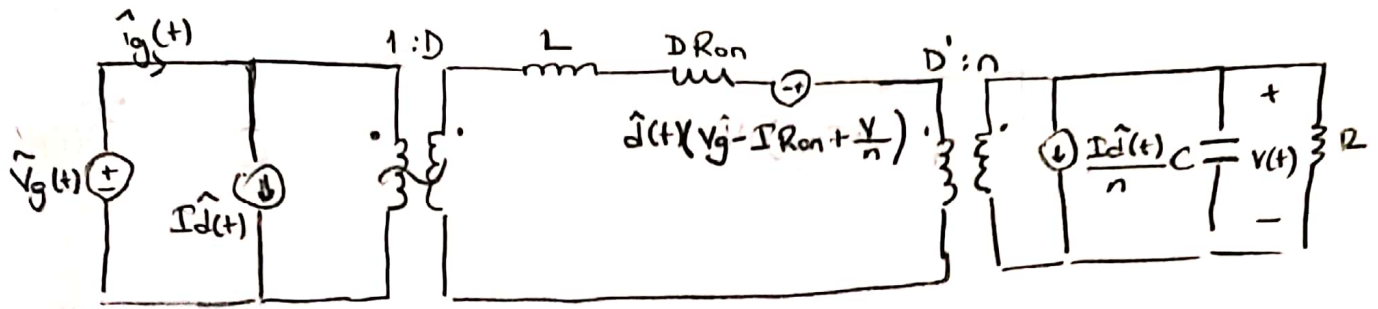
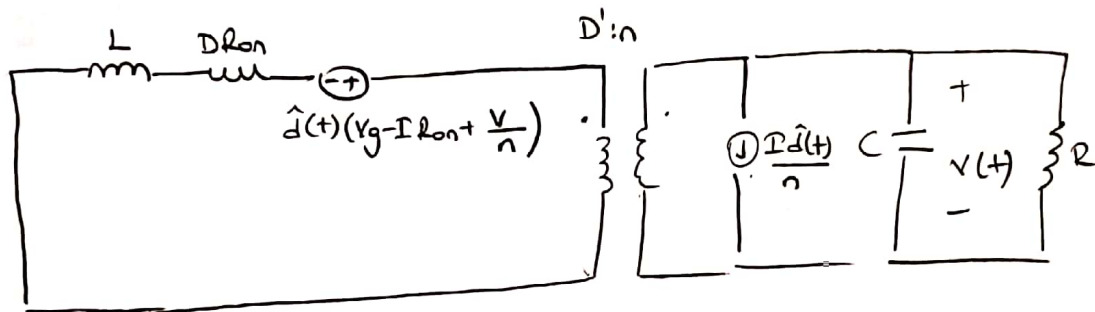


CCM Flyback Control-to-Output Transfer Function Derivation

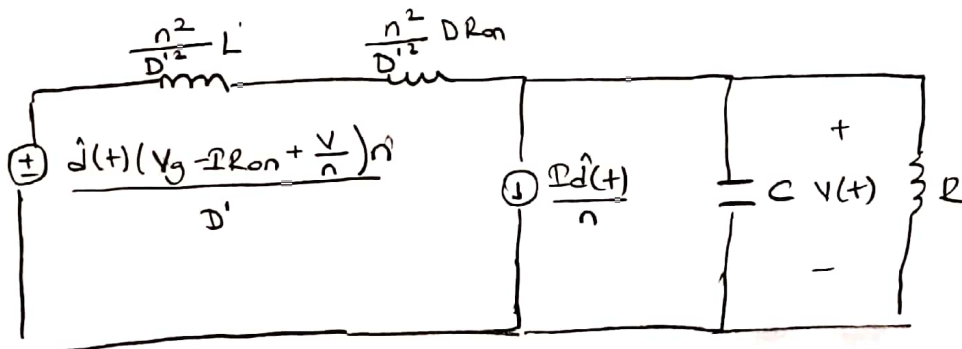


Erickson's Litabindon small signal model

$\hat{V}_g(t) = 0$ for control to output tf. Therefore, circuit becomes

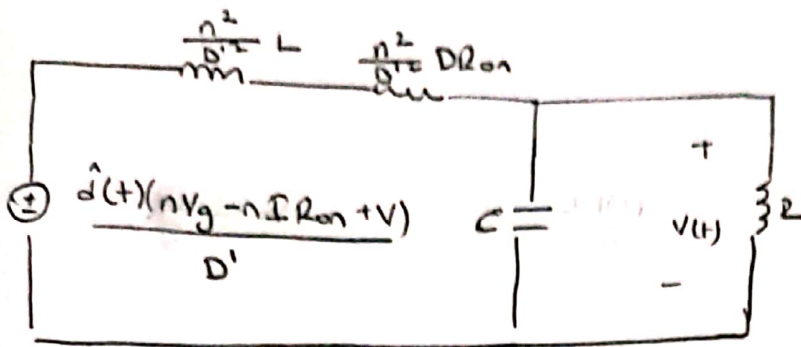


Referring everything to secondary side



Superposition:

Killing Current Source:

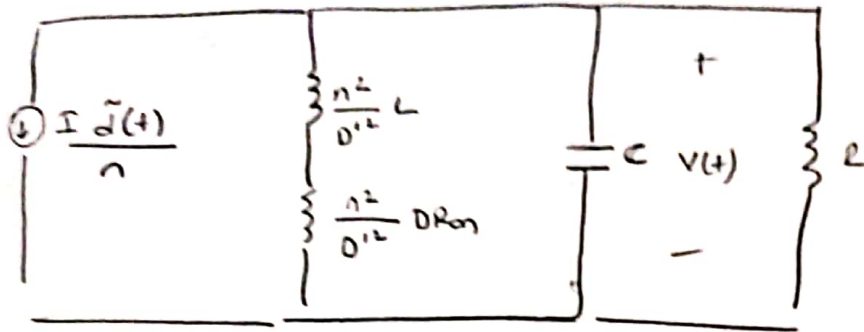


$$\frac{\tilde{V}}{D'} = \frac{(nV_g - nIR_{on} + V)}{D'} \times \frac{(R \parallel \frac{1}{sC})}{(sL + DR_{on})\frac{n^2}{D'^2} + (R \parallel \frac{1}{sC})}$$

$$\frac{\tilde{V}}{D'} = \frac{(nV_g - nIR_{on} + V) D' R}{n^2(sL + DR_{on})(sCR + 1) + D'^2 R}$$

(2)

Killing Voltage Source



$$\frac{V}{d} = \frac{-I}{n} \times \left(\frac{1}{sC} \parallel R \parallel (sL + DRon) \frac{n^2}{D'^2} \right)$$

$$\frac{R}{sCR+1} \parallel (sL + DRon) \frac{n^2}{D'^2}$$

$$\frac{V}{d} = \frac{-I}{n} \times \frac{(sL + DRon) n^2 R}{2D'^2 + (sL + DRon) n^2 (sCR + 1)}$$

$$\frac{V_{out}}{V_{in}} =$$

$$\frac{V}{d} = \frac{-V(sL + DRon)n}{2D'^2 + (sL + DRon)n^2(sCR + 1)} + \frac{D'RnVg - nVDRonD' + VD'R}{n^2(sL + DRon)(sCR + 1) + 2D'^2}$$

$$\frac{V}{d} = \frac{-nVLs - DRon nV - D'Ron nV + D'RnVg + VD'R}{n^2(sCR + 1)(sL + DRon) + 2D'^2}$$

$$\frac{V}{d} = \frac{-n \frac{VgD}{D'n} Ls - R on n \frac{VgD}{D'n} + D'RnVg + \frac{VgD}{D'n} D'R}{n^2(sCR + 1)(sL + DRon) + 2D'^2}$$

(3)

$$\frac{V}{d} = \frac{(-V_g D L s - R_{on} V_g D + D'^2 R_{on} V_g) n + V_g D D' R}{D' n [n^2 (s C R + 1) (s L + D R_{on}) + R D'^2]}$$

$$= \frac{-V_g (D L n s + R_{on} D n - D'^2 R n^2 - D D' R)}{D' n [n^2 (s C R + 1) (s L + D R_{on}) + R D'^2]}$$

where $D' = 1 - D$