Lecture 7

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• Generator Model

- Synchronous Generator
 - * Consists of a rotor (rotating piece)
 - * And a stator
 - * Rotating part consists of a coil receiving D.C. current, with a magnetic orientation
 - * The rotation results in a flux, which passes through the stator
 - * From this, we can obtain (with $\lambda = N\phi$):

$$\frac{d\lambda}{dt} = e = \omega k \sin(\omega t)$$
$$|\hat{E}_f| = 4.44 f N \phi_{max} \propto I_{dc}, \omega$$
$$\lambda = k \cos(\omega t)$$

* The terminal voltage may be written as:

$$\hat{V}_t = \hat{E}_f - (r + jX_s)\hat{I}_a$$

- * We see that terminal voltage may be controlled using \hat{E}_f
- * The net injected current at different buses (substations) may be calculated using:

$$\hat{I}_i = \frac{(P_{Gi} + jQ_{Gi})^*}{\hat{V}_i^*}$$

- * For buses without a generator, there is no source injection or load, so there is no net current injection (zero-injection bus)
 - · Such substations may be used as 'switching' substations

• Transmission Lines

- For a transmission line with resistance r and impedance jx, we add two capacitors, one on each side of the impedance, with value jb
- With this model, we may write:

$$jb = \frac{1}{2}jb_{lc}$$

- * Where b_{lc} is the total line charging susceptance of the line
- At a bus with a load, we may find the current as:

$$\hat{I}_2 = \frac{(\hat{V}_2 - \hat{V}_1)}{r_{12} + jx_{12}} + \hat{V}_2 j b_{12} + \frac{(\hat{V}_2 - \hat{V}_3)}{r_{23} + jx_{23}} + \hat{V}_2 j b_{23} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \frac{(\hat{V}_2 - \hat{V}_4)}{r_{24} + jx_{24}} + \hat{V}_2 j b_{24} + \hat{V}_2 j$$

- Bus Admittance Matrix
 - We may build a bus admittance matrix (Y_{bux}) may be built by inspection:

 $Y_{bus}(i,i) = \text{sum of admittances of all branches incident to bus } i$ $Y_{bus}(i,j) = \text{negative of the admittance of the branch connecting bus } i \text{ and } j$

$$Y_{bus}(i,j) = Y_{bus}(j,i)$$

- Properties of Y_{bus} :
 - * Symmetric square matrix
 - * Has complex entries
 - * Super sparse (i.e. majority of the entries are zero)
 - * Y_{bus} is non-singular only if there exists at least one branch connecting a bus to ground
 - * $(Y_{bus})^{-1} = Z_{bus}$ the bus impedance matrix!
- Properties of Z_{bus} :
 - * It is a full matrix
 - * It is a symmetric matrix
 - * Diagonal entries are equal to the Thévenin equivalent impedances looking into the network at that bus
 - · This means Thévenin equivalents may be formulated by finding Z_{bus} and finding the corresponding diagonal entry for a bus