Prinzipien der komplexen FM-Synthese

Matthias Kemmer

Gliederung

- Parallelschaltung
- Kaskadenschaltung
- Feedbackschaltung
- Native Instruments' FM8

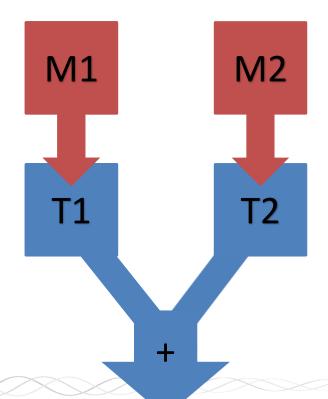
Parallelschaltung

2 Träger, **jeweils eigener** Modulator

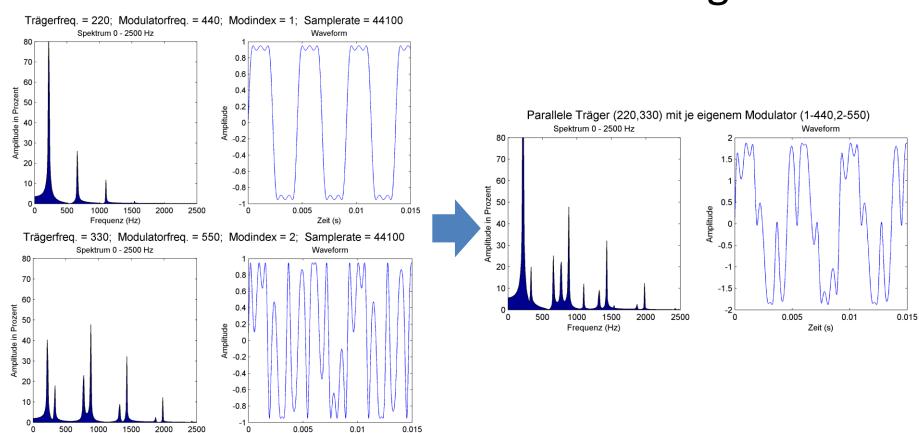
Pro Träger-Modulator-Paar gilt:

$$\sin(w_c t + I\sin(w_m t))$$

$$= \sum_{n=-\infty}^{\infty} J_n(I)\sin(w_c t + nw_m t)$$



Einzel- vs. Parallelschaltung



500

1000

Frequenz (Hz)

1500

2000

2500

0.005

Zeit (s)

0.01

0.015

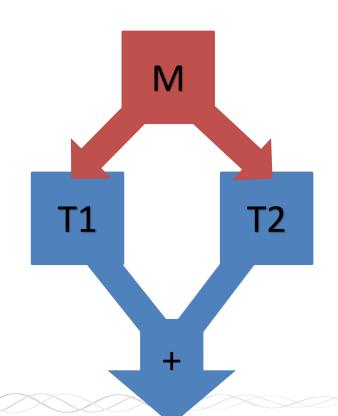
Parallelschaltung

2 Träger, selber Modulator

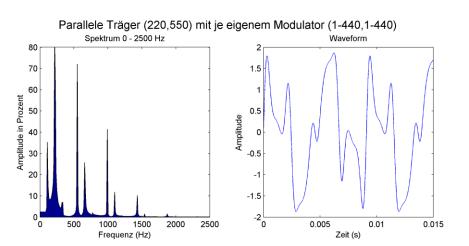
Pro Träger-Modulator-Paar gilt:

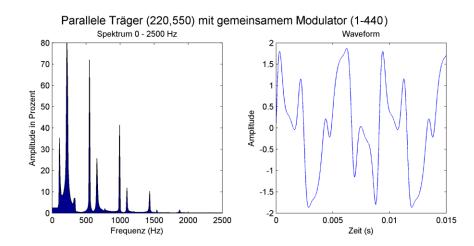
$$\sin(w_c t + I\sin(w_m t))$$

$$=\sum_{n=-\infty}^{\infty} J_n(I)\sin(w_c t + nw_m t)$$



2 Träger mit 2 Modulatoren mit gleichen Einstellungen vs. 2 Träger mit demselben Modulator





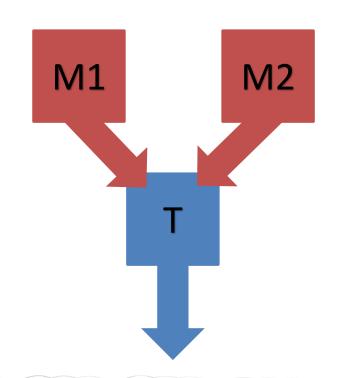
Parallelschaltung

1 Träger,

2 unabhängige Modulatoren

$$f_{FMparallel}(t) = \sin(w_c t + I_1 \sin(w_{m1}t) + I_2 \sin(w_{m2}t))$$

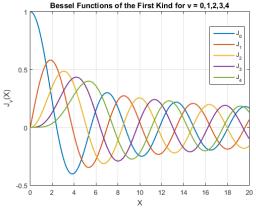
$$= \sum_{i=-\infty}^{\infty} \sum_{k=-\infty}^{\infty} J_i(I_1) J_k(I_2) \sin(w_c t + i w_{m1} t + k w_{m2} t)$$



Additionsterme der Seitenbänder bei 2 parallelen Modulatoren

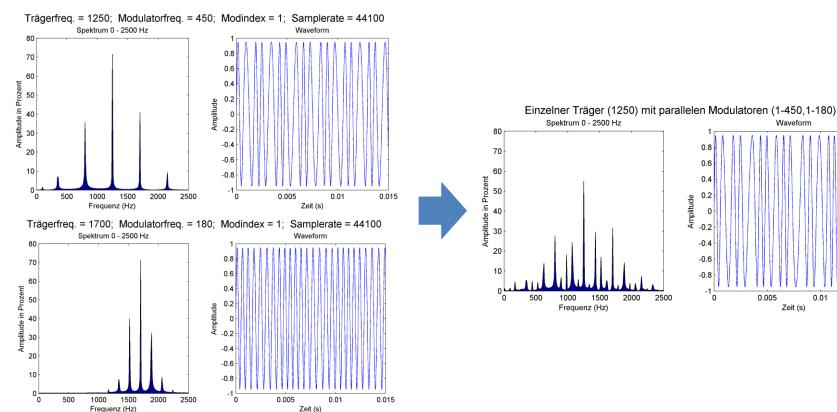
```
\sin(w_c t + I_1 \sin(w_{m1} t) + I_2 \sin(w_{m2} t))
 = J_0(I_1)J_0(I_2)\sin(w_c t)
 + J_0(I_1)J_1(I_2)\sin(w_ct + w_{m2}t) - J_0(I_1)J_1(I_2)\sin(w_ct - w_{m2}t)
 + J_0(I_1)J_2(I_2)\sin(w_ct + 2w_{m2}t) + J_0(I_1)J_1(I_2)\sin(w_ct - 2w_{m2}t)
 + J_1(I_1)J_0(I_2)\sin(w_ct + w_{m1}t) - J_1(I_1)J_0(I_2)\sin(w_ct - w_{m1}t)
+ J_1(I_1)J_1(I_2)\sin(w_ct + w_{m1}t + w_{m2}t) - J_1(I_1)J_1(I_2)\sin(w_ct + w_{m1}t - w_{m2}t)
 -J_1(I_1)J_1(I_2)\sin(w_ct-w_{m1}t+w_{m2}t)+J_1(I_1)J_1(I_2)\sin(w_ct-w_{m1}t-w_{m2}t)
 + J_1(I_1)J_2(I_2)\sin(w_ct + w_{m1}t + 2w_{m2}t) + J_1(I_1)J_2(I_2)\sin(w_ct + w_{m1}t - 2w_{m2}t)
 -J_1(I_1)J_2(I_2)\sin(w_ct-w_{m1}t+2w_{m2}t)-J_1(I_1)J_2(I_2)\sin(w_ct-w_{m1}t-2w_{m2}t)
 + J_2(I_1)J_0(I_2)\sin(w_ct + 2w_{m1}t) + J_2(I_1)J_0(I_2)\sin(w_ct - 2w_{m1}t)
 + J_2(I_1)J_1(I_2)\sin(w_ct + 2w_{m1}t + w_{m2}t) + J_2(I_1)J_1(I_2)\sin(w_ct + 2w_{m1}t - w_{m2}t)
 + J_2(I_1)J_1(I_2)\sin(w_ct - 2w_{m1}t + w_{m2}t) - J_2(I_1)J_1(I_2)\sin(w_ct - 2w_{m1}t - w_{m2}t)
 + \left. J_2(I_1)J_2(I_2)\sin(2w_ct + 2w_{m1}t + 2w_{m2}t) + J_2(I_1)J_2(I_2)\sin(2w_ct + 2w_{m1}t - 2w_{m2}t) \right.
 +J_2(I_1)J_2(I_2)\sin(2w_ct-2w_{m1}t+2w_{m2}t)+J_2(I_1)J_2(I_2)\sin(2w_ct-2w_{m1}t-2w_{m2}t)
 + ...
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$$J_{-n}(x) = (-1)^n J_n(x)$$



Bildquelle: http://de.mathworks.com/help/ matlab/ref/besselj.html

Spektrum der Parallelschaltung für 1 T, 2 M



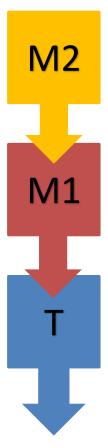
0.015

0.01

Kaskadenschaltung

$$f_{FMkaskade}(t) = \sin(w_c t + I_1 \sin(w_{m1}t + I_2 \sin(w_{m2}t)))$$

$$= \sum_{n=-\infty}^{\infty} \sum_{k=-\infty}^{\infty} J_n(I_1) J_k(\mathbf{n}I_2) \sin(w_c t + nw_{m1}t + kw_{m2}t)$$



FM-Synthese 22.06.2015

Formel Spektrum Parallelschaltung vs. Formel Spektrum Kaskadenschaltung

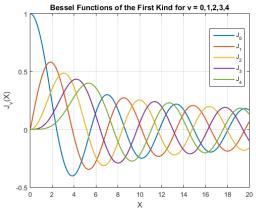
$$\sum_{i=-\infty}^{\infty} \sum_{k=-\infty}^{\infty} J_i(I_1) J_k(I_2) \sin(w_c t + i w_{m1} t + k w_{m2} t)$$

$$\sum_{n=1}^{\infty} \sum_{k=1}^{\infty} J_n(I_1)J_k(\mathbf{n}I_2)\sin(w_ct + nw_{m1}t + kw_{m2}t)$$

Additionsterme der Seitenbänder bei 2 Modulatoren in Reihe

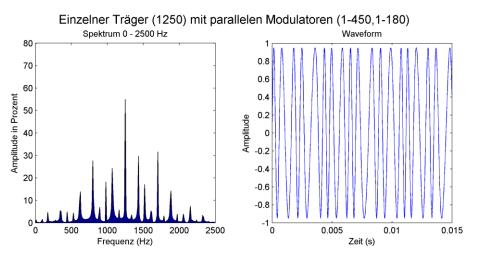
```
\sin(w_c t + I_1 \sin(w_{m1}t) + I_2 \sin(w_{m2}t))
= J_0(I_1)J_0(\mathbf{0}I_2)\sin(w_c t)
+ J_0(I_1)J_1(0I_2)\sin(w_ct + w_{m2}t) - J_0(I_1)J_1(0I_2)\sin(w_ct - w_{m2}t)
+ J_0(I_1)J_2(0I_2)\sin(w_ct + 2w_{m2}t) + J_0(I_1)J_1(0I_2)\sin(w_ct - 2w_{m2}t)
+ J_1(I_1)J_0(1I_2)\sin(w_ct + w_{m1}t) - J_1(I_1)J_0(1I_2)\sin(w_ct - w_{m1}t)
+J_1(I_1)J_1(1I_2)\sin(w_ct+w_{m1}t+w_{m2}t)-J_1(I_1)J_1(1I_2)\sin(w_ct+w_{m1}t-w_{m2}t)
-J_1(I_1)J_1(1I_2)\sin(w_ct-w_{m1}t+w_{m2}t)+J_1(I_1)J_1(1I_2)\sin(w_ct-w_{m1}t-w_{m2}t)
+J_1(I_1)J_2(1I_2)\sin(w_ct+w_{m1}t+2w_{m2}t)+J_1(I_1)J_2(1I_2)\sin(w_ct+w_{m1}t-2w_{m2}t)
-J_1(I_1)J_2(1I_2)\sin(w_ct-w_{m1}t+2w_{m2}t)-J_1(I_1)J_2(1I_2)\sin(w_ct-w_{m1}t-2w_{m2}t)
+ J_2(I_1)J_0(2I_2)\sin(w_ct + 2w_{m1}t) + J_2(I_1)J_0(2I_2)\sin(w_ct - 2w_{m1}t)
+J_2(I_1)J_1(2I_2)\sin(w_ct+2w_{m1}t+w_{m2}t)+J_2(I_1)J_1(2I_2)\sin(w_ct+2w_{m1}t-w_{m2}t)
+J_2(I_1)J_1(2I_2)\sin(w_ct-2w_{m1}t+w_{m2}t)-J_2(I_1)J_1(2I_2)\sin(w_ct-2w_{m1}t-w_{m2}t)
+J_2(I_1)J_2(2I_2)\sin(2w_ct+2w_{m1}t+2w_{m2}t)+J_2(I_1)J_2(2I_2)\sin(2w_ct+2w_{m1}t-2w_{m2}t)
+J_2(I_1)J_2(2I_2)\sin(2w_ct-2w_{m1}t+2w_{m2}t)+J_2(I_1)J_2(2I_2)\sin(2w_ct-2w_{m1}t-2w_{m2}t)
+...
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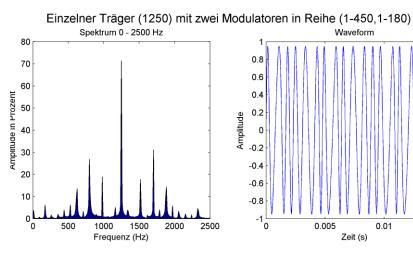
$$J_{-n}(x) = (-1)^n J_n(x)$$



Bildquelle: http://de.mathworks.com/help/ matlab/ref/besselj.html

Vergleich: Parallel- und Kaskadenschaltung

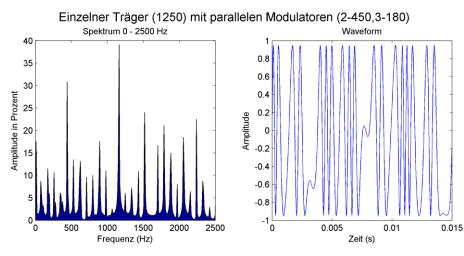


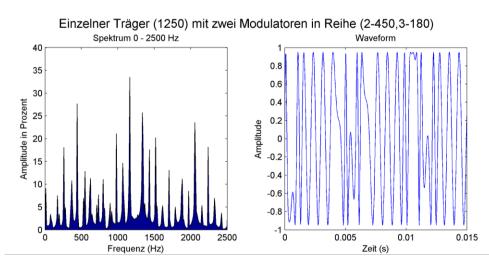


0.01

0.015

Vergleich mit Modulationsindizes 2 und 3



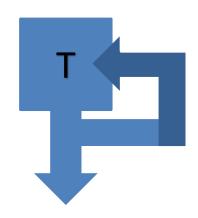


Feedbackschaltung

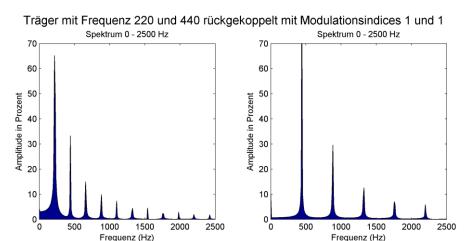
$$f_{FMfeedback}(t_n) = sin(w_c t_n + If_{FMfeedback}(t_{n-1}))$$

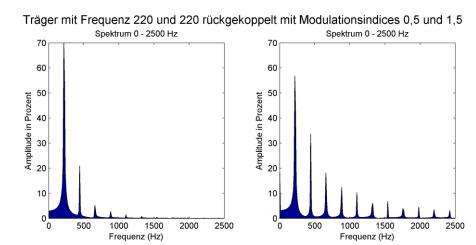
$$mit f_{FMfeedback}(t_0) = 0$$

$$f_{FMfeedback}(t) = \sum_{n=1}^{\infty} \frac{2}{nI} J_n(nI) \sin(nw_c t)$$



Spektrum der Feedbackschaltung





Praxisbeispiel: Modulationsmatrix FM8



Fazit

Komplexe FM-Synthese ist extrem m\u00e4chtig

Resultierendes Spektrum schwer abschätzbar

• Durch moderne Synths wie FM8 Trial & Error einfach

Quellen

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- [Cho73] John M. Chowning. The synthesis of complex audio spectra by means of frequency modulation. *Journal of the Audio Engineering Society*, pages 526–534, 1973.
- $[Sch] \hspace*{0.2in} B. \hspace*{0.2in} Schottstaedt. \hspace*{0.2in} Introduction \hspace*{0.2in} to \hspace*{0.2in} fm. \hspace*{0.2in} \hspace*{0.2in} https://ccrma.stanford.edu/software/snd/snd/fm. \hspace*{0.2in} html. \hspace*{0.2in} the top the substance of the substance$
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Vielen Dank für eure Aufmerksamkeit!