### MCNP Report

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2019-03-09

Abstract Abstract yet to be written

## 1 Introduction

#### 1.1 Exercise 1

Write something

Will have to finish later

(Explain in outline what your modelling is trying to achieve and what you are setting out to achieve. Provide some relevant background information)

## 2 Method

Computing facility For the following exercise all parts are created using the ENDL92 library (which is the most recently updated library available), and ran on the phymat server of University of Birmingham School of Physics and Astronomy, which is a Scientific Linux 7.3 (Nitrogen) system with 16 CPU's (Intel(R) Xeon(R) CPU E5-2630 v3 @ 2.40GHz) (though it is important to note that only 1 CPU is used at a time because this version of MCNP does not support parallel computing).

**Geometry definition** The geometry for exercise 1 and 3 were set to the dimensions as required by the problem sheet; the cross-sections of their geometries are shown in Figure 2 and 3 in the Appendices.

**Energy cutoff** Energy cutoff is not applied so that very slow (thermalized) neutrons are allowed to interact and let further reactions take place.

# 2.1 Exercise 1 Simple Neutron Source in a Bucket of Water

Therefore for exercise 1, the lower bound of the  $1^{st}$  bin of each tally is E=0.

The temperature of the cross-section data in databse 42(ENDL92, acquired by Lawrence Livermore National Laboratory) were acrquired at T=300K, as shown in 91-99, and is subsequently adjusted down to  $20.4~^{o}C$  ( $2.53 \times 10^{-8} MeV$ ) when running the simulation. Either way, thermal effects should significantly affect that falls into the first 3 energy bins. (0-10<sup>-9</sup>MeV,  $10^{-9}$ - $10^{-8} MeV$ ,  $10^{-8}$ - $10^{-7} MeV$  respectively).

Note that the  $1^{st}$  bin (0 to  $1 \times 10^{-9}$  MeV) is below the thermal energy of room temperature; neutrons of these energies are strongly affected by the free gas thermal treatment of the interaction cross sections; additionally due to the large cross section in the thermal region which increases as the neutron slows, very few neutrons of these energies can travel far enough to be counted by these surface flux tallies. Therefore this bin always have the largest relative errors among all bins.

To ensure that no bins have relative error larger than 0.10 such that the results are reliable, enough histories must be ran to allow this energy bin in all 3 tallies to be filled sufficiently, in addition to passing all 10 statistical checks.

The tally probability distributions (histograms shown in table 161's) all show reasonably Gaussian distributions (and the cumulative probability distributions all show reasonably sigmoidal distributions) without the majority of the counts falling into a particular bin; therefore there is no inherent reason for using a finer spacing; but for the purpose of visualizing the spectrum with a higher resolution, a finer group structure with trifolded bin density (still logarithmically spaced, 3 bins per decade) was used.

Even when the spacing of energy groups is trisected in this manner, the  $1^{st}$  bin (0 to  $1 \times 10^{-9}$  MeV) is still the bin that receives the least counts. In a real problem this would have been merged with the  $2^{nd}$  bin to form a single, larger bin to tally up all the completely thermalized neutrons, increasing its count so that it converges to a precise enough value in a shorter CPU time; but according to the constraint of the problem, there must be one bin with  $10^{-9}$  MeV as the upper limit. Therefore the only option left is to increase the number of histories such that the results of this bin converges.

## 2.2 Exercise 3: Criticality

Note that there is no delayed neutron cross section data available in ENDL92 (or any other nuclear databases available on phymat), so the simulation may deviate from reality slightly. There is no workaround for this issue; but one can assume, for the purpose of this simulation, that a cross-section database without delayed neutron cross-section should be accurate enough.

**Geometry definition** It is easier geometry to define the geometry if a sphere was used to define the graveyard (void) outside; but a cuboidal geometry was chosen instead to allow the surface flux detectors (F2) to tally particles passing through lateral surfaces separately from particles passing through horizontal surfaces.

All components except the concrete floor had the same neutron importance. Neutron importance in concrete started off at 1 but was subsequently reduced to 0.1 such that the simulation runs faster by ignoring particles that enter the concrete, since they will otherwise undergo a lot of collision (each requiring a lot of CPU time) to slow down, without causing multiplication.

If the mean free path to absorption  $\lambda_{\rm abs}$  is known, the dimension of the concrete floor can be chosen to extend from the stainless steel tank by  $N\lambda_{\rm abs}$  where N is some arbitrary threshold factor (e.g. 3).

However only the mean free path to collision for neutron is found on a cell particle activity table (using PRINT 126). Since concrete is only a weakly neutron-absorbing medium, this cannot be used as the proxy for  $\lambda_{abs}$ .

Instead the fraction of neutrons escaping the concrete block into the void was measured. This was done by comparing the number of neutrons travelling from the concrete to the void region (where neutron importance = 0) (measured with a surface flux tally card) to the neutron population in the concrete. The quantity "population" instead of "tracks entering" was used because the latter re-counts particles re-entering the same cell, thus the former is a more accurate measurement of how many distinct neutrons have been present in the concrete block. The simulation is considered accurate when the ratio of these two numbers is less than 1%, i.e. < 1% of the neutrons entering the concrete were "killed" (by entering the void region) instead of being absorbed in the concrete/reflected back towards the tank. The dimension of the concrete block was increased until this ratio is lower than 1%.

This resulted in a concrete floor block of 160.4cm in the x- and y-directions and 50 cm in the z-direction, resulting in 0.21621209% and 0.04494092% of neutrons escaping through the lateral planes and the horizontal plane (plane separating the concrete block from the void below) respectively. This was used as the final dimension for the concrete block.

**Source definition** Using the KSRC card a "generic Watt spectrum" [1] of neutrons was created at the center points of each cylinder.

This allowed for very fast convergence of the results, where the  $k_{eff}$  value settled down to a stable value in less than 10 generations. The  $k_{eff}$  estimation started after that.

The alternatives of using an SDEF card with a cookie cutter(CCC) rejection/CEL rejection OR 5 uniform cylindrical sources overlayed onto cell 11-15 (all the uranium cylinder cells) were attempted, but were not applied in the end because it is likely to distribute neutrons close to the non-re-entrant surfaces where they can escape, reducing the effectiveness of the source and potentially increasing the number of cycles that needs to be skipped. [2]

Choices of number of cycles 3000 particles per cycle were shown to give a  $k_{eff}$  that converges in 10 cycles; 5000 particles per cycles were shown to give faster convergence of  $k_{eff}$  value (in > 5 cycles), but further increase in number of particles per cycles to 8000 did not show significant improvemence in speed of convergence. Therefore the number of particles were chosen to be 5000, and the first 10 cycles were skipped (ikz=10).

At 5000 particles per cycle, the  $k_{\rm eff}$  value was shown to converge sufficiently by the 500 cycles; further increase in total number of cycles yields deminishing marginal at the cost of increasing computing time, asymptotically approaching 0; thus only 500 cycles was ran, requiring 10.27 minutes of computing time.

The number of cycles to run per simulation were later changed when the  $k_{\rm eff}$  changed. For details see 4.1.1

Alteration to the weight fraction of Boron When attempting to find a concentration of Boron that gives a solution, only the unnormalized weight fraction of Boron was changed between iterations, letting MCNP to normalize the weight fraction of Boron in water and printing the resulting normalized weight fraction of boron in table 40.

## 3 Result

By examining the first 50 particles (using PRINT 110), the source was confirmed to be a point source 2cm above the centre of the bottom of the tank's internal surface; and the majority of the particles have initial energy E < 4 MeV as expected when they are distributed according to the Watt spectrum for neutron generated by  $^{235}U+n$  (thermal).

plot variation of VoV, fom, and etc. metrics as nps increases to 20000

Insert spectrum (histograms) of the 3 tallies

create table for total neutron fluence [dividing by the difference in upper and lower class boundaries so that it gives number density instead?]

create table for the neutron mean energy of the three tallies

# 4 Analysis and discussion

Note from the Watt spectrum above that there is a small but non-zero probability of getting neutrons of very high energy. This leads to some warning messages when the occassional particle scores above the upper limit of the largest tallying bin in Exercise 1.

# 4.1 Answer to questions for Exercise 1

1. These results are not reliable because the statistical checks (
insert number of them not passed) are not passed, meaning that some reactions are not

sampled enough for us to be confidence about the frequencies of their occurance. Additionally, some bins in the PDF are empty (seen table 161 of tally 22) suggesting that insufficient number of neutrons is sampled to approximate a continuous distribution.

2. The total fluences  $\Phi$  are simplay calculated by formula  $NA\sum_{i}(\Psi_{i})$  where each  $\Psi_{i}$  refers to the flux calculated for the i<sup>th</sup> energy bin per history.

A = Effective area for surface flux tallying, where the particle passing through still had non-zero weight.

N = number of histories

Giving (insert table of neutron total fluence)

#### 3. The neutron spectra

The average standard flux  $\phi$  i.e. number of neutrons passing through each unit surface area of interest, and the implication (fewer gets their because of the inverse square law) Quote table and spectra above for neutron mean energy

The hardness of neutron spectrum decreases as follows: hardness at base (Tally 32)>long side (Tally 12)>short side (Tally 22), because distance of them increases in that order. More neutrons can penetrate the base at the energy its creation energy without being moderated by the water; therefore the  $1^{st}$  bin of tally 32 more filled than that of tally 12.

The ratio of neutron flux in the slow/Cadmium region (<0.01 MeV) to neutron flux in the resonance regions (>0.01MeV) builds up since the latter gets slowed down/captured by the resonance peaks much faster than the rate of consumption of the former, as they travel through the material.

#### 4.1.1 Number of histories required to converge

Even after running 500,000 histories, the relative error for this  $1^{st}$  bin remains high (0.2599, 0.4236, 0.3681, for tally 12, 22, and 32, respectively) despite the fact that all other statistical checks were passed after running 500,000 histories, and the fom has already converged to a reasonably stable asymptotic limit.

If one does not care for the accuracy of the  $1^{st}$  bin, then running 2,800,000 histories is sufficient, as it passess all statistical test, such as the figure of merit having stablized enough by the 2,800,000 history, in a reasonable computing time of 1.98 minutes. However, 16,000,000 histories are required for the convergence of the  $1^{st}$  bin, requiring 12.79 minutes of coputing time, which is quite long for a simple problem.

Additionally, the statistics of tally 22 is poor, leading to a fluctuating Figure of Merit being recorded, leading to what appears to be a decreasing trend in FoM the last half of the simulation, missing the fom statistical check. Therefore the result of this bin is less reliable than the result of the rest of the bins concerned.

## 4.1.2 $10^{10}$ n./s conversion factor

If this simulation is meant to represent a  $10^{10}s^{-1}$  neurton source, then a multiplication factor = nps × area ×  $10^{10}s^{-1}$  should be multiplied onto the values given in the output file, giving

## 4.2 Answer to questions for Exercise 3

 $\bullet$  The final  $k_{\rm eff}$  estimate and its standard deviation is reported in line 4174-4178 of the output file for 20wt.% enriched Uranium with no Boron addition as follows:

"the final estimated combined collision/absorption/track-length keff = 1.01798 with an estimated standard deviation of 0.00046

the estimated 68, 95, & 99 percent keff confidence intervals are 1.01752 to 1.01843, 1.01707 to 1.01888,and 1.01677 to 1.01918"

The average combined  $k_{eff}$  was observed to decrease slightly at the beginning, converging onto and the value of 1.01798, and then stablize around this value, with decreasing standard deviation as the simulation progresses.

Examine and report upon the estimate of  $k_{\text{eff}}$  with cycle number given in the output.

- The final results of  $k_{eff} = 1.01798 \pm 0.00046$  is fairly reliable, considering the following items, as suggested by [3]:
  - all cells with fissile isotopes (i.e. all U cylinders) were sampled
  - the average combined  $k_{\rm eff}$  appeared to be varying randomly about the average  $k_{\rm eff}$  for the average cycles
  - no noticable trend was present in the later stage of the average combined  $k_{\rm eff}$
  - the confidence intervals from the batched combined  $k_{\rm eff}$  does not appear to differ significantly from the final result, meaning there are no cyclic variations
  - the Figure of Merit for combined  $k_{\rm eff}$  is stable.

and lastly,

- the lack of delayed neutron cross section library should only make an insignificant difference to the final  $k_{\text{eff}}$  because they shouldn't care
- In addition to Monte Carlo stochastic uncertainties what other uncertainties may need to be considered in a criticality safety assessment?

The  $k_{\rm eff}$  increased up to  $1.06627\pm0.00045$  when the enrichment increased up to 25% as expected, since more neutrons are absorbed by fissile atom causing fission. However addition of Boron at  $\approx 0.3 {\rm wt.\%}$  (i.e.  $3000 {\rm ppm}$ , similar concentration to those found in PWR) was already sufficient to decrease the  $k_{\rm eff}$  down to  $0.76681\pm0.00063$ .

Subsequent iterative simulations with decreasing boron concentration shows that

- The magnitude of combined k<sub>eff</sub> variation between cycles is larger compared to the case when no boron was present, possibly due to the increased number of neutrons being absorbed by the Boron in water;
- The computing time per cycle decreased, likely due to the lowered k<sub>eff</sub>;

This leads to the decisions to

- $\bullet$  increase the total number of cycles to 800 to reduce the uncertainty on  $k_{\rm eff}$  such that a lower minimum concentration of Boron can be calculated while maintaining sufficient confidence that it will keep the  $k_{\rm eff} < 0.8$
- increase the number of particles per simulation was also doubled to 10000 to counteract the increased uncertainty introduced by the absorbing power of Boron.
- $\bullet$  increase the number of cycle skipped at the beginning to 100 to account for the slower convergence due to the increased cycle-to-cycle fluctuation in  $k_{\rm eff}$

Which still leads to a acceptable computing time of < 8 minutes per simulation.

The 3  $\sigma$  envelope of  $k_{eff}$  was found to remain under 0.8 when Boron concentration > 1.39804ppm (input file's unnormalized weight fraction of boron =0.14% times the water's weight fraction); any higher (i.e. at 1.29831ppm) and the 3  $\sigma$  confidence interval begins to cross over the  $k_{eff} > 0.8$  threshold, i.e. there will be a larger than 0.0675% chance of its  $k_{eff} > 0.8$  (See Figure 1).

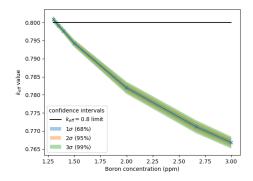


Figure 1: The  $k_{eff}$  only remains below 0.8 at Boron concentration  $\approx < 14$  ppm.

# Appendices

# A Figures

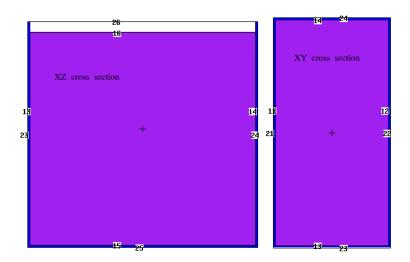


Figure 2: The XZ and XY cross section of the bucket at the origin (z=0 and y=0 respectively)

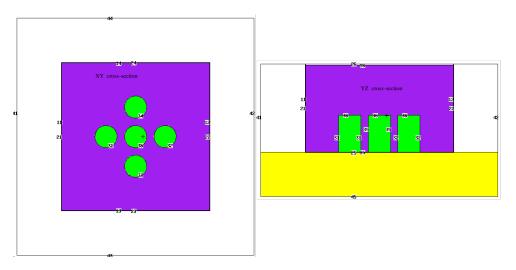


Figure 3: The XZ and XY cross section of the bucket at the origin (z=0 and y=0 respectively)

## B Tables

# C References

- [1] MCNP4C2: Monte Carlo N-Particle Transport Code System Abstract (Diagnostics Applications Group, Los Alamos National Laboratory, Los Alamos, New Mexico.) p.2-160 (June 2001.)
- [2] MCNP4C2: Monte Carlo N-Particle Transport Code System Abstract (Diagnostics Applications Group, Los Alamos National Laboratory, Los Alamos, New Mexico.) p.4-30 (June 2001.)
- [3] MCNP4C2: Monte Carlo N-Particle Transport Code System Abstract (Diagnostics Applications Group, Los Alamos National Laboratory, Los Alamos, New Mexico.) p.2-180 (June 2001.)