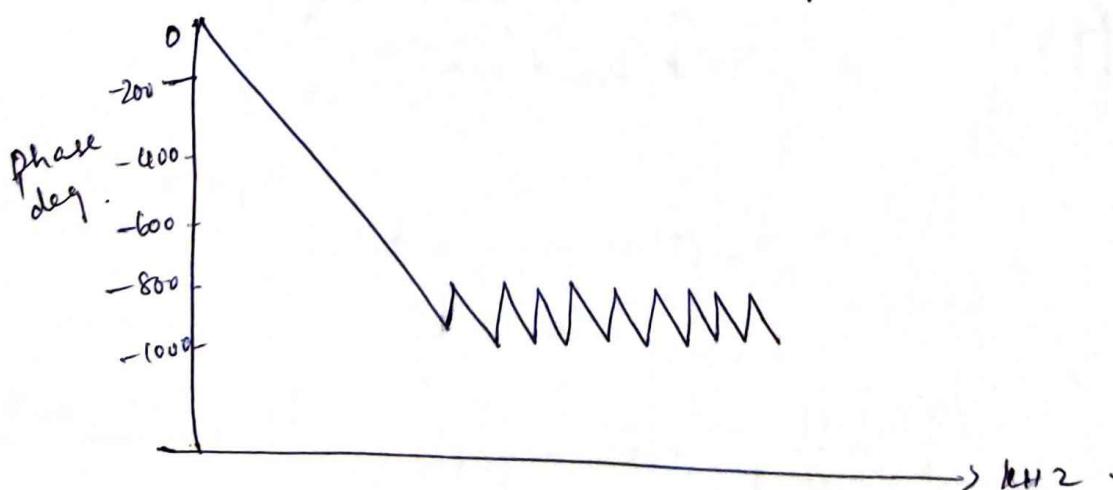
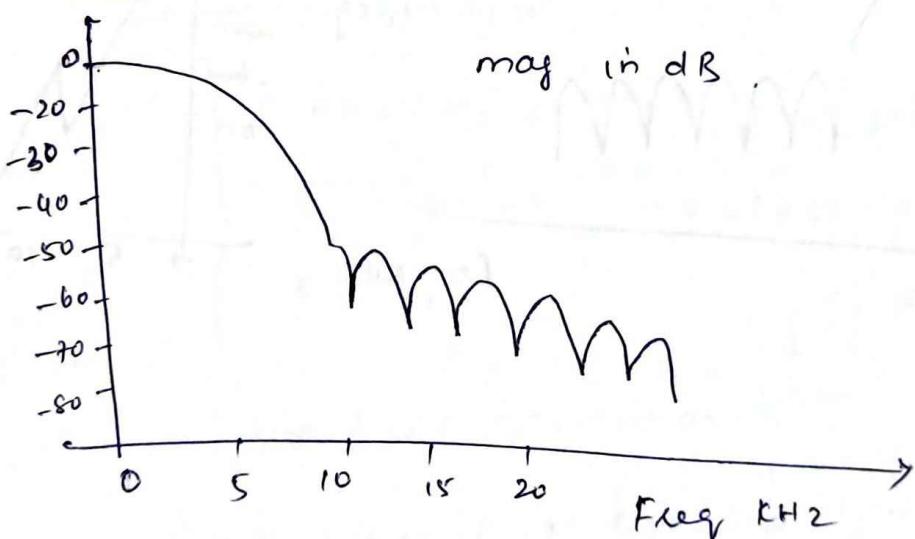
$\alpha = 0.5$ in raised cosine window.

$$w_{hn} = 0.5 + 0.5 \cos\left(\frac{2\pi n}{N-1}\right) , \quad \frac{N-1}{2} \geq n \geq -\frac{N-1}{2}$$



$$W_{hn}(e^{j\omega}) = 0.5 \frac{\sin \omega N/2}{\sin \omega/2} + 0.25 \left\{ \begin{array}{l} \frac{\sin(\omega - \frac{2\pi}{N-1}) \frac{N}{2}}{\sin(\omega - \frac{2\pi}{N-1})^2} + \frac{\sin(\omega + \frac{2\pi}{N-1}) \frac{N}{2}}{\sin(\omega + \frac{2\pi}{N-1})^2} \\ \end{array} \right.$$

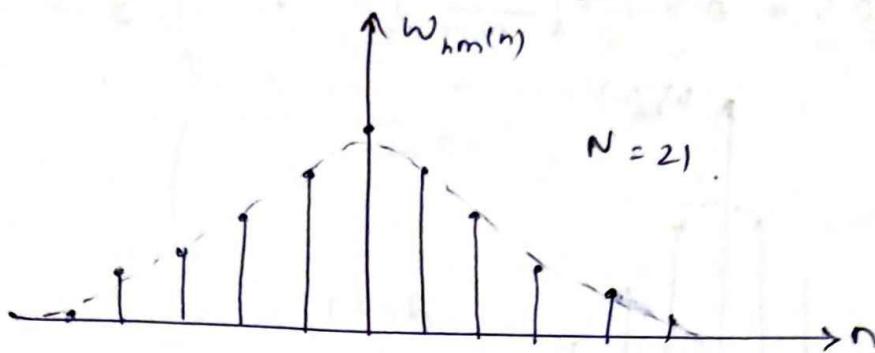
mag response



Hamming window

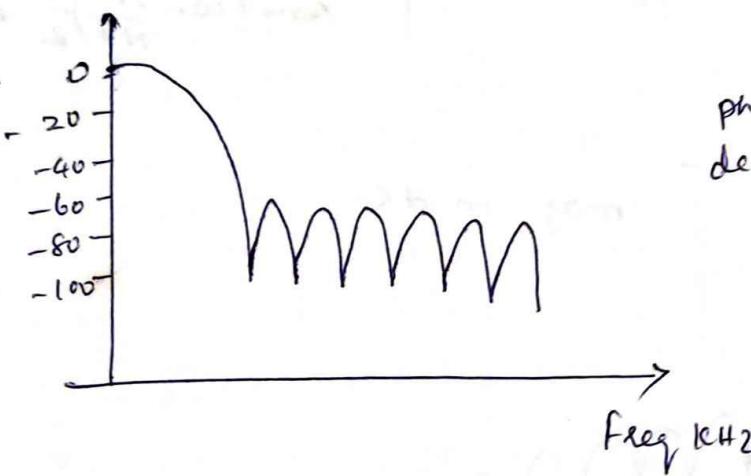
$$\alpha = 0.54$$

$$w_{hm}(n) = 0.54 + 0.46 \cos\left(\frac{2\pi n}{N-1}\right) \quad , \quad \left(\frac{N-1}{2}\right) \geq n \geq -\left(\frac{N-1}{2}\right)$$

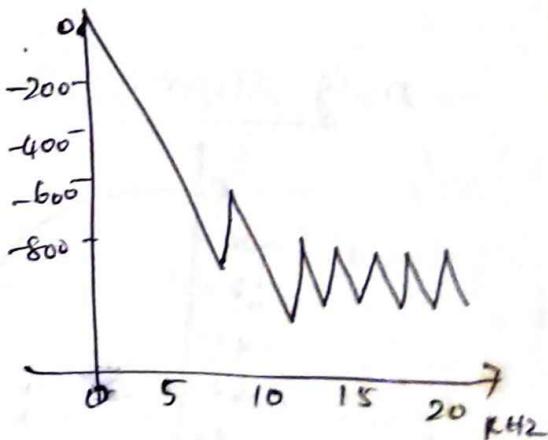


$$W_{hm}(e^{j\omega}) = 0.54 \frac{\sin(\omega N/2)}{\sin(\omega/2)} + 0.23 \left\{ \frac{\sin(\omega - 2\pi/N) \frac{N}{2}}{\sin(\omega - 2\pi/(N-1)) \frac{1}{2}} + \frac{\sin(\omega + 2\pi/N) \frac{N}{2}}{\sin(\omega + 2\pi/(N-1)) \frac{1}{2}} \right\}$$

dB mag



phase deg.



KAI SER WINDOW

(19)

It has control over ripples by means of an additional parameter characterizing the window.

$$W_K(\alpha, n) = \begin{cases} \frac{I_0 \left[\alpha \sqrt{1 - \left(\frac{2n}{N-1} \right)^2} \right]}{I_0(\alpha)}, & \frac{N-1}{2} \geq n \geq -\frac{N-1}{2} \\ 0, & \text{otherwise.} \end{cases}$$

where

$$I_0(\alpha) = \sum_{k=0}^{\infty} \left[\frac{(\alpha/2)^k}{k!} \right]^2$$

$I_0(\alpha) \rightarrow$ modified Bessel function of its first kind of order zero.

$\alpha \rightarrow$ adjustable parameter.

$$\alpha = \begin{cases} 0.1102(\alpha_s' - 8.7) & \alpha_s' > 50 \\ 0.5842(\alpha_s' - 21)^{0.4} + 0.07886(\alpha_s' - 21), 50 \geq \alpha_s' \geq 21 \\ 0 & \alpha_s' \leq 21. \end{cases}$$

$\alpha_s' \rightarrow$ stop band attenuation factor. $\alpha_s' = -20 \log_{10} \delta$
 $\delta = \min(\delta_s, \delta_p)$

$\delta_s \rightarrow$ minimal of stopband ripple

$\delta_p \rightarrow$ ^{minimal} pass band ripple

$\delta \rightarrow$ ripple factor

stop band ripple

$$\alpha_s = -20 \log_{10} \delta_s$$

$$\delta_s = 10^{-0.05 \alpha_s}$$

pass band ripple

$$\alpha_p = -20 \log_{10} \left[\frac{1 + \delta_p}{1 - \delta_p} \right]$$

$$\delta_p = \left[\frac{10^{0.05 \alpha_p} - 1}{10^{0.05 \alpha_p} + 1} \right]$$

$$\delta_3 \geq \delta_p$$

order of Kaiser

$$N = \begin{cases} \frac{\alpha_s' - 7.95}{14.36(\Delta f)} & , \alpha_s' > 21 \\ \frac{0.4611}{\Delta f} & , \alpha_s' \leq 21 \end{cases}$$

$\Delta f \rightarrow$ desired transition width.

Frequency response of Kaiser window.

Taking f.T of $w_k(\alpha, n)$

$$w_k(e^{j\omega}) = F.T [w_k(n)]$$

$$w_k(e^{j\omega}) = \frac{2 \sin \left\{ \left(\frac{N-1}{2} \right) \left[\omega^2 - \left(\frac{2\alpha}{N-1} \right)^2 \right]^{1/2} \right\}}{I_0(\alpha) \left[\omega^2 - \left(\frac{2\alpha}{N-1} \right)^2 \right]^{1/2}}$$

Design a linear phase FIR filter using Hamming and Hanning windows for the following desired freq response

$$H_d(\omega) = \begin{cases} e^{-j3\omega} & , \frac{\pi}{4} \leq |\omega| \leq \pi \\ 0 & , \text{otherwise} \end{cases}$$

$$\omega_c = \frac{\pi}{4}$$

$$\frac{M-1}{2} = 3 \therefore \text{filter length} = 7.$$

$$h(n) = h_d(n) \cdot w_{ham}(n)$$

$$\begin{aligned}
 h_d(n) &= \frac{1}{2\pi} \int_{-\pi}^{-\omega_c} e^{-j3\omega} \cdot e^{j\omega n} d\omega + \frac{1}{2\pi} \int_{\omega_c}^{\pi} e^{-j3\omega} \cdot e^{j\omega n} d\omega. \quad (20) \\
 &= \text{...} \quad \frac{1}{2\pi} \left[\frac{e^{j(n-3)\omega}}{j(n-3)} \right]_{-\pi}^{-\omega_c} + \frac{1}{2\pi} \left[\frac{e^{j(n-3)\omega}}{j(n-3)} \right]_{\omega_c}^{\pi} \\
 &= \frac{1}{2\pi} \left[\frac{e^{-j(n-3)\omega_c}}{j(n-3)} - \frac{e^{-j(n-3)\pi}}{j(n-3)} \right] \\
 &\quad + \frac{1}{2\pi} \left[\frac{e^{j(n-3)\pi}}{j(n-3)} - \frac{e^{j(n-3)\omega_c}}{j(n-3)} \right] \\
 &= \frac{1}{2\pi j(n-3)} \left[e^{-j(n-3)\omega_c} - e^{j(n-3)\omega_c} + e^{j(n-3)\pi} - e^{-j(n-3)\pi} \right] \\
 &= -\frac{\sin(n-3)\omega_c}{(n-3)\pi} \quad n \neq 3.
 \end{aligned}$$

$$\begin{aligned}
 h_d(3) &= \frac{1}{2\pi} \left[\int_{-\pi}^{-\omega_c} d\omega + \int_{\omega_c}^{\pi} d\omega \right] \\
 &= \frac{\pi - \omega_c}{\pi}.
 \end{aligned}$$

$$\omega_c = \frac{\pi}{4}$$

$$h_d(n) = \frac{\sin \frac{\pi}{4}(n-3)}{\pi(n-3)} \quad n \neq 3$$

$$h_d(3) = \frac{\pi - \frac{\pi}{4}}{\pi} = \frac{4\pi - \pi}{4\pi} = \frac{3}{4} = 0.75$$

$$h_d(0) = h_d(6) = -0.07506$$

$$h_d(1) = h_d(5) = -0.15923$$

$$h_d(2) = h_d(4) = -0.22586$$

Hamming window -

$$W_{ham}(n) = 0.54 - 0.46 \cos\left(\frac{2\pi n}{6}\right) \quad 0 \leq n \leq N-1$$

$$W_{ham}(0) = W_{ham}(6) = 0.08$$

$$W_{ham}(1) = W_{ham}(5) = 0.31$$

$$W_{ham}(2) = W_{ham}(4) = 0.77$$

$$W_{ham}(3) = 1$$

$$h(n) = h_d(n) \cdot W_{ham}(n)$$

$$= \left\{ -0.006, -0.04936, -0.17391, 0.75, -0.17396, \right. \\ \left. -0.04936, -0.006 \right\}$$

Hamming window

$$W_{ham}(n) = 0.5 - 0.5 \cos \frac{2\pi n}{6}$$

$$W_{ham}(0) = W_{ham}(6) = 0$$

$$W_{ham}(1) = W_{ham}(5) = 0.25$$

$$W_{ham}(2) = W_{ham}(4) = 0.75$$

$$W_{ham}(3) = 1$$

$$h(n) = h_d(n) W_{ham}(n) = \left\{ 0, -0.0398, -0.16939, 0.75, \right. \\ \left. -0.16939, -0.0398, 0 \right\}$$

$$\text{when } n < \frac{N-1}{2} \text{ or } n > \frac{N+1}{2}, \quad h(n) = h_d(n) \cdot W_{ham}(n)$$

$$= \left\{ 0, -0.0398, -0.16939, 0.75, -0.16939, -0.0398, 0 \right\}$$

use $H(z) = h(0) + \sum_{n=1}^{\infty} h(n)(z^{n+2})$

and multiply with $\frac{1}{2}(1+z^{-2})$

$$H(z) = 0.02 - 0.0398z^{-1} - 0.16939z^{-2} + 0.75z^{-3} - 0.16939z^{-4} - 0.0398z^{-5} \\ + 0.02z^{-6}$$

STRUCTURE REALIZATION OF FIR SYSTEM

In general, the FIR system is a non-recursive system, described by the difference equation

$$y(n) = \sum_{k=0}^{M-1} b_k x(n-k)$$

Taking Z-transform

$$Y(z) = \sum_{k=0}^{M-1} b_k z^{-k} X(z)$$

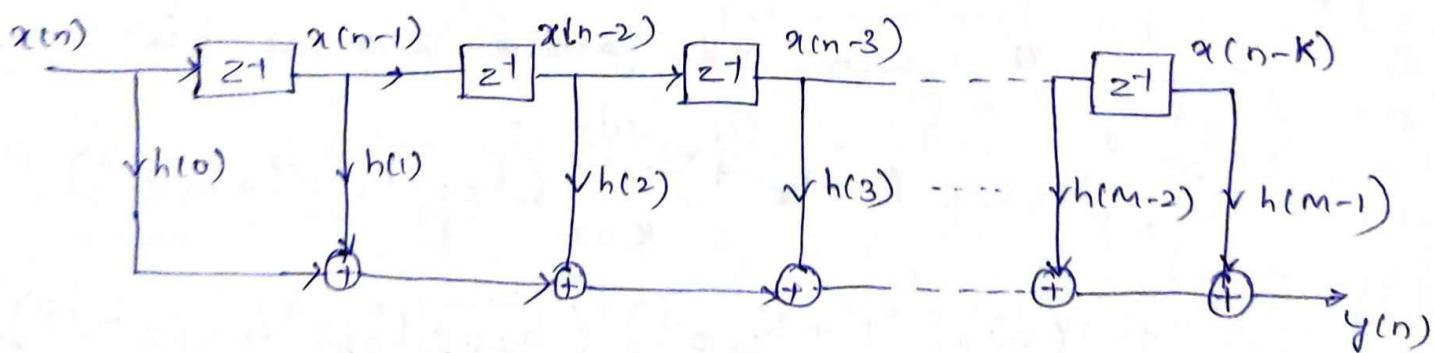
$$\frac{Y(z)}{X(z)} = H(z) = \sum_{k=0}^{M-1} b_k z^{-k}.$$

where M = length of the FIR filter.

$$h(n) = \begin{cases} b_k, & 0 \leq n \leq M-1 \\ 0 & \text{otherwise.} \end{cases}$$

Duct form (or) Transversal structure

$$H(z) = \sum_{n=0}^{M-1} h(n) z^{-n}$$



The structure has $M-1$ memory locations

$M \rightarrow$ complex multiplication

M-1 → additions .

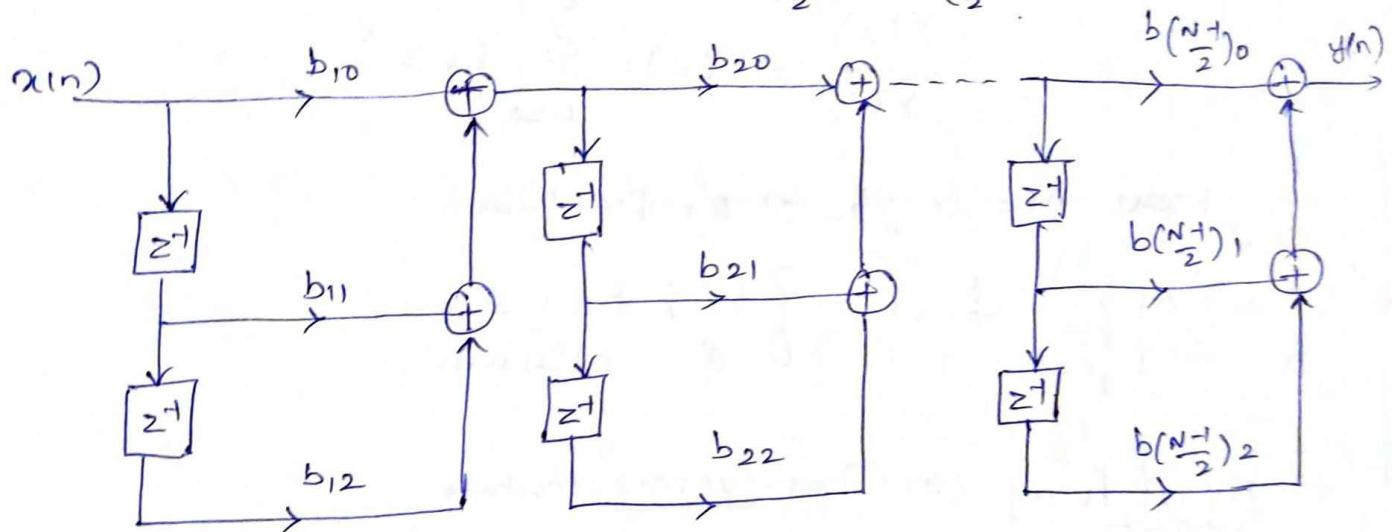
Cascade structure realization

$$H(z) = \sum_{n=0}^{N-1} h(n) z^{-n}$$

(1) when $N = \text{odd}$.

$$H(z) = \prod_{k=1}^{\left(\frac{N-1}{2}\right)} (b_{k0} + b_{k1}z^{-1} + b_{k2}z^{-2})$$

$$H(z) = (b_{10} + b_{11}z^{-1} + b_{12}z^{-2}) (b_{20} + b_{21}z^{-1} + b_{22}z^{-2}) \dots \left(b_{\left(\frac{N-1}{2}\right)0} + b_{\left(\frac{N-1}{2}\right)1}z^{-1} + b_{\left(\frac{N-1}{2}\right)2}z^{-2} \right)$$



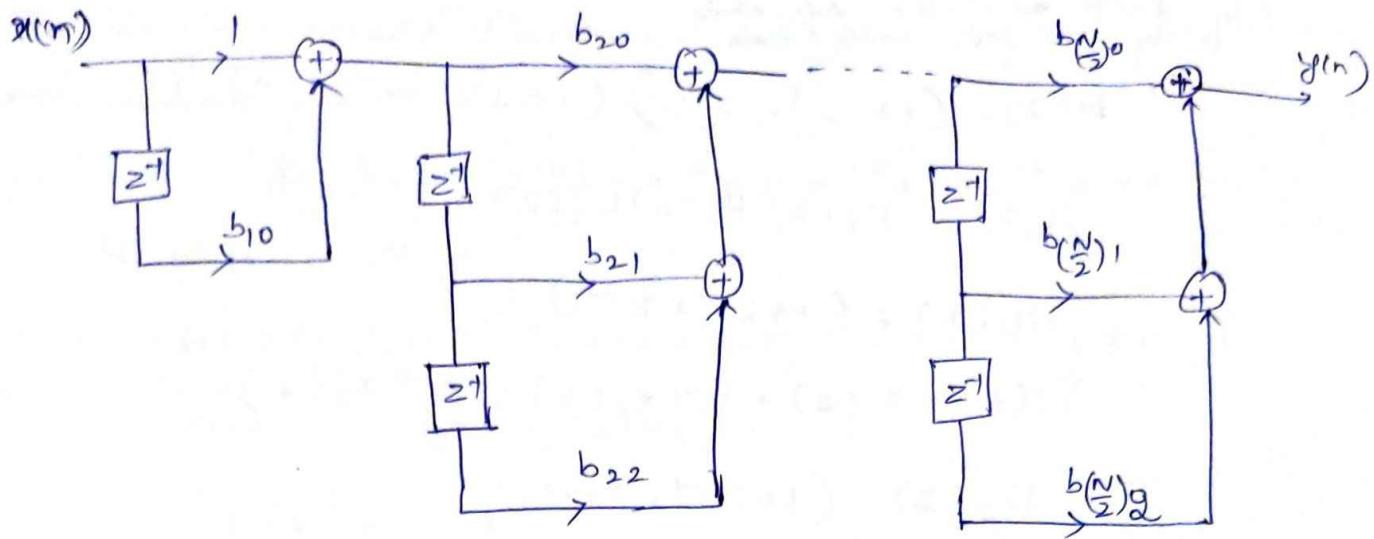
$\frac{N-1}{2} \rightarrow \text{second order factors}$

(2) when $N = \text{even}$.

$\frac{N-1}{2}$ second order factors and one first order factor

$$H(z) = (1 + b_{10}z^{-1}) \prod_{k=2}^{N/2} (b_{k0} + b_{k1}z^{-1} + b_{k2}z^{-2})$$

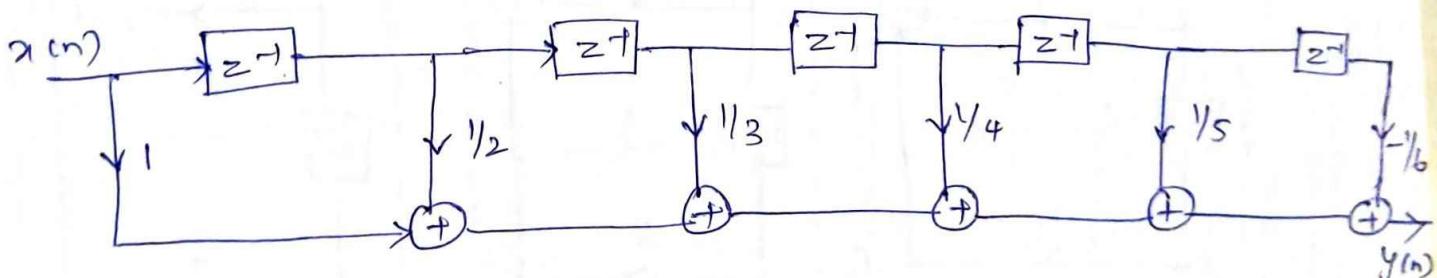
$$H(z) = (1 + b_{10}z^{-1}) \cdot (b_{20} + b_{21}z^{-1} + b_{22}z^{-2}) + \dots \\ (b_{30} + b_{31}z^{-1} + b_{32}z^{-2}) \dots \\ (b_{\left(\frac{N}{2}\right)0} + b_{\left(\frac{N}{2}\right)1}z^{-1} + b_{\left(\frac{N}{2}\right)2}z^{-2})$$



(1) Obtain the direct form structure realization of the non-recursive system.

$$H(z) = 1 + \frac{1}{2}z^{-1} + \frac{1}{3}z^{-2} + \frac{1}{4}z^{-3} + \frac{1}{5}z^{-4} - \frac{1}{6}z^{-5}$$

$$Y(z) = X(z) + \frac{1}{2}z^{-1}X(z) + \frac{1}{3}z^{-2}X(z) + \frac{1}{4}z^{-3}X(z) + \frac{1}{5}z^{-4}X(z) - \frac{1}{6}z^{-5}X(z)$$



(2) obtain the cascade structure realization the given non-recursive system.

$$H(z) = 1 + 6z^{-1} + 19z^{-2} + 35z^{-3} + 42z^{-4} + 29z^{-5} + 12z^{-6}$$

$$N-1 = 6 \quad N = 7$$

odd.

On factorizing the equation

$$H(z) = (1 + z^{-1} + z^{-2})(1 + 2z^{-1} + 3z^{-2})(1 + 3z^{-1} + 4z^{-2})$$

$$H(z) = H_1(z) H_2(z) H_3(z)$$

$$H_1(z) = (1 + z^{-1} + z^{-2})$$

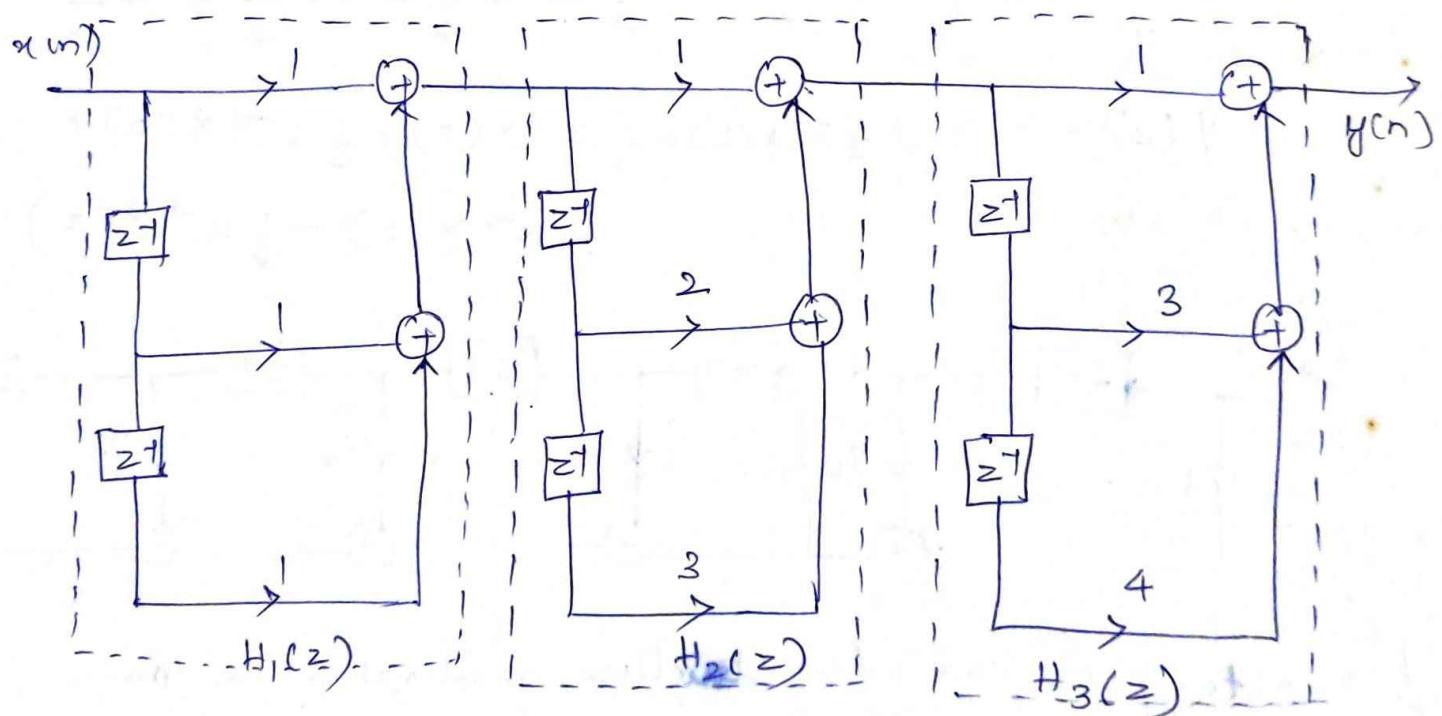
$$Y_1(z) = X_1(z) + z^{-1}X_1(z) + z^{-2}X_2(z)$$

$$H_2(z) = (1 + 2z^{-1} + 3z^{-2})$$

$$Y_2(z) = X_2(z) + 2z^{-1}X_2(z) + 3z^{-2}X_3(z)$$

$$H_3(z) = 1 + 3z^{-1} + 4z^{-2}$$

$$Y_3(z) = X_3(z) + 3z^{-1}X_3(z) + 4z^{-2}X_3(z)$$



Obtain the cascade structure realization of the given non recursive system

$$H(z) = 1 + 8z^{-1} + 21z^{-2} + 35z^{-3} + 28z^{-4} + 15z^{-5}.$$

$$N-1=5 \therefore N=6.$$

$$H(z) = (1+5z^{-1})(1+z^{-1}+z^{-2})(1+2z^{-1}+3z^{-2})$$

$$H(z) = H_1(z) H_2(z) H_3(z)$$

$$H_1(z) = 1+5z^{-1}$$

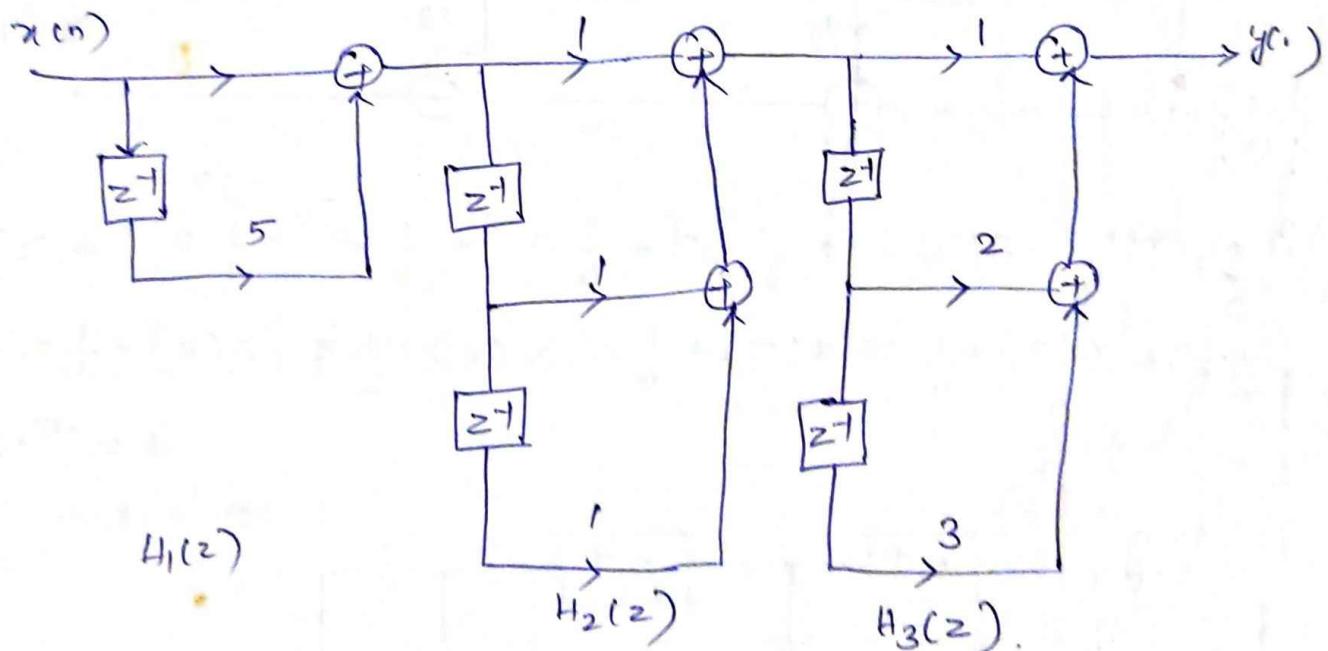
$$Y_1(z) = X_1(z) + 5z^{-1}X_1(z)$$

$$H_2(z) = 1+z^{-1}+z^{-2}$$

$$Y_2(z) = X_2(z) + z^{-1}X_2(z) + z^{-2}X_2(z)$$

$$H_3(z) = 1+2z^{-1}+3z^{-2}$$

$$Y_3(z) = X_3(z) + 2 \cdot z^{-1}X_3(z) + 3 \cdot z^{-2}X_3(z)$$



LINEAR PHASE FIR SYSTEM

$$h(n) = h(N-1-n)$$

(1) Realize a direct form structure for a linear phase FIR system.

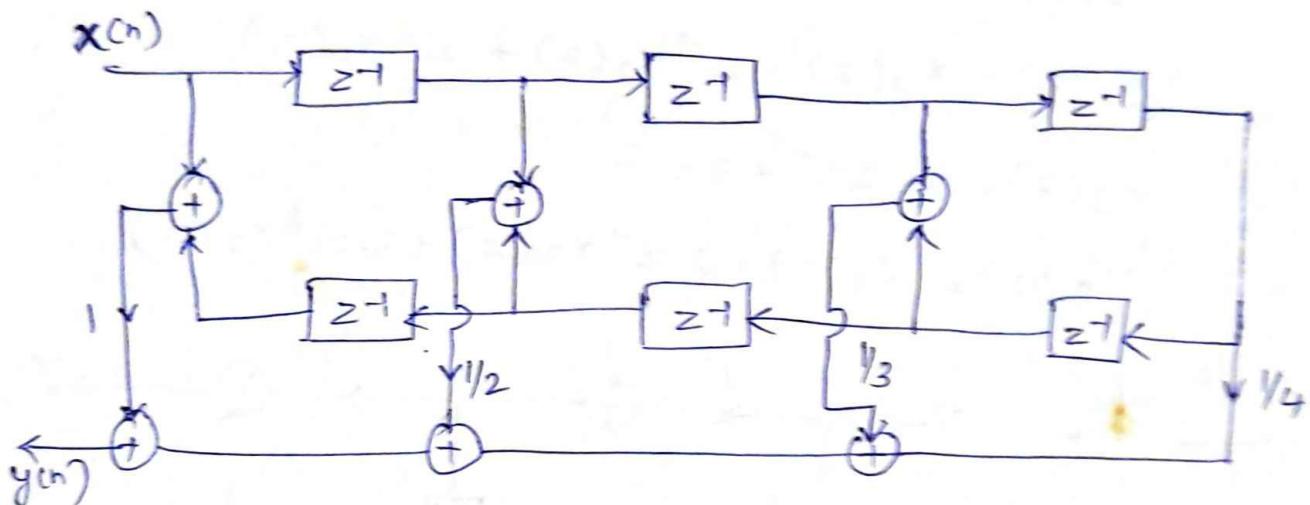
$$H(z) = 1 + \frac{1}{2}z^{-1} + \frac{1}{3}z^{-2} + \frac{1}{4}z^{-3} + \frac{1}{3}z^{-4} + \frac{1}{2}z^{-5} + z^{-6}$$

$$Y(z) = X(z) + \frac{1}{2}z^{-1}X(z) + \frac{1}{3}z^{-2}X(z) + \frac{1}{4}z^{-3}X(z) + \frac{1}{3}z^{-4}X(z) + \frac{1}{2}z^{-5}X(z) + z^{-6}X(z)$$

N odd

$$N - 1 = 6 \quad N = 7$$

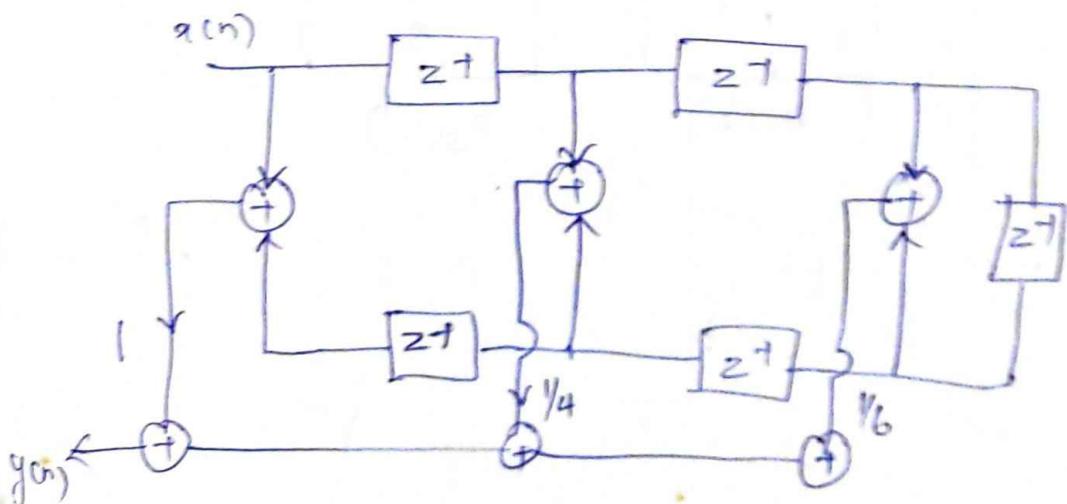
$$+ \frac{1}{2}z^{-5}X(z) + z^{-6}X(z)$$



(2) N even

$$H(z) = 1 + \frac{1}{4}z^{-1} + \frac{1}{6}z^{-2} + \frac{1}{6}z^{-3} + \frac{1}{4}z^{-4} + z^{-5}$$

$$Y(z) = X(z) + \frac{1}{4}z^{-1}X(z) + \frac{1}{6}z^{-2}X(z) + \frac{1}{6}z^{-3}X(z) + \frac{1}{4}z^{-4}X(z) + z^{-5}X(z)$$



Linear phase realization

$$h(n) = h(N-1-n)$$

$$H(z) = \sum_{n=0}^{N-1} h(n) z^{-n}$$

Never

$$\begin{aligned} H(z) &= \sum_{n=0}^{\frac{N-2}{2}} h(n) z^{-n} + \sum_{n=\frac{N}{2}}^{N-1} h(n) z^{-n} \\ &= \sum_{n=0}^{\frac{N-2}{2}} h(n) z^{-n} + \sum_{n=0}^{\frac{N-2}{2}} h(N-1-n) z^{-(N-1-n)} \\ &= \sum_{n=0}^{\frac{N-2}{2}} h(n) [z^{-n} + z^{-(N-1-n)}] \end{aligned}$$

$\frac{N}{2}$ multipliers required.

N odd

$$\begin{aligned} H(z) &= \sum_{n=0}^{\frac{N-3}{2}} h(n) z^{-n} + \sum_{n=\frac{N+1}{2}}^{N-1} h(n) z^{-n} + h\left(\frac{N+1}{2}\right) z^{-(N-1)/2} \\ &= h\left(\frac{N-1}{2}\right) z^{-(N-1)/2} + \sum_{n=0}^{\frac{N-3}{2}} h(n) [z^{-n} + z^{-(N-1-n)}] \end{aligned}$$

$\frac{N+1}{2}$ multipliers required.

h