```
% Static force analysis of 2D MitchelTruss (Fig 3.3 of Skelton & de Oliviera 2009)
% By Thomas Bewley, UC San Diego (+ faculty fellow at JPL)
clear; clf; figure(1);
beta = pi/6;
phi = pi/16;
r0 = 1;
r1 = r0*sin(beta)/(sin(beta+phi));
r2 = r1*sin(beta)/(sin(beta+phi));
r3 = r2*sin(beta)/(sin(beta+phi));
r4 = r3*sin(beta)/(sin(beta+phi));
% Free [Q=Q (dim x q)] and fixed [Q=Q (dim x q)] node locations
Q(:,1) = [r0; 0];
Q(:,2) = [r1*cos(phi); r1*sin(phi)];
Q(:,3) = [r1*cos(phi); -r1*sin(phi)];
Q(:,4) = [r2*cos(phi*2); r2*sin(phi*2)];
Q(:,5) = [r2,0];
Q(:,6) = [r2*cos(phi*2); -r2*sin(phi*2)];
Q(:,7) = [r3*cos(phi*3); r3*sin(phi*3)];
Q(:,8) = [r3*cos(phi); r3*sin(phi)];
Q(:,9) = [r3*cos(phi); -r3*sin(phi)];
Q(:,10) = [r3*cos(phi*3); -r3*sin(phi*3)];
P(:,1) = [r4*cos(phi*4); r4*sin(phi*4)];
P(:,2) = [r4*cos(phi*2); r4*sin(phi*2)];
P(:,3) = [r4; 0];
P(:,4) = [r4*cos(phi*2); -r4*sin(phi*2)];
P(:,5) = [r4*cos(phi*4); -r4*sin(phi*4)];
[\dim, q] = \operatorname{size}(Q), p = \operatorname{size}(P, 2), n = q + p;
% Connectivity matrix
b = 20;
C(:,1) = conVect(1,2,15);
C(:,2) = conVect(1,3,15);
C(:,3) = conVect(2,5,15);
C(:,4) = conVect(3,5,15);
C(:,5) = conVect(2,4,15);
C(:,6) = conVect(3,6,15);
C(:,7) = conVect(4,7,15);
C(:,8) = conVect(4,8,15);
C(:,9) = conVect(5,8,15);
C(:,10) = conVect(5,9,15);
C(:,11) = conVect(6,9,15);
C(:,12) = conVect(6,10,15);
C(:,13) = conVect(7,11,15);
C(:,14) = conVect(7,12,15);
C(:,15) = conVect(8,12,15);
C(:,16) = conVect(8,13,15);
C(:,17) = conVect(9,13,15);
C(:,18) = conVect(9,14,15);
C(:,19) = conVect(10,14,15);
C(:,20) = conVect(10,15,15); s = 0; m=b+s;
C=C';
```

```
% Applied external force U=U (dim x q)
U(1:dim, 1:q) = 0; U(2,1) = -10;
% Solve for the forces at equilibrium, and plot
[c_bars,t_strings,V]=tensegrity_statics(b,s,q,p,dim,Q,P,C,U);
tensegrity plot(Q,P,C,b,s,U,V,true,2.0); grid on;
function C_vect = conVect(start,finish,total_nodes)
C vect = zeros(1,total_nodes);
C \text{ vect}(1, \text{start}) = -1;
C \operatorname{vect}(1, \operatorname{finish}) = 1;
return
end
\ensuremath{\text{\%}} end script MitchelTruss4
dim =
      2
q =
    10
p =
      5
mhat =
    20
nhat =
    20
r =
    20
Ase is not potentially inconsistent. Good.
```

Bar compressions and string tensions with loads as specified,

-10.0000 10.0000 2.2527 -2.2527 -10.9342 10.9342 -11.9557

least squares solution (i.e., NO pretensioning):

c bars =

Columns 1 through 7

Columns 8 through 14

2.4632 -2.9706 2.9706 -2.4632 11.9557 -13.0726 2.6933

Columns 15 through 20

-3.8030 3.3625 -3.3625 3.8030 -2.6933 13.0726

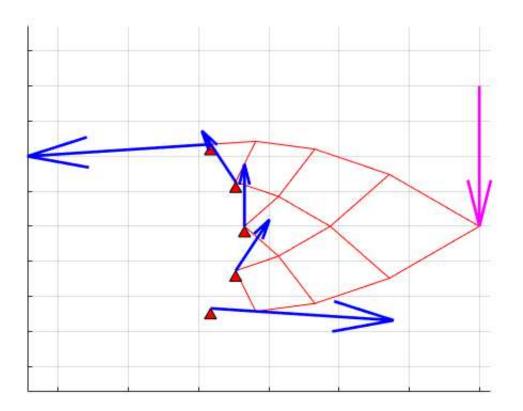
Note: some bars not under compression. Maybe replace them with strings?

t strings =

1×0 empty double row vector

Some strings not under tension. Needs different tensioning or external loads.

Ase is not underdetermined (thus, it is not tensionable). The above solution is unique.



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