



*la passion du rail*



# Friction control in wheel-rail contacts

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01.12.2025

# MATISA Matériel Industriel SA

## MATISA Matériel Industriel SA

Crissier SUISSE

On Track Machines (OTM) development and construction



Website: <https://www.matisa.ch/fr/index.php>

### Videos

P95 - Renewal train (7min) [Videos/P 95 MATISA GCF.mp4](#)

B66UC - Tamping machine (4min) [Videos/B 66 UC MATISA MONTI.mp4](#)

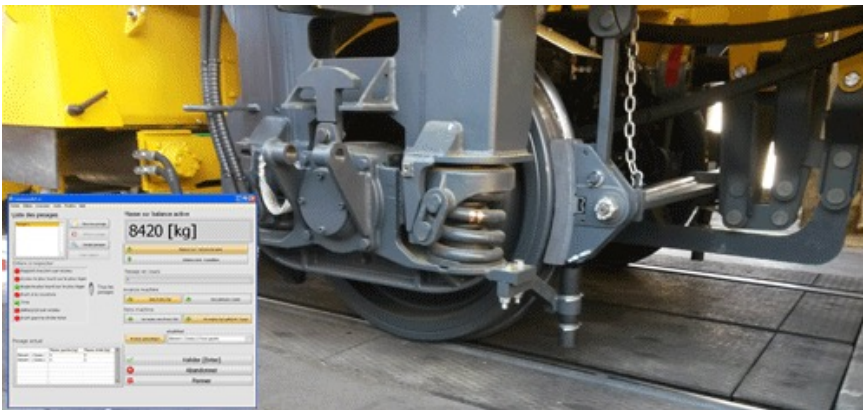


# MATISA Matériel Industriel SA

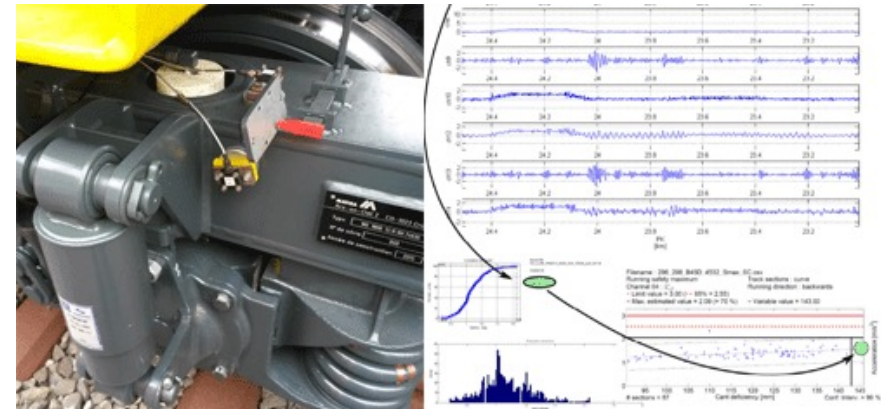
## Accredited EN 17025 Laboratory

Website: [https://www.matisa.ch/en/matisa-testing\\_laboratory%20.php](https://www.matisa.ch/en/matisa-testing_laboratory%20.php)

### Weighing wheel by wheel EN 15654-2



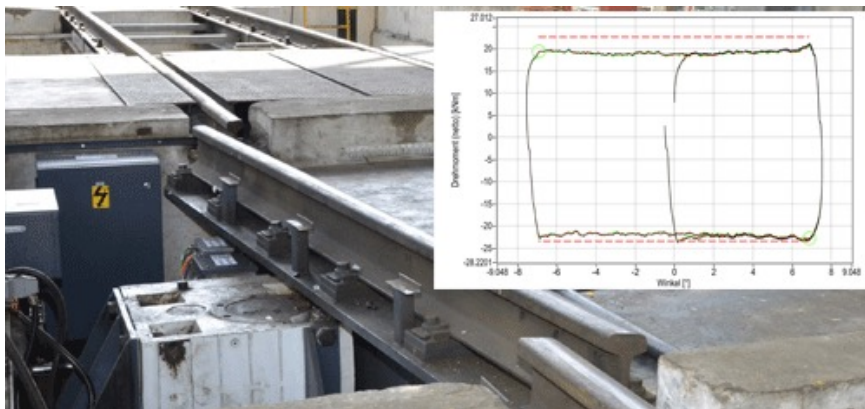
### Running behaviour EN 14363 §7



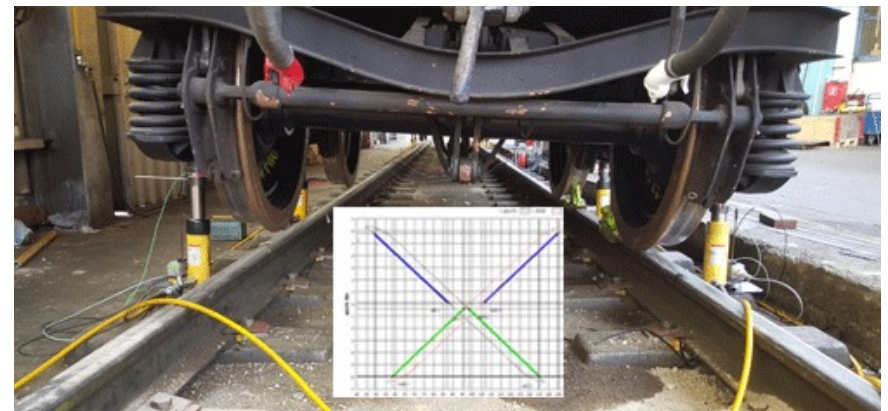
## Accredited EN 17025 Laboratory

Website: [https://www.matisa.ch/en/matisa-testing\\_laboratory%20.php](https://www.matisa.ch/en/matisa-testing_laboratory%20.php)

Resistance against bogie rotation  
EN 14363 §6



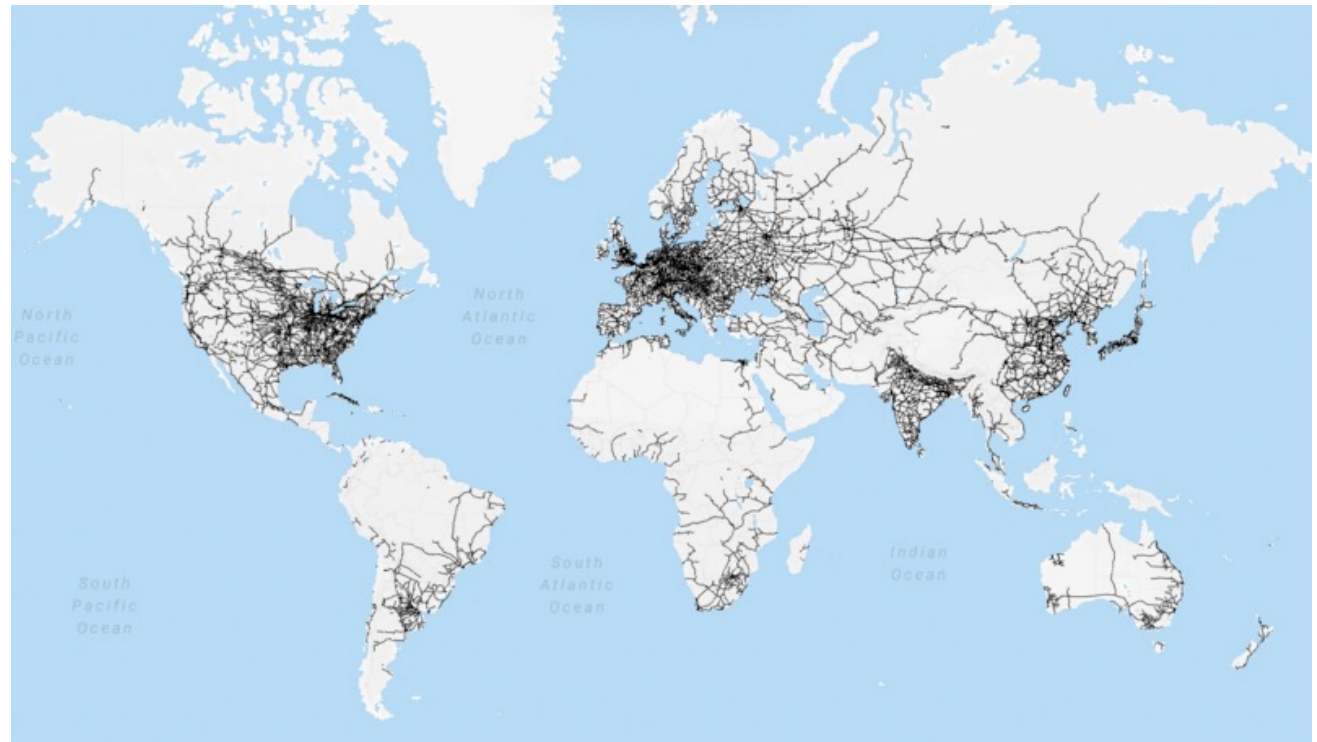
Safety against derailment on  
twisted track - EN 14363 §6





# Railway transport network

Country / Area	km
World	1,374,000
USA	220,000
China	159,000
EU-28	211,400
Switzerland	5,300



## Modal transport volume

Passenger transport volume  
EU-28 (2015)

Mode	Billion p-km	%
Sea	22	0.3
Road	5 388	81.6
Rail	544	8.2
Air	649	9.8
<b>Total</b>	<b>6 603</b>	<b>100.0</b>

eea.europa.eu

Freight transport volume  
Worldwide (2015)

Mode	Trillion t-km	%
Sea	78.0	72.2
Road	19.8	18.3
Rail	10.0	9.3
Air	0.2	0.2
<b>Total</b>	<b>108.0</b>	<b>100.0</b>

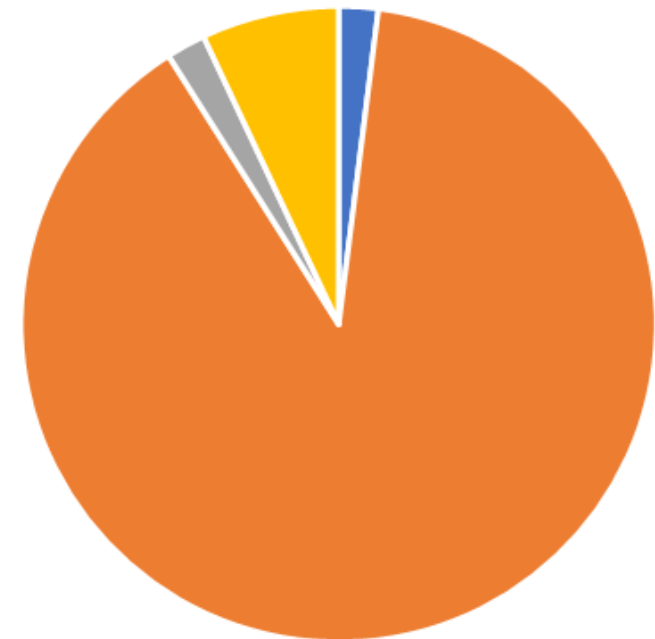
"Global Freight Demand to Triple by 2050". The  
Maritime Executive. May 27, 2019

## Modal transport energy consumption

Energy consumption in transport  
IEA countries (2018)

Mode	Trillion MJ	%	% MJ/p-km	% MJ/t-km
Sea	2.1	2.0	74.6	0.1
Road	93.9	89.0	13.6	11.3
Rail	2.1	2.0	3.0	0.5
Air	7.4	7.0	8.8	88.1
<b>Total</b>	<b>105.5</b>	<b>100.0</b>	<b>100.0</b>	<b>100.0</b>

% Modal energy consumption



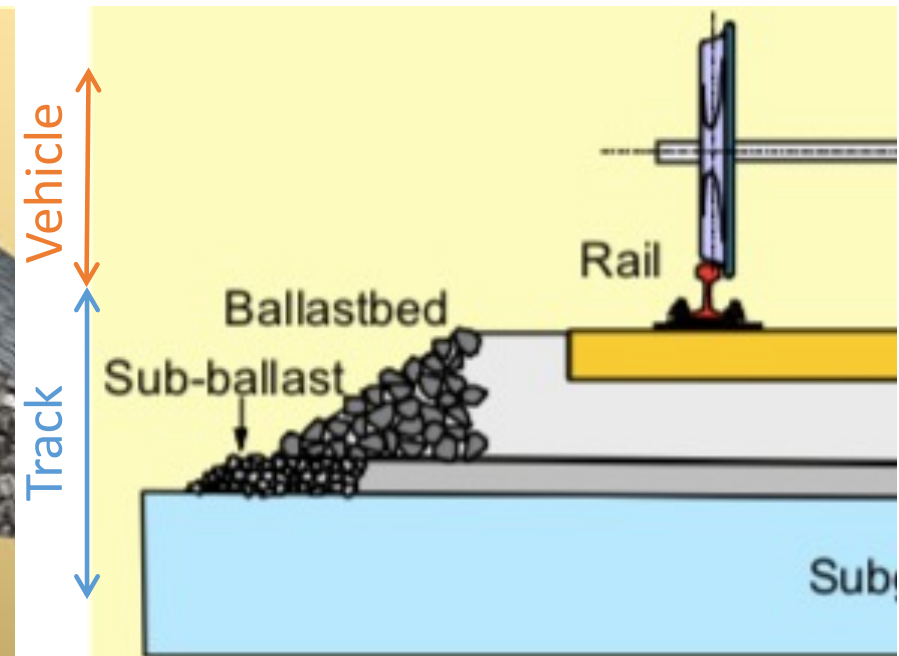
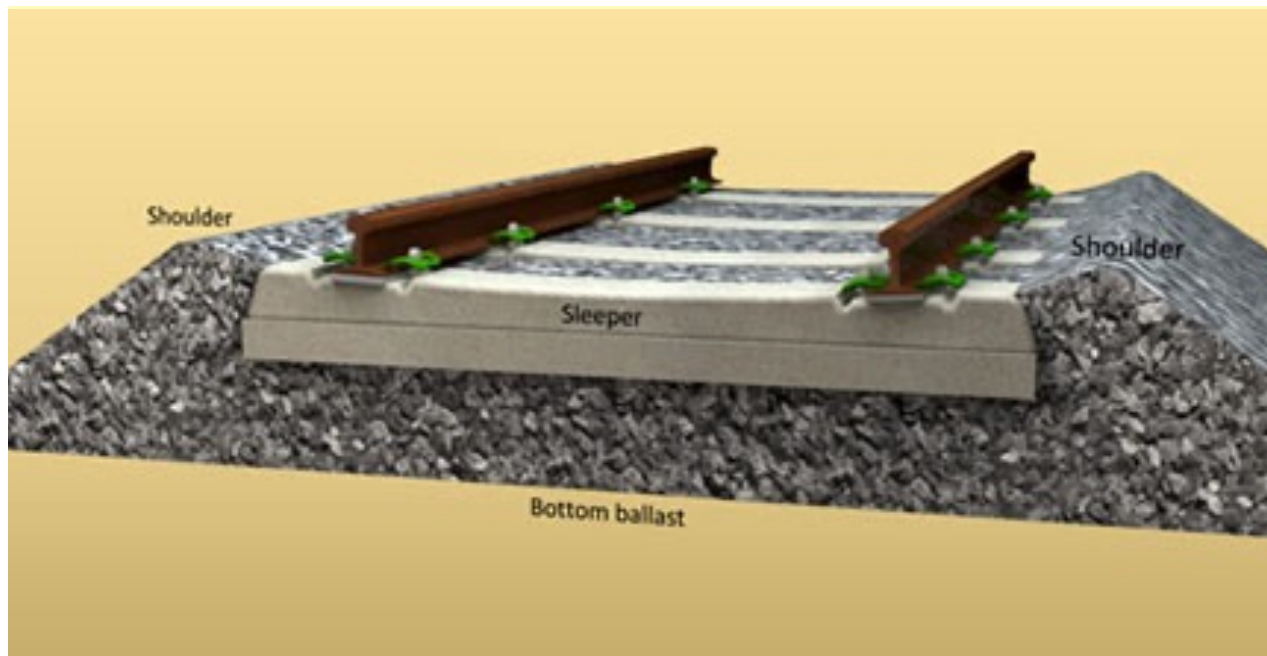
■ Sea ■ Road ■ Rail ■ Air

**Why using the rail transport system?**

**Let's have a look in the wheel-rail contact**

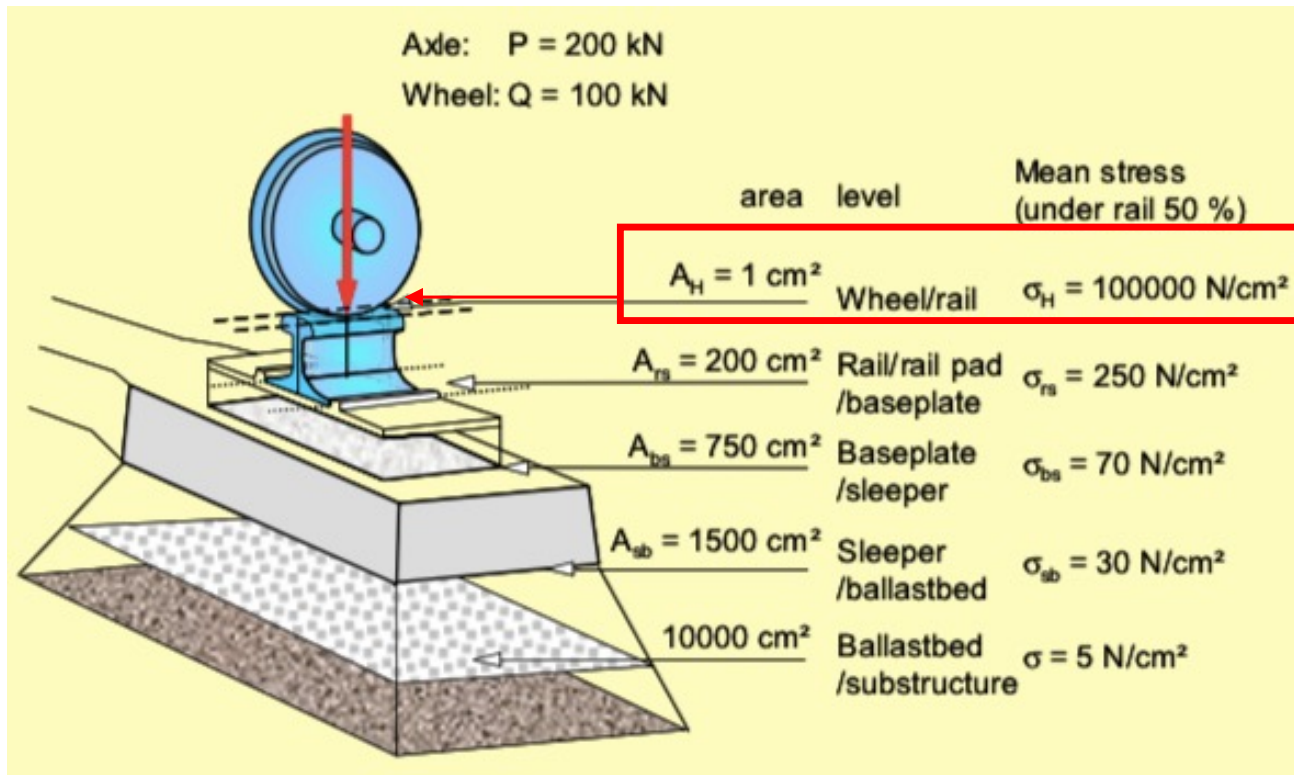


# Railway (conventional) track structure and wheelset



Esvel, C. (2001) Modern Railway Track.  
2nd Edition, MRT-Productions

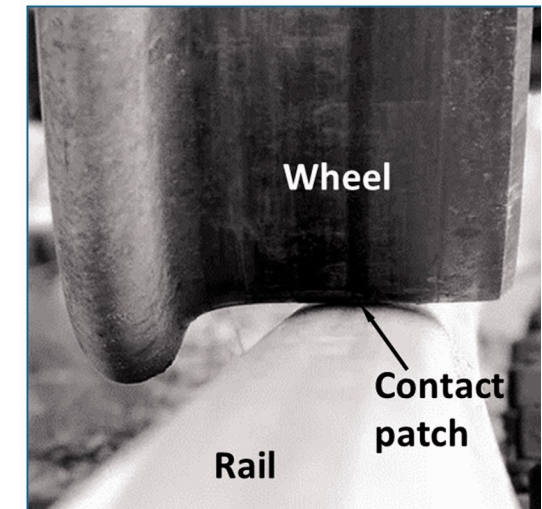
# Load bearing function of the track (conventional)



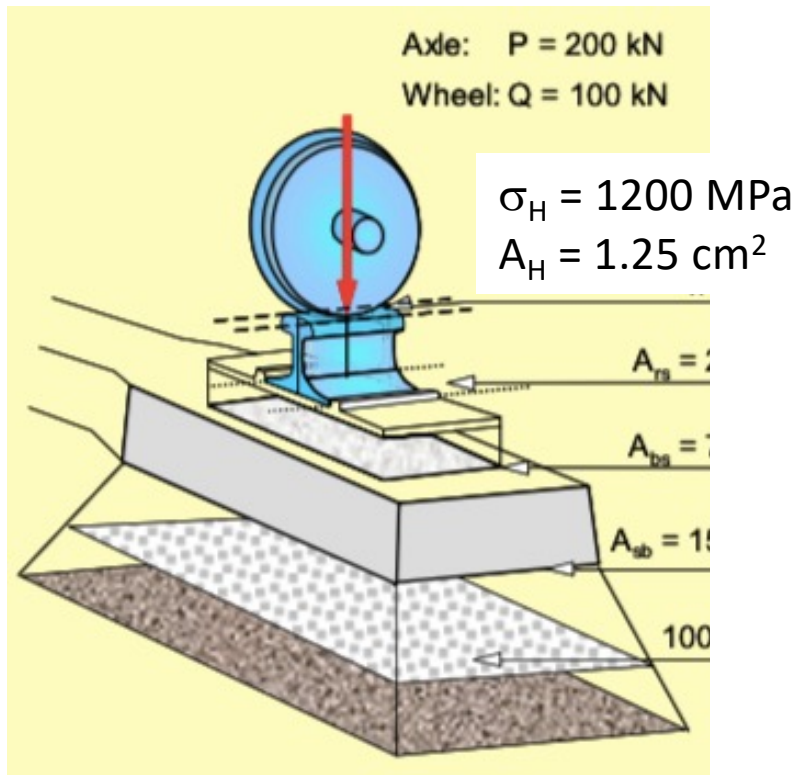
Esveld, C. (2001) Modern Railway Track.  
2nd Edition, MRT-Productions

## Rail transport advantages

- High Loads  $\sigma_H = 1000 \text{ MPa}$
- Low rolling friction ( $\sim 0.0004$ )



## Load bearing function of the track (conventional)



Esveld, C. (2001) Modern Railway Track.  
2nd Edition, MRT-Productions

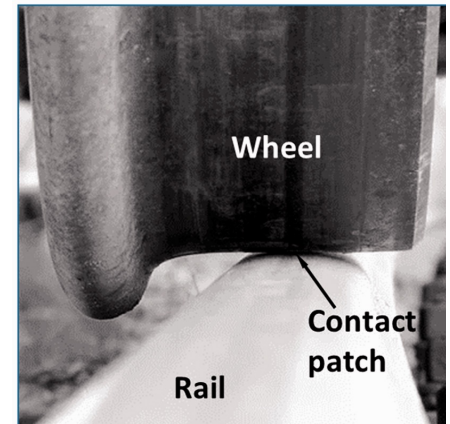
### Wheel rail contact

Non-conformal contact

$R_w = 500 \text{ mm (y)}$   $R_r = 300 \text{ mm (x)}$

Steel on steel  $E = 210 \text{ GPa}$   $\nu = 0.3$

Normal load  $F_n = 100 \text{ kN}$



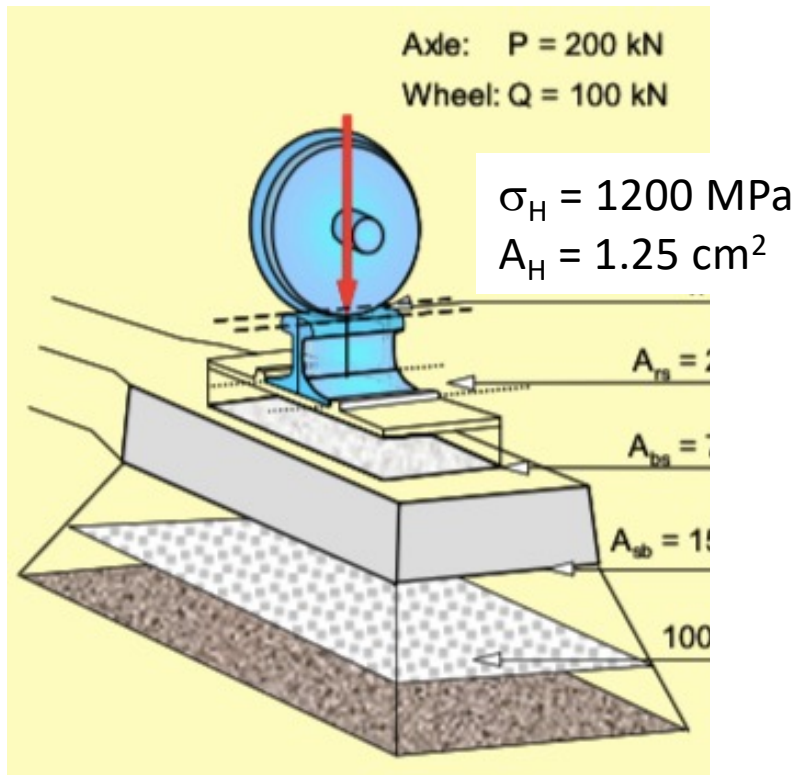
### Hertz theory

$E^* = 230.77 \text{ GPa}$   $R^* = 187.43 \text{ mm}$

Contact ellipse  $a / b = 7.557 / 5.282 \text{ mm}$

$P_{avg} = 798 \text{ MPa}$  /  $P_{max} = 1200 \text{ MPa}$

# Load bearing function of the track (conventional)



Esveld, C. (2001) Modern Railway Track.  
2nd Edition, MRT-Productions

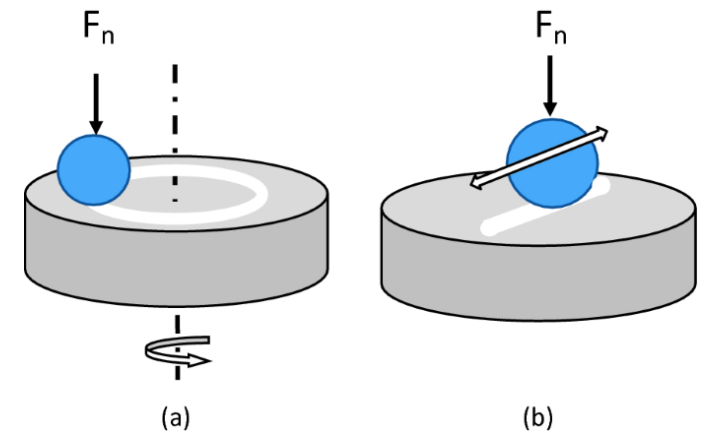
## Laboratory setups

Ball on flat contact

Alumina ball  $\phi = 3 \text{ mm}$

Steel sample

Normal load  $F_n = 5 \text{ N}$

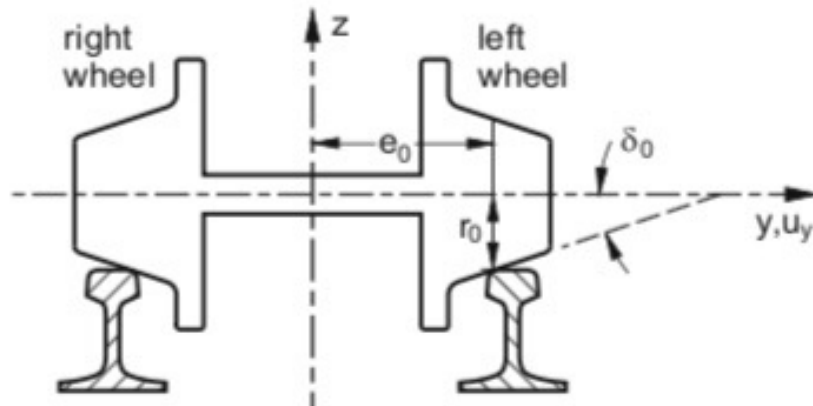


## Hertz theory

Contact ellipse  $a, b = 0.0442 \text{ mm}$  Area =  $0.0061 \text{ mm}^2$

$P_{\text{avg}} = 816 \text{ MPa}$  /  $P_{\text{max}} = 1225 \text{ MPa}$

## Guiding function: Hunting motion



$r_0$  : rolling radius (nominal)  
 $2e_0$  : contact points lateral distance  
 $\delta_0$  : conicity (cone angle)

$$L = 2\pi \sqrt{\frac{e_0 r_0}{\delta_0}} \quad \text{Hunting wavelength}$$

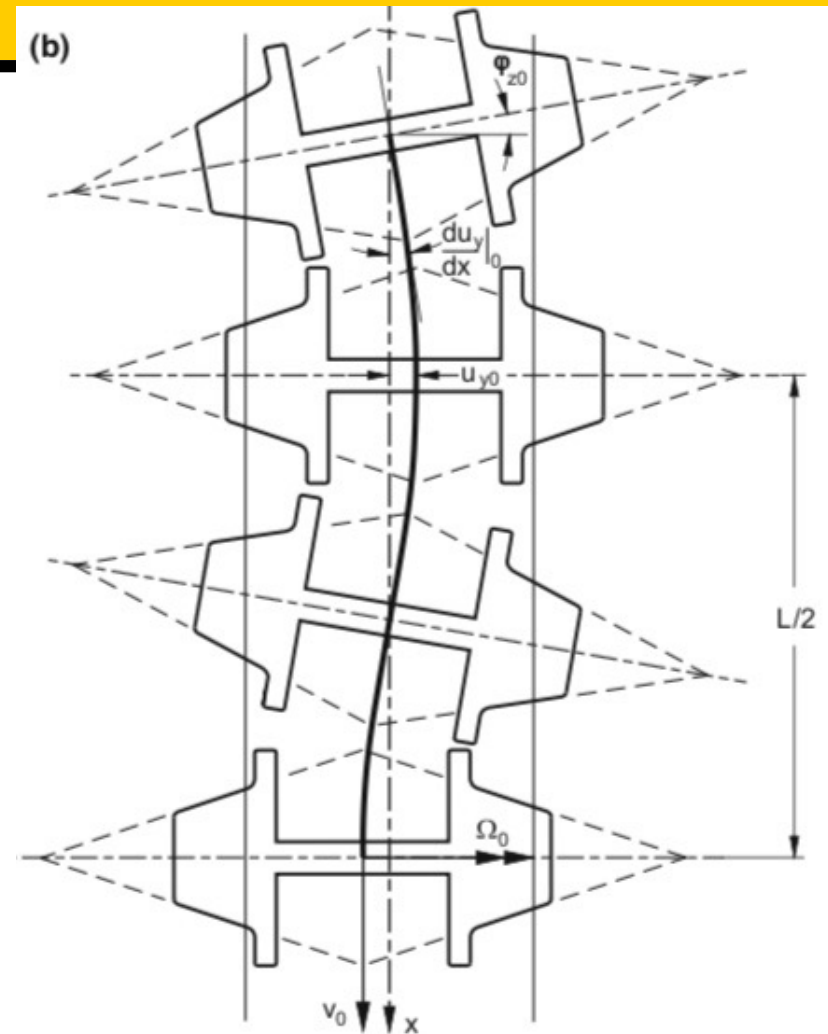
$v_0$  : wheelset longitudinal speed  
 $\Omega_0$  : wheelset rotational speed

$$v_0 = \Omega_0 r_0 \quad f = v_0/L$$

## Videos

Guidance (2min) [Videos/Guidance By Railway Tracks.mp4](#)

Knothe, K. (2017) "Rail Vehicle Dynamics"  
Springer





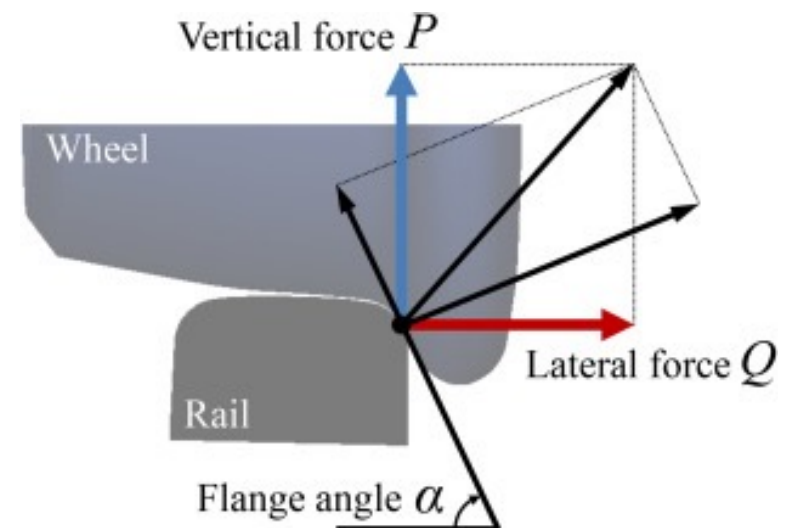
## Guiding function problems

### Instability

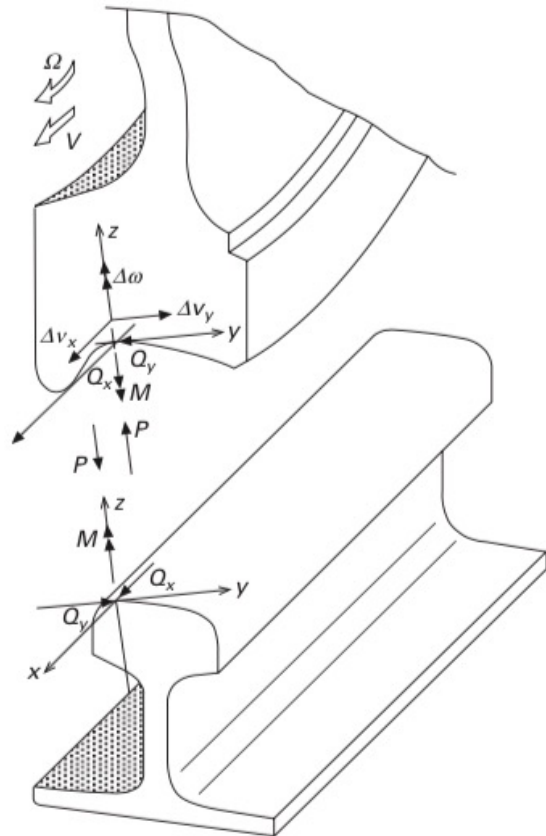


Track displacement after high-speed test of SNCF 1955

### Flange-climb derailment



# Wheel-rail contact parameters



Lewis, R. (2009) "Wheel-Rail Interaction Handbook" Elsevier

$R$  = wheel rolling radius / rail radius  
 $V$  = wheel travelling speed  
 $\Omega$  = wheel rotational speed  
 $P$  = normal force

Running parameters

$Q_x$  = longitudinal creep force  $T_\xi$   
 $Q_y$  = lateral creep force  $T_\eta$   
 $M$  = spin moment  $M_\zeta$

Contact forces

$\Delta v_i$  = relative in-plane translation velocity between contacting bodies,  $i \in \{x, y\}$   
 $\Delta \omega$  = relative rotation velocity between contacting bodies

$a$  = longitudinal contact ellipse semi-axis  
 $b$  = lateral contact ellipse semi-axis  
 $t$  = time  
 $v_x$  = longitudinal creep ratio  $\nu_\xi$   
 $v_y$  = lateral creep ratio  $\nu_\eta$   
 $\phi$  = spin ratio  $\nu_\zeta$

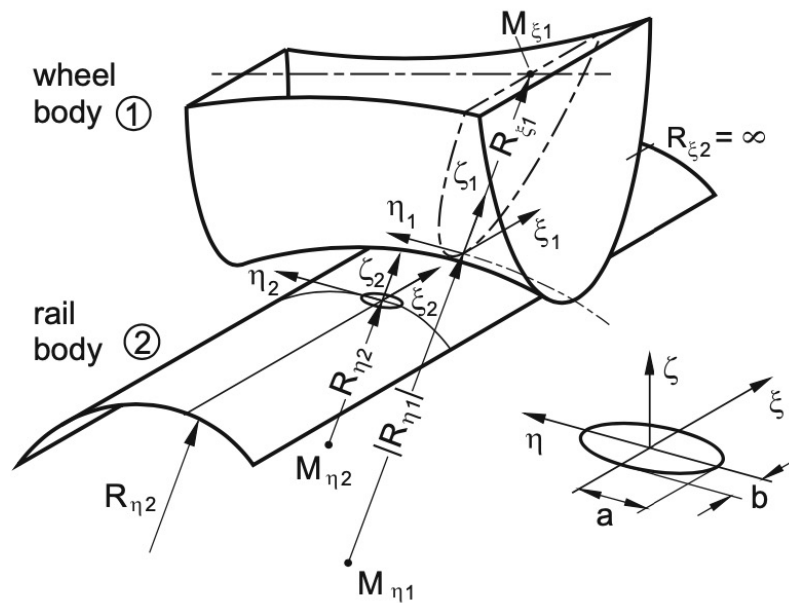
Geometric and kinematic contact parameters

$p$  = contact pressure  
 $q_x$  = tangential stress component in longitudinal direction  
 $q_y$  = tangential stress component in lateral direction  
 $\mu$  = coefficient of friction  
 $\alpha$  = traction coefficient

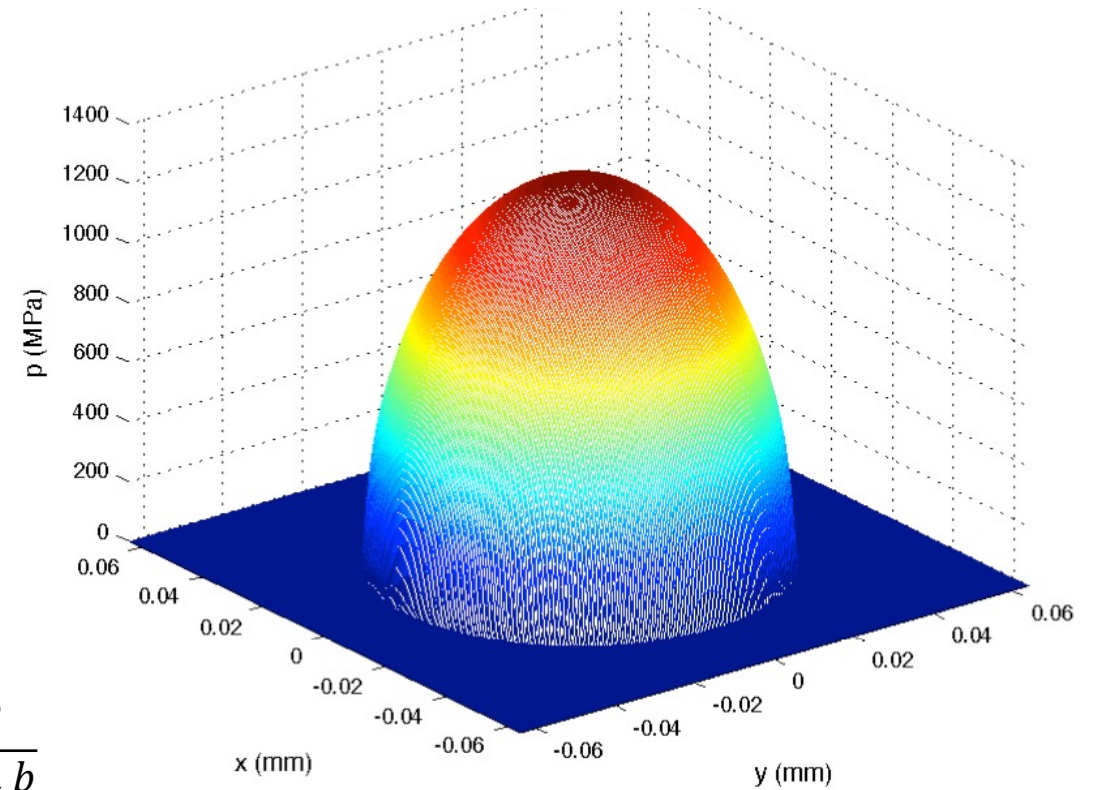
Contact pressure distributions



# Wheel-rail normal contact: Hetzian distribution



Contact pressure distribution  $p(x,y)$

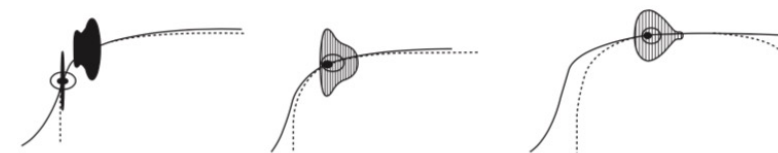
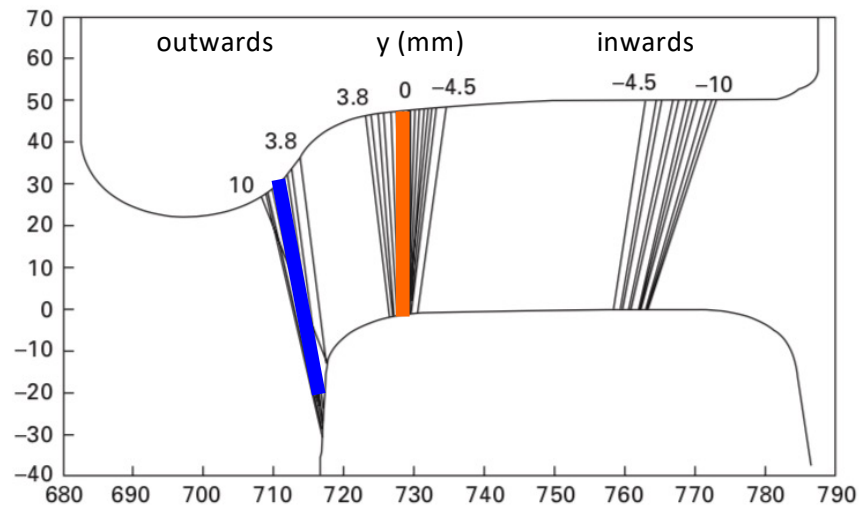


$$p_0 = \frac{3P}{2\pi ab}$$

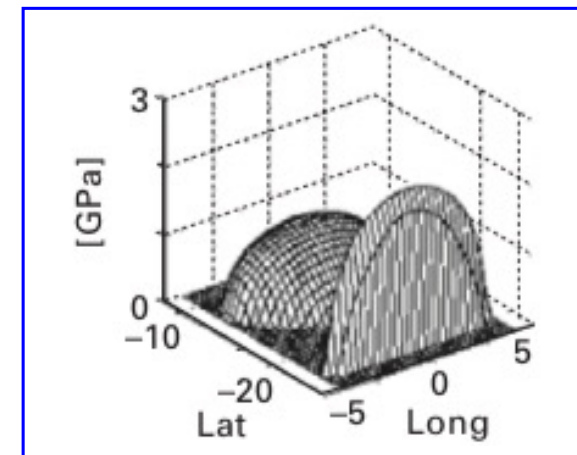
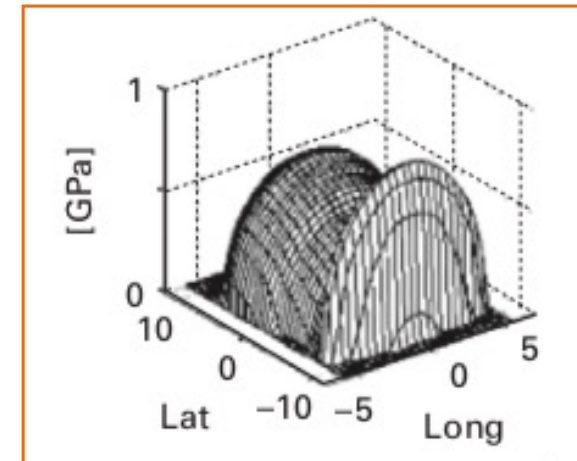
$$p(\xi, \eta) = p_0 \sqrt{1 - (\eta/a)^2 - (\xi/b)^2}$$

2D contact  $p(\xi) = p_0 \sqrt{1 - (\xi/b)^2}$

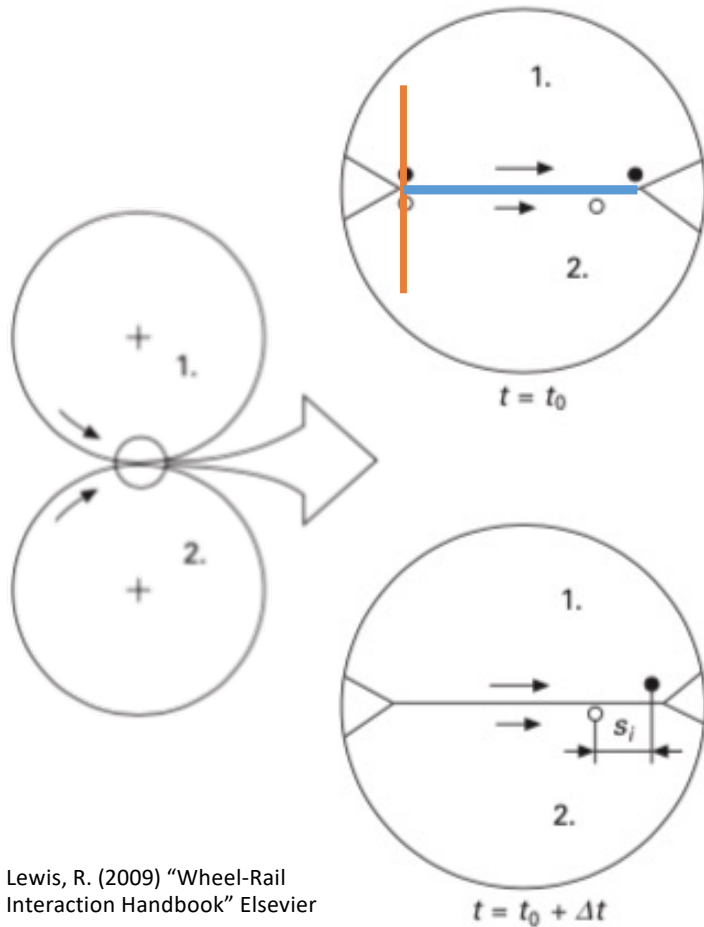
# Wheel-rail normal contact: non-Hertzian distributions



Lewis, R. (2009) "Wheel-Rail Interaction Handbook" Elsevier



# Wheel-rail tangential contact: slip, creep and adhesion



Lewis, R. (2009) "Wheel-Rail Interaction Handbook" Elsevier

## 2D problem

Tangential distribution

$$q_1(\xi) = \frac{\mu p_0}{a} \sqrt{a^2 - \xi^2} = \mu p(\xi)$$

$$q_2(\xi^*) = -\frac{\mu p_0}{a^*} \sqrt{a^{*2} - \xi^{*2}}$$

slip

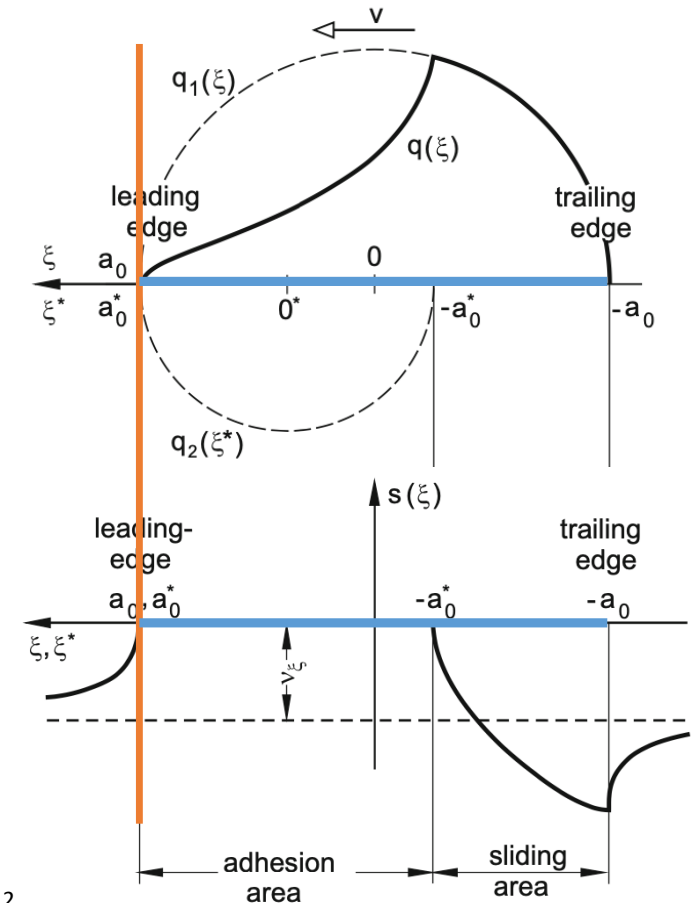
$s$

creep

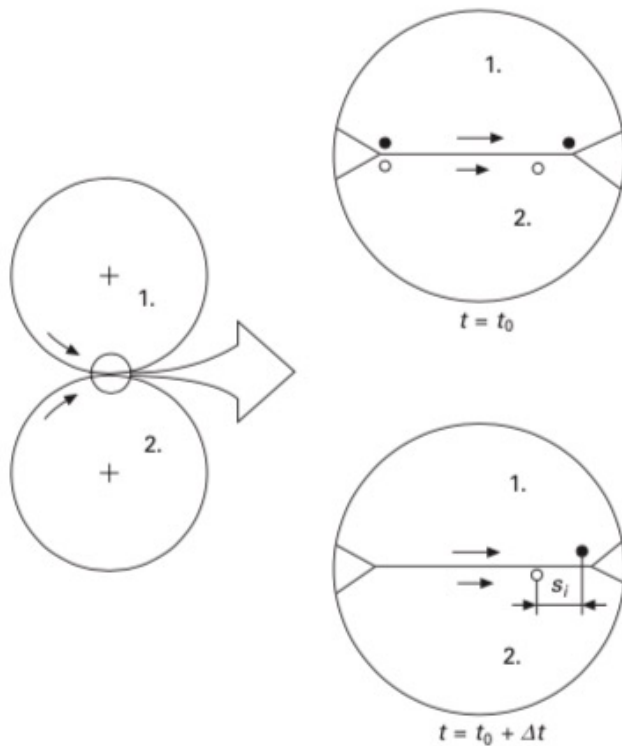
$$v_x = (s/\Delta t)/V$$

## Local creepage

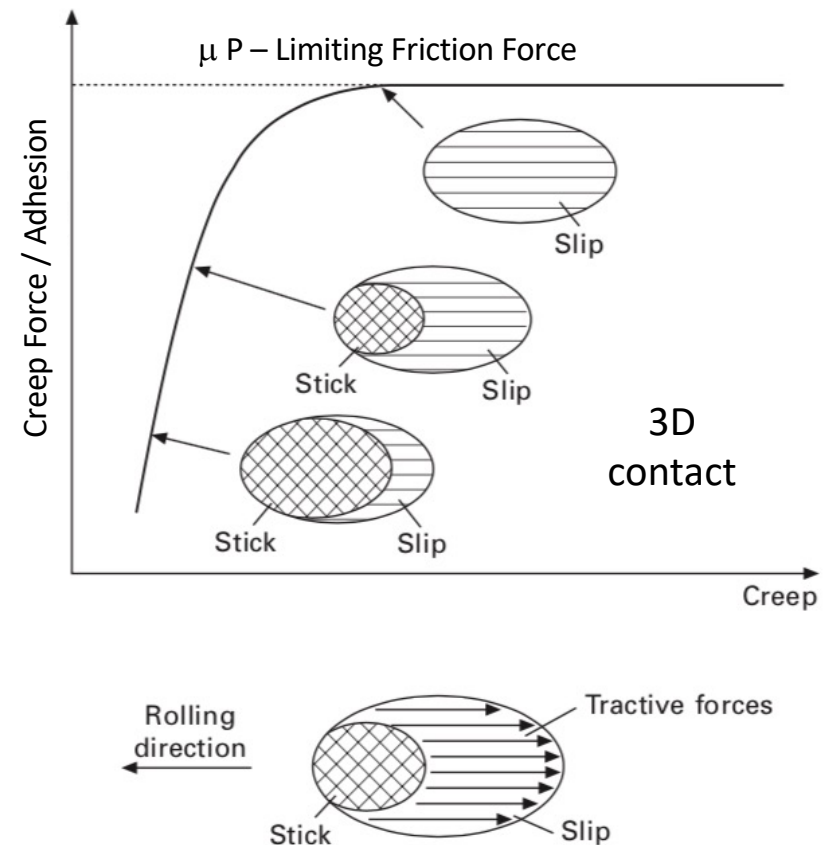
Carter (1926) Proc.R. Soc. L. A 112



# Wheel-rail tangential contact: slip, creep and adhesion



Slip  $s$   
 Creep  $v_x = (s/\Delta t)/V$   
 Creep force  $Q_x$   
 Adhesion  $\alpha = Q_x/P$



# Creep influence in wheel-rail contact conditions

Types of creep:

- 1) Longitudinal creepage ( $v_\xi$ ): spinning and skidding in running direction
- 2) Lateral creepage ( $v_\eta$ ): the angle of attack or skew
- 3) Spin creepage ( $v_\zeta$ ): the contact plane inclination and steering

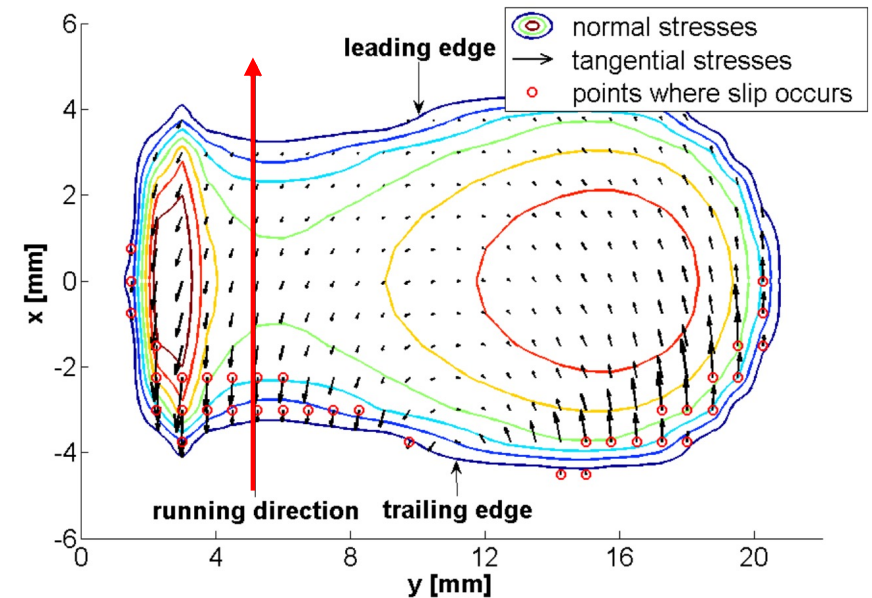
## 3D tangential contact

$$\begin{Bmatrix} T_\xi \\ T_\eta \\ M_\zeta \end{Bmatrix}_{\text{lin}} = Gab \begin{bmatrix} C_{11} & 0 & 0 \\ 0 & C_{22} & \sqrt{ab} C_{23} \\ 0 & -\sqrt{ab} C_{23} & ab C_{33} \end{bmatrix} \begin{Bmatrix} \nu_\xi \\ \nu_\eta \\ \nu_\zeta \end{Bmatrix}.$$

$T_{\xi,\eta}, M_\zeta$  : Creep forces  
 $C_{ij}$  : Kalker's coefficients  
 $\nu_{\xi,\eta,\zeta}$  : Creepages

Railway steel on steel contacts:

- Free running (no creep) → small rolling resistance
- Creep motion → higher friction

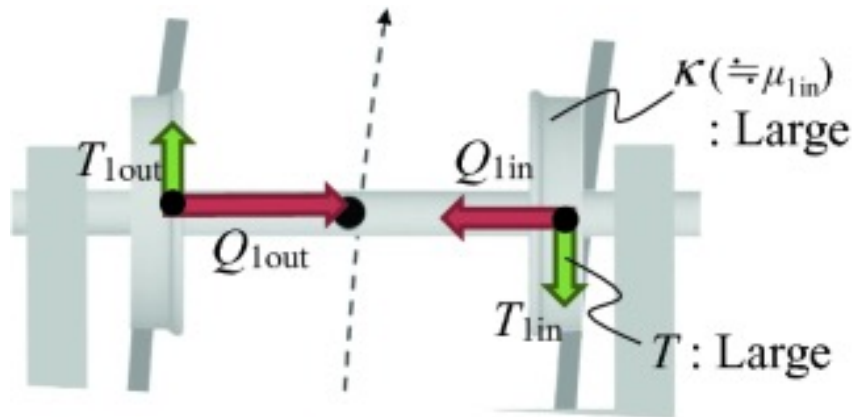


## Key role of creep forces in vehicle-track interaction

- Traction and braking
- Stability (hunting), oscillation behavior
- Safety against derailment, wheel-rail forces, track loading in curves
- Wear
- Rolling contact fatigue (RCF)
- Squeal noise

# Key role of creep forces in vehicle-track interaction

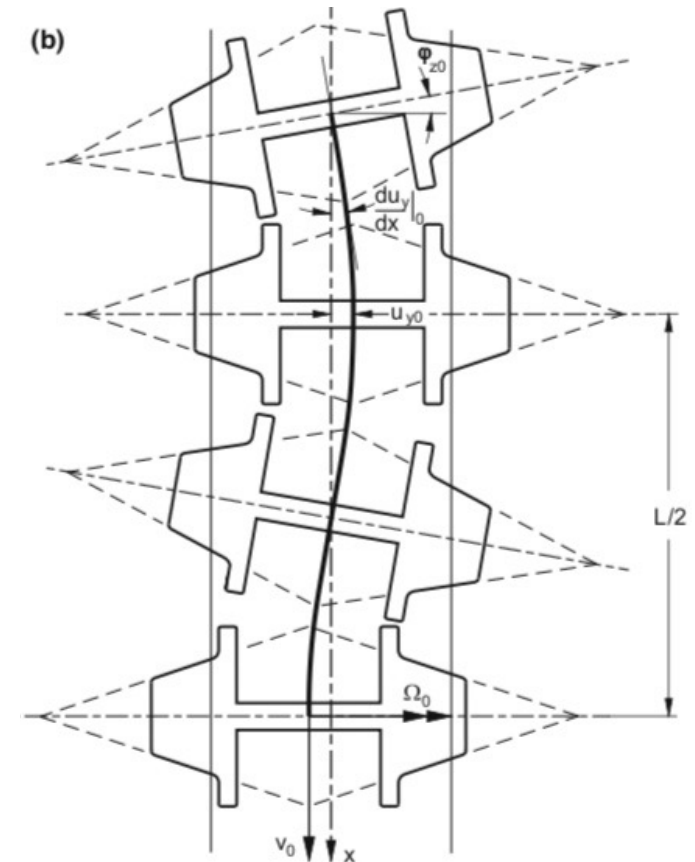
- Stability (hunting), oscillation behavior



Creep forces

$$\begin{aligned} T &= T_{\xi} \\ Q &= T_{\eta} \end{aligned} \quad \begin{bmatrix} T_{\xi} \\ T_{\eta} \\ M_{\zeta} \end{bmatrix}_{\text{lin}} = Gab \begin{bmatrix} C_{11} & 0 & 0 \\ 0 & C_{22} & \sqrt{ab} C_{23} \\ 0 & -\sqrt{ab} C_{23} & ab C_{33} \end{bmatrix} \begin{bmatrix} \nu_{\xi} \\ \nu_{\eta} \\ \nu_{\zeta} \end{bmatrix}.$$

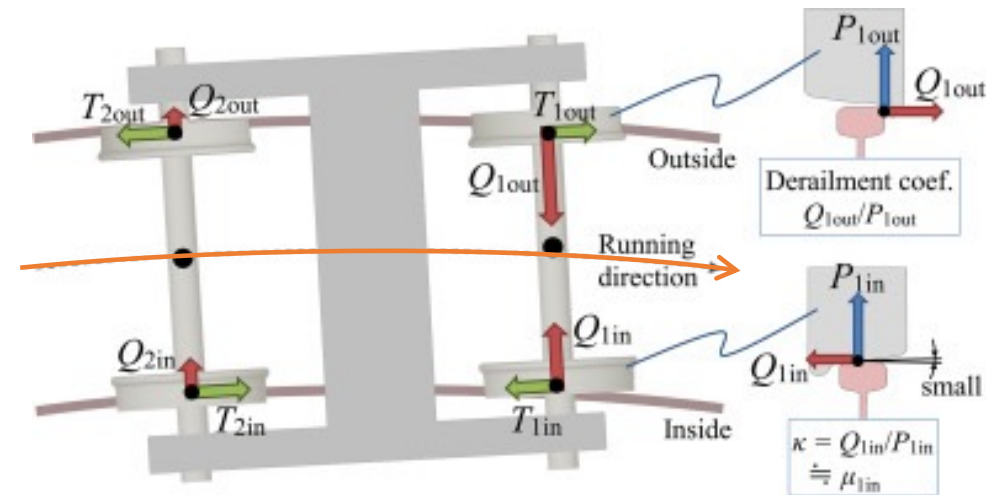
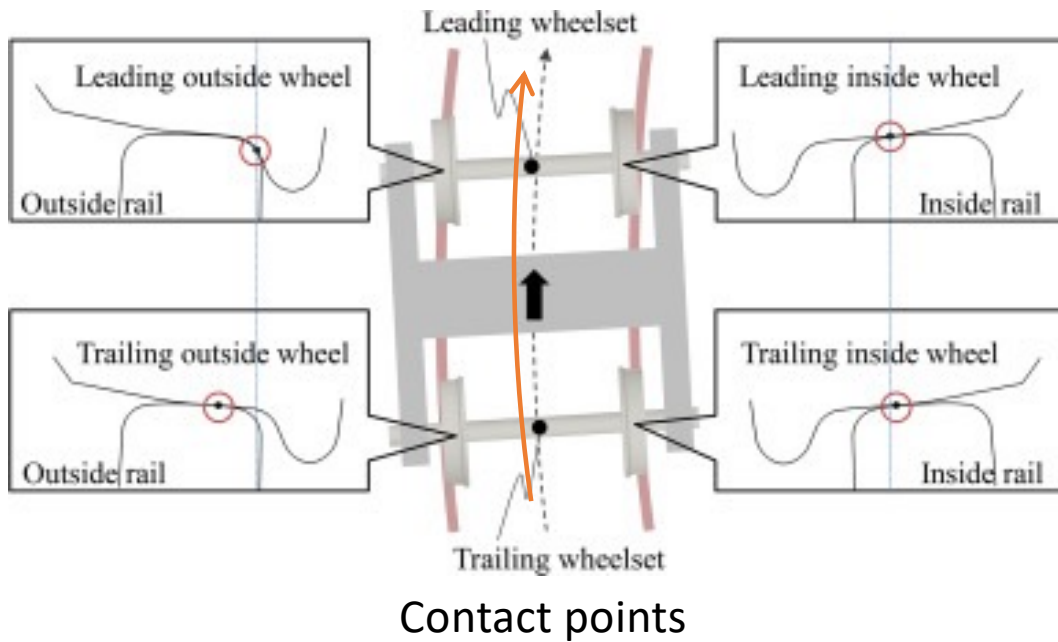
Pure rolling





# Key role of creep forces in vehicle-track interaction

- Safety against derailment, wheel-rail forces, track loading in curves



## Creep forces

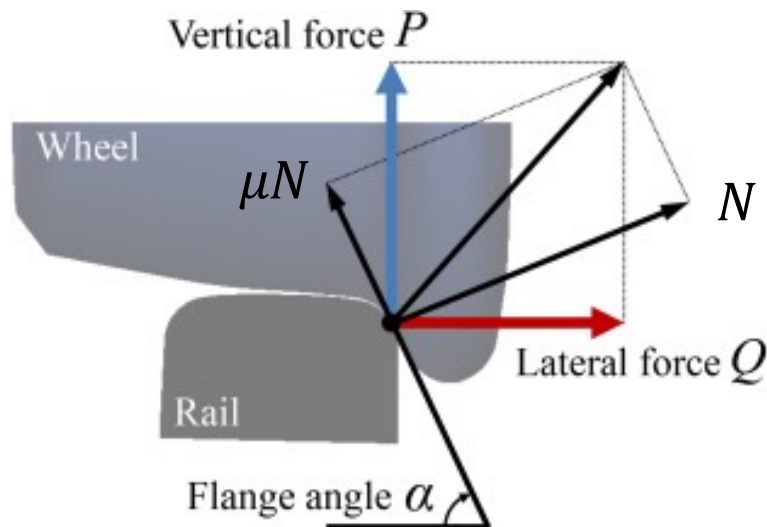
$$T = T_{\xi}$$

$$Q = T_{\eta}$$

$$\begin{Bmatrix} T_{\xi} \\ T_{\eta} \\ M_{\zeta} \end{Bmatrix}_{lin} = Gab \begin{bmatrix} C_{11} & 0 & 0 \\ 0 & C_{22} & \sqrt{ab} C_{23} \\ 0 & -\sqrt{ab} C_{23} & ab C_{33} \end{bmatrix} \begin{Bmatrix} \nu_{\xi} \\ \nu_{\eta} \\ \nu_{\zeta} \end{Bmatrix}$$

## Key role of creep forces in vehicle-track interaction

- Safety against derailment, wheel-rail forces, track loading in curves



$\mu$  coefficient of friction

Nadal's criteria

$$\frac{Q}{P} \leq \frac{\tan \alpha - \mu}{1 + \mu \tan \alpha} \quad \begin{array}{l} \approx 1.64 \quad (\alpha = 70^\circ; \mu = 0.20) \\ \approx 1.20 \quad (\alpha = 70^\circ; \mu = 0.36) \\ \approx 0.95 \quad (\alpha = 70^\circ; \mu = 0.50) \end{array}$$

$$Q = N \sin \alpha - \mu N \cos \alpha$$

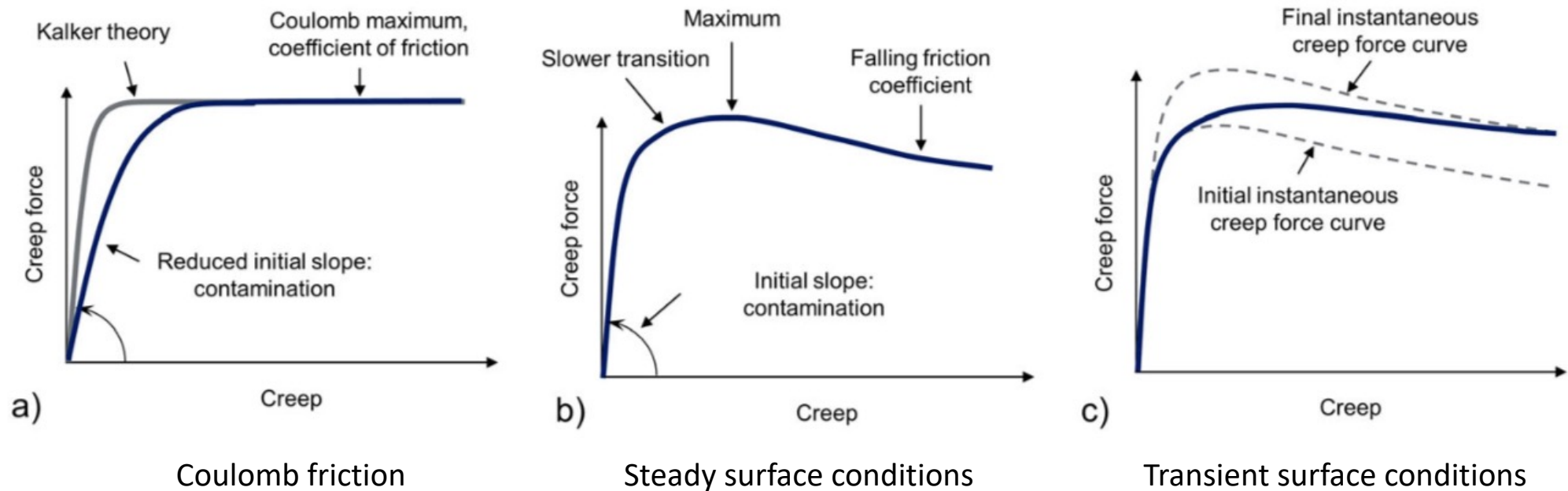
$$P = N \cos \alpha + \mu N \sin \alpha$$

$N$  : Normal contact load

$\mu N$  : maximum Tangential contact load

Nadal, M.J. (1908)

# Adhesion-creep behavior



Vollebregt, E. (2021) VSD 59 (7)

# Coefficient of friction

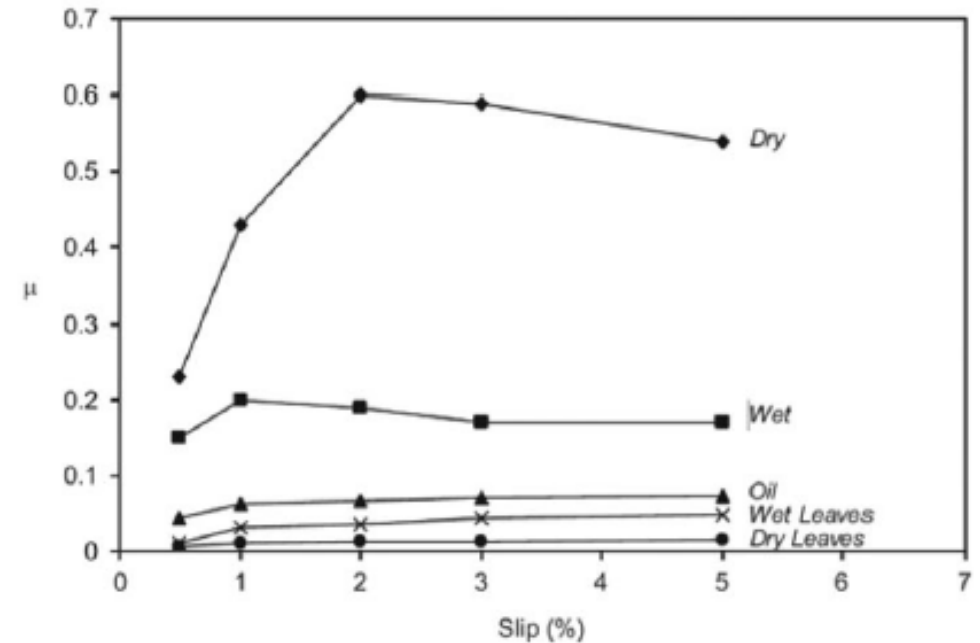
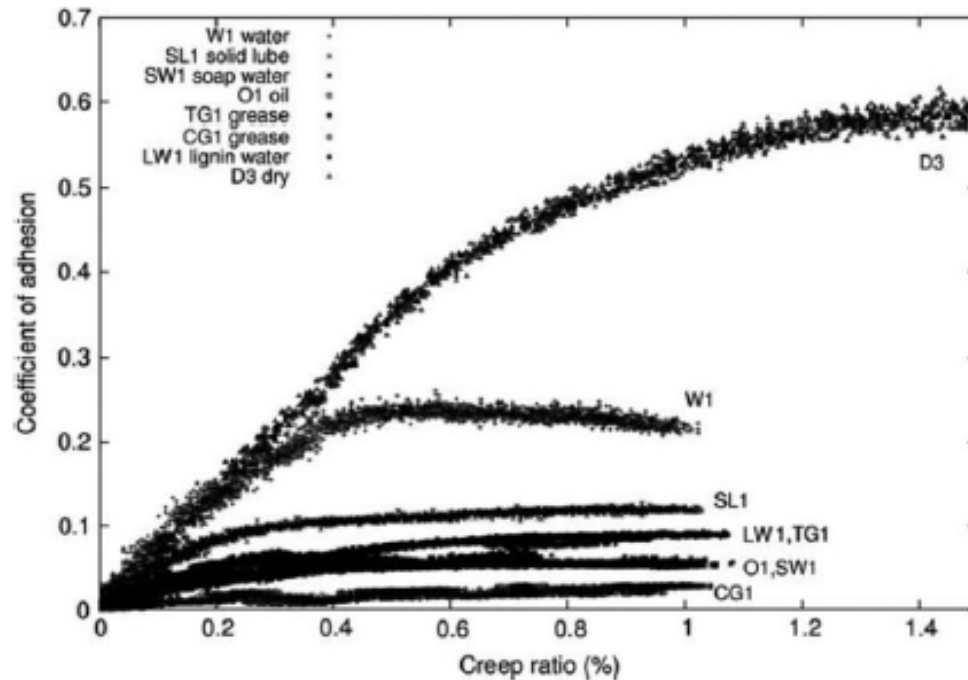
## Environmental conditions

- |                           |                                       |                                    |
|---------------------------|---------------------------------------|------------------------------------|
| • Humidity                | 0.55 (10 %HR) - 0.3 (100 %HR)         | Beagley, TM. et al. (1975) Wear 33 |
| • Clean/Oil contamination | 0.7 → 0.15                            | Beagley, TM. et al. (1975) Wear 31 |
| • Temperature             | 0.5 (20°C) – 0.4 (30°C) – 0.25 (50°C) | Baek, K. et al. (2008) Wear 265    |

## Standards

- |            |                            |                        |                                    |
|------------|----------------------------|------------------------|------------------------------------|
| • EN 14363 | 0.36 (dynamic simulations) | 0.49 (flange climbing) |                                    |
| • USA      | 0.5 (flange climbing)      |                        |                                    |
| • Japan    | 0.7 (accident measurement) |                        | Matsumoto, A. et al. (2012) VSD 50 |

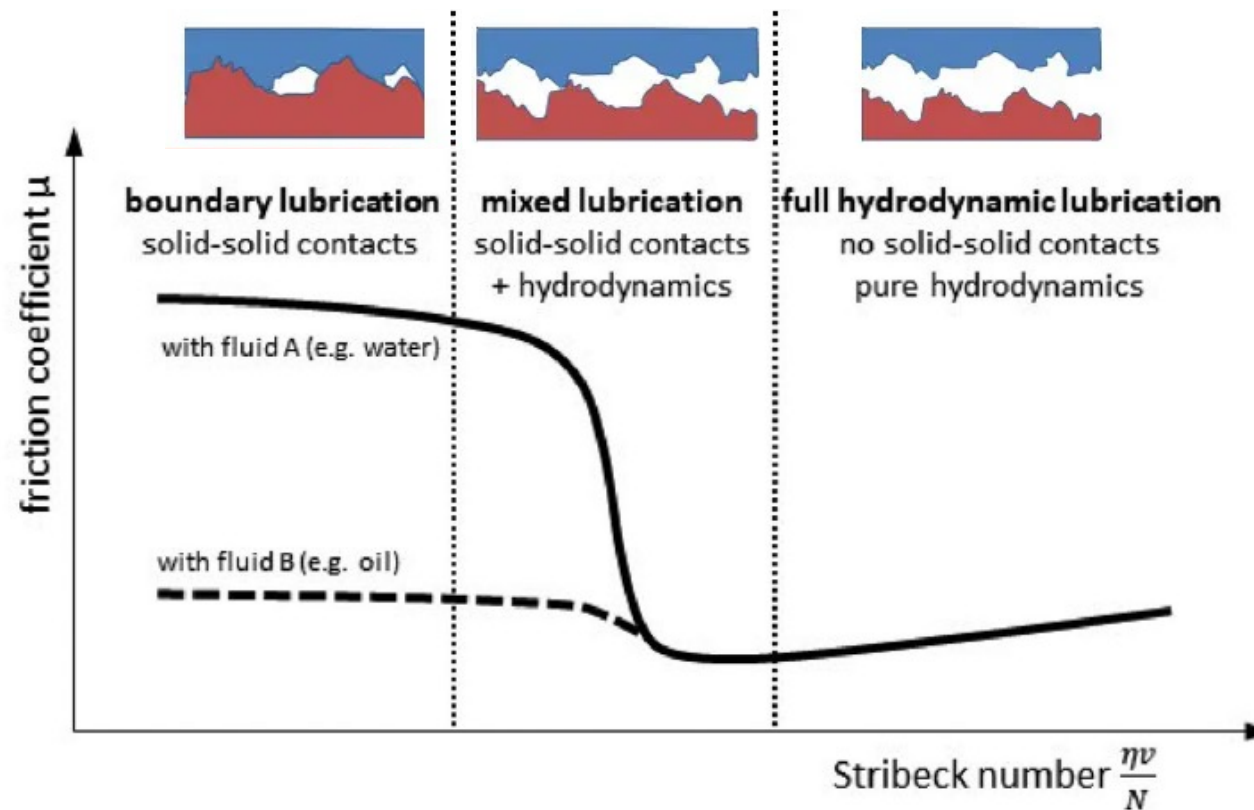
# Creep forces and contamination



- Temperature
- Interfacial solid layers
- Fluids (water, oil, mixtures)

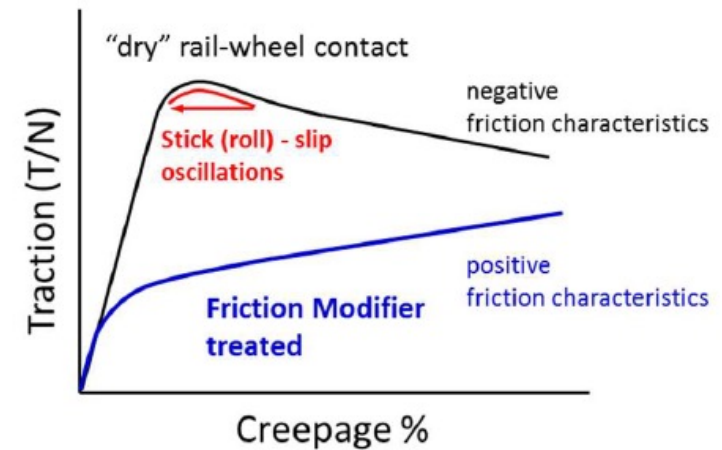
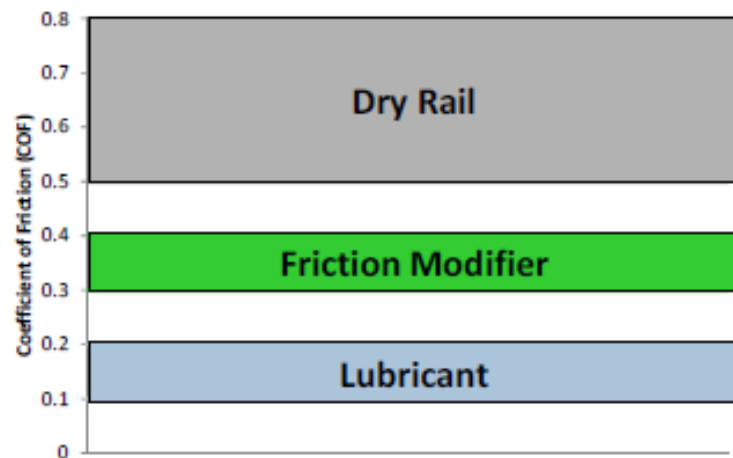
Vollebregt, E. (2021) VSD 59 (7) 1026

## Coefficient of friction in fluid lubrication



## Friction modifiers (FM)

- An additive that modifies the frictional properties of a lubricant.
- Goal: to provide one intermediate friction level and/or hold friction constant over a range conditions.

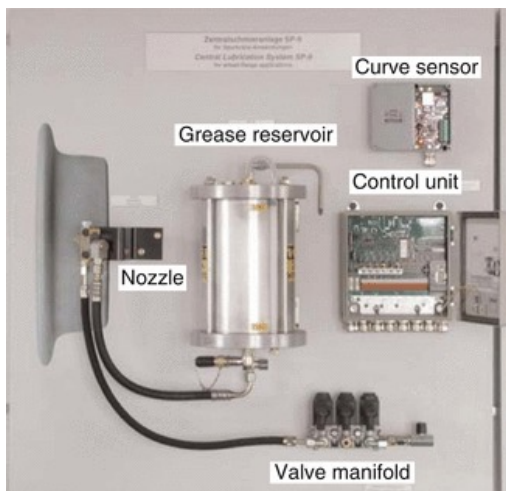




## Friction management practices: FM classification

Wheel flange and rail gauge face and gauge corner

- Aim: to **reduce friction** → to reduce wear, damage, etc.
- Practice: wheel flange lubrication systems (on vehicle side) or wayside lubrication systems (on track side)



# Friction management practices: FM classification

Wheel tread and top of the rail

## Reduce friction

- Top of Rail Friction Modifiers (ToR-FM)  $\mu : 0.5-0.7 \rightarrow 0.3-0.4$
- Aim: to reduce wear, damage, noise, energy consumption, etc.
- Attention: not to reduce the coefficient of friction to very small values  $\rightarrow$  Braking and traction - SAFETY

## Increase friction

- Adhesion or traction enhancers (sands and traction gels)
- Aim: to mitigate low adhesion and restore friction  $\rightarrow$  Braking and traction - SAFETY

## Friction modifiers drawback: liquid crack interaction

Test conditions: twin disc instrument at 1.5 GPa, 1% creep and 400 rpm

Studied cases:

- (1) dry after 4,000 cycles;
- (2) dry after 25,000 cycles;
- (3) water after 25,000 cycles;
- (4) TOR-FM after 25,000 cycles;
- (5) GF lubricant after 25,000 cycles;
- (6) TOR lubricant (oil) after 25,000 cycles;
- (7) TOR lubricant (grease) after 25,000 cycles;
- (8) TOR hybrid after 25,000.





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**EPFL**

## **Friction control in wheel-rail contacts**

**THANK YOU FOR YOUR ATTENTION**

Alejandro Roda

Head Railway Testing Laboratory HOM

01.12.2025