

**Lab Three**  
**Fundamentals of Electronics**  
**EECE2412/3**

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### **Abstract**

The purpose of this laboratory experiment is to familiarize ourselves with bipolar junction transistor (BJT)-based amplifiers and the underlying concepts. This includes sensitivity to clipping, the frequency response of the gain, and the construction of a stable amplifier. This is all synthesized to then design a stable amplifier with high gain.

KEYWORDS: BJT, amplifier, clipping, frequency response, gain

## Contents

<b>1 Equipment</b>	<b>4</b>
<b>2 Experimental Procedure</b>	<b>5</b>
2.1 Confirming Active State . . . . .	6
2.2 Calculating Transconductance Gain . . . . .	6
2.3 Calculating the DC Gain ( $\beta_{DC}$ ) . . . . .	6
2.4 Calculating $r_\pi$ . . . . .	6
2.5 Calculating the Voltage Gain . . . . .	7
2.6 Experimentally Obtaining Voltage Gain . . . . .	7
2.7 Output Clipping . . . . .	7
2.7.1 Gain Sensitivity to Supply Voltage . . . . .	7
2.8 Frequency Response of the Gain . . . . .	8
2.9 Stabilizing the Amplifier . . . . .	8
2.10 Constructing A Stable Amplifier . . . . .	8
<b>3</b>	<b>11</b>
<b>4 Conclusion</b>	<b>11</b>

## List of Figures

1 Common Emitter Amplifier with: $R_B = 309[\text{k}\Omega]$ , $R_C = 1[\text{k}\Omega]$ , $C_B = 1.5[\mu\text{F}]$ , $V^+ = 10[\text{V}]$ , and $V_{in} = 10[\text{mV}_{0p}]$ . . . . .	5
2 Constructed Amplifier (Unstable) . . . . .	5
3 Stable BJT Amplifier . . . . .	9
4 Constructed Amplifier . . . . .	9
5 Stable Amplifier, $V^+ = 8[\text{V}]$ . . . . .	10
6 Stable Amplifier, $V^+ = 10[\text{V}]$ . . . . .	10
7 Stable Amplifier, $V^+ = 12[\text{V}]$ . . . . .	11

# **1 Equipment**

Available equipment included:

- 2N3904 Bipolar Junction Transistors
- Basic Circuit Components (Wires, Inductors, Capacitors, etc.)
- Keysight EDU36311A Dual DC Power Supply
- Keysight EDU33212A Function Generator
- Keysight DSOX1204G Digital Oscilloscope
- BNC Cables

## 2 Experimental Procedure

We begin by constructing the following Common-Emitter Amplifier circuit:

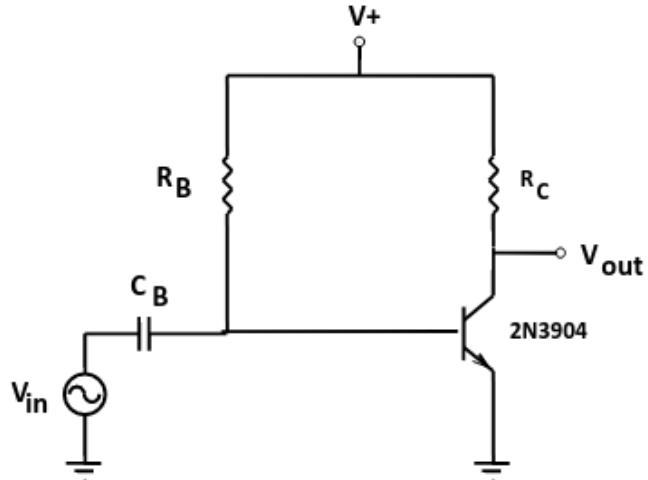


Figure 1: Common Emitter Amplifier with:  $R_B = 309[\text{k}\Omega]$ ,  $R_C = 1[\text{k}\Omega]$ ,  $C_B = 1.5[\mu\text{F}]$ ,  $V^+ = 10[\text{V}]$ , and  $V_{in} = 10[\text{mV}_{0p}]$

Physically, this looked like:

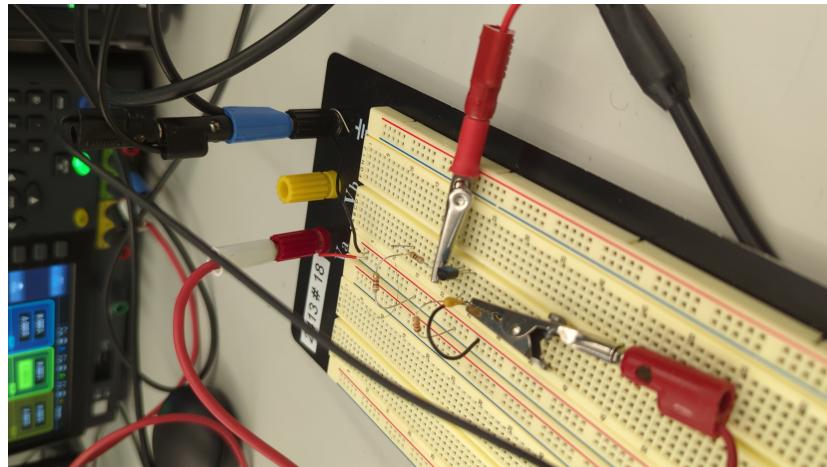


Figure 2: Constructed Amplifier (Unstable)

## 2.1 Confirming Active State

Based on the parameters described in Figure 1, we measure:  $V_{CE} = 2.75[\text{V}]$  and  $V_{BE} = .715[\text{V}]$ . Given that  $V_{CE} > V_{BE}$ , we conclude that the above amplifier is biased in the forward active region.

## 2.2 Calculating Transconductance Gain

We now calculate the collector current as:

$$I_C = \frac{V_{CE} - .7}{1k}$$

$$I_C = \frac{2.75 - .7}{1k}$$

$I_C = 2.05[\text{mA}]$

Since we know that, at room temperature,  $V_T = 26[\text{mV}]$ , we may calculate:

$$g_m = \frac{2.05}{26}$$

$g_m = 78.896[\text{mS}]$

## 2.3 Calculating the DC Gain ( $\beta_{DC}$ )

We may experimentally determine the gain by finding:

$$I_B = \frac{.715 - .7}{1k}$$

$I_B = 15[\mu\text{A}]$

Which gives us:

$$\beta_{DC} = \frac{I_C}{I_B}$$

$$\beta_{DC} = \frac{2.05}{.015}$$

$\beta_{DC} = 136.67$

## 2.4 Calculating $r_\pi$

We may use our obtained values from above to find:

$$r_\pi = \frac{\beta}{g_m}$$

$$r_\pi = \frac{136.67}{.078846}$$

$r_\pi = 1733.4[\Omega]$

## 2.5 Calculating the Voltage Gain

We may obtain the voltage gain using:

$$A_v = -g_m R_C$$
$$A_v = -(0.078846)(1k)$$

$A_v = -78.846$

Note that the measured voltage gain was approximately  $-80$ , which is in line with the calculated gain.

## 2.6 Experimentally Obtaining Voltage Gain

Measuring the input voltage, we find that, zero-to-peak, it is a nominal  $7[mV]$ , while the output was  $560[mV]$ , and phase shifted by  $180^\circ$ . This gives us an experimental gain of:

$$A_v = \frac{-560}{7}$$

$A_v = -80$

When  $r_b = 200[\Omega]$ , the voltage gain meets a slight division, which gives us:

$$A_v = -g_m \left( \frac{r_\pi}{r_b + r_\pi} \right)$$
$$A_v = -(0.78846) \left( \frac{1733.4}{200 + 1733.4} \right)$$

$A_v = -70.69$

We may observe that, in such a case, the voltage gain is slightly reduced.

## 2.7 Output Clipping

Experimentally, we observe clipping at  $.15[V]$  and  $0[V]$ . We may explain the minimum because there is no negative voltage swing with the BJT. In the other hand, there is a maximum because the voltage gain times  $.15[V]$  is greater than the supply voltage (as experienced with operational amplifiers).

### 2.7.1 Gain Sensitivity to Supply Voltage

Changing the supply voltage to  $8[V]$ , we see the voltage gain become:

$$A_v = -\frac{4.8}{.053}$$

$A_v = -90.566$

Changing the input to the  $12[V]$ , we see the gain magnitude increases to:

$$A_v = -\frac{5.6}{.047}$$

$$A_v = -119.15$$

We may determine that the amplifier is sensitive to changes in the supply voltage because the collector current depends on the collector-to-emitter voltage, and the collector-to-emitter voltage, in turn, depends on the supply voltage. Because the transconductance gain of the amplifier depends on the collector current, a change in the collector-to-emitter voltage results in a change in the gain, which depends on the transconductance gain.

## 2.8 Frequency Response of the Gain

We may observe that the upper corner frequency occurs at, approximately,  $f_{crit} = 730[\text{kHz}]$ . On the other hand, the lower corner frequency occurs at, approximately,  $f_{crit} = 14[\text{kHz}]$ . According to these values, though not ideal, this amplifier is best suited for an AM Radio. It can operate at a lower frequency by using a different capacitor value, which we observed by increasing the capacitance value.

## 2.9 Stabilizing the Amplifier

After introducing the changes to the amplifier, we see that the voltage gain is:

$$A_v = -4.7$$

and, thus, it is insensitive to changes in  $V^+$ . As expected, the gain decreased. Calculating the gain, we find that  $A_v = -4$ , which is just a bit lesser in magnitude than the value above. Introducing refrigerant increased the magnitude of the gain to  $A_v = -21$ , with the peak-to-peak output voltage going from  $8.2 \rightarrow 8[\text{V}]$ , and the input voltage remaining at  $.44[\text{V}]$

## 2.10 Constructing A Stable Amplifier

With values derived in the pre-lab, we construct a stable amplifier as follows:

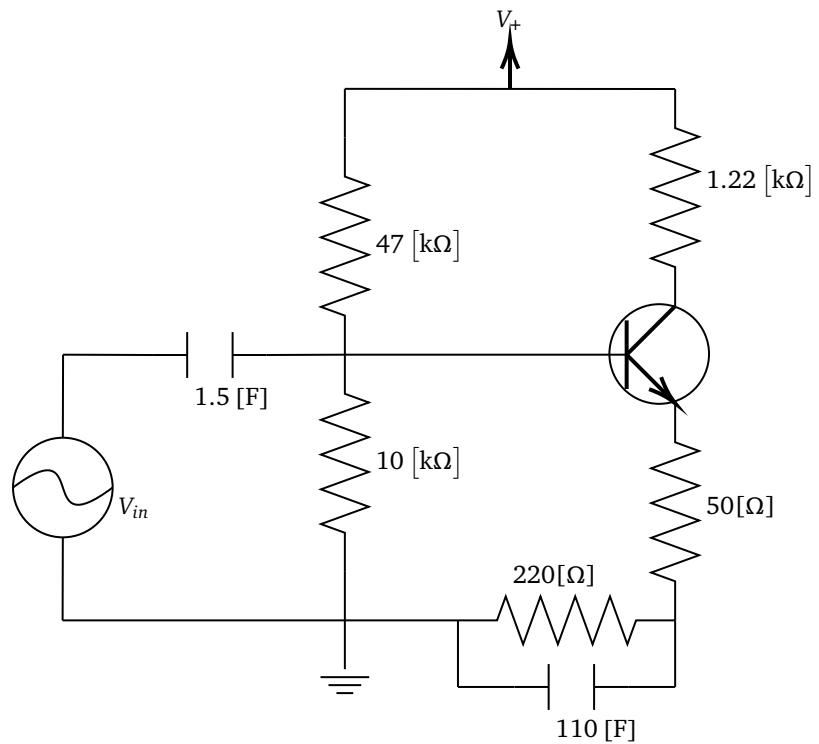


Figure 3: Stable BJT Amplifier

Physically, the circuit was constructed as shown below:

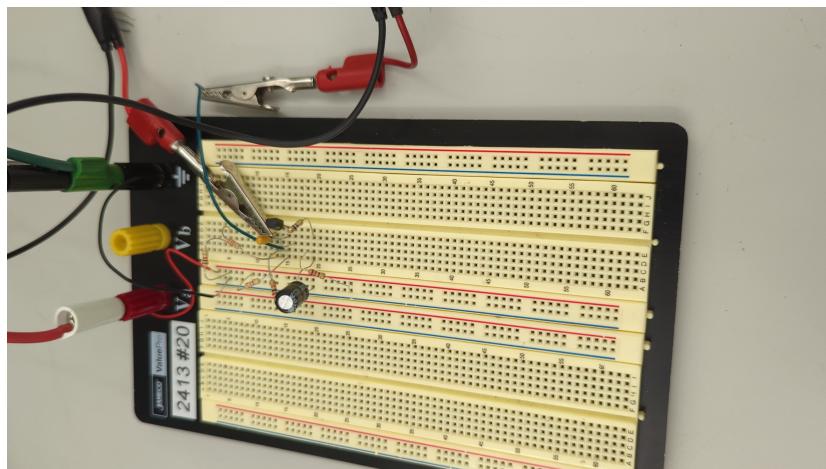


Figure 4: Constructed Amplifier

The output for  $V^+ = 8$ , 10, and 12[V] is shown in Figures 5-7:



Figure 5: Stable Amplifier,  $V^+ = 8[V]$



Figure 6: Stable Amplifier,  $V^+ = 10[V]$

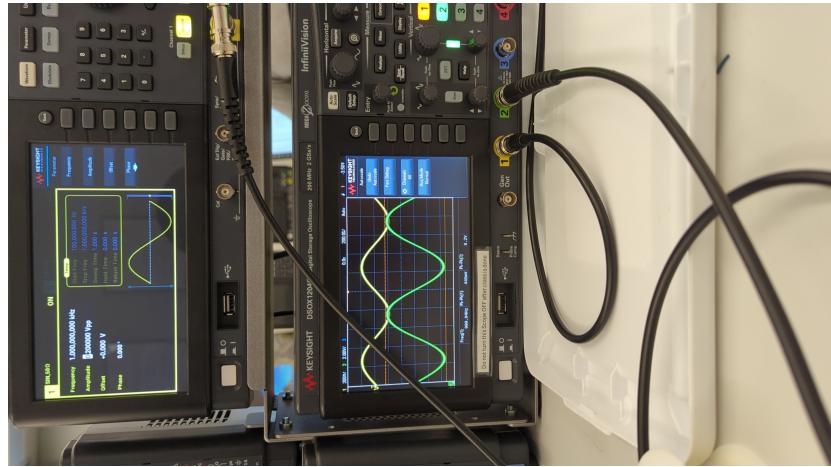


Figure 7: Stable Amplifier,  $V^+ = 12[V]$

We may see that, though at a lower supply voltage there is slight clipping (which is to be expected), the amplifier meets the performance requirements.

## 2.11 Virtual Simulation

## 3 Conclusion