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(71) **Applicant (for all designated States except US):** **FRAC-**
TUS, S.A. [ES/ES]; Avenida Alcalde Barnils, 64-68, Ed-
ificio Testa - Módulo C, Parque Empresarial Sant Joan,
E-08190 Sant Cugat del Valles (ES).

(72) **Inventors; and**

(75) **Inventors/Applicants (for US only):** **SOLER CASTANY,**
Jordi [ES/ES]; c/ Fray Luis de León, 19-21 àtic, E-08302
Mataró (ES). **ANGUERA PROS, Jaume** [ES/ES]; P.
Blasco Ibáñez N° 15 2°, 12500 Vinaròs (Castelló) (ES).
PUENTE BALIARDA, Carles [ES/ES]; c/Londres, 57 4°

2a, E-08036 Barcelona (ES). **BORJA BORAU, Carmen**
[ES/ES]; Tvra. de Dalt, 67, E-08024 Barcelona (ES).
MUMBRU FORN, José [ES/ES]; c/Rector Ubach 25, 2°
1a, E-08021 Barcelona (ES).

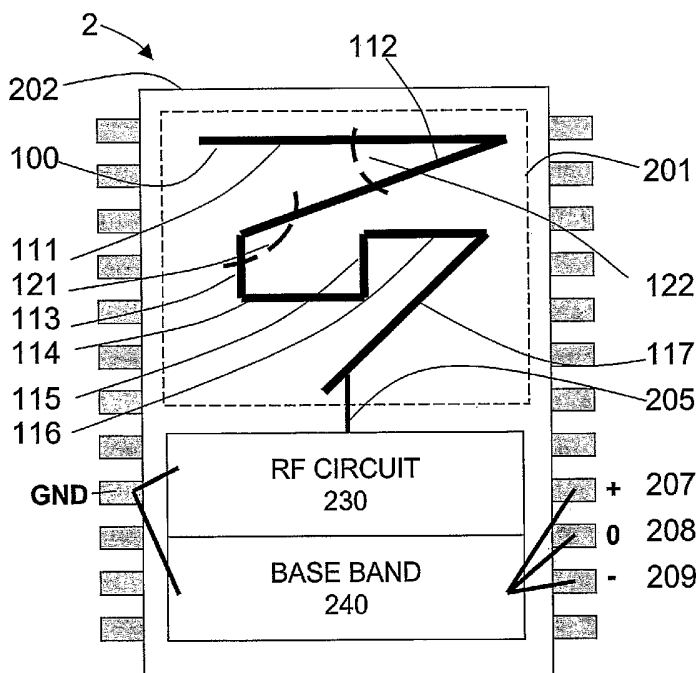
(74) **Agents:** **BRACHMANN, Roland** et al.; Prinzregenten-
strasse 11, 80538 München (DE).

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- (54) Title:** RADIO-FREQUENCY SYSTEM IN PACKAGE INCLUDING ANTENNA



- (57) Abstract:** A system comprising at least one antenna and a circuit, wherein the circuit is at least in part not a semiconductor chip or a die. The at least one antenna and the circuit are arranged on a package. Alternatively described is a system comprising at least one antenna and at least one circuit, wherein the at least one antenna and the at least one circuit are arranged on a package, wherein the at least one circuit performs a radio-frequency and optionally a base-band and/or a digital functionality.



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Radio-Frequency System in Package including Antenna

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Background of the Invention

10 The present invention relates generally to novel integrated circuit packages that include a new family of miniature antennas in the package.

There is a trend in the semiconductor industry towards the so-called System on Chip (SoC) and System on Package (SoP) concepts. The full integration of
15 systems or subsystems into a single chip, package or module provides many advantages in terms of cost, size, weight, consumption, performance and product design complexity. Several electronic components for consumer applications, such as handsets, wireless devices, personal digital assistants (PDAs) or personal computers (PCs) are becoming more and more integrated into SoP/SoC products.

20

The concept of integrating a miniature antenna into a package or module is especially attractive owing to the tremendous growth and success of cellular and wireless systems. In particular, there is a new generation of short/medium range wireless applications such as BluetoothTM, Hyperlan, IEEE802.11 and ultra wide
25 band (UWB), Wimax and Zig Bee systems where the progressive system integration into a single, compact product is becoming a key success factor (see for instance [1]).

This concept of integrating a miniature antenna into a package or module is
30 especially attractive as well in GSM, UMTS, PCS1900, KPCS, CDMA, WCDMA, and GPS.

There have been reported several attempts to integrate an antenna in a package or module. These designs feature two important limitations: first the operating frequency must be large enough to allow a conventional antenna to fit inside the chip; second the antenna performance is poor in terms of gain, mainly due to the losses in the semiconductor material. According to D. Singh, et al., the smallest frequency in which an antenna has been integrated together with an electronic system inside the same was 5.98 GHz. Typical gains that have been achieved with such designs are around -10 dBi.

10

In general, there is a trade-off between antenna performance and miniaturization. The fundamental limits on small antennas were theoretically established by H. Wheeler and L. J. Chu in the middle 1940's. They stated that a small antenna has a high quality factor (Q), because of the large reactive energy stored in the antenna vicinity compared to the radiated power. Such a high quality factor yields a narrow bandwidth; in fact, the fundamental derived in such theory imposes a maximum bandwidth given a specific size of an small antenna. Related to this phenomenon, it is also known that a small antenna features a large input reactance (either capacitive or inductive) that usually has to be compensated with an external matching/loading circuit or structure. It also means that it is difficult to pack a resonant antenna into a space which is small in terms of the wavelength at resonance. Other characteristics of a small antenna are its small radiating resistance and its low efficiency (see [2]).

15

Some antenna miniaturization techniques rely basically on the antenna geometry to achieve a substantial resonant frequency reduction while keeping efficient radiation. For instance, patent application WO 01/54225 A1 discloses a set of space-filling antenna geometries (SFC) that are suitable for this purpose. Another advantage of such SFC geometries is that in some cases they feature a multiband response.

25

30

The dimension (D) is a commonly used parameter to mathematically describe the complexity of some convoluted curves. There exist many different mathematical definitions of dimension but in the present document the box-counting dimension (which is well-known to those skilled in advanced mathematics theory) is used to
5 characterize some embodiments (see discussion on the mathematical concept of dimension in [3] or [4]).

So-called chip-antennas are described in [5] or [6]. Those are typically single component antenna products that integrate only the antenna inside a surface-
10 mount device. To achieve the necessary wavelength compression, those antennas are mainly constructed using high permittivity materials such as ceramics. The drawbacks of using such high permittivity materials are that the antenna has a very narrow bandwidth, the material introduces significant losses, and the manufacturing procedure and materials are not compatible with most package
15 manufacturing techniques; therefore they do not currently include other components or electronics besides the antenna, and they are not suitable for a FWSoc or FWSop.

There have been recently disclosed some RF SoP configurations that also include
20 antennas on the package. Again, most of these designs rely on a conventional microstrip, shorted patch or PIFA antenna that is suitable for large frequencies (and therefore small wavelengths) and feature a reduced gain. In [7] a SoP including an RF front-end with an integrated antenna is described. The antenna comprises a microstrip patch backed by a cavity which is made with shorting pins
25 and operates at 5.8 GHz . As mentioned in [7], it is difficult to extend those designs in the 1-6 GHz frequency range where most current wireless and cellular services are located, mainly due to the size of conventional antennas at such large wavelengths. Another design for an antenna on a package is disclosed in [8]. Although the antenna operates at the BluetoothTM band (2.4GHz), the IC package
30 is substantially large (15x15 mm) and the antenna performance is poor (gain is below -9dBi).

Patent application EP1126522 describes a particular double S-shaped antenna design that is mounted on a BGA package. Although no precise data is given on the package size in the application, typically, S-shaped slot antennas resonate at a wavelength on the order of twice the unfolded length of the S-shaped pattern. Again, this makes the whole package too large for typical wireless applications where the wavelength is above 120 mm. Also, this design requires a combination with high permittivity materials that, in turn, reduce the antenna bandwidth, increase its cost and decreases the overall antenna efficiency.

10

Regarding the package construction and architecture, there are several standard configurations depending mainly on the application. Some basic architectures are: single-in-line (SIL), dual-in-line (DIL), dual-in-line with surface mount technology DIL-SMT, quad-flat-package (QFP), pin grid array (PGA) and ball grid array (BGA) and small outline packages. Other derivatives are for instance: plastic ball grid array (PBGA), ceramic ball grid array (CBGA), tape ball grid array (TBGA), super ball grid array (SBGA), micro ball grid array BGA[®] and leadframe packages or modules. A description of several standard packaging architectures can be found on the websites of several package manufacturers, e.g.: www.amkor.com (see also [9]).

20

In PCT/EP02/12427 (filed as well by the applicant, but not published when this current application was filed), attempts have been made in order to incorporate a miniature antenna to a package together with a semiconductor die.

25

Although this arrangement is suitable for certain applications it involves some disadvantages. More components in the package leads to a bigger size of the system. Another reason not to have a fully integrated solution is that some manufacturers incorporate their own processors onto the printed circuit board (PCB) and prefer to incorporate a package or module antenna rather than a fully integrated package. Moreover, having a circuit in the same package or module as the die itself, can increase the amount of heat to be dissipated and might lead to an

30

increase of temperature of the whole system causing a malfunction of the die. Besides, interference between the antenna and the die might occur. This could lead to a decrease in the performance of the system.

5 In the last few years, several improvements in packaging technology have appeared mainly due to the development of Multichip Module (MCM) applications (see for instance [10]). Those consist of an integrated circuit package that typically contains several chips (i.e., several semiconductor dies) and discrete miniature components (biasing capacitors, resistors, inductors). Depending on the
10 materials and manufacturing technologies, MCM packages are classified in three main categories: laminated (MCM-L), ceramic (MCM-C) and deposited (MCM-D). Some combinations thereof are possible as well, such as e.g. MCM-L/D and other derivations such as Matsushita ALIVH. These MCM packaging techniques cover a wide range of materials for the substrate (for instance E-
15 glass/epoxy, E-glass/polyimide, woven Kevlar/epoxy, s-glass/cyanate ester, quartz/polymide, thermount/HiT^a epoxy, thermount/polyimide, thermount/cyanate ester, PTFE, RT-Duroid 5880, Rogers RO3000[®] and RO4000[®], polyolefin, alumina, sapphire, quartz glass, Corning glass, beryllium oxide and even intrinsic GaAs and silicon) and manufacturing processes (thick film, thin film, silicon thin
20 film, polymer thin film, LTCC, HTCC).

Summary of the Invention

25 The objective technical problem to be solved by the invention is to provide a system with improved characteristics in view of the prior art, said device being applicable in various ways.

This problem is solved by the features of the independent claims. Further
30 embodiments of this invention result from the dependent claims.

The present invention generally relates to novel integrated circuit packages, modules or systems comprising a new family of miniature antennas according to the any independent claim. Also, the invention relates to several novel ways of arranging the materials and components of the package to include the antenna.

5 Particularly, main advantages of the invention are as follows:

- the small size of the antenna, which allows the use of very small packages (such as for instance CSP packages) at typical wireless wavelengths;
- the antenna geometry that enables such a miniaturization;
- the arrangement of the antenna in the package;
- 10 – the compatibility of the antenna design with virtually any state of the art packaging architecture;
- scaled and distributed devices can be put together in an economical and efficient way;
- the heating-up effect of the package can be dissipated to an external
- 15 component or an additional package, reducing the risk of malfunction of the device;
- several packages can be combined/put together, e.g. packages of RF circuits and/or antennas to be e.g. maintained by a processor to combine signals to be used in a multiple input multiple output (MIMO)
- 20 environment. This might lead to a scalability of the packages according to the demands of the respective environment or system.

In contrast to the chip-antennas as described in [5], the present invention relies on the specific novel design of the antenna geometry and its ability to use the

25 materials that are currently being used for integrated circuit package construction, so that the cost is minimized while allowing a smooth integration with the rest of the system.

The objective problem is solved by a system comprising at least one antenna and a

30 circuit, wherein the circuit is at least in part not a silicon chip or a die. The at least one antenna and the circuit are arranged on a package.

The problem is also solved by a system comprising at least one antenna and at least one circuit, wherein the at least one antenna and the at least one circuit are arranged on a package, wherein the at least one circuit performs a base-band
5 and/or a digital functionality.

This base-band functionality comprises e.g.:

- 10 – Conversion from a digital bitstream to a sequence of symbols in transmission, or symbol acquisition and digital data regeneration in reception;
- Clock recovery and symbol synchronization;
- Automatic gain control;
- Error correction algorithms;
- Data encryption/decryption;
- 15 – Channel estimation for adaptive detection;
- Memory blocks (for example for temporary data storage, for programming other digital blocks, etc.);
- Transmission/Reception buffers for storage of received packets and packets to be transmitted; or
- 20 – Microprocessors and/or microcontrollers to carry out data processing, control tasks (like data handshaking with other chips), implement communication ports protocols (like USB) or audio features (like an audio CODEC).

25 In an embodiment of the invention the (at least one) circuit comprises a radio-frequency circuit (RF-circuit). In particular, the coupling between the at least one antenna and the radio-frequency circuit can be a reactive coupling, in particular a capacitive or inductive coupling.

30 In another embodiment, the radio-frequency circuit is connected to or located on a ground plane.

Yet another embodiment is directed to at least some of the connections of the radio-frequency circuit being balanced.

- 5 In another embodiment, a radio-frequency component is arranged outside the package. In particular, this radio-frequency component could be a matching network. As a further option, the radio-frequency component can be a matching network, a bypass or a through-connection.
- 10 Optionally, the radio-frequency circuit on the package can be a matching network, a bypass or a through-connection.

It is to be noted that the radio-frequency component arranged outside the package could be an external circuit as well as an external sub-circuit, the latter e.g. being
15 part of a larger circuit. This external circuit or sub-circuit can be or comprise a radio-frequency circuit, respectively.

Furthermore, the radio-frequency component outside the package as well as the radio-frequency circuit on the package can be a power amplifier, respectively.
20

Some other possibilities of components that could be part of the radio-frequency circuit (internal) or radio-frequency component (external to the package) are:

- Power amplifier;
- Low noise amplifier;
- 25 – Filters;
- Diplexer;
- Local oscillators (like a quartz crystal oscillator);
- Modulator/demodulator;
- Switch;
- 30 – Mixer;
- (Signal) Detector;

- Phase shifter; or
- balun.

In yet another embodiment the at least one antenna is connected to the radio-frequency circuit and at least in part the radio-frequency circuit is connected to the radio-frequency component outside the package.

In an additional embodiment, the at least one antenna is connected to the to the radio-frequency component outside the package directly.

Furthermore, the radio-frequency circuit can comprise a balun. Preferably, this balun can be incorporated as a printed circuit or as a discrete component. Additionally, the balun can be placed inside the package or outside of the package.

In another embodiment, the ground plane is not located underneath or on top of the at least one antenna. In particular, the projection of the antenna should not be on a ground plane.

In particular, the package can be an integrated circuit package (IC package).

Another embodiment is directed to a system, wherein the radio-frequency circuit or the radio-frequency component includes at least one filter. Preferably, this filter is or comprises a band-pass characteristics. Additionally, other filter types as high-pass or low-pass filters or combinations thereof can be provided.

A next embodiment is directed to the at least one antenna being connected to an input/output connector of the package and at least a part of the circuit being connected to an input/output connector of the package. Said connectors can be the same or different ones.

In another embodiment the at least one antenna is a space filling antenna.

Preferably, the space filling antenna has a dimension bigger than 1.

In fact, there exist several definitions of the dimension, e.g. a box counting
5 dimension and a grid dimension. Preferably, these dimensions amount to numbers
between 1 and 2, respectively, in particular the dimensions amount to 1.0, 1.1, 1.2,
1.3, 1.4, 1.5, 1.6, 1.7, 1.8, 1.9, 2.0. The respective value depend on the
miniaturization of the packet size.

In particular, space filling is directed to the ability of filling the space
10 where the curve is located. This space could be an approximated surface or some
sort of three-dimensional volume.

In general, increasing the number of segments, reducing the size of the
segments, narrowing the angles between the segments and increasing the
dimension of the curve will lead to further miniaturization, respectively.

15

As a subsequent embodiment, the antenna can comprise a conducting pattern at
least a portion of which includes a curve, wherein said curve comprises at least
five segments. Each of the at least five segments forming a pair of angles with
each adjacent segment in said curve and at least three of said segments are shorter
20 than 1/10 of the longest free-space operating wavelength of said at least one
antenna.

In particular, the smaller angle of the pair of angles between adjacent
segments is less than 180° and at least two of said smaller angles between
adjacent section segments are less than 115° , wherein at least two of the angles,
25 which are on the same side of the curve and are formed from adjacent segments of
the group of said at least five segments, are different.

As a subsequent option, said conducting pattern fits inside a rectangular
area, the longest side of said rectangular area being shorter than 1/5 of the longest
free-space operating wavelength of said at least one antenna.

30 The number of "at least five" segments can as well be in particular seven,
nine, eleven, fifteen, twenty or twenty-five segments.

In another embodiment, at least the at least one antenna and/or the radio frequency circuit comprise(s) a connection with a radio-frequency input/output connector. In addition, the radio-frequency component outside the package can as well comprise such a connection with a radio-frequency input/output connector.

5

In particular, the at least one antenna can be a modular or a discrete component. As an option, the modular or discrete component can be a surface mount technique component (SMT component).

10 In a further embodiment, both ends of the at least one antenna can be connected to the package, in particular to Input/Output connectors of the package. In a particular embodiment, both ends of the antenna are connected to Input/Output connectors of the package.

15 Another embodiment is directed to the at least one antenna being a parasitic element. This parasitic element can be incorporated inside the package or, as an alternative, outside the package.

In yet another embodiment the system comprises at least one external antenna.

20

In addition, the system can comprise a switch. This switch can be placed outside or on the package. As a next embodiment, the switch can be used to commute between the at least one (internal) antenna and the at least one external antenna.

25 The switch can be a jumper or a bypass, or any mechanical switch with several positions to select manually a distinct antenna from several available antennas. The switch can also be an electromechanical switch (like a relay), or an electronic switch like a transistor, FET, FLIP-FLOP or the like.

The use of a switch to select between the at least one (internal) antenna
30 and the at least one external antenna could be used to implement an antenna diversity system. The technique of antenna diversity consists of providing several

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antennas to the receiver as a way to protect the receiver from signal fading in the communication channel. The antennas must be arranged so that there is little, or no, correlation between the signals received by each one of them.

- 5 In an alternative embodiment, the at least one antenna is not physically connected to any other component. This might as well apply to the external antenna mentioned above.

Furthermore, the at least one antenna could be a balanced or an unbalanced
10 antenna.

In addition, the at least one antenna can be loaded with discrete reactive components, e.g. capacitors and/or inductors.

- 15 As another embodiment, the antenna can be loaded with external loads.

Another embodiment comprises several systems as described above, wherein the antennas are forming a multiple antenna communication system.

- This multiple antenna communication system can be a multiple-input-
20 multiple-output system, a smart antenna system, a phased array system or a sensor network.

For certain applications it is advantageous as well to separate the radio frequency band from the base band, because of interference problems between both parts.

- 25 Higher quality components, which might need more space could be used if one part of the signal processing circuit is placed outside the package.

- The technique of having a separate outside part of the (functional) circuit systematically opens the possibility to use existing components outside the
30 package, such as e.g. clocks, oscillators or filters.

Brief Description of the Drawings

Embodiments of the invention will be illustrated and explained hereinafter on the
5 basis of the drawings:

Fig.1 shows an embodiment of a package including an antenna and a circuit;

Fig.2 shows an embodiment of a package including an antenna and a circuit
10 composed by a base band circuit;

Fig.3 shows an embodiment of a package including a dipole antenna and a
radio-frequency circuit together with an additional circuit outside the
package;
15

Fig.4 shows an embodiment of a package including a monopole antenna and
a circuit, both connected to a matching network outside the package;

Fig.5 shows an embodiment of a package including a balanced antenna and a
radio-frequency circuit together with an additional circuit outside the
package;
20

Fig.6 shows an embodiment of a package including a balanced antenna with a
reactive loading;
25

Fig.7 shows examples of space filling curves;

Fig.8 (Fig.8A to Fig.8D) shows an example of how the grid counting
dimension is calculated;
30

Fig.9 (Fig.9A and Fig.9B) shows an example of how the box counting dimension is calculated.

5 Detailed Description of the Embodiments

Fig.1 shows an embodiment of a package 1 including an antenna 100 in an area 101 and a circuit 130. Both, the antenna 100 and the circuit 130 are arranged on a substrate 102. Preferably, there is no ground plane underneath the antenna 100,
10 i.e. the area 101 is free of any conductive material, at least in 50% of the surface above or below area 101. Particularly, the only metal that is placed below or above the antenna pattern are the connectors (such as for instance wire bonds or metal strips).

The antenna 100 is a monopole antenna with a single radiating arm
15 comprising seven segments 111 through 117. Preferably, the side length of the rectangular area 101 is the longest operating wavelength for the antenna divided by five. The antenna 100 forms at least two angles such as angle 121 and angle 122 being less than 115° . Although not required, it is preferred that at least two of the angles that are less than 180° are defined in the clock-wise and counter clock-
20 wise directions at the opposite sides of the curve (right side for 121, left for 122). The antenna curve 100 is fed through a connection 105 to a pad on the circuit 130, such a connection including, but not limited to, a wire bond.

The circuit 130 preferably is embodied as a radio-frequency circuit (RF circuit).
25 The antenna 100 is connected to the RF circuit 130, transferring the unbalanced signal of the antenna 100 to the RF circuit 130. The RF circuit 130 can be connected to the ground plane of the antenna 100. The RF circuit provides some RF functionality needed in an RF front-end, like e.g. antenna impedance matching, unbalanced-to-balanced transformation, power amplifying, filtering,
30 mixing, frequency conversion, etc.

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The output connection of the RF circuit 130, as represented in the embodiment can be a balanced device. Optionally, the RF circuit 130 comprises a connection to a "0" level reference.

Alternatively, the output connection of the RF circuit 130 can be
5 unbalanced. In such case the common ground "GND" is an input signal for the RF circuit 130.

The RF circuit 130 is connected to the monopole antenna 100 and comprises optional connections to terminals like common ground "GND", 108 "0", 107 "+"
10 and/or 109 "-".

Fig.2 shows an embodiment of a package 2 including the antenna 100 in an area 201 and a radio-frequency circuit (RF circuit) 230 together with a base band
15 component 240 arranged on a substrate 202.

The antenna 100 has been described in Fig.1 above. It comprises seven segments 111 through 117 and forms at least two angles 121 and 122 being less than 115°. The antenna 100 is connected to the RF circuit 230 by a connection 205.
20

The RF circuit 230 and the base band component 240 are connected to the ground connector GND. The base band component 240 is connected to the terminals "+" 207, "0" 208 and "-" 209.

25 The base band component 240 provides at least some of the base band functionality required in the system, like for example conversion from a digital bitstream to a sequence of symbols, symbol acquisition, digital data regeneration, clock recovery, symbol synchronization, automatic gain control, error correction algorithms, data encryption and/or decryption, channel estimation for adaptive
30 detection, analog-to-digital conversion, etc.

The RF circuit 230 performs at least some of the RF functionality needed in an RF front-end, like for example antenna impedance matching, balanced-to-unbalanced transformation, power amplifying, filtering, mixing, frequency conversion, etc.

5

Fig.3 shows an embodiment of a package 3 including a dipole antenna 300 and a radio-frequency circuit 330. An external circuit 350 is located outside the package 3. The dipole antenna 300 comprises two radiating arms 303 and 304 and is fed by a differential input/output terminal 305, which is provided by a couple of close connectors such as for instance two wire bonds. Other suitable feeding means could include two conducting strips placed on the same layer as the antenna, the two strips reaching directly or by means of a via hole, the solder balls of a flip-chip, or the pad connection region of a flip-chip connected by means of tape automatic bonding (TAB).

15

A substrate 302 can be embodied as a single layer or a multilayer, but in any case it leaves a clearance with no conducting material of at least 50% of the area 301 where the antenna is enclosed, in any of the layers above or below the layer on which the antenna is lying.

20

The antenna 300 is connected to the RF circuit 330, transferring the balanced signal to the RF circuit 330. The RF circuit 330 can be connected to ground. The RF circuit 330 performs at least some of the RF functionality needed in an RF front-end, like for example antenna impedance matching, balanced-to-unbalanced transformation, power amplifying, filtering, mixing, frequency conversion, etc.

25

The output signal 331 of the RF circuit 330 is unbalanced, and afterwards connected to an external circuit 350, which can be an external chip.

Alternatively, the output connection 331 of the RF circuit 330 can be balanced. In such case, two connections to different pins (two pins instead of one pin 331) of

30

the package, preferably labeled as “+” and “-” are necessary, with the option of the presence of a third pin being the “0” level reference.

5 **Fig.4** shows an embodiment of a package 4 including a (unbalanced) monopole antenna 100 (as described in Fig.1) and an RF circuit 430, both connected to an external RF circuit 450, which is located outside the package 4.

10 A substrate 402 can be arranged as a single layer or a multilayer, but in any case it leaves a clearance with no conducting material of at least 50% of the area 401 where the antenna is enclosed, in any of the layers above or below the layer on which the antenna is lying.

15 The antenna 100 and the RF circuit 430 are connected to at least one Input/Output connector (which can be a pin) of the package 4, respectively, i.e. pin 431 for the antenna 100 and pin 432 for the RF circuit 430. An interconnection between the antenna 100 and the RF circuit 430 is provided by the external RF circuit 450, which is preferably another RF (sub-)circuit external to the package. Preferably, the external RF circuit 450 can be a matching network, a bypass or a through-
20 connection.

25 The RF circuit 430 could also be connected to the antenna 100, hence performing at least some RF functionality needed in an RF front-end. The external RF circuit 450 provides additional RF functionality, e.g. it could be a short circuit that establishes direct electrical contact between antenna 100 and RF circuit 430.

30 As indicated by Fig.4, the output between the RF circuit 430 and the external RF circuit 450 (e.g. matching network) is unbalanced, but it could also be balanced instead.

As an alternative, the antenna 100 could be directly connected to the RF circuit 430, which is connected to the external RF circuit 450, which can optionally be a matching network.

5

Fig.5 shows an embodiment of a package 5 including a balanced antenna 300 (as described in Fig.3) and a radio-frequency circuit 530 (RF circuit). An additional circuit 550 is placed outside the package 5.

10 A substrate 502 can be arranged as a single layer or a multilayer, but in any case it leaves a clearance with no conducting material of at least 50% of the area 501 where the antenna is enclosed, in any of the layers above or below the layer on which the antenna is lying.

15 Both arms 303 and 304 of the antenna 300 are connected to a respective terminal of the package 5, i.e. arm 303 is connected to terminal 551 and arm 304 is connected to terminal 552. These terminals 551 and 552 of the package 5 are connected to the external circuit 550. Via terminals 531 and 532 the RF circuit 530 of the package 5 is connected to the circuit 550, whereas the RF circuit 530 is
20 further connected to terminals 533 and 534 of the package 5. These terminals 533 and 534 are the input/output connectors to which an external RF front-end (not shown) can be connected.

This embodiment is similar to what has been described with Fig.3, but the antenna
25 100 being balanced. Preferably, all connections shown in Fig.5 are balanced, although at least some of them could be unbalanced as well.

This embodiment is advantageous to be applied for an external power amplifier (PA), because this amplifier typically is differential (i.e. balanced) in order to
30 enable noise suppression and in order to minimize unnecessary heating-up of the amplifier.

Fig.6 shows an embodiment of a package 6 including a balanced antenna 300 with a reactive loading 610 and 620. The antenna 300 has been described in Fig.3
5 above. The arm 303 is connected to a load 610 and the arm 304 is connected to a load 620. The antenna 300 is connected via connection 606 (for arm 303) and connection 605 (for arm 304) with an RF circuit 630, which is also attached to the package 6 onto the substrate 602. The RF circuit 630 is connected to a terminal 632 of the package 6 to which also a chip 650 is attached. Furthermore, the RF
10 circuit 630 is connected to a terminal 631.

The reactive loads 610 and/or 620 could be place at the beginning of the conductive pattern of the antenna or, alternatively, at the end of it. Optionally, the loads 610 and/or 620 can be placed to any intermediate point. Moreover, the
15 reactive loads 610 and/or 620 can be placed outside the package if the necessary connections via terminals of the package 6 are provided.

This scheme of reactive loading is advantageous for further miniaturization purposes of the antenna.

20

Fig.7 shows examples of space filling curves. Filling curves 701 through 714 are examples of prior art space filling curves for antenna designs. Other types of multiband antennas that also feature a reduced size are multilevel antennas as
25 disclosed in WO 01/22528, which herewith is incorporated by reference.

Fig.8 (Fig.8A to Fig.8D) shows an example of how the grid dimension is calculated.

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-20-

The grid dimension of a curve may be calculated as follows: A first grid having square cells of length L1 is positioned over the geometry of the curve, such that the grid completely covers the curve. The number of cells (N1) in the first grid that enclose at least a portion of the curve are counted. Next, a second grid having square cells of length L2 is similarly positioned to completely cover the geometry of the curve, and the number of cells (N2) in the second grid that enclose at least a portion of the curve are counted. In addition, the first and second grids should be positioned within a minimum rectangular area enclosing the curve, such that no entire row or column on the perimeter of one of the grids fails to enclose at least a portion of the curve. The first grid preferably includes at least twenty-five cells, and the second grid preferably includes four times the number of cells as the first grid. Thus, the length (L2) of each square cell in the second grid should be one-half the length (L1) of each square cell in the first grid. The grid dimension (Dg) may then be calculated with the following equation:

$$D_g = -\frac{\log(N2) - \log(N1)}{\log(L2) - \log(L1)}.$$

For the purposes of this application, the term grid dimension curve is used to describe a curve geometry having a grid dimension that is greater than one (1). The larger the grid dimension, the higher the degree of miniaturization that may be achieved by the grid dimension curve in terms of an antenna operating at a specific frequency or wavelength. In addition, a grid dimension curve may, in some cases, also meet the requirements of a space-filling curve, as defined above. Therefore, for the purposes of this application a space-filling curve is one type of grid dimension curve.

25

Fig.8A shows an example two-dimensional antenna 800 forming a grid dimension curve with a grid dimension of approximately two (2). **Fig.8B** shows the antenna 800 of Fig.8A enclosed in a first grid 801 having thirty-two (32) square cells, each with a length L1. **Fig.8C** shows the same antenna 800 enclosed in a second grid 802 having one hundred twenty-eight (128) square cells, each with a length L2.

30

The length (L1) of each square cell in the first grid 801 is twice the length (L2) of each square cell in the second grid 802 ($L2 = 2 \times L1$). An examination of Fig.8A and Fig.8B reveal that at least a portion of the antenna 800 is enclosed within every square cell in both the first and second grids 801, 802. Therefore, the value of N1 in the above grid dimension (Dg) equation is thirty-two (32) (i.e., the total number of cells in the first grid 801), and the value of N2 is one hundred twenty-eight (128) (i.e., the total number of cells in the second grid 802). Using the above equation, the grid dimension of the antenna 800 may be calculated as follows:

$$D_g = -\frac{\log(128) - \log(32)}{\log(2 \times L1) - \log(L1)} = 2$$

10

For a more accurate calculation of the grid dimension, the number of square cells may be increased up to a maximum amount. The maximum number of cells in a grid is dependant upon the resolution of the curve. As the number of cells approaches the maximum, the grid dimension calculation becomes more accurate. If a grid having more than the maximum number of cells is selected, however, then the accuracy of the grid dimension calculation begins to decrease. Typically, the maximum number of cells in a grid is one thousand (1000).

For example, **Fig.8D** shows the same antenna 800 enclosed in a third grid 803 with five hundred twelve (512) square cells, each having a length L3. The length (L3) of the cells in the third grid 803 is one half the length (L2) of the cells in the second grid 802, shown in Fig.8C. As noted above, a portion of the antenna 800 is enclosed within every square cell in the second grid 802, thus the value of N for the second grid 802 is one hundred twenty-eight (128). An examination of Fig.8D, however, reveals that the antenna 800 is enclosed within only five hundred nine (509) of the five hundred twelve (512) cells of the third grid 803. Therefore, the value of N for the third grid 803 is five hundred nine (509). Using Fig.8C and Fig.8D, a more accurate value for the grid dimension (D) of the antenna 800 may be calculated as follows:

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$$D_s = -\frac{\log(509) - \log(128)}{\log(2 \times L2) - \log(L2)} \approx 1.9915$$

Fig.9 (Fig.9A and Fig.9B) shows an alternative example of how the box counting dimension is calculated.

The antenna comprises a conducting pattern, at least a portion of which includes a curve, and the curve comprises at least five segments, each of the at least five segments forming an angle with each adjacent segment in the curve, at least three of the segments being shorter than one-tenth of the longest free-space operating wavelength of the antenna. Each angle between adjacent segments is less than 180° and at least two of the angles between adjacent sections are less than 115°, and wherein at least two of the angles are not equal. The curve fits inside a rectangular area, the longest side of the rectangular area being shorter than one-fifth of the longest free-space operating wavelength of the antenna.

One of the advantages of the package arrangements of the present invention is that they allow a high package density including the antenna. In some embodiments the antenna can be fitted in a rectangular area, the longest edge of which is shorter than one-twentieth of the longest free-space operating wavelength of the antenna. Alternatively, the arrangement of the package in terms of layout, antenna and chip arrangement allows the whole package to be smaller than one-twentieth of the free-space operating wavelength.

One aspect of the present invention is the box-counting dimension of the curve that forms at least a portion of the antenna. For a given geometry lying on a surface, the box-counting dimension is computed in the following way: First a grid with boxes of size L1 is placed over the geometry, such that the grid completely covers the geometry, and the number of boxes N1 that include at least a point of the geometry are counted; secondly a grid with boxes of size L2 (L2

-23-

being smaller than L1) is also placed over the geometry, such that the grid completely covers the geometry, and the number of boxes N2 that include at least a point of the geometry are counted again. The box-counting dimension D is then computed as:

$$D = -\frac{\log(N2) - \log(N1)}{\log(L2) - \log(L1)}$$

In terms of the present invention, the box-counting dimension is computed by placing the first and second grids inside the minimum rectangular area enclosing the curve of the antenna and applying the above algorithm.

10

The first grid should be chosen such that the rectangular area is meshed in an array of at least 5 x 5 boxes or cells, and the second grid is chosen such that L2 = 1/2 L and such that the second grid includes at least 10 x 10 boxes. By the minimum rectangular area it will be understood such area wherein there is not an entire row or column on the perimeter of the grid that does not contain any piece of the curve. Thus, some of the embodiments of the present invention will feature a box-counting dimension larger than 1.17, and in those applications where the required degree of miniaturization is higher, the designs will feature a box-counting dimension ranging from 1.5 up to 3, inclusive. For some embodiments, a curve having a box-counting dimension of about 2 is preferred. For very small antennas, that fit for example in a rectangle of maximum size equal to one-twentieth of the longest free-space operating wavelength of the antenna, the box-counting dimension will be necessarily computed with a finer grid. In those cases, the first grid will be taken as a mesh of 10 x 10 equal cells, while the second grid will be taken as a mesh of 20 x 20 equal cells, and then D is computed according to the equation above. In the case of small packages with of planar designs, i.e., designs where the antenna is arranged in a single layer on a package substrate, it is preferred that the dimension of the curve included in the antenna geometry have a value close to D=2.

30

In general, for a given resonant frequency of the antenna, the larger the box-counting dimension the higher the degree of miniaturization that will be achieved by the antenna. One way of enhancing the miniaturization capabilities of the antenna according to the present invention is to arrange the several segments of the curve of the antenna pattern in such a way that the curve intersects at least one point of at least 14 boxes of the first grid with 5 x 5 boxes or cells enclosing the curve. Also, in other embodiments where a high degree of miniaturization is required, the curve crosses at least one of the boxes twice within the 5 x 5 grid, that is, the curve includes two non-adjacent portions inside at least one of the cells or boxes of the grid.

An example of how the box-counting dimension is computed according to the present invention is shown in **Fig.9A** and **Fig.9B**. An example of a curve 900 according to the present invention is placed under a 5x5 grid 901 and under a 10x10 grid 902. As seen in the graph, the curve 900 touches $N_1=25$ boxes in grid 901 while it touches $N_2=78$ boxes in grid 902. In this case the size of the boxes in grid 901 is twice the size of the boxes in 902. By applying the equation above it is found that the box-counting dimension of curve 902 is, according to the present invention, equal to $D=1.6415$. This example also meets some other characteristic aspects of some preferred embodiments within the present invention. The curve 900 crosses more than 14 of the 25 boxes in grid 901, and also the curve crosses at least one box twice, that is, at least one box contains two non adjacent segments of the curve. In fact, 900 is an example where such a double crossing occurs in 13 boxes out of the 25 in 901.

The package arrangements in which the antenna is built on a single layer of a package substrate are very convenient in terms of cost because a single mask can be used for processing the antenna pattern on such a layer. In some embodiments the antenna is arranged in a single layer and fed in one tip of the curve, such that no conductor crossing over the curve is required. Although not required, a further simplification and cost reduction is achieved by means of those embodiments in

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the present invention wherein the antenna and the chip are mounted on the same layer of a package substrate.

It is noted that, according to the present invention, the antenna structure is not
5 limited to a planar structure, because the package can include several portions or parts of the antenna in multiple layers or components of the package.

In the case of non-planar, multi-layer or volumetric structures for the antenna pattern within the package, the box-counting algorithm can be computed by
10 means of a three-dimensional grid, using parallelepiped cells instead of rectangular and meshes with 5 x 5 x 5 cells and 10 x 10 x 10 or 20 x 20 x 20 cells, respectively. In those cases, such a curve can take a dimension larger than two and in some cases, up to three.

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Claims:

1. System comprising
 - at least one antenna,
 - 5 – a circuit, wherein the circuit is at least in part not a semiconductor chip,
 - wherein the at least one antenna and the circuit are arranged on a package.
2. System comprising
 - at least one antenna,
 - 10 – at least one circuit,
 - wherein the at least one antenna and the at least one circuit are arranged on a package,
 - wherein at least one circuit performs a base-band functionality.
- 15 3. System comprising
 - at least one antenna,
 - at least one circuit,
 - wherein the at least one antenna and the at least one circuit are arranged on a package.
 - 20 – wherein at least one circuit performs a digital functionality.
4. System according to one of the previous claims, wherein the circuit comprises a radio-frequency circuit.
- 25 5. System according to claim 4, wherein a coupling between the antenna and the radio-frequency circuit is a reactive coupling.
6. System according to one of the claims 4 or 5, wherein the radio-frequency circuit is connected to a ground plane.

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7. System according to one of the claims 4 to 6, wherein at least some of the connections of the radio-frequency circuit are balanced
8. System according to one of the previous claims, comprising a radio-
5 frequency component outside the package.
9. System according to claim 8, wherein the radio-frequency component outside the package is a matching network.
- 10 10. System according to claim 8, wherein radio-frequency component outside the package is a bypass or a through-connection.
11. System according to one of the claims 8 to 10, wherein the radio-frequency component outside the package comprises a power amplifier.
- 15 12. System according to one of the claims 4 to 7 and one of the claims 8 to 11, wherein the at least one antenna is connected to the radio-frequency circuit and at least a part of this radio-frequency circuit is connected to the radio-frequency component outside the package.
- 20 13. System according to one of the claims 4 to 7 and one of the claims 8 to 11, wherein the at least one antenna is connected to the radio-frequency component outside the package.
- 25 14. System according to one of the claims 4 to 13, wherein the radio-frequency circuit comprises a balun.
15. System according to claim 14, wherein the balun is a printed circuit.
- 30 16. System according to claim 14, wherein the balun is a discrete component.

17. System according to one of the previous claims, wherein no ground plane is located underneath or on top of the at least one antenna.
18. System according to one of the previous claims, wherein the package is an integrated circuit (IC) package.
19. System according to one of the previous claims, wherein the at least one antenna is connected to an input/output connector of the package and at least a part of the circuit is connected to an input/output connector of the package.
20. System according to one of the previous claims, wherein the antenna is a space filling antenna.
21. System according to claim 20, wherein the space filling antenna has a dimension bigger than 1.
22. System according to claim 21, wherein the dimension is computed as a grid dimension or a box counting dimension.
23. System according to one of the previous claims, wherein the antenna comprises
- a conducting pattern, at least a portion of which includes a curve,
 - wherein said curve comprises
 - at least five segments,
 - each of said at least five segments forming a pair of angles with each adjacent segment in said curve,
 - at least three of said segments being shorter than one-tenth of the longest free-space operating wavelength of said antenna.
24. System according to claim 23, wherein the smaller angle of the pair of angles between adjacent segments is less than 180° and at least two of said smaller

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angles between adjacent section segments are less than 115° , wherein at least two of the angles, which are on the same side of the curve and are formed from adjacent segments of the group of said at least five segments, are different.

5

25. System according to claim 24, wherein said conducting pattern fits inside a rectangular area, the longest side of said rectangular area being shorter than one-fifth of the longest free-space operating wavelength of said antenna.

10 26. System according to one of the previous claims, wherein at least the antenna and/or the radio-frequency circuit comprise(s) a connection with a radio-frequency input/output connector.

15 27. System according to one of the previous claims, wherein the antenna is a modular or a discrete component.

28. System according to claim 27, wherein the modular or discrete component is a surface mount technique (SMT) component.

20 29. System according to one of the previous claims, wherein both ends of the antenna are connected to the package.

30. System according to claim 29, wherein at least on end of the antenna is connected to an Input/Output connector of the package.

25

31. System according to claim 29, wherein both ends of the antenna are connected to Input/Output connectors of the package.

30 32. System according to one of the previous claims, wherein the antenna has a parasitic element.

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33. System according to claim 32, wherein the parasitic element is inside the package.
34. System according to claim 32, wherein the parasitic element is outside the package.
35. System according to one of the previous claims comprising at least one external antenna.
36. System according to claim 35 comprising a switch.
37. System according to claims 35 or 36 comprising at least a switch outside or on the package.
38. System according to claims 36 or 37, wherein the switch commutes between the at least one (internal) antenna and the at least one external antenna.
39. System according to one of the previous claims, wherein the at least one antenna is not physically connected to any other component.
40. System according to one of the previous claims, wherein the antenna is a balanced antenna.
41. System according to one of the previous claims, wherein the antenna is an unbalanced antenna.
42. System according to one of the previous claims, wherein the antenna is loaded with discrete reactive components.
43. System according to claim 42, wherein the antenna is loaded with external loads.

44. System according to one of the previous claims, wherein the radio-frequency circuit or the radio-frequency component includes at least one filter.
- 5 45. System comprising several systems according to one of the previous claims, wherein the antennas are forming a multiple antenna communication system.
46. System according to claim 45, wherein the multiple antenna communication system is a multiple-input-multiple-output system, a smart antenna system, a
10 phased array system or a sensor network.

Fig.1

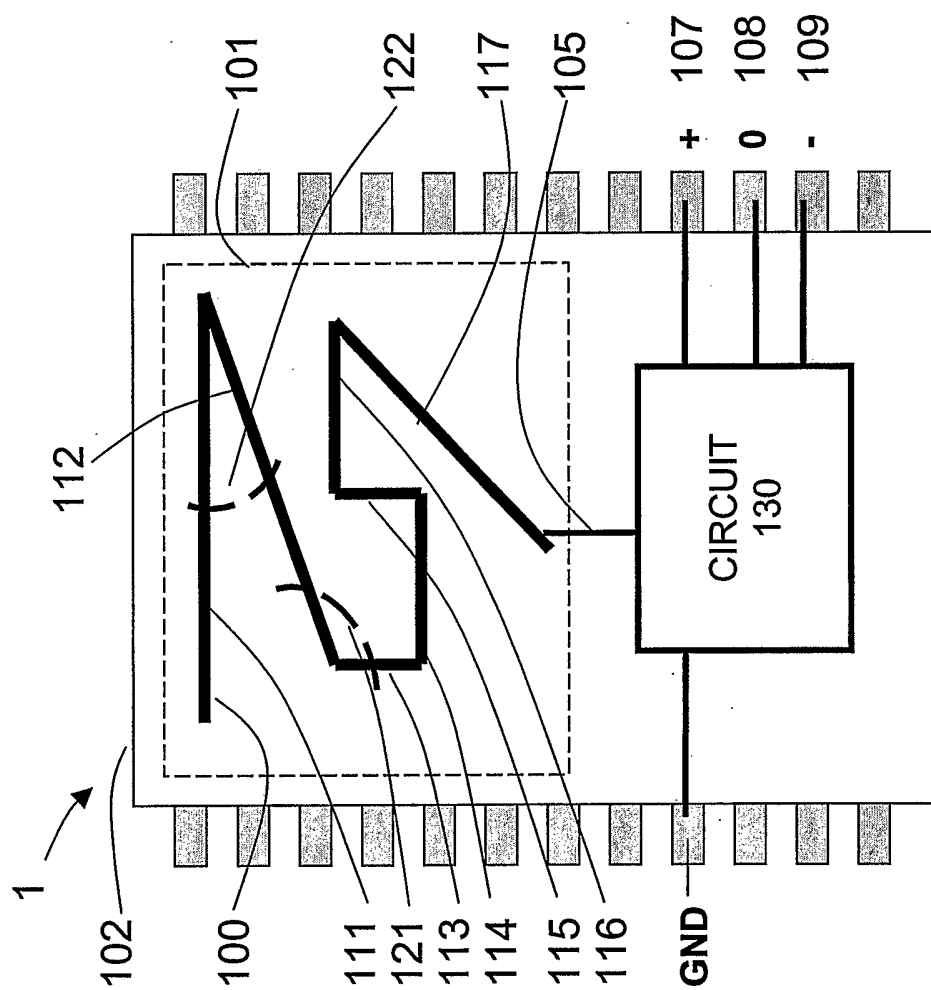
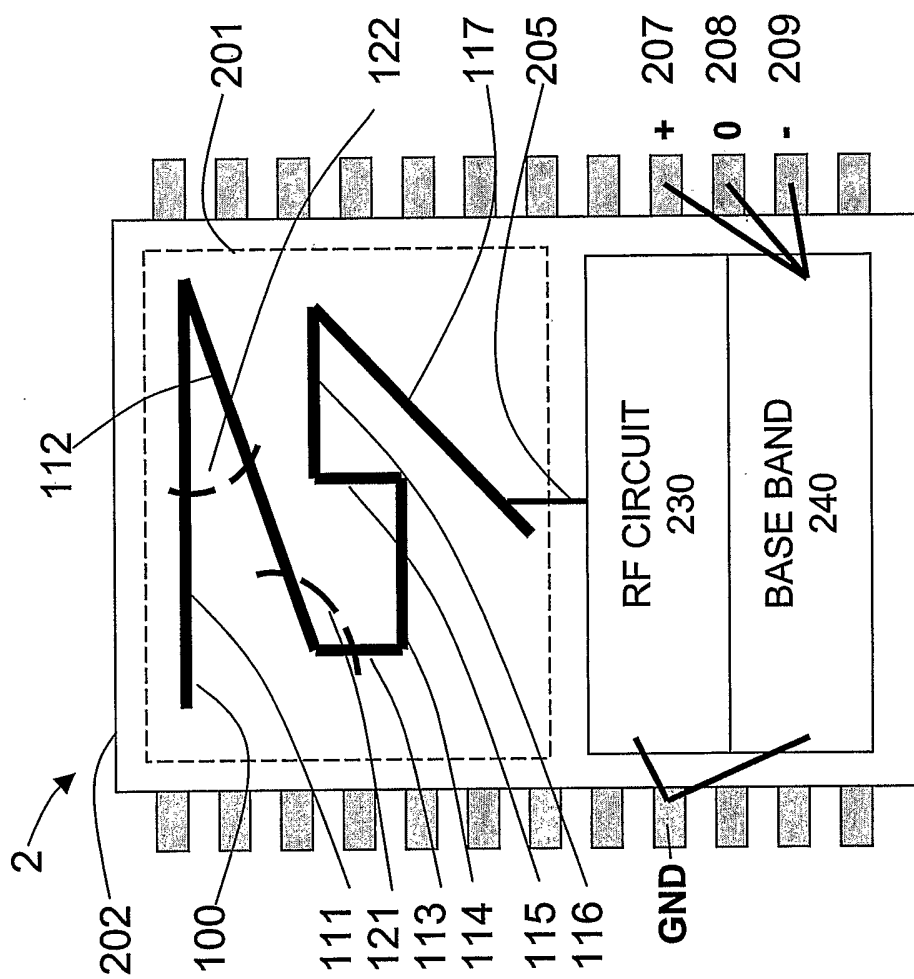
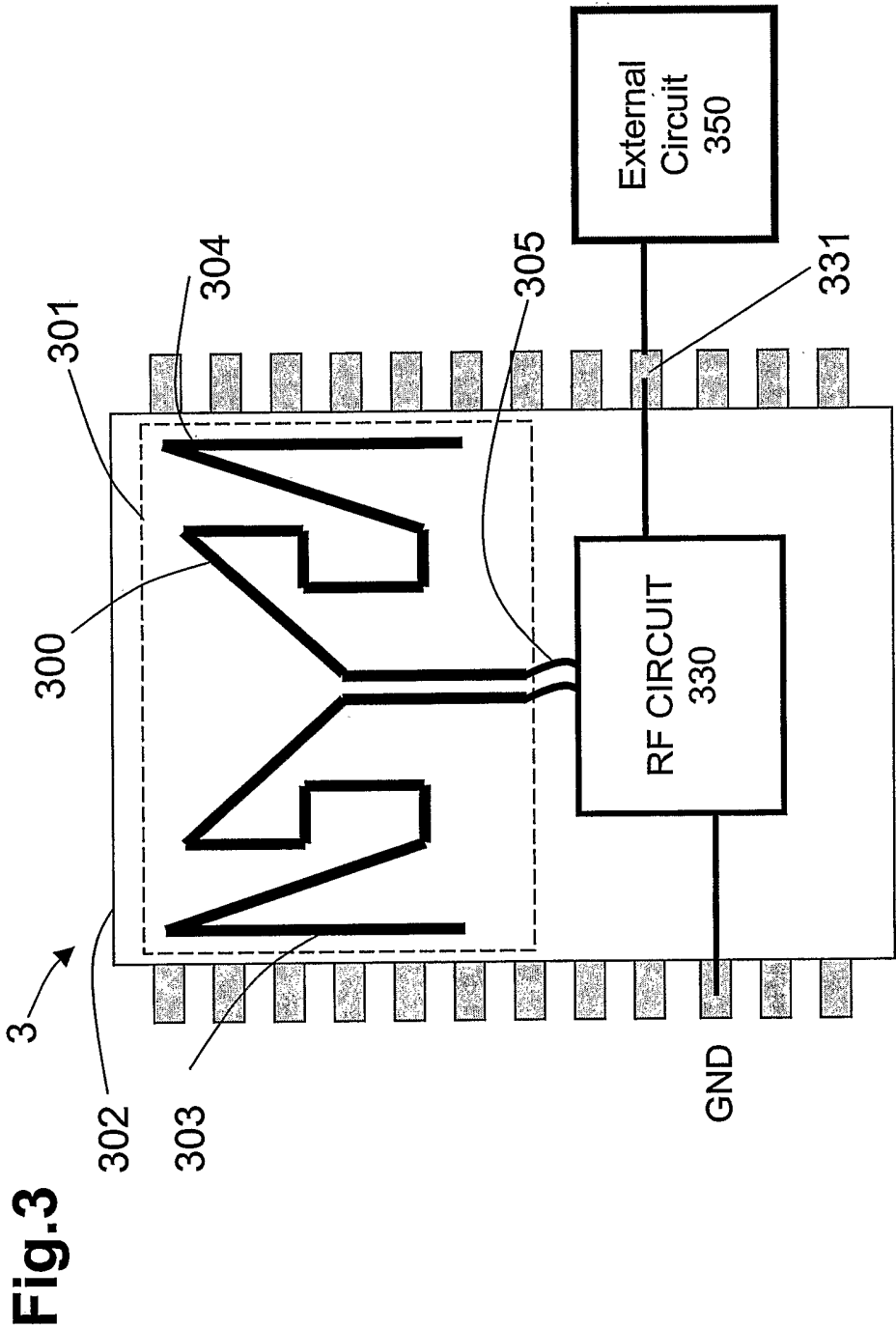


Fig. 2





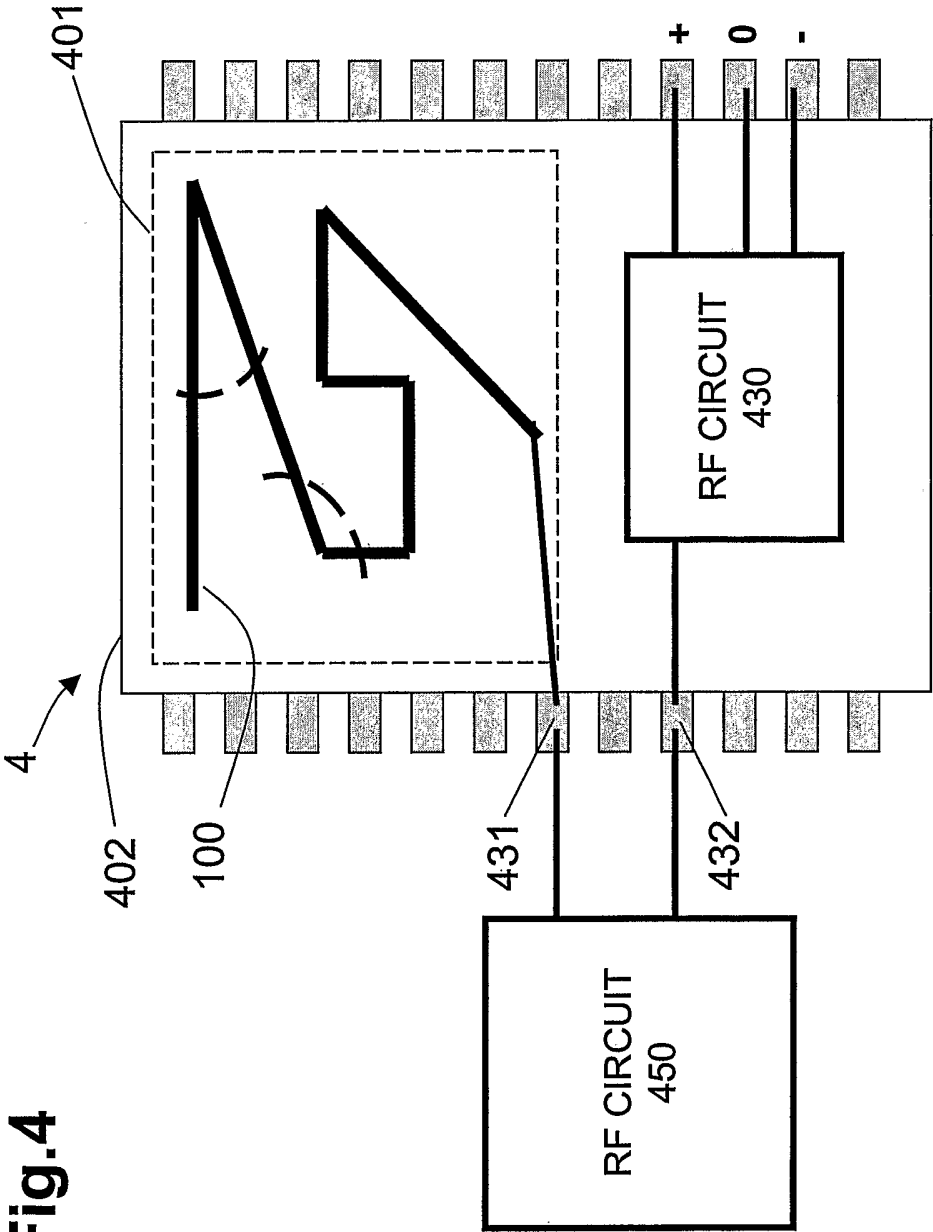
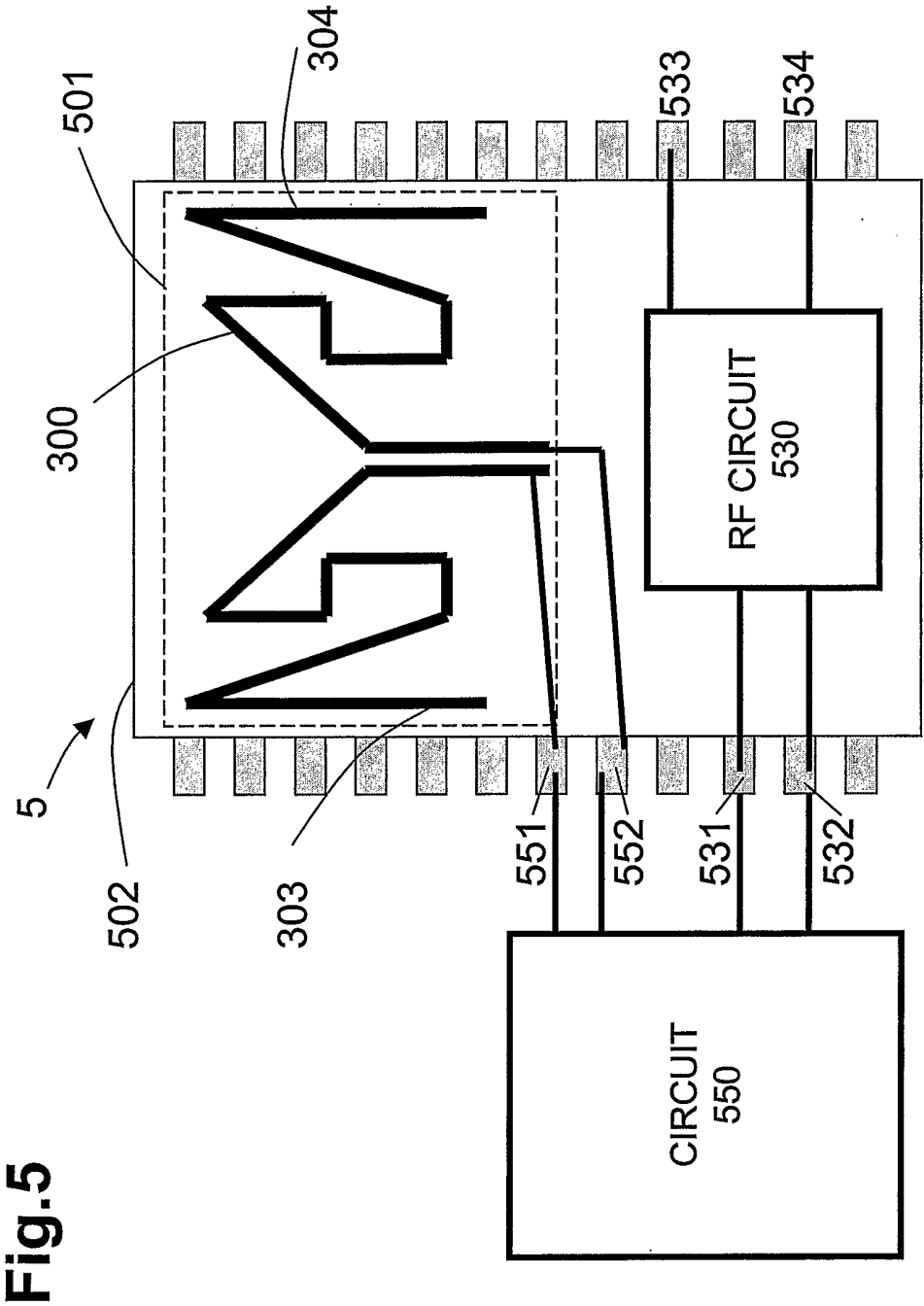
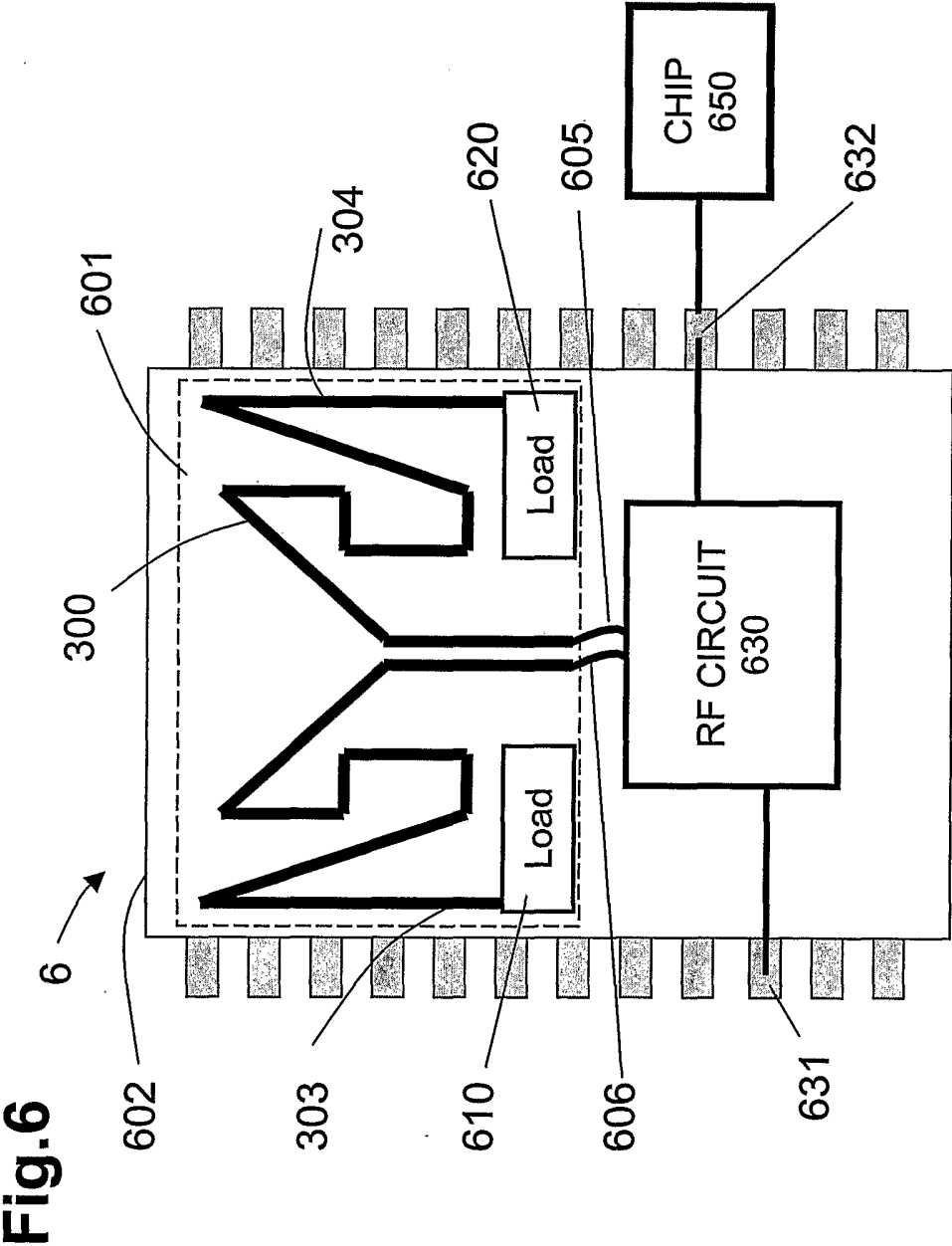


Fig.4





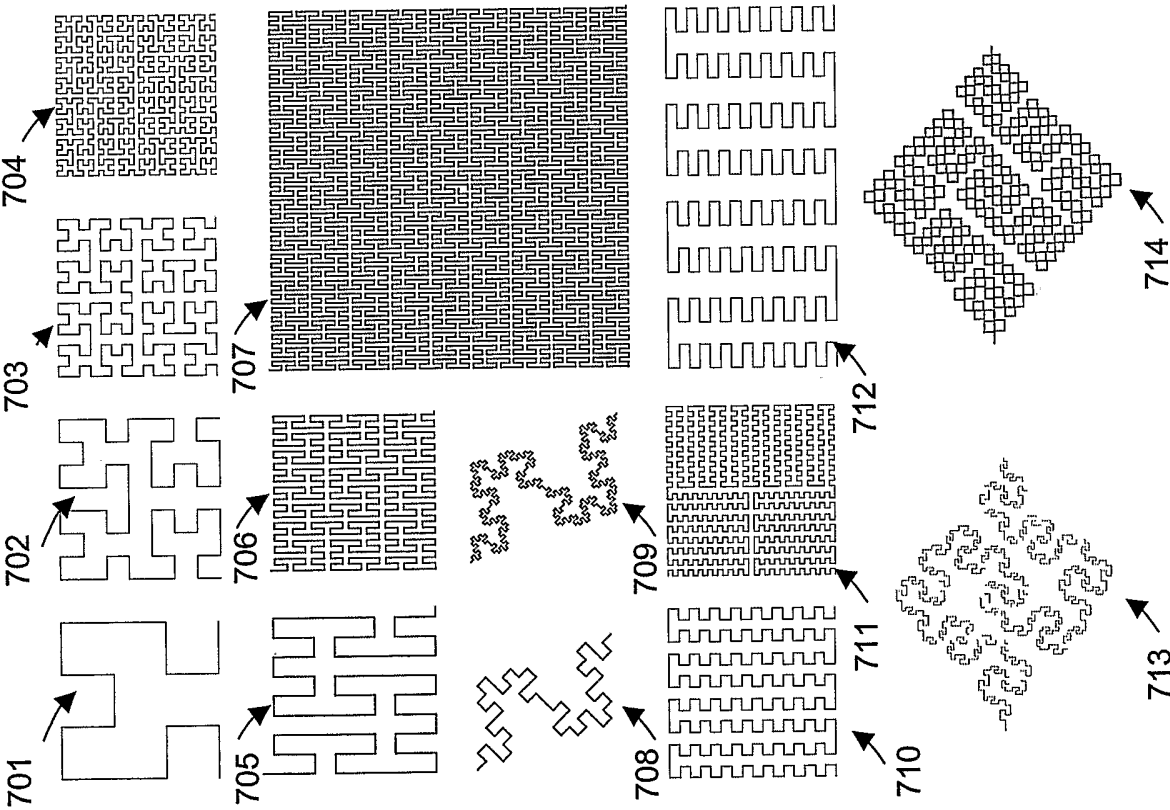


Fig. 7

Fig.8B

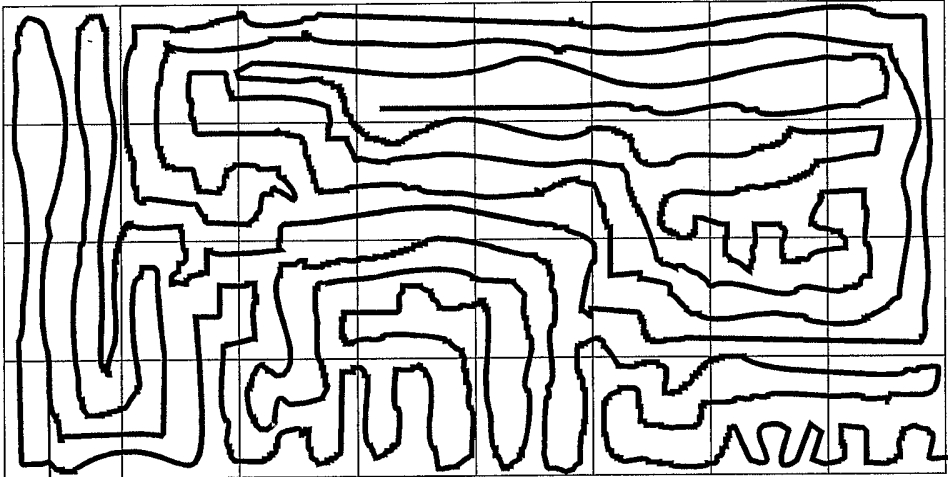


Fig.8A

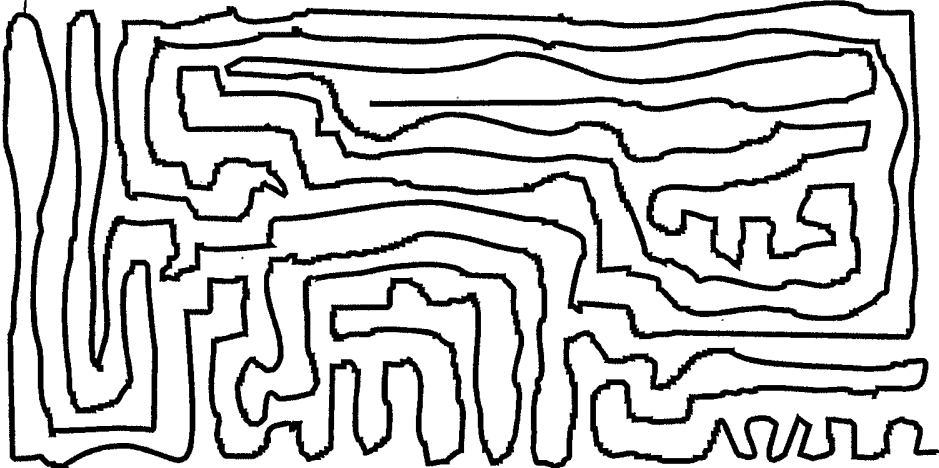


Fig.8D

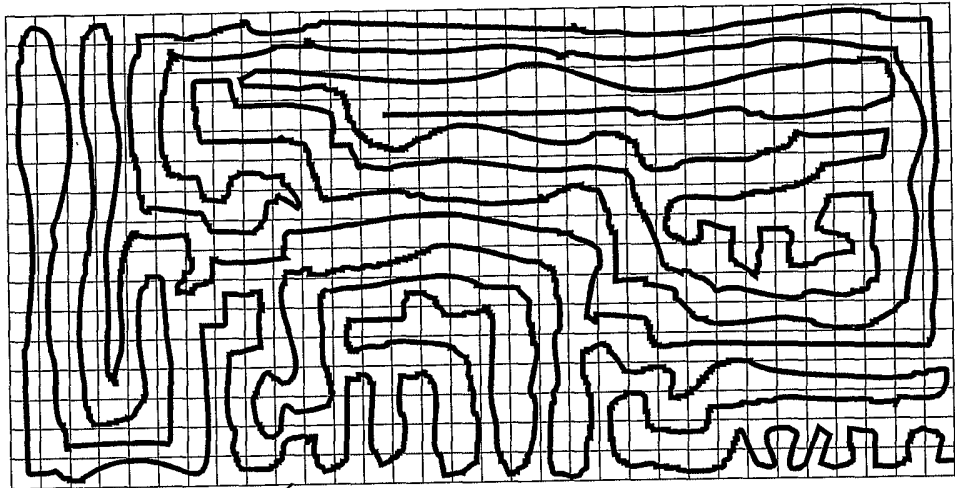
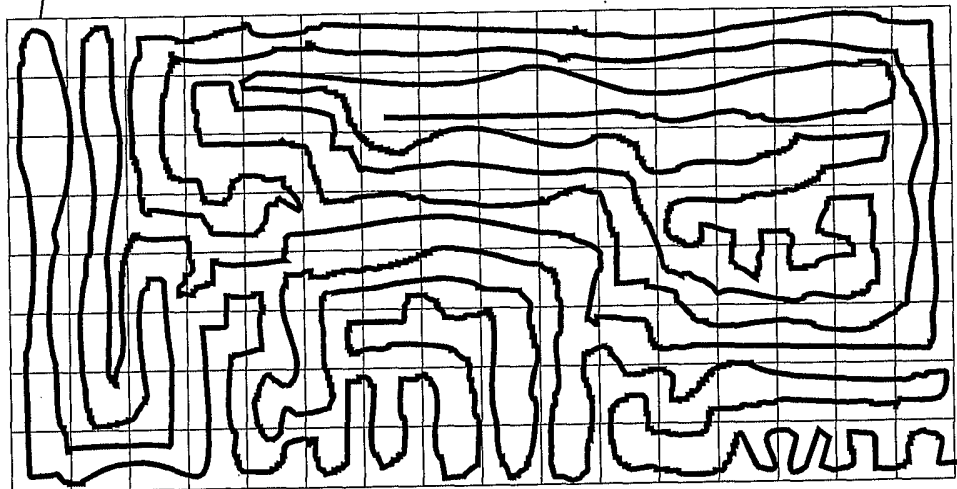


Fig.8C



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Fig.9B

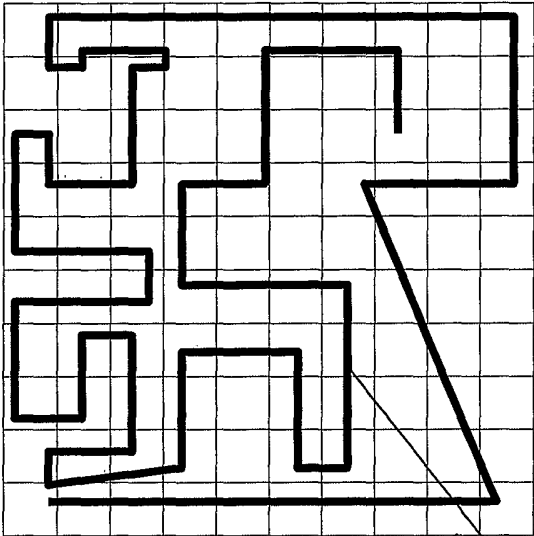
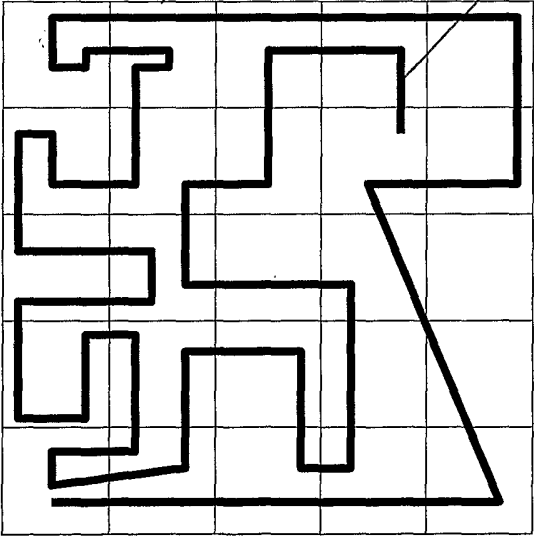


Fig.9A



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INTERNATIONAL SEARCH REPORT

International Application No

PCT/EP2004/004851

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 G06K19/073 H01L23/66 H01Q1/36

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 G06K H01L H01Q

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, PAJ

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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Y		20-25, 45, 46
Y	column 4, line 37 - column 9, line 53 -----	36, 37
Y	WO 01/54225 A (FRACTUS S A ; ANGUERA PROS JAIME (ES); PUENTE BALIARDA CARLES (ES); RO) 26 July 2001 (2001-07-26) column 9, line 11 - column 11, line 18 -----	20-25, 45, 46
Y	US 2004/014428 A1 (FRANCA-NETO LUIZ M) 22 January 2004 (2004-01-22) paragraph '0015! - paragraph '0019! ----- -/--	36, 37

☒ Further documents are listed in the continuation of box C.☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

9 December 2004

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Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

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Geiger, J-W

INTERNATIONAL SEARCH REPORT

International Application No

PCT/EP2004/004851

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