# Numerical solution of the advection-diffusion equation coupled with Darcy's law

Margaux Bruliard Mathieu RIGAL

Supervised by Fayssal Benkhaldoun

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## Contents

1	Introduction			1	
	1.1	Motiv	ation	1	
	1.2	Model	ing transfers	2	
2	Numerical solution of the linear problem				
	2.1	Doma	in and time discretization	3	
	2.2	A finit	te volume approach for the pressure field	4	
		2.2.1	The diamond scheme	4	
		2.2.2	Non-homogeneous Dirichlet boundary conditions	8	
	2.3	Comp	uting the velocity	9	
	2.4	4 Computing the concentration		10	
		2.4.1	A flux approach	10	
		2.4.2	Modified equation and error behavior	11	
		2.4.3	Von Neumann analysis and the CFL condition	13	
	2.5		rical results	15	
$\mathbf{A}$	Properties of the diamond scheme			17	
	A.1	Existe	ence and uniqueness of the solution	17	
	A.2	An op	timality argument for the interface harmonic mean	18	
Bi	bliog	graphy		21	

M. Bruliard & M. Rigal, Numerical Solution of the Advection-Diffusion Equation coupled with Darcy's law, 2018, Sup'Galilée

## Chapter 1

## Introduction

#### 1.1 Motivation

Advection and diffusion are two physical phenomena referring to the transfer of a quantity in some domain. Although these two phenomena represent passive processes affecting the transport, they derive from quite different causes. The next lines emphasize the distinction between these two:

**Advection** is the macroscopic effect of general motion due to a bulk flow, such as the fluid motion of a river.

**Diffusion** constitutes a transformation through random motion of particles at a microscopic level, without any bulk flow being required for it.

Various types of quantities can be considered, but most of the time heat, energy or concentration are being dealt with. When one is analyzing the transfer disregarding its causes — meaning taking into account advection and diffusion at the same time — we speak of *convection*.

The study of the aforesaid transfers is of great interest. In fact many substances are moving through the natural environment, impacting us more or less directly. A better comprehension of these processes can lead to a more efficient prediction of hazardous outcomes, as illustrated in the following examples:

- 1. Ecosystem Dynamics. In order to create energy, living organisms need food resources, and more precisely *nutrients* (oxygen, carbon dioxide, phosphorus and nitrogen among others). Thus the growth or decay of a species population in water can be anticipated through the observation of *nutrients* transfer [2, chap. 1]. An example of this is the green algae bloom that occurred on Brittany beaches in 2009, as a response to phytoplankton and zooplankton dynamics which have been altered by agriculture pollution (76 000 tons of nitrogen was discharged into the sea in 2008 according to the Loire-Brittany Water Agency). This resulted in the death of a worker, and several animal bodies have been found near the coast (including dogs, wild boars and horses).
- 2. **Toxicity.** Many industrial processes involve the production or use of chemical substances, which at some point may lead to an increase of toxic concentration. In the interest of the worker and population security, it is then essential to keep the probability of such increase as low as possible within reasonable budget. Studying transfers also helps better handle a crisis situation following an accident. This was the case with the Fukushima incident that took place after an offshore earthquake and a tsunami on March 11<sup>th</sup>, 2011. The radiation

2 Introduction

leakage into the atmosphere and the sea that came after was considerable, reaching exceptionally high levels in the direct surrounding of the power plant. A simulation of the radioactive dispersion allowed for a greater understanding of the underlying consequences, and more pertinent counter-actions were decided [4].

3. **Global Climate Change.** Unwanted effects of some chemical species on the atmosphere is pushing us consider ways to reduce their concentration.

#### 1.2 Modeling transfers

In our case, we are interested in the transfer of concentration of a constituent in a porous media. Concentration can refer to the molar concentration (amount of a constituent in moles divided by the volume of the mixture, in  $\text{mol/m}^3$ ), or the number concentration (number of entities of the species divided by the volume of the mixture, in  $1/\text{m}^3$ ). The system of partial differential equations describing this is given below:

(1.1) 
$$\begin{cases}
-\nabla \cdot (K(h(\mathbf{x}), \mathbf{x}) \overrightarrow{\nabla} h(\mathbf{x})) = f_1 & (1.1a) \\
\frac{\partial C}{\partial t} + \nabla \cdot (\mathbf{q}C) = \nabla \cdot (D\nabla C) + f_2 & (1.1b) \\
\mathbf{q} = -K \overrightarrow{\nabla} h & (1.1c)
\end{cases}$$

where:

- $C: \mathbb{R} \times \mathbb{R} \to \mathbb{R}$  is the concentration;
- $D \in \mathcal{M}_2(\mathbb{R})$  is the matrix of diffusion coefficients;
- $\mathbf{q} : \mathbb{R} \times \mathbb{R} \to \mathcal{M}_{2,1}(\mathbb{R})$  is the velocity;
- $K : \mathbb{R} \times \mathbb{R} \to \mathcal{M}_2(\mathbb{R})$  is Darcy's permeability;
- $f_1$  and  $f_2$  are two source functions;

If the permeability matrix K does not depend on the pressure h, then system (1.1) is linear. This is the case whenever a change of concentration does not impact the dynamics of the media. In the opposite case, the assumption that K is pressure-independent is not valid anymore, and (1.1) becomes nonlinear.

## Chapter 2

## Numerical solution of the linear problem

In this section, we discuss a numerical method for solving the linear system, which can be done in three main steps. We will first have to determine the pressure given by equation (1.1a) and Dirichlet boundary conditions, which will allow us to compute the velocity through Darcy's law (1.1c). Finally, we will use a flux approach with equation (1.1b) in order to approximate the concentration. It is interesting to note that in the linear case, the pressure can be calculated one time, since it does not depend on the concentration. This is quite convenient given the fact that the first step can be very demanding in terms of number of operations.

roadmap

#### 2.1 Domain and time discretization

Before going any further, we must introduce a discretization of the domain  $\Omega \subset R^2$ , and to simplify the problem we shall choose  $\Omega = ]0,1[\times]0,1[$ . Then we divide this domain in a collection of rectangular cells  $(\mathcal{C}_{ij})_{i,j}$  part of a structured mesh. Let  $N_x, N_y \in \mathbb{N}$  such that  $N_x$  is the number of columns and  $N_y$  the number of rows forming the grid , and we note  $\Delta x = 1/N_x$  and  $\Delta y = 1/N_y$ . For each pair  $(i,j) \in [\![0,N_x-1]\!] \times [\![0,N_y-1]\!]$ , we consider the index  $k=i+(N_x-1)j$  in order to have the bijective mapping  $\mathcal{C}_k \leftrightarrow \mathcal{C}_{ij}$ , as shown in fig. 2.1.

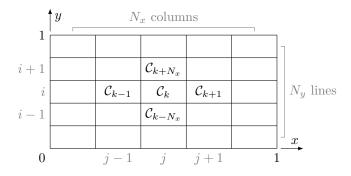


Figure 2.1: Rectangular grid

We define  $\mathcal{N}_k$  the index set of all neighbors of cell  $\mathcal{C}_k$ :

$$\mathcal{N}_k = \{i \in [0, N_x N_y - 1], \ \mathcal{C}_k \cap \mathcal{C}_i \text{ is a segment}\}$$

We will call  $\gamma_{kl}$  the frontier between the  $k^{\text{th}}$  cell and the  $l^{\text{th}}$  cell, with  $l \in \mathcal{N}_k$ . Thus we have:  $\forall k \in [0, N_x N_y - 1]$  such that  $\mathcal{C}_k$  is not a border cell,  $\partial \mathcal{C}_k = \bigcup_{l \in \mathcal{N}_k} \gamma_{kl}$ .

As for time discretization, we will divide an interval of time [0, T] into  $N_t$  sub-intervals, meaning that we will get  $N_t + 1$  points of time discretization.

## 2.2 A finite volume approach for the pressure field

#### 2.2.1 The diamond scheme

pressure approximation

Now that the domain is discretized, we start by approximating the pressure h. To achieve this, we use a finite volume approach that will lead us to the diamond scheme. Because we are considering Dirichlet boundary conditions, the values of h on the border of the domain are already known. For this reason, in what follows we restrict ourselves to indices k or (i,j) that are not referring to a border cell. Put in other words, we solve the problem on the mesh exluding its first and last rows and columns, which will be referred to as the truncated mesh of  $N_x-2$  columns and  $N_y-2$  rows. With this in mind, we first integrate equation (1.1a) over a cell  $\mathcal{C}_k$  for a fixed k:

$$\int_{\mathcal{C}_k} f_1 dx = -\int_{\mathcal{C}_k} \nabla \cdot (K \overrightarrow{\nabla} h) dx = -\int_{\partial \mathcal{C}_k} K \overrightarrow{\nabla} h \cdot \mathbf{n} \, d\sigma$$

$$\Longrightarrow |\mathcal{C}_k| f_{1,\mathcal{C}_k} = -\sum_{l \in \mathcal{N}_k} \int_{\gamma_{kl}} K \overrightarrow{\nabla} h \cdot \mathbf{n} \, d\sigma \quad \text{with } f_{1,\mathcal{C}_k} = \frac{1}{|\mathcal{C}_k|} \int_{\mathcal{C}_k} f_1 dx \quad (2.1)$$

The intermediate step here is to approximate  $\overrightarrow{\nabla}h = (\partial_x h, \partial_y h)^T$ . In this regard, we do the following assumption: the pressure gradient is a constant on every diamond cell  $\mathcal{D}_{kl}$ , where  $\mathcal{D}_{kl}$  is a quadrilateral cell such that  $\gamma_{kl} \subset \mathcal{D}_{kl}$  (see fig. 2.2). From this new perspective, finding the pressure gradient on  $\gamma_{kl} \forall l \in \mathcal{N}_k$  can be completed by finding its value on  $\mathcal{D}_{kl} \forall l \in \mathcal{N}_k$ .

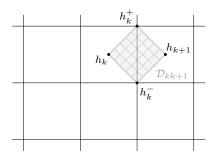


Figure 2.2: Diamond cell centered on the border  $\gamma_{kk+1}$ 

Figure 2.2 illustrates the diamond cell centered around  $\gamma_{kk+1}$ . The values  $h_k^-$  and

diamond cell

#### 2.2 A finite volume approach for the pressure field

 $\boldsymbol{h}_k^+$  can be approximated at the second order as described below:

$$\begin{cases} h_{k} = h_{k}^{-} - \frac{\Delta x}{2} \partial_{x} h_{k}^{-} + \frac{\Delta y}{2} \partial_{y} h_{k}^{-} + \mathcal{O}(\Delta x^{2} + \Delta y^{2}) \\ h_{k+1} = h_{k}^{-} + \frac{\Delta x}{2} \partial_{x} h_{k}^{-} + \frac{\Delta y}{2} \partial_{y} h_{k}^{-} + \mathcal{O}(\Delta x^{2} + \Delta y^{2}) \\ h_{k-N_{x}} = h_{k}^{-} - \frac{\Delta x}{2} \partial_{x} h_{k}^{-} - \frac{\Delta y}{2} \partial_{y} h_{k}^{-} + \mathcal{O}(\Delta x^{2} + \Delta y^{2}) \\ h_{k+1-N_{x}} = h_{k}^{-} + \frac{\Delta x}{2} \partial_{x} h_{k}^{-} - \frac{\Delta y}{2} \partial_{y} h_{k}^{-} + \mathcal{O}(\Delta x^{2} + \Delta y^{2}) \\ \Longrightarrow h_{k}^{-} = \frac{h_{k-N_{x}} + h_{k+1-N_{x}} + h_{k} + h_{k+1}}{4} + \mathcal{O}(\Delta x^{2} + \Delta y^{2}) \end{cases}$$
(2.2)

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Following the same idea we have:

$$h_k^+ = \frac{h_k + h_{k+1} + h_{k+N_x} + h_{k+1+N_x}}{4} + \mathcal{O}(\Delta x^2 + \Delta y^2)$$
 (2.3)

Lastly, we need to characterize the frontier  $\partial \mathcal{D}_{kl}$  of  $\mathcal{D}_{kl}$ . We define the segments  $(d_i)_{1 \leq i \leq 4}$  such that  $\partial \mathcal{D}_{kl} = \bigcup_{1 \leq i \leq 4} d_i$ ,  $d_1$  being the lower right diamond border,  $d_2$  the upper right,  $d_3$  the upper left and  $d_4$  the lower left. It is clear that  $\forall 1 \leq i \leq 4$ ,  $|d_i| = \frac{1}{2} \sqrt{\Delta x^2 + \Delta y^2}$ , and the associated unit normal vectors are:

$$\mathbf{n}_{d_1} = \frac{1}{2|d_1|} \begin{pmatrix} \Delta y \\ -\Delta x \end{pmatrix} = -\mathbf{n}_{d_3}, \quad \mathbf{n}_{d_2} = \frac{1}{2|d_1|} \begin{pmatrix} \Delta y \\ \Delta x \end{pmatrix} = -\mathbf{n}_{d_4}$$

We carry on by integrating  $\vec{\nabla} h$  over  $\mathcal{D}_{kl}$ :

$$\int_{\mathcal{D}_{i,j}} \vec{\nabla} h dx = \int_{\partial \mathcal{D}_{i,j}} h \mathbf{n}_{kl} d\sigma \tag{2.4}$$

Knowing that  $\overrightarrow{\nabla} h$  is a constant in  $\mathcal{D}_{kl}$  we can write:

$$|\mathcal{D}_{kl}| \overrightarrow{\nabla} h_{|\mathcal{D}_{kl}} = \int_{\partial \mathcal{D}_{kl}} h \mathbf{n}_d d\sigma \Longrightarrow \overrightarrow{\nabla} h_{|\gamma_{kl}} = \frac{1}{|\mathcal{D}_{kl}|} \int_{\partial \mathcal{D}_{kl}} h \mathbf{n}_d d\sigma$$

$$\overrightarrow{\nabla} h_{|\gamma_{kl}} = \frac{2}{|\mathcal{C}_k|} \int_{\partial \mathcal{D}_{kl}} h \mathbf{n}_d d\sigma \qquad (2.5)$$

Going back to equation (2.1) we have:

$$-|\mathcal{C}_{k}|f_{1,\mathcal{C}_{k}} = \sum_{l \in \mathcal{N}_{k}} \int_{\gamma_{kl}} K \overrightarrow{\nabla} h \cdot \mathbf{n} d\sigma$$

$$= \sum_{l \in \mathcal{N}_{k}} |\gamma_{kl}| K \overrightarrow{\nabla} h_{|\gamma_{kl}|} \cdot \mathbf{n}_{kl}$$

$$= \sum_{l \in \mathcal{N}_{k}} \frac{|\gamma_{kl}|}{|\mathcal{D}_{kl}|} \left( K \int_{\partial \mathcal{D}_{kl}} h \mathbf{n}_{d} d\sigma \right) \cdot \mathbf{n}_{kl}$$
(2.6)

Then we rewrite the integrals as below:

$$\int_{\partial \mathcal{D}_{kk+1}} h \mathbf{n}_d d\sigma$$

$$= \frac{|d_{1}|}{2} (h_{k}^{-} + h_{k+1}) \mathbf{n}_{d_{1}} + \frac{|d_{2}|}{2} (h_{k+1} + h_{k}^{+}) \mathbf{n}_{d_{2}} + \frac{|d_{3}|}{2} (h_{k}^{+} + h_{k}) \mathbf{n}_{d_{3}} 
+ \frac{|d_{4}|}{2} (h_{k} + h_{k}^{-}) \mathbf{n}_{d_{4}} + (\Delta x + \Delta y) \vec{\varepsilon} (\Delta x, \Delta y) 
= \frac{|d_{1}|}{2} \Big( h_{k}^{-} (\mathbf{n}_{d_{1}} + \mathbf{n}_{d_{4}}) + h_{k} (\mathbf{n}_{d_{3}} + \mathbf{n}_{d_{4}}) + h_{k+1} (\mathbf{n}_{d_{1}} + \mathbf{n}_{d_{2}}) 
+ h_{k}^{+} (\mathbf{n}_{d_{2}} + \mathbf{n}_{d_{3}}) \Big) + (\Delta x + \Delta y) \vec{\varepsilon} (\Delta x, \Delta y) 
= \frac{1}{2} \Big( -h_{k}^{-} \begin{pmatrix} 0 \\ \Delta x \end{pmatrix} - h_{k} \begin{pmatrix} \Delta y \\ 0 \end{pmatrix} + h_{k+1} \begin{pmatrix} \Delta y \\ 0 \end{pmatrix} + h_{k}^{+} \begin{pmatrix} 0 \\ \Delta x \end{pmatrix} \Big) 
+ (\Delta x + \Delta y) \vec{\varepsilon} (\Delta x, \Delta y) 
= \frac{1}{8} \begin{pmatrix} 0 \\ \Delta x \end{pmatrix} (h_{k+N_{x}} + h_{k+1+N_{x}} - h_{k-N_{x}} - h_{k+1-N_{x}}) 
+ \frac{1}{2} \begin{pmatrix} \Delta y \\ 0 \end{pmatrix} (h_{k+1} - h_{k}) + (\Delta x + \Delta y) \vec{\varepsilon} (\Delta x, \Delta y)$$
(2.7)

We do the same for the three other borders:

$$\int_{\partial \mathcal{D}_{kk+N_x}} h \mathbf{n}_d d\sigma = \frac{1}{8} \begin{pmatrix} \Delta y \\ 0 \end{pmatrix} (h_{k+1+N_x} + h_{k+1} - h_{k-1+N_x} - h_{k-1}) 
+ \frac{1}{2} \begin{pmatrix} 0 \\ \Delta x \end{pmatrix} (h_{k+N_x} - h_k) + (\Delta x + \Delta y) \overrightarrow{\varepsilon} (\Delta x, \Delta y) \qquad (2.8)$$

$$\int_{\partial \mathcal{D}_{kk-1}} h \mathbf{n}_d d\sigma = \frac{1}{8} \begin{pmatrix} 0 \\ \Delta x \end{pmatrix} (h_{k-1+N_x} + h_{k+N_x} - h_{k-1-N_x} - h_{k-N_x}) 
+ \frac{1}{2} \begin{pmatrix} \Delta y \\ 0 \end{pmatrix} (h_k - h_{k-1}) + (\Delta x + \Delta y) \overrightarrow{\varepsilon} (\Delta x, \Delta y) \qquad (2.9)$$

$$\int_{\partial \mathcal{D}_{kk-N_x}} h \mathbf{n}_d d\sigma = \frac{1}{8} \begin{pmatrix} \Delta y \\ 0 \end{pmatrix} (h_{k+1} + h_{k+1-N_x} - h_{k-1} - h_{k-1-N_x}) 
+ \frac{1}{2} \begin{pmatrix} 0 \\ \Delta x \end{pmatrix} (h_k - h_{k-N_x}) + (\Delta x + \Delta y) \overrightarrow{\varepsilon} (\Delta x, \Delta y) \qquad (2.10)$$

Substituting equations (2.7) to (2.10) into (2.6) we get a nine points finite volume scheme:

$$\begin{split} -4|\mathcal{C}_{k}|^{2}f_{1,\mathcal{C}_{k}} &= -\Delta x \Big[K_{21}\Delta y(h_{k+1} + h_{k+1-N_{x}} - h_{k-1} - h_{k-1-N_{x}}) \\ &\quad + 4K_{22}\Delta x(h_{k} - h_{k-N_{x}})\Big] \\ &\quad - \Delta y \Big[4K_{11}\Delta y(h_{k} - h_{k-1}) \\ &\quad + K_{12}\Delta x(h_{k-1+N_{x}} + h_{k+N_{x}} - h_{k-1-N_{x}} - h_{k-N_{x}})\Big] \\ &\quad + \Delta y \Big[4K_{11}\Delta y(h_{k+1} - h_{k}) \\ &\quad + K_{12}\Delta x(h_{k+N_{x}} + h_{k+1+N_{x}} - h_{k-N_{x}} - h_{k+1-N_{x}})\Big] \\ &\quad + \Delta x \Big[K_{21}\Delta y(h_{k+1+N_{x}} + h_{k+1} - h_{k-1+N_{x}} - h_{k-1}) \end{split}$$

#### 2.2 A finite volume approach for the pressure field

$$+4K_{22}\Delta x(h_{k+N_x} - h_k) \Big]$$

$$+\mathcal{O}(\Delta x^2 + \Delta y^2)$$

$$-4|\mathcal{C}_k|^2 f_{1,\mathcal{C}_k} = (K_{12} + K_{21})\Delta x \Delta y h_{k-1-N_x} + 4K_{22}\Delta x^2 h_{k-N_x}$$

$$-(K_{12} + K_{21})\Delta x \Delta y h_{k+1-N_x} + 4K_{11}\Delta y^2 h_{k-1}$$

$$-8(K_{22}\Delta x^2 + K_{11}\Delta y^2)h_k + 4K_{11}\Delta y^2 h_{k+1}$$

$$-(K_{12} + K_{21})\Delta x \Delta y h_{k-1+N_x} + 4K_{22}\Delta x^2 h_{k+N_x}$$

$$+(K_{12} + K_{21})\Delta x \Delta y h_{k+1+N_x}$$

$$+\mathcal{O}(\Delta x^2 + \Delta y^2)$$

$$(2.11)$$

Finally we give the matrix form of (2.11):

$$\mathbf{R}\mathbf{h} = \mathbf{b} \tag{2.12}$$

The rigidity matrix R and the vectors  $\mathbf{h}, \mathbf{b}$  are defined below:

$$R = \begin{pmatrix} A & B^{T} \\ B & A & B^{T} \\ & \ddots & \ddots & \ddots \\ & & B & A & B^{T} \\ & & & B & A \end{pmatrix} \quad \mathbf{h} = \begin{pmatrix} h_{k} \end{pmatrix}_{\substack{0 \le k \le N_{x}N_{y} - 1 \\ C_{k} \text{ not a border cell}}}$$

$$\mathbf{b} = \begin{pmatrix} -4\Delta x^{2} \Delta y^{2} f_{1,C_{k}} \end{pmatrix}_{\substack{0 \le k \le N_{x}N_{y} - 1 \\ C_{k} \text{ not a border cell}}}$$

$$A = \begin{pmatrix} \alpha & \beta & & & & & & \\ \beta & \alpha & \beta & & & & \\ & \ddots & \ddots & \ddots & & & \\ & & \beta & \alpha & \beta & & \\ & & & \beta & \alpha \end{pmatrix} \quad \text{with } \begin{cases} \alpha = -8(K_{22}\Delta x^{2} + K_{11}\Delta y^{2}) \\ \beta = 4K_{11}\Delta y^{2} \end{cases}$$

$$B = \begin{pmatrix} \gamma & -\delta & & & & \\ \delta & \gamma & -\delta & & & \\ & \ddots & \ddots & \ddots & & \\ & & \delta & \gamma & -\delta \end{pmatrix} \quad \text{with } \begin{cases} \gamma = 4K_{22}\Delta x^{2} \\ \delta = (K_{12} + K_{21})\Delta x\Delta y \end{cases}$$

In virtue of what has been stated regarding the Dirichlet boundary conditions, the problem is being solved on a mesh of size  $(Nx-2)(N_y-2)$ , and thus  $R \in \mathcal{M}_{(N_x-2)(N_y-2)}(\mathbb{R})$ ,  $A,B \in \mathcal{M}_{N_x-2}(\mathbb{R})$ , and  $\mathbf{b},\mathbf{h} \in \mathcal{M}_{(N_x-2)(N_y-2),1}(\mathbb{R})$ . Since we excluded the boundary values of  $\mathbf{h}$ , they do not appear in the system  $R\mathbf{h} = \mathbf{b}$  which is true if  $h_{|\partial\Omega} = 0$ . Therefore, expression (2.12) is appropriate only when considering the homogeneous Dirichlet conditions, the non-homogeneous case being treated in subsection 2.2.2.

Since we would like to solve (2.12), we give a condition under which the rigidity matrix R is nonsingular. If  $K_{11} \neq 0$ ,  $K_{22} \neq 0$  and  $K_{12} = K_{21} = 0$  are satisfied, we can prove that R is a weakly chained diagonally dominant matrix, and thus is inversible. In fact for each line i in R we verify that  $|R_{ii}| - \sum_{j \neq i} |R_{ij}| \geq 0$ . Furthermore, for each row that is not strictly diagonally dominant there exist a walk in the directed graph of R ending at a strictly diagonally dominant row. This can be seen by considering the diagonal, upper-diagonal and lower-diagonal of R

which contain only non-zero coefficients. A more general result gives us existence and uniqueness of the solution h — and thus the nonsingularity of R — when K is positive-definite (see appendix A.1).

In the more general case where the permeability K has different values depending on the position, the rigidity and second member matrix are more complex to express. Without detailing it, from (2.1) we would have found for all k:

$$4|\mathcal{C}_{k}|^{2}f_{1,\mathcal{C}_{k}} = -(\tilde{K}_{12}^{k,k-1} + \tilde{K}_{21}^{k,k-N_{x}})\Delta x\Delta y \, h_{k-1-N_{x}} \\ -(\tilde{K}_{12}^{k,k-1}\Delta x\Delta y - \tilde{K}_{12}^{k,k+1}\Delta x\Delta y + 4\tilde{K}_{22}^{k,k-N_{x}}\Delta x^{2})h_{k-N_{x}} \\ +(\tilde{K}_{12}^{k,k+1} + \tilde{K}_{21}^{k,k-N_{x}})\Delta x\Delta y \, h_{k+1-N_{x}} \\ -(\tilde{K}_{21}^{k,k-N_{x}}\Delta x\Delta y - \tilde{K}_{21}^{k,k+N_{x}}\Delta x\Delta y + 4\tilde{K}_{11}^{k,k-1}\Delta y^{2})h_{k-1} \\ +4(\tilde{K}_{11}^{k,k-1}\Delta y^{2} + \tilde{K}_{11}^{k,k+1}\Delta y^{2} + \tilde{K}_{22}^{k,k-N_{x}}\Delta x^{2} + \tilde{K}_{22}^{k,k+N_{x}}\Delta x^{2})h_{k} \\ -(\tilde{K}_{21}^{k,k+N_{x}}\Delta x\Delta y - \tilde{K}_{21}^{k,k-N_{x}}\Delta x\Delta y + 4\tilde{K}_{11}^{k,k+1}\Delta y^{2})h_{k+1} \\ +(\tilde{K}_{12}^{k,k-1} + \tilde{K}_{21}^{k,k+N_{x}})\Delta x\Delta y h_{k-1+N_{x}} \\ -(\tilde{K}_{12}^{k,k+1}\Delta x\Delta y - \tilde{K}_{12}^{k,k-1}\Delta x\Delta y + 4\tilde{K}_{22}^{k,k+N_{x}}\Delta x^{2})h_{k+N_{x}} \\ -(\tilde{K}_{12}^{k,k+1} + \tilde{K}_{21}^{k,k+N_{x}})\Delta x\Delta y h_{k+1+N_{x}} \\ +\mathcal{O}(\Delta x^{2} + \Delta y^{2})$$
 (2.13)

with  $\tilde{K}_{ij}^{k,l}$  being the harmonic mean between coefficients  $K_{ij}$  respectively at the center of cells  $C_k$  and  $C_l$ :

$$\tilde{K}_{ij}^{k,l} = 2 \frac{K_{ij}^k K_{ij}^l}{K_{ij}^k + K_{ij}^l}$$
 (2.14)

This choice is justified in appendix A.2.

#### 2.2.2 Non-homogeneous Dirichlet boundary conditions

upper left corner

Taking into account non-homogeneous Dirichlet conditions can be achieved by modifying the second member vector **b**. As a matter of fact, if we take for example the upper left corner of our truncated mesh, we see that the nine points diamond scheme (2.11) cannot be computed directly, since it would require some additional cells. More specifically five points are out of the sub-mesh previously defined, and don't relate to any of the unkowns  $(h_k)_k$  (see fig. 2.3).

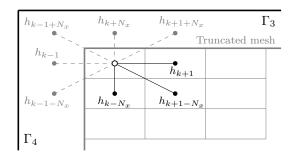


Figure 2.3: Upper left cell  $C_{(N_x-2)(N_y-2)}$ . Gray nodes refer to "virtual" points that would exist if there was one more line and one more column in the truncated mesh. In reality, these "virtual" points are replaced by the known Dirichlet boundary conditions.

If we note  $\Gamma_1$  the lower border of the domain,  $\Gamma_2$  the right border,  $\Gamma_3$  the upper border,  $\Gamma_4$  the left border, and  $h_{\Gamma_1},...,h_{\Gamma_4}$  the corresponding Dirichlet boundary adapting the diamond conditions, the nine points scheme could be replaced at the level of  $\mathcal{C}_{(N_x-2)(N_y-2)}$ 

$$-4|\mathcal{C}_{k}|^{2} f_{1,\mathcal{C}_{k}} = \delta h_{\Gamma_{4}} (1 - 2\Delta y) + \gamma h_{k-N_{x}} - \delta h_{k+1-N_{x}} + \beta h_{\Gamma_{4}} (1 - \Delta y) + \alpha h_{k} + \beta h_{k+1} - \delta h_{\Gamma_{4}} (1) + \gamma h_{\Gamma_{3}} (\Delta x) + \delta h_{\Gamma_{3}} (2\Delta x) + \mathcal{O}(\Delta x^{2} + \Delta y^{2})$$
(2.15)

And thus the new line in the matrix system is:

$$\sum_{j=1}^{N_x} \mathbf{R}_{N_y j} h_j = \tilde{b}_{N_y}$$
with  $\tilde{b}_{N_y} = b_{N_y} - \delta h_{\Gamma_4} (1 - 2\Delta y) - \beta h_{\Gamma_4} (1 - \Delta y) + \delta h_{\Gamma_4} (1)$ 

$$- \gamma h_{\Gamma_3} (\Delta x) - \delta h_{\Gamma_3} (2\Delta x) \tag{2.16}$$

#### Computing the velocity 2.3

Up to this point, we managed to approximate the pressure field across the mesh. We continue by computing the velocity  $\mathbf{q}$  thanks to Darcy's law (1.1c). Using Taylor expansions, we know that for each non-boreder cell  $\mathcal{C}_k$  the pressure gradient verifies:

$$\vec{\nabla} h_{|\gamma_{kl}} = \begin{pmatrix} (h_l - h_k)/\Delta x \\ (h_{k-1}^+ - h_{k-1}^-)/\Delta y \end{pmatrix} + \vec{\varepsilon} (\Delta x, \Delta y) \quad \text{if } l = k - 1$$

$$\vec{\nabla} h_{|\gamma_{kl}} = \begin{pmatrix} (h_l - h_k)/\Delta x \\ (h_k^+ - h_k^-)/\Delta y \end{pmatrix} + \vec{\varepsilon} (\Delta x, \Delta y) \quad \text{if } l = k + 1$$

$$\vec{\nabla} h_{|\gamma_{kl}} = \begin{pmatrix} (h_k^- - h_{k-1}^-)/\Delta x \\ (h_l - h_k)/\Delta y \end{pmatrix} + \vec{\varepsilon} (\Delta x, \Delta y) \quad \text{if } l = k - N_x$$

$$\vec{\nabla} h_{|\gamma_{kl}} = \begin{pmatrix} (h_k^+ - h_{k-1}^+)/\Delta x \\ (h_l - h_k)/\Delta y \end{pmatrix} + \vec{\varepsilon} (\Delta x, \Delta y) \quad \text{if } l = k + N_x$$

If  $i \in \{0, N_x - 1\}$  or  $j \in \{0, N_y - 1\}$ , we will apply Neumann boundary conditions as indicated below:

$$\begin{split} \partial_x h(x_0, y_j) &= \frac{h(x_1, y_j) - h(x_0, y_j)}{\Delta x} + \mathcal{O}(\Delta x) \\ \partial_x h(x_{N_x - 1}, y_j) &= \frac{h(x_{N_x - 1}, y_j) - h(x_{N_x - 2}, y_j)}{\Delta x} + \mathcal{O}(\Delta x) \\ \partial_y h(x_i, y_0) &= \frac{h(x_i, y_1) - h(x_i, y_0)}{\Delta y} + \mathcal{O}(\Delta y) \\ \partial_y h(x_y, y_{N_y - 1}) &= \frac{h(x_i, y_{N_y - 1}) - h(x_i, y_{N_y - 2})}{\Delta y} + \mathcal{O}(\Delta y) \end{split}$$

At last the velocity is deduced from the matrix product:

$$\mathbf{q} = -K \vec{\nabla} h$$

#### 2.4 Computing the concentration

#### 2.4.1 A flux approach

We assume to know the concentration state at time  $t_n \in [0,T]$ . In order to approximate it at time  $t_{n+1} = t_n + \Delta t$  we integrate (1.1b) (with D = 0 and  $f_2 = 0$ ) over a given cell  $C_k$  between times  $t_n$  and  $t_{n+1}$ :

$$\int_{t_n}^{t_{n+1}} \int_{\mathcal{C}_k} \frac{\partial C}{\partial t} dx dt + \int_{t_n}^{t_{n+1}} \int_{\mathcal{C}_k} \nabla \cdot (\mathbf{q}C) dx dt = 0$$

$$\implies |\mathcal{C}_k| (C_k^{n+1} - C_k^n) = -\int_{t_n}^{t_{n+1}} \int_{\partial \mathcal{C}_k} (\mathbf{q} \cdot \mathbf{n}) C d\sigma dt$$

$$\implies C_k^{n+1} = C_k^n - \frac{\Delta t}{|\mathcal{C}_k|} \sum_{l \in \mathcal{N}_k} |\gamma_{kl}| \, \mathbf{q}_{|\gamma_{kl}} \cdot \mathbf{n}_{|\gamma_{kl}|} \, \phi_{\gamma_{kl}}(C^n, \mathbf{q})$$

with  $\phi_{\gamma_{kl}}$  the flux term corresponding to border  $\gamma_{kl}$ , which is defined as:

$$\forall k, \ \forall l \in \mathcal{N}_k, \ \phi_{\gamma_{kl}}(C^n, \mathbf{q}) = \begin{cases} C_k^n & \text{if } \mathbf{q}_{|\gamma_{kl}} \cdot \mathbf{n}_{|\gamma_{kl}} \ge 0\\ C_{k-N_x}^n & \text{if } \mathbf{q}_{|\gamma_{kl}} \cdot \mathbf{n}_{|\gamma_{kl}} \le 0 \text{ and } l = k - N_x\\ C_{k-1}^n & \text{if } \mathbf{q}_{|\gamma_{kl}} \cdot \mathbf{n}_{|\gamma_{kl}} \le 0 \text{ and } l = k - 1\\ C_{k+1}^n & \text{if } \mathbf{q}_{|\gamma_{kl}} \cdot \mathbf{n}_{|\gamma_{kl}} \le 0 \text{ and } l = k + 1\\ C_{k+N_x}^n & \text{if } \mathbf{q}_{|\gamma_{kl}} \cdot \mathbf{n}_{|\gamma_{kl}} \le 0 \text{ and } l = k + N_x \end{cases}$$

Then we can write:

$$C_{k}^{n+1} = C_{k}^{n} - \frac{\Delta t}{\Delta x} (q_{x \mid \gamma_{kk+1}} \phi_{\gamma_{kk+1}} (C^{n}, \mathbf{q}) - q_{x \mid \gamma_{kk-1}} \phi_{\gamma_{kk-1}} (C^{n}, \mathbf{q})) - \frac{\Delta t}{\Delta y} (q_{y \mid \gamma_{kk+N_{x}}} \phi_{\gamma_{kk+N_{x}}} (C^{n}, \mathbf{q}) - q_{y \mid \gamma_{kk-N_{x}}} \phi_{\gamma_{kk-N_{x}}} (C^{n}, \mathbf{q}))$$
(2.17)

Since in our case fluxes are modeled by the displacement of the concentration in a cell to its direct neighbors, the step of time has to verify the following condition:

$$\Delta t \le \min\left(\frac{\Delta x}{\max(|q_x|)}, \frac{\Delta y}{\max(|q_y|)}\right)$$
 (2.18)

As a matter of fact this condition ensures that at each iteration the transport of the concentration will not be greater than the width or height of a cell, which constitutes a constraint inherent to our scheme.

In order to take charge of the diffusion phenomenon represented by  $\nabla \cdot (D \overrightarrow{\nabla} C)$  in the continuous equation, we detail its discretization:

$$\begin{split} \frac{1}{|\mathcal{C}_k|} \int_{t_n}^{t_{n+1}} \int_{\mathcal{C}_k} \nabla \cdot (D \overrightarrow{\nabla} C) \, dx &= \frac{1}{|\mathcal{C}_k|} \int_{t_n}^{t_{n+1}} \int_{\partial \mathcal{C}_k} D \overrightarrow{\nabla} C \cdot \mathbf{n}_{|\gamma_{kl}} \, d\sigma \\ &\approx \frac{\Delta t}{|\mathcal{C}_k|} \sum_{l \in \mathcal{N}_k} |\gamma_{kl}| D \overrightarrow{\nabla} C_{|\gamma_{kl}} \cdot \mathbf{n}_{|\gamma_{kl}} \end{split}$$

The concentration gradient is approximated exactly the same way than what has been done for the pressure gradient. One should then add the above quantity to the right hand side of the scheme (2.17):

$$C_{k}^{n+1} = C_{k}^{n} - \frac{\Delta t}{\Delta x} (q_{x \mid \gamma_{kk+1}} \phi_{\gamma_{kk+1}} (C^{n}, \mathbf{q}) - q_{x \mid \gamma_{kk-1}} \phi_{\gamma_{kk-1}} (C^{n}, \mathbf{q}))$$

$$- \frac{\Delta t}{\Delta y} (q_{y \mid \gamma_{kk+N_{x}}} \phi_{\gamma_{kk+N_{x}}} (C^{n}, \mathbf{q}) - q_{y \mid \gamma_{kk-N_{x}}} \phi_{\gamma_{kk-N_{x}}} (C^{n}, \mathbf{q}))$$

$$+ \frac{\Delta t}{|\mathcal{C}_{k}|} \sum_{l \in \mathcal{N}_{k}} |\gamma_{kl}| D \overrightarrow{\nabla} C_{|\gamma_{kl}} \cdot \mathbf{n}_{|\gamma_{kl}}$$

$$(2.19)$$

To compute the diffusion coefficients between two cells, we chose the harmonic mean as we did for the permeability matrix in previous lines.

#### 2.4.2 Modified equation and error behavior

From now on, we try to get an insight on the error induced by the upwind scheme. First we write the corresponding modified equation in the case where there is no diffusion. This modified equation is solved with a better accuracy by the studied scheme than the original equation. The terms appearing in the new expression will inform us on the behavior of the error, as shown below:

error behavior

$$\partial_t C + \frac{\Delta t}{2} \partial_{tt}^2 C + \nabla \cdot (\mathbf{q}C) - \frac{\Delta x}{2} \partial_{xx}^2 (q_x C) - \frac{\Delta y}{2} \partial_{yy}^2 (q_y C) = 0$$

$$\Longrightarrow \partial_t C + \nabla \cdot (\mathbf{q}C) = -\frac{\Delta t}{2} \partial_{tt}^2 C + \frac{\Delta x}{2} \partial_{xx}^2 (q_x C) + \frac{\Delta y}{2} \partial_{yy}^2 (q_y C)$$

If we suppose that **q** does not depend on the position, we get:

$$\begin{split} \partial_{tt}^2 C + q_x \partial_{tx}^2 C + q_y \partial_{ty}^2 C &= -\frac{\Delta t}{2} \partial_{ttt}^3 C + q_x \frac{\Delta x}{2} \partial_{txx}^3 C + q_y \frac{\Delta y}{2} \partial_{tyy}^3 C \\ q_x \partial_{xt}^2 C + q_x^2 \partial_{xx}^2 C + q_x q_y \partial_{xy}^2 C &= -q_x \frac{\Delta t}{2} \partial_{xtt}^3 C + q_x^2 \frac{\Delta x}{2} \partial_{xxx}^3 C + q_x q_y \frac{\Delta y}{2} \partial_{xyy}^3 C \\ q_y \partial_{yt}^2 C + q_x q_y \partial_{yx}^2 C + q_y^2 \partial_{yy}^2 C &= -q_y \frac{\Delta t}{2} \partial_{ytt}^3 C + q_x q_y \frac{\Delta x}{2} \partial_{yxx}^3 C + q_y^2 \frac{\Delta y}{2} \partial_{yyy}^3 C \end{split}$$

By subtracting the second and third lines to the first one we find:

$$\partial_{tt}^{2}C = q_{x}^{2}\partial_{xx}^{2}C + 2q_{x}q_{y}\partial_{xy}^{2}C + q_{y}^{2}\partial_{yy}^{2}C + \mathcal{O}(\Delta t, \Delta x, \Delta y)$$

Substituting  $\partial_{tt}^2 C$  in the modified equation holds:

$$\partial_t C + \nabla \cdot (\mathbf{q}C) = -\frac{\Delta t}{2} (q_x^2 \partial_{xx}^2 C + 2q_x q_y \partial_{xy}^2 C + q_y^2 \partial_{yy}^2 C) + q_x \frac{\Delta x}{2} \partial_{xx}^2 C + q_y \frac{\Delta y}{2} \partial_{yy}^2 C + \mathcal{O}(\Delta t^2, \Delta t \Delta x, \Delta t \Delta y)$$

$$\partial_t C + \nabla \cdot (\mathbf{q}C) = (\Delta x - q_x \Delta t) \frac{q_x}{2} \partial_{xx}^2 C + (\Delta y - q_y \Delta t) \frac{q_y}{2} \partial_{yy}^2 C - q_x q_y \Delta t \partial_{xy}^2 C + \mathcal{O}(\Delta t^2, \Delta t \Delta x, \Delta t \Delta y)$$
 (2.20)

In the above equation, the first two right terms are diffusive ones only if their respective coefficients are positive, meaning that if  $\Delta t \leq \min\left(\frac{\Delta x}{|q_x|},\frac{\Delta y}{|q_y|}\right)$  the scheme will effectively diffuse the concentration through the domain. If in the contrary  $\Delta t > \min\left(\frac{\Delta x}{|q_x|},\frac{\Delta y}{|q_y|}\right)$ , the solution will condense toward its center prior to the direction in which the last inequality is realized.

isotropic term

The third term can be interpreted as an-isotropic diffusion in the direction normal to the flow, and anti-diffusion in the direction of the flow . Since  $\Delta t > 0$ , this term never disappears, and its impact can be seen through the elongated shape of the concentration perpendicularly to the velocity, and flattened in the velocity direction (see fig. 2.4).

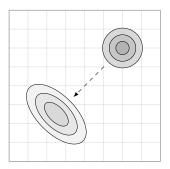


Figure 2.4: An-isotropic diffusion

This behavior has been reproduced in practice through a MATLAB program. The figures 2.5 below show how the trade-off between an-isotropic diffusion and isotropic diffusion is influenced by the step of time  $\Delta t$ . The first picture gives the initial condition at  $t=t_0$ . The next pictures correspond to the same state  $t=t_1$  but for different values of  $\Delta t$ : from left to right  $\Delta t$  is being multiplied by a factor 3/2, so that the time step in the last picture is nearly five times bigger than for the picture number 2.

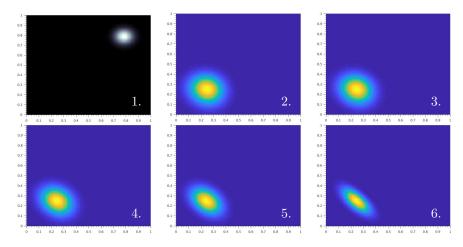


Figure 2.5: Comparison of diffusion phenomena for different values of  $\Delta t$ 

We see that in all cases diffusion occurs, but the an-isotropic contribution is greater for bigger values of  $\Delta t$ , as we could have expected it from equation (2.20). Running this simulation for a greater  $\Delta t$  than the one of the last picture would have led to instability, meaning a large deviation from the exact solution. In the next section we seek a condition under which the upwind scheme is stable.

#### 2.4.3 Von Neumann analysis and the CFL condition

Let suppose that the solution takes the form  $C_k^n = \phi_n e^{i(l\Delta x + m\Delta y)}$ , with l, m two integers verifying  $k = l + (m-1)N_x$ . We are looking for a condition that will ensure us the stability of the scheme. This is the case whenever the modulus of  $C_k^n$  decreases as n increases, so the condition  $|\phi_{n+1}| < |\phi_n|$  is satisfying. We split our problem in two parts: first we will get such a condition only considering the advection, and then only by considering the diffusion. Injecting the new form of  $C_k^n$  in (2.17) leads to:

$$\begin{split} \frac{\phi_{n+1} - \phi_n}{\Delta t} e^{i(l\Delta x + m\Delta y)} \\ &= + \frac{\phi_n}{\Delta x} e^{im\Delta y} \Big[ \quad |q_x|_{\gamma_{kk+1}}| (-e^{il\Delta x} \mathbbm{1}_{q_x > 0} + e^{i(l+1)\Delta x} \mathbbm{1}_{q_x \le 0}) \\ & \quad + |q_x|_{\gamma_{kk-1}}| (e^{i(l-1)\Delta x} \mathbbm{1}_{q_x > 0} - e^{il\Delta x} \mathbbm{1}_{q_x \le 0}) \Big] \\ & \quad + \frac{\phi_n}{\Delta y} e^{il\Delta x} \Big[ \quad |q_y|_{\gamma_{kk+N_x}}| (-e^{im\Delta y} \mathbbm{1}_{q_y > 0} + e^{i(m+1)\Delta y} \mathbbm{1}_{q_y \le 0}) \\ & \quad + |q_y|_{\gamma_{kk-N_x}}| (e^{i(m-1)\Delta y} \mathbbm{1}_{q_y > 0} - e^{im\Delta y} \mathbbm{1}_{q_y \le 0}) \Big] \end{split}$$

Multiplying both sides by  $\Delta t/e^{i(l\Delta x + m\Delta y)}$  we find:

$$\begin{split} \phi_{n+1} &= \phi_n \left[ 1 + \frac{\Delta t}{\Delta x} \, |q_x|_{\gamma_{kk+1}} | (-\mathbbm{1}_{q_x > 0} + e^{i\Delta x} \mathbbm{1}_{q_x \le 0}) \right. \\ &\quad + \frac{\Delta t}{\Delta x} \, |q_x|_{\gamma_{kk-1}} | (e^{-i\Delta x} \mathbbm{1}_{q_x > 0} - \mathbbm{1}_{q_x \le 0}) \\ &\quad + \frac{\Delta t}{\Delta y} \, |q_y|_{\gamma_{kk+N_x}} | (-\mathbbm{1}_{q_y > 0} + e^{i\Delta y} \mathbbm{1}_{q_y \le 0}) \\ &\quad + \frac{\Delta t}{\Delta y} \, |q_y|_{\gamma_{kk-N_x}} | (e^{-i\Delta y} \mathbbm{1}_{q_y > 0} - \mathbbm{1}_{q_y \le 0}) \right] \end{split}$$

As in the previous section, we make the assumption that  $\mathbf{q}$  does not depend on the position. To further simplify the problem we shall suppose that  $q_x, q_y > 0$  with no loss of generality. We then express the amplification factor A as in [3]:

$$A = \frac{\phi_{n+1}}{\phi_n} = \alpha + i\beta, \quad \text{with } \left\{ \begin{array}{l} \alpha = 1 - Z_x(1 - \cos(\Delta x)) - Z_y(1 - \cos(\Delta y)) \\ \beta = -Z_x\sin(\Delta x) - Z_y\sin(\Delta y) \\ Z_x = q_x\frac{\Delta t}{\Delta x}, \ Z_y = q_y\frac{\Delta t}{\Delta y} \end{array} \right.$$

If  $Z_x + Z_y > 1$ , we can find values of  $\Delta x$  and  $\Delta y$  for which the magnitude of A is strictly greater than 1, meaning that the scheme is unstable. We can for instance take  $0 < \Delta x = \Delta y \le 1$  and  $\Delta t$  great enough so that  $Z_x + Z_y > 1$ :

$$A = (1 - (Z_x + Z_y)(1 - \cos(\Delta x))) - i(Z_x + Z_y)\sin(\Delta x)$$

$$\implies |A|^2 = 1 - 2(Z_x + Z_y)(1 - \cos(\Delta x)) + (Z_x + Z_y)^2(1 - \cos(\Delta x))^2$$

$$+ (Z_x + Z_y)^2\sin^2(\Delta x)$$

$$= 1 - 2(Z_x + Z_y)(1 - \cos(\Delta x)) + 2(Z_x + Z_y)^2 - 2(Z_x + Z_y)^2\cos(\Delta x)$$

$$> 1 - 2(Z_x + Z_y)^2(1 - \cos(\Delta x)) + 2(Z_x + Z_y)^2 - 2(Z_x + Z_y)^2\cos(\Delta x)$$

$$> 1$$

If in the contrary  $Z_x + Z_y \le 1$  we prove that the scheme is stable. Noting  $\mathbf{e}_x$ ,  $\mathbf{e}_y$  and  $\mathbf{x}$  the vectors defined as:

$$\mathbf{e}_{x} = \begin{pmatrix} \cos(\Delta x) \\ -\sin(\Delta x) \end{pmatrix}, \quad \mathbf{e}_{y} = \begin{pmatrix} \cos(\Delta y) \\ -\sin(\Delta y) \end{pmatrix}$$
$$\mathbf{x} = \begin{pmatrix} \alpha \\ \beta \end{pmatrix} = Z_{x}\mathbf{e}_{x} + Z_{y}\mathbf{e}_{y} + \begin{pmatrix} 1 - Z_{x} - Z_{y} \\ 0 \end{pmatrix}$$

we can write the magnitude of A:

$$|A| = ||\mathbf{x}|| \le Z_x + Z_y + |1 - Z_x - Z_y| = 1$$

Finally we obtain the scheme stability under the Courant–Friedrichs–Lewy condition (CFL):

$$\Delta t \le \frac{\Delta x \Delta y}{\Delta y \max|q_x| + \Delta x \max|q_y|} \tag{2.21}$$

One can easily verify that this inequality is more restrictive than the previous condition (2.18) inherent to the flux-scheme, and assures us the isotropic diffusion established with the modified equation (2.20).

Now that we know a sufficient condition to have a stable scheme in an advection setting, we search a similar condition for a purely diffusive problem. We start from scheme (2.19) with all flux terms set to zero:

$$\begin{split} &\frac{|\mathcal{C}_{k}|}{\Delta t}(\phi_{n+1}-\phi_{n})e^{i(l\Delta x+m\Delta y)} = \sum_{s\in\mathcal{N}_{k}}|\gamma_{ks}|D\overrightarrow{\nabla}C_{|\gamma_{ks}}\cdot\mathbf{n}_{|\gamma_{ks}} \\ &= -\Delta x \Big(D_{21}\frac{C_{k+1}^{n}+C_{k+1-N_{x}}^{n}-C_{k-1}^{n}-C_{k-1-N_{x}}^{n}}{4\Delta x} + D_{22}\frac{C_{k}^{n}-C_{k-1}^{n}}{\Delta y}\Big) \\ &+ \Delta y \Big(D_{11}\frac{C_{k+1}^{n}-C_{k}^{n}}{\Delta x} + D_{12}\frac{C_{k+N_{x}}^{n}+C_{k+1+N_{x}}^{n}-C_{k-N_{x}}^{n}-C_{k+1-N_{x}}^{n}}{4\Delta y}\Big) \\ &+ \Delta x \Big(D_{21}\frac{C_{k+1}^{n}+C_{k+1+N_{x}}^{n}-C_{k-1}^{n}-C_{k-1+N_{x}}^{n}+D_{22}\frac{C_{k+N_{x}}^{n}-C_{k}^{n}}{\Delta y}\Big) \\ &- \Delta y \Big(D_{11}\frac{C_{k}^{n}-C_{k-1}^{n}}{\Delta x} + D_{12}\frac{C_{k+N_{x}}^{n}+C_{k-1+N_{x}}^{n}-C_{k-N_{x}}^{n}-C_{k-1-N_{x}}^{n}}{4\Delta y}\Big) \\ &= \frac{D_{12}+D_{21}}{4}(C_{k+1+N_{x}}^{n}+C_{k-1-N_{x}}^{n}-C_{k-1+N_{x}}^{n}-C_{k+1-N_{x}}) \\ &+ D_{22}\Delta x \frac{C_{k+N_{x}}^{n}-2C_{k}^{n}+C_{k-N_{x}}^{n}}{\Delta y} + D_{11}\Delta y \frac{C_{k+1}^{n}-2C_{k}^{n}+C_{k-1}^{n}}{\Delta x} \end{split}$$

Dividing by  $e^{i(l\Delta x + m\Delta y)}$  and factorizing by  $\phi_n$  leads to:

$$\begin{split} \phi_{n+1} - \phi_n \\ &= \frac{\Delta t}{\Delta x \Delta y} \, \phi_n \Big[ D_{11} \frac{\Delta y}{\Delta x} (e^{i\Delta x} + e^{-i\Delta x} - 2) + D_{22} \frac{\Delta x}{\Delta y} (e^{i\Delta y} + e^{-i\Delta y} - 2) \\ &\quad + \frac{D_{12} + D_{21}}{4} (e^{i(\Delta x + \Delta y)} + e^{-i(\Delta x + \Delta y)}) \\ &\quad - \frac{D_{12} + D_{21}}{4} (e^{i(-\Delta x + \Delta y)} + e^{i(\Delta x - \Delta y)}) \Big] \\ \phi_{n+1} &= \phi_n \Big[ 1 + 2D_{11} \frac{\Delta t}{\Delta x^2} (\cos \Delta x - 1) + 2D_{22} \frac{\Delta t}{\Delta y^2} (\cos \Delta y - 1) \end{split}$$

2.5 Numerical results

+ 
$$\frac{\Delta t}{2\Delta x \Delta y}$$
 $(D_{12} + D_{21})(\cos(\Delta x + \Delta y) - \cos(\Delta x - \Delta y))$ 

By denoting  $A = \phi_{n+1}/\phi_n$  the amplification factor, we are searching the conditions under which  $|A| \leq 1$ :

$$-2 \le \left\{ \begin{array}{l} 2D_{11} \frac{\Delta t}{\Delta x^2} (\cos \Delta x - 1) + 2D_{22} \frac{\Delta t}{\Delta y^2} (\cos \Delta y - 1) \\ -\frac{\Delta t}{\Delta x \Delta y} (D_{12} + D_{21}) \sin \Delta x \sin \Delta y \end{array} \right\} \le 0$$

If  $D_{12} = D_{21} = 0$  we simply have:

$$-1 \le D_{11} \frac{\Delta t}{\Delta x^2} (\cos \Delta x - 1) + D_{22} \frac{\Delta t}{\Delta y^2} (\cos \Delta y - 1)$$

A sufficient condition to satisfy this inequality is to chose  $\Delta t$  such that:

$$2\Delta t \left(\frac{D_{11}}{\Delta x^2} + \frac{D_{22}}{\Delta y^2}\right) \le 1 \Longleftrightarrow \Delta t \le \frac{\Delta x^2 \Delta y^2}{2D_{11}\Delta y^2 + 2D_{22}\Delta x^2} \tag{2.22}$$

Finally, in order to guarantee the stability of the scheme disregarding the nature of the transport we can chose:

$$\Delta t = \frac{\alpha}{2} \min \left( \frac{\Delta x \Delta y}{\Delta y \max |q_x| + \Delta x \max |q_y|}, \; \frac{\Delta x^2 \Delta y^2}{2D_{11} \Delta y^2 + 2D_{22} \Delta x^2} \right), \quad \alpha \in [0, 1]$$

#### 2.5 Numerical results

In this section we will be presenting the results obtained with a MATLAB program implementing the numerical schemes discussed in previous pages. This linear solver allows to compute both advection and diffusion phenomena combined together. It also handles heterogeneous media in the sense where one can specify the permeability and diffusion matrix for given areas of the domain. In order to offer better performances, the solver has been optimized thanks to *vectorization*, which is the process of revising loop-based, scalar-oriented code to use MATLAB matrix and vector operations instead. A useful tool for assessing critical parts of the code in terms of efficiency is the MATLAB *profiler*, and has been of great help to optimize this solver.

First we take a look at the convergence rate of the diamond scheme. For this purpose we define the pressure  $h_{\text{exact}}(x,y) = 1 + \frac{1}{4}(x^3 + y^4)$ , the permeability  $K = 2 I_2$  and we search  $f_1$  such that:

$$-\nabla \cdot (K\overrightarrow{\nabla}h_{\text{exact}}) = f_1(x,y) \Longrightarrow f_1(x,y) = -\nabla \cdot \left(\frac{3}{2}x^2 + 2y^3\right) = -3x - 6y^2$$

Then we approximate the pressure  $h_{\text{exact}}$  using the diamond scheme, and we calculate the  $L^{\infty}$ -error on the domain  $[-0.2, 1] \times [0, 1]$ . Doing so for different mesh sizes, we get the curve 2.6. We find a second order convergence as expected.

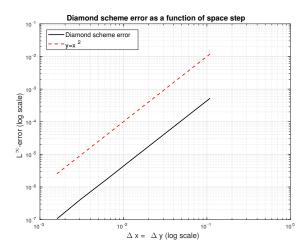
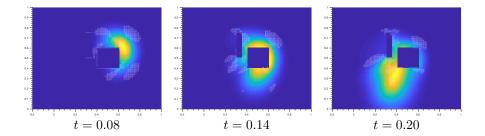


Figure 2.6: Diamond scheme  $L^{\infty}\text{-error}$ 

We give the outcome of a computation for a more complex case (diffusion plus two sub-domains playing the role of obstacles):



## Appendix A

## Properties of the diamond scheme

#### A.1 Existence and uniqueness of the solution

In order to prove the existence and uniqueness of the solution for the diamond scheme with a constant permeability matrix K, we introduce two discrete derivation operators d and  $\mathbf{g}$ , which respectively correspond to discretized vertions of the divergence and the gradient:

$$(\mathbf{g}h)_{k+1/2} = \begin{pmatrix} (h_{k+1} - h_k)/\Delta x \\ (h_k^+ - h_k^-)/\Delta y \end{pmatrix}, \quad (\mathbf{g}h)_{k+N_x/2} = \begin{pmatrix} (h_k^+ - h_{k-1}^+)/\Delta x \\ (h_{k+N_x} - h_k)/\Delta y \end{pmatrix}$$
 (A.1)

$$(\mathbf{d}\mathbf{w})_{k} = \frac{w_{k+1/2}^{1} - w_{k-1/2}^{1}}{\Delta x} + \frac{w_{k+N_{x}/2}^{2} - w_{k-N_{x}/2}^{2}}{\Delta y} \quad \forall \mathbf{w} = \begin{pmatrix} w^{1} \\ w^{2} \end{pmatrix}$$
(A.2)

Using these operators we write for a given non-border cell  $C_k$ :

$$(d(K\mathbf{g}h))_{k} = K_{11} \frac{(\mathbf{g}h)_{k+1/2}^{1} - (\mathbf{g}h)_{k-1/2}^{1}}{\Delta x} + K_{12} \frac{(\mathbf{g}h)_{k+1/2}^{2} - (\mathbf{g}h)_{k-1/2}^{2}}{\Delta x} + K_{21} \frac{(\mathbf{g}h)_{k+N_{x}/2}^{1} - (\mathbf{g}h)_{k-N_{x}/2}^{1}}{\Delta y} + K_{22} \frac{(\mathbf{g}h)_{k+N_{x}/2}^{2} - (\mathbf{g}h)_{k-N_{x}/2}^{2}}{\Delta y}$$

Multiplying by the squared surface of  $C_k$  we find:

$$|\mathcal{C}_{k}|^{2}(\mathrm{d}(K\mathbf{g}h))_{k} = K_{11}\Delta y^{2}(h_{k+1} - 2h_{k} + h_{k-1}) + K_{12}\Delta x \Delta y \left( (h_{k}^{+} - h_{k}^{-}) - (h_{k-1}^{+} - h_{k-1}^{-}) \right) + K_{21}\Delta x \Delta y \left( (h_{k}^{+} - h_{k-1}^{+}) - (h_{k}^{-} - h_{k-1}^{-}) \right) + K_{22}\Delta x^{2}(h_{k+N_{x}} - 2h_{k} + h_{k-N_{x}})$$
(A.3)

By comparing the right term of (A.3) with equation (2.11) we can deduce the following equality:

$$|\mathcal{C}_k|^2 (\mathrm{d}(K\mathbf{g}h))_k = -2|\mathcal{C}_k|^2 f_{1,\mathcal{C}_k} \Longrightarrow (\mathrm{d}(K\mathbf{g}h))_k = -f_{1,\mathcal{C}_k}$$
(A.4)

with  $f_{1,\mathcal{C}_k} = \frac{1}{|\mathcal{C}_k|} \int_{\mathcal{C}_k} f_1 dx$ .

18

It is interesting to draw the parallel between the discrete pressure equation and the continuous one:

Continuous equation (1.1a)	Discrete equation (A.4)
$-\nabla \cdot (K\overrightarrow{\nabla}h) = f_1$	$-(\mathrm{d}(K\mathbf{g}h))_k = f_{1,\mathcal{C}_k}  \forall \mathcal{C}_k \text{ non-border cell}$

Proving the existence and uniqueness of the solution of (2.12) with Dirichlet conditions is equivalent to prove these properties for the new problem:

$$\begin{cases} -(\mathrm{d}(K\mathbf{g}h))_k = f_{1,\mathcal{C}_k} & \forall k \text{ such that } \mathcal{C}_k \text{ is not a border cell} \\ h_k = \sigma_k \text{ with } \sigma_k \text{ known} & \forall k \text{ such that } \mathcal{C}_k \text{ is a border cell} \end{cases}$$
(A.5)

discrete scalar products

For this purpose we then introduce two discrete scalar products on the truncated mesh denoted  $\mathcal{T}$ :

$$\langle u, v \rangle_{\mathcal{C}} = \sum_{\mathcal{C}_i \text{ non-border cell}} |\mathcal{C}_i| u_i v_i$$
 (A.6)

$$\langle \mathbf{u}, \mathbf{v} \rangle_{\mathcal{D}} = \sum_{\mathcal{C}_i \text{ non-border cell}} \left( \sum_{k \in \mathcal{N}_i} |\mathcal{D}_{ik}| \mathbf{u}_{|\mathcal{D}_{ik}} \cdot \mathbf{v}_{|\mathcal{D}_{ik}} \right)$$
(A.7)

discrete Green formula

We can show the discrete Green formula:

$$\langle d\mathbf{u}, v \rangle_{\mathcal{C}} = -\langle \mathbf{u}, \mathbf{g}v \rangle_{\mathcal{D}} + \beta \sum_{\mathcal{C}_i \text{ border cell}} v_i \mathbf{u}_i \cdot \mathbf{n}_i$$
 (A.8)

with  $\beta \in \mathbb{R}$  a constant that can be determined by calculation, and  $\mathbf{n}_i$  the normal unit vector of the domain border at the level of cell  $\mathcal{C}_i$  if  $\mathcal{C}_i$  is not a corner, and the sum of the two corresponding normal unit vector at the level of  $\mathcal{C}_i$  if it is a corner.

variational formulation

If in the problem (A.5) we have  $f_{1,C_k} = 0$  for all non border cell  $C_k$  and  $\sigma_i = 0$  for all border cell  $C_i$ , we necessarily have:

$$\forall (\omega_i)_i, -\langle d(K\mathbf{g}h), \omega \rangle_{\mathcal{C}} = 0 \iff \langle K\mathbf{g}h, \mathbf{g}\omega \rangle_{\mathcal{D}} = 0$$

Choosing  $\omega = h$  and assuming that K is positive-definite for the usual scalar product we get:

$$\langle K\mathbf{g}h, \mathbf{g}h \rangle_{\mathcal{D}} = 0 \Longleftrightarrow (\mathbf{g}h)_{k\pm 1/2} = (\mathbf{g}h)_{k\pm N_r/2} = 0_{\mathbb{R}^2}$$
 for all non-border cell  $\mathcal{C}_k$ 

Since the Dirichlet conditions are homogeneous, we conclude that  $h_k = 0$  for all index k. Therefore if the solution exists it is unique as soon as K is positive-definite. Because the system (A.5) is linear, the uniqueness of the solution is equivalent to its existence for all second member  $f_1$ .

Finally we have proved that if K is positive-definite, there is existence and uniqueness of the solution of (2.12) with Dirichlet conditions, and thus the rigidity matrix R is nonsingular.

## A.2 An optimality argument for the interface harmonic mean

In previous sections, we stated that permeability and diffusion matrix would be evaluated on cells' interfaces by taking the harmonic mean at the level of the two

neighbors cells. For instance, on the border  $\gamma_{kl}$  we would compute the permeability coefficient  $K_{ij}$  and diffusion coefficient  $D_{ij}$  as below:

$$K_{ij}^{\gamma_{kl}} = 2 \; \frac{K_{ij}^{\mathcal{C}_k} K_{ij}^{\mathcal{C}_l}}{K_{ij}^{\mathcal{C}_k} + K_{ij}^{\mathcal{C}_l}}, \qquad D_{ij}^{\gamma_{kl}} = 2 \; \frac{D_{ij}^{\mathcal{C}_k} D_{ij}^{\mathcal{C}_l}}{D_{ij}^{\mathcal{C}_k} + D_{ij}^{\mathcal{C}_l}}$$

Chosing these values is indeed optimal in the sense where it respects the principle of flux conservation, central in finite volume: the concentration leaving a cell enters a new one. We shall prove it for the permeability matrix, and we restrain to the simplified case where K is diagonal. Recalling the assumption under which the pressure gradient is constant over every diamond cell  $\mathcal{D}_{kl}$  — and thus on every interface  $\gamma_{kl}$  — we can write:

$$\int_{\gamma_{kl}} -K \overrightarrow{\nabla} h \cdot \mathbf{n}_{\gamma_{kl}} d\sigma = |\gamma_{kl}| K_{rr}^{\gamma_{kl}} \left( \frac{h_k - h_l}{\operatorname{dist}(\mathcal{C}_k, \mathcal{C}_l)} \right), \quad r = \begin{cases} 1 \text{ if } \gamma_{kl} \text{ is vertical} \\ 2 \text{ if } \gamma_{kl} \text{ is horizontal} \end{cases}$$
 with  $\operatorname{dist}(\mathcal{C}_k, \mathcal{C}_l)$  the distance between the centers of  $\mathcal{C}_k, \mathcal{C}_l$ 

However the principle of flow concervation allows to write:

$$\int_{\gamma_{kl}} -K \overrightarrow{\nabla} h \cdot \mathbf{n}_{\gamma_{kl}} d\sigma = |\gamma_{kl}| K_{rr}^{\mathcal{C}_k} \left( \frac{h_k - h_{|\gamma_{kl}}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} \right) = |\gamma_{kl}| K_{rr}^{\mathcal{C}_l} \left( \frac{h_{|\gamma_{kl}} - h_l}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} \right)$$

$$\Longrightarrow K_{rr}^{\mathcal{C}_k} \left( \frac{h_k - h_{|\gamma_{kl}}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} \right) = K_{rr}^{\mathcal{C}_l} \left( \frac{h_{|\gamma_{kl}} - h_l}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} \right)$$

$$\Longrightarrow \left( \frac{K_{rr}^{\mathcal{C}_k}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} + \frac{K_{rr}^{\mathcal{C}_l}}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} \right) h_{|\gamma_{kl}} = \frac{K_{rr}^{\mathcal{C}_k}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} h_k + \frac{K_{rr}^{\mathcal{C}_l}}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} h_l$$

$$\Longrightarrow h_{|\gamma_{kl}} = \left( \frac{K_{rr}^{\mathcal{C}_k}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} + \frac{K_{rr}^{\mathcal{C}_l}}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} \right)^{-1} \left( \frac{K_{rr}^{\mathcal{C}_k}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} h_k + \frac{K_{rr}^{\mathcal{C}_l}}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} h_l \right)$$

We re-inject this result in the flux expression:

$$\begin{split} \int_{\gamma_{kl}} -K \overrightarrow{\nabla} h \cdot \mathbf{n}_{\gamma_{kl}} \, d\sigma &= |\gamma_{kl}| K_{rr}^{\mathcal{C}_k} \left( \frac{h_k - h_{|\gamma_{kl}}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} \right) \\ &= |\gamma_{kl}| \frac{K_{rr}^{\mathcal{C}_k}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} \left[ h_k \right. \\ &- \left( \frac{K_{rr}^{\mathcal{C}_k}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} + \frac{K_{rr}^{\mathcal{C}_l}}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} \right)^{-1} \left( \frac{K_{rr}^{\mathcal{C}^k}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} h_k + \frac{K_{rr}^{\mathcal{C}^l}}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} h_l \right) \right] \\ &= |\gamma_{kl}| \frac{K_{rr}^{\mathcal{C}_k}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} \left( \frac{K_{rr}^{\mathcal{C}_k}}{\operatorname{dist}(\mathcal{C}_k, \gamma_{kl})} + \frac{K_{rr}^{\mathcal{C}_l}}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} \right)^{-1} \times \\ &\times \left( \frac{K_{rr}^{\mathcal{C}_l}}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} h_k - \frac{K_{rr}^{\mathcal{C}_l}}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} h_l \right) \\ &= |\gamma_{kl}| \frac{K_{rr}^{\mathcal{C}_k}/\operatorname{dist}(\mathcal{C}_k, \gamma_{kl}) \times K_{rr}^{\mathcal{C}_l}/\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})}{K_{rr}^{\mathcal{C}_k}/\operatorname{dist}(\mathcal{C}_k, \gamma_{kl}) + K_{rr}^{\mathcal{C}_l}/\operatorname{dist}(\mathcal{C}_l, \gamma_{kl})} (h_k - h_l) \\ &= |\gamma_{kl}| \frac{K_{rr}^{\mathcal{C}_k}/\operatorname{dist}(\mathcal{C}_k, \gamma_{kl}) \times K_{rr}^{\mathcal{C}_l}/\operatorname{dist}(\mathcal{C}_k, \gamma_{kl}) K_{rr}^{\mathcal{C}_l}}{\operatorname{dist}(\mathcal{C}_l, \gamma_{kl}) K_{rr}^{\mathcal{C}_l}} \left( \frac{h_k - h_l}{\operatorname{dist}(\mathcal{C}_k, \mathcal{C}_l)} \right) \\ &= 2|\gamma_{kl}| \frac{K_{rr}^{\mathcal{C}_k}K_{rr}^{\mathcal{C}_l}}{K_{rr}^{\mathcal{C}_k} + K_{rr}^{\mathcal{C}_l}} \left( \frac{h_k - h_l}{\operatorname{dist}(\mathcal{C}_k, \mathcal{C}_l)} \right) \\ &\text{because in our case dist}(\mathcal{C}_k, \gamma_{kl}) = \operatorname{dist}(\mathcal{C}_l, \gamma_{kl}) = \frac{1}{2} \operatorname{dist}(\mathcal{C}_k, \mathcal{C}_l) \end{split}$$

Finally we identify these terms with the permeability  $K_{rr}^{\gamma_{kl}}$ :

$$\int_{\gamma_{kl}} -K \overrightarrow{\nabla} h \cdot \mathbf{n}_{\gamma_{kl}} d\sigma = |\gamma_{kl}| K_{rr}^{\gamma_{kl}} \left( \frac{h_k - h_l}{\operatorname{dist}(\mathcal{C}_k, \mathcal{C}_l)} \right)$$

$$= 2|\gamma_{kl}| \frac{K_{rr}^{\mathcal{C}_k} K_{rr}^{\mathcal{C}_l}}{K_{rr}^{\mathcal{C}_k} + K_{rr}^{\mathcal{C}_l}} \left( \frac{h_k - h_l}{\operatorname{dist}(\mathcal{C}_k, \mathcal{C}_l)} \right)$$

$$\Longrightarrow K_{rr}^{\gamma_{kl}} = 2 \frac{K_{rr}^{\mathcal{C}_k} K_{rr}^{\mathcal{C}_l}}{K_{rr}^{\mathcal{C}_k} + K_{rr}^{\mathcal{C}_l}}$$

We just proved that respecting the principle of flow conservation was leading us to approximate K over the interfaces by taking their harmonic mean.

M. Bruliard & M. Rigal, Numerical Solution of the Advection-Diffusion Equation coupled with Darcy's law, 2018, Sup'Galilée

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