Homework 4

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1. (a) Let us assume the diode is in forward bias. In this case, the circuit consists simply of the source and resistor, which gives us current:

$$I = \frac{v_{in}}{R}$$

Given that this value is sinusoidal, when greater than zero, we know that our initial assumption was true. When the voltage is zero or negative, the ideal diode is reverse-biased. We can now proceed to say:

$$v_o = \begin{cases} v_{in}, & v_{in} > 0 \\ 0, & v_{in} \le 0 \end{cases}$$

Given that the given equation is:

$$v_{in} = 10\sin(200\pi t)$$

we know that v_{in} is positive when $2n\pi \le 200\pi t \le (2n+1)\pi$, with $n=0,1,2\cdots$. This gives: $(n/100) \le t \le (2n+1)/200$, which we can use to plot the transfer function (v_o/v_{in}) :

$$H(t) = \frac{v_o}{v_{in}} = \begin{cases} 1, & (n/100) \le t \le (2n+1)/200 \\ 0, & \text{otherwise} \end{cases}$$

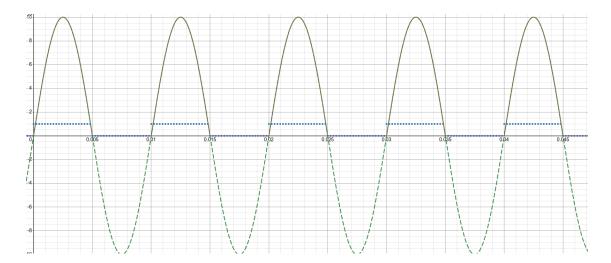


Figure 1: H(t) (blue), v_{in} (green), and v_o (red) in Time Domain

Plotting v_o versus v_{in} , we find a linear relationship:

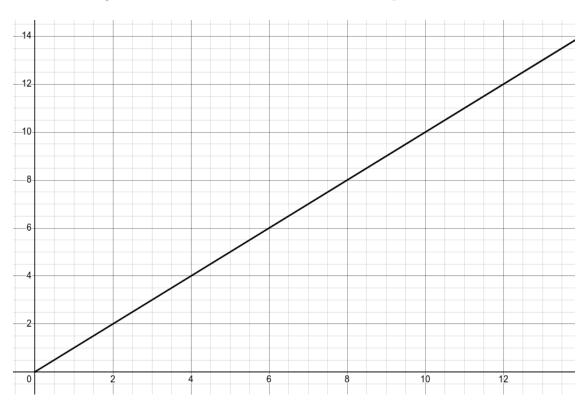


Figure 2: v_o versus v_{in} (1:1 relationship)

(b) Similar to part (a), let us assume this diode is forward biased. In this case, we have the same current flow, indicating that this assumption is correct; however, the cycle is reversed in that v_o is zero when the diode is forward-biased, and $v_o = v_{in}$ when it is reverse biased. Thus, we may write this as:

$$v_o = \begin{cases} v_{in}, & v_{in} \leq 0 \\ 0, & v_{in} > 0 \end{cases}$$

$$H(t) = \frac{v_o}{v_{in}} = \begin{cases} 0, & (n/100) \leq t \leq (2n+1)/200 \\ 1, & \text{otherwise} \end{cases}$$

This gives us the following plot:

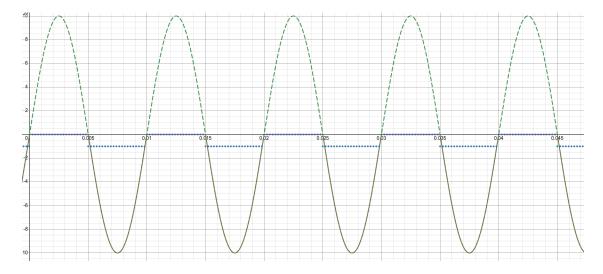


Figure 3: H(t) (blue), v_{in} (green), and v_o (red) in Time Domain

Plotting v_o versus v_{in} , we find a linear relationship:

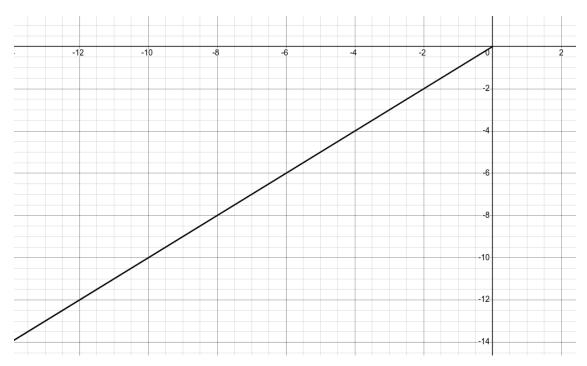


Figure 4: v_o versus v_{in} (1:-1 relationship)

(c) Using a non-ideal, constant voltage drop (CVD) model, we know that, since there is one diode in each circuit, the output will be .7[V] less for a forward-biased diode. For circuit 1, this gives us:

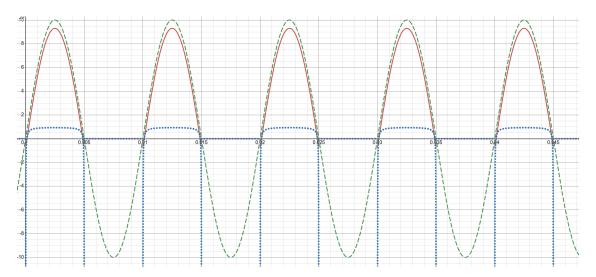


Figure 5: H(t) (blue), v_{in} (green), and v_o (red) in Time Domain

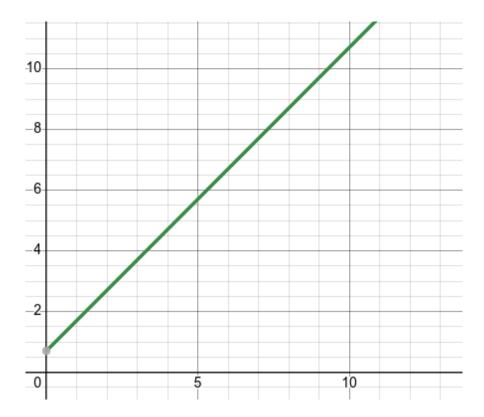


Figure 6: v_o versus v_{in}

Since the voltage was, initially, just zero when the diode was forward-biased (in the ideal case), with CVD we get:

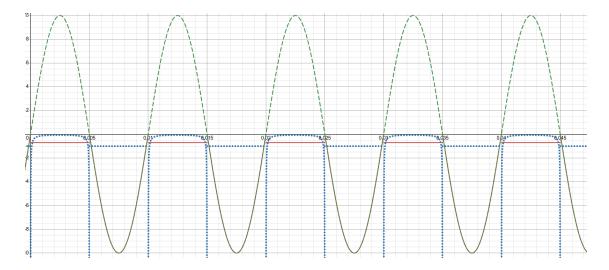


Figure 7: H(t) (blue), v_{in} (green), and v_o (red) in Time Domain

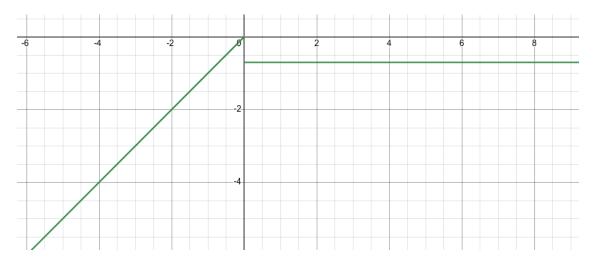


Figure 8: H(t) (blue), v_{in} (green), and v_o (red) in Time Domain

2. (a) We begin by finding the maximum voltage value of the rectifier. Since we know the peak-to-peak ripple, we find the extrema:

$$V_{ext} = V_{avg} \pm \frac{V_{pp}}{2}$$
$$V_{ext} = 9 \pm 1$$

Thus, we see the minimum load voltage is 8[V], with:

$$V_{max} = 10[V]$$

(b) We know that the peak secondary voltage must be 10[V]. Given this, we can write the turns ratio as (note we need to convert to RMS value):

$$n = \frac{N_1}{N_2} = \frac{V_1}{V_2}$$
$$n = \frac{220}{10\sqrt{2}}$$
$$n = 15.6$$

(c) We can write the equation for capacitance as:

$$C = \frac{I_L T}{V_r}$$

$$C = \frac{(.1)(.01667)}{2}$$

$$C = .833[\text{mF}]$$

We can now construct the circuit and get:

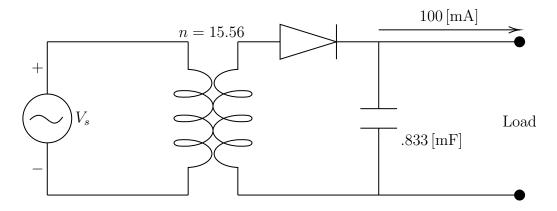


Figure 9: Half-Wave Rectifier Circuit, $V_{max} = 10[V]$

3. (a) We can see that, if the diode is forward-biased, the current through D can be found as (since the AC source can be omitted in the CVD model):

$$I_D = \frac{7 - .7}{5k}$$

$$I_D = 1.26[\text{mA}]$$

The output voltage is simply the drop across the diode, or:

$$V_D = .7[V]$$

Since the sinusoid can not exceed -1[V], we see that the current is always positive, and, therefore, D is always forward-biased.

(b) We may write the Shockley equation as:

$$I_D = I_S \left(e^{\frac{V_D}{nV_T}} - 1 \right)$$

Using the given values, we obtain:

$$I_D = 10^{-14} \left(e^{\frac{V_D}{(.025)}} - 1 \right)$$

Using I_D from part (a), we get:

$$(2 \cdot 10^{10}) (6.3) + 1 = e^{40V_D}$$
$$V_D = \ln[(2 \cdot 10^{10}) (6.3) + 1]$$
$$V_D = .639[V]$$

(c) The dynamic resistance formula may be written as:

$$r_d = \frac{nV_T}{I_D}$$

Which gets us:

$$r_d = \frac{(.025)}{1.26 \cdot 10^{-3}}$$
$$r_d = 19.841[\Omega]$$

This means that, in the small-signal model, the diode acts as a resistor, which means we have a voltage divider. We can find the AC voltage across the diode using:

$$V_{ac} = (7 - .7 + V_s) \frac{19.841}{19.841 + 5000}$$
$$V_{ac} = (.02445 + .0039525\sin(120\pi t))$$

This gets us:

$$V_{ac} = .02445 + .0039525 \sin(120\pi t) [V]$$

Summing the AC and DC components (the DC value would be from the CVD model), we get:

$$V_D = .72445 + (3.953 \cdot 10^{-3}) \sin(120\pi t) [V]$$

4. We may begin by analyzing the circuit response to various values of V_s . Let us begin with the case when $V_s = 0$. Here, D_1 would form an open circuit, which lets us calculate the current:

$$I = \frac{5 - .7}{6k}$$
$$I = .7167[\text{mA}]$$

Thus, we can find V_o :

$$V_o = 5 - 5k(I)$$
$$V_o = 1.4167[V]$$

Here, let us call the node above the single kilo-ohm resistor and ground as V_n . We know that, when $V_s - .7 < V_x$, D_1 remains off, while D_2 is on, so the response remains the same as above (note: $V_x = .7167[V]$ when D_1 is off); however, let us test $V_s - .7 \ge V_n$. In this case, D_2 is on until $V_n < 4.3[V]$, or $V_s < 5[V]$, at which point we can see:

$$V_o = V_s$$

In the case that $V_s \geq 5[V]$, D_2 shuts off, and the output is simply 5[V]. Now that we have the pieces, we may plot the entire transfer function:

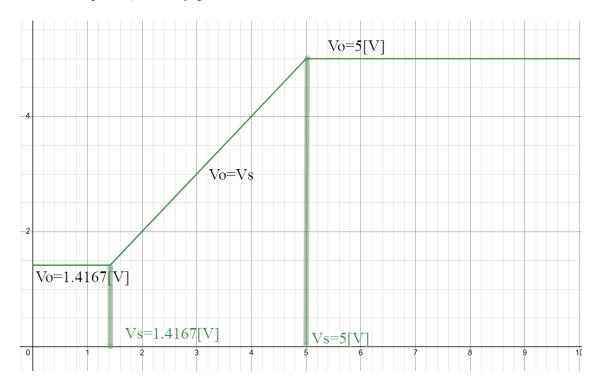


Figure 10: Transfer Characteristics of Given Circuit

5. We begin by generating the schematic:

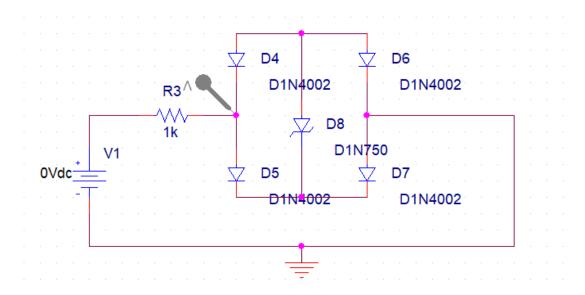


Figure 11: Schematic for DC Sweep

From here, we can simulate with the range $-15 \le V_{in} \le 15$:

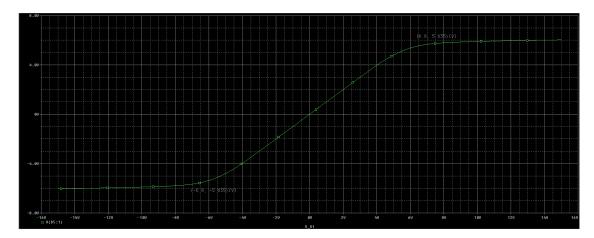


Figure 12: DC Sweep Transfer Characteristics

With the sweep, we may see that the maximum voltage magnitude is approximately 6[V], as expected for the circuit. Furthermore, the knee values occur at, approximately, the voltage value of the zener diode, or $V_z = 6.8[V]$. We can test the same circuit with an AC input:

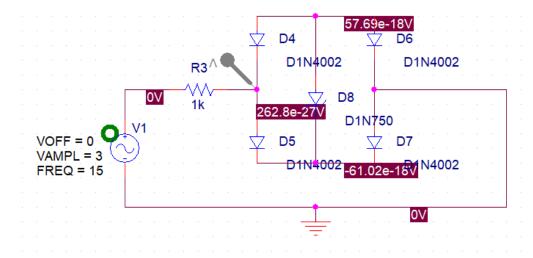


Figure 13: Schematic for AC Sweep

Using this circuit, we obtain the results for a wave with magnitude 3[V] and 12[V]:



Figure 14: Transfer Characteristics for $3[\mathrm{V}]$ Amplitude Input



Figure 15: Transfer Characteristics for 12[V] Amplitude Input

We may note that, for the 3[V] amplitude, the transfer characteristics are a perfect line, with a slope of 1. This is due to the fact that $\pm 3[V]$ is within the permitted voltage range of the diodes; however, the 12[V] amplitude exceeds the $\pm 6[V]$ input range. This causes the curve to become 'S' shaped, where it tapers off as the magnitudes approach 6[V]. Furthermore, note that the knee values occur at the same points, indicating that, for diodes, only the magnitude, and not frequency, of the input make a difference.