

## Application Note

# Motor Control Application Tuning (MCAT) Tool for 3-Phase PMSM

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## 1 Introduction

This application note describes a Freescale motor control tuning solution known as Motor Control Application Tuning (MCAT) tool. MCAT is a graphical tool dedicated to motor control developers and the operators of modern electrical drives. The main feature of proposed approach is automatic calculation and real-time tuning of selected control structure parameters. Connecting and tuning new electric drive setup becomes easier because the MCAT tool offers a possibility to split the control structure and consequently to control the motor at various levels of cascade control structure.

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## 2 Motivation

An electric drive is known as a set of several subsystems such as electric motor with load, controlled supply source, control unit and wide range of sensors, which provide a conversion of electric energy to a specific mechanical movement. Performing the mechanical movement according to certain specifications requires a suitable control strategy of the electric motor. Based on the motor type and the application requirements there are several dedicated control methods. In general, the control techniques are very complex and require knowing of controlled system parameters and control structure parameters. This is a matter of experience in the motor control theory which can cause difficulties to motor control





#### **SULWARE Concept**

developers or users. To avoid these problems and make the tuning of the motor control applications easier, Freescale has developed software solution to control and tune the electrical drives from a graphical environment running on a host PC.

The MCAT tool runs under FreeMASTER online monitor, which allows the real-time tuning of the motor control application. Respecting the parameters of the controlled drive, the correct values of control structure parameters are calculated, which can be directly updated to the application or stored in an application static configuration file. The electrical subsystems are modeled using physical laws and the parameters estimation algorithms are based on Pole-placement method.

The given solution is a graphical user-friendly tool that allows tuning of the application within minutes and will save the user much of the work.

## 3 Software Concept

The MCAT tool is a user-friendly graphical plug-in tool for Freescale's FreeMASTER dedicated to debugging the motor control application. The environment of MCAT tool is based on HTML language whereas the tool engine is based on Jscript language. The HTML and Jscript are widely used on the Internet so the design can be made with the help of the webauthoring tools which are commercially available or even free on the Internet.

Proper displaying of the MCAT tool as an HTML code is provided by the FreeMASTER software exploiting Microsoft Internet Explorer. FreeMASTER software implements an ActiveX object, which is used to enable access to and control the target board application.

More details about FreeMASTER tool can be found in [1].

An integration of MCAT tool into the development process chain is shown in Figure 1.

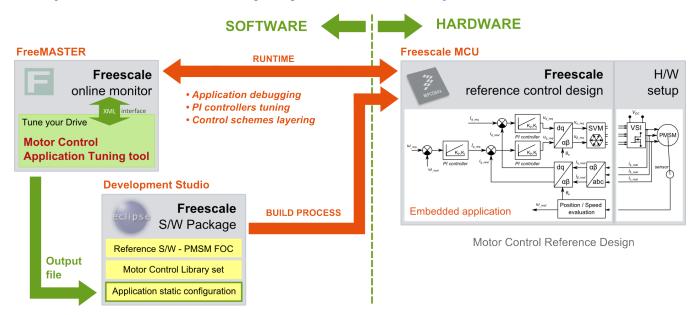


Figure 1. The software concept of MCAT tool utilization

FreeMASTER, as a tool for hard-real time applications monitoring, allows MCAT tool to utilize the runtime debugging features in order to tune the embedded application. Once the application is tuned properly, MCAT tool offers a possibility to store all constants in a file and export them as static configuration, see Figure 1. The application static configuration represents a part of Freescale reference S/W package and will be added into the reference S/W as a header file.

#### NOTE

The MCAT tool can be linked only with FreeMASTER version 1.3.16 or higher.



## 4 Key Features

The given approach is designed to tune the motor control applications, in other words it provides the support for embedded applications. The application meets the following performance specifications:

- Supports up to three motor applications. Keeping an independent access to each motor.
- Supports embedded applications that are compliant with MCAT tool standards
- Utilizes a Pole Placement method for control parameters estimation
- Real-time tuning and updating of control parameters
- Offers a preview of the static configuration of tuned parameters
- Generates an output file with static configuration of tuned parameters
- MCU independent. It supports platforms such as Kinetis, MPC and DSC.
- Applicable for Freescale microcontrollers only
- Plug-in tool for FreeMASTER, not available as a stand-alone tool
- · Offers basic and expert tuning mode
- Modular S/W concept, easily configurable

## 5 Target Applications

In recent times, there are plenty of servo-drive applications employing various types of electric motors. Freescale, based on its experiences, mainly focuses on permanent magnet types of electric drives such as Permanent Magnet Synchronous Motor (PMSM) and Brushless Direct Current (BLDC) motor. Both of them are very popular in wide variety of the motor control applications due to their performance, efficiency, reliability, easy controlling and so on. Another type of motors - Asynchronous Induction Motor (ACIM) or Switched Reluctance Motor (SRM) are not widely used as servo-drives, however they are still popular due to their absence of expensive permanent magnets.

The application note describes the PMSM application tuning variant as a first motor module of MCAT tool.

From a wide spectrum of PMSM control techniques the most common one has been chosen for the purpose of electric drives tuning by using MCAT tool. The most popular and widely used control strategy for PMSM motors is Field Oriented Control (FOC) which is characterized by smooth rotation over the entire speed range of the motor, full torque control at zero speed, and fast acceleration/deceleration.

## 5.1 PMSM Field Oriented Control

Field Oriented Control [2] also called vector control, is based on the cascade structure with inner current loop and outer speed loop, Figure 2. The control loops arranged in series represents hierarchical structure which is characteristic by a feedback, hence the name closed loop system. Proportional-integral (PI) controllers are the most commonly used as feedback controllers, that provide an "error" calculation as the difference between a measured process variable and desired "reference" variable. The PI controller attempts to minimize the control loop error by adjusting the actuating signal in other words the controller output signal.



#### rarget Applications

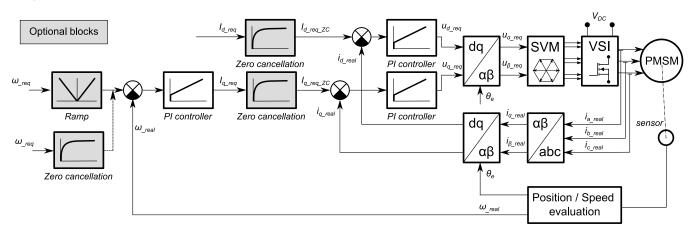


Figure 2. Cascade structure, speed FOC of PMSM

There are two types of PI controllers mostly used in the control algorithms. We distinguish between parallel and recurrent form of the PI controller. Based on the form, the PI controller algorithm involves two separate constant parameters: the proportional component  $K_P$  and integral component  $K_I$  for parallel form or their equivalents CC1 and CC2 for recurrent form. Setting of these constants depends on the required control loop behavior such as the loop bandwidth or attenuation.

As seen in Figure 2, the control structure can be extended by additional optional blocks placed in the feed-forward path of the control loop. They are called Zero Cancellation blocks and play an important role in term of compensation of a closed loop "zero" introduced by a PI controller. Ramp block modifies the edges of speed step change command and introduces a slope behavior to the reference speed request.

Proposed MCAT tool helps the user to properly calculate the constants of the control structure with respecting the overall system parameters as well as the parameters of the control.

## 5.2 Application cases tree

The MCAT tool was designed to tune and control the applications employing up to three motors. Such a strategy covers wide range of the multiple motor applications with different conditions. Cascade control approach allows the PMSM motor to be controlled by following the FOC principles. Additional feature of the MCAT tool is an open loop scalar control of PMSM motor. The last but definitely not least feature of the MCAT tool is position/speed feedback option. In recent times, there are plenty of various sensors such as resolver or encoder demanded. Very popular and often required is also sensorless design of a PMSM control. All main MCAT tool features reflecting the possible application cases are summarized in Figure 3.



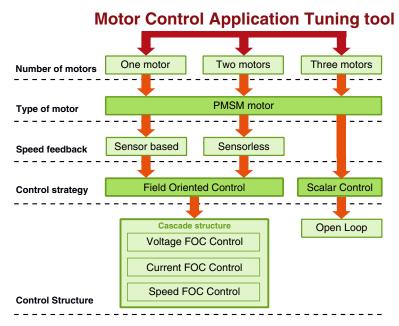


Figure 3. The application cases tree diagram

## 6 MCAT tool for 3-phase PMSM

The MCAT tool is a graphical tool with friendly environment and intuitive control. As can be seen in Figure 4, the tool consists of motor selector bar, tab menu and the workspace. The proposed approach supports up to three PMSM motors, while each motor has its own tab menu and workspace.

The MCAT tool represents a modular concept that consists of several sub-modules. Each sub-module represents one tab in the tab menu. The arrangement of the sub-modules is flexible according to the needs of embedded application. Several tab menu combinations can be created based on the type of application, for instance sensorless applications do not need any POSPE Sensors tab, torque control applications do not need any Speed Loop tab and so on.

Based on this, the initial setting of the MCAT tool will be provided by Freescale team developing the motor control reference designs.



#### INICAT tool for 3-phase PMSM

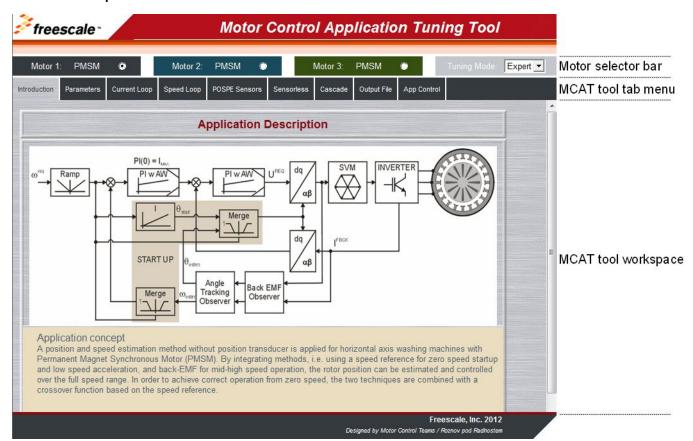


Figure 4. MCAT tool environment

Predefined MCAT tool will be a part of reference software for dedicated MCU. Since the tuning tool cannot be used as a standalone, it will be included in the FreeMASTER project by default.

The MCAT tool workspace is unique for each tab and detailed overview of each available tab is provided in the following chapters.

## 6.1 Introduction tab

An Introduction tab can be considered as a voluntary tab. It provides a room for describing or introducing the targeted MC application, Figure 4.

## 6.2 Parameters tab

A Parameters tab is dedicated for entering the input application parameters. It is a mandatory tab due to its high level of dependency with other tabs. To ensure proper MCAT tool functionality and control parameter calculation accuracy an attention must be paid when entering the input application parameters into required cells. An impact of each required input is shown in Table 1. Number of input parameters that need to be filled depends on the selected application tuning mode. The application tuning mode can be changed on the right side of motor selector bar and offers two options: basic and expert mode.

Application tuning modes available in Parameters tab are as follows:



- Basic highly recommended for users who are not enough experienced in motor control theory. The number of required input parameters is reduced according to the Table 1. The mandatory cells are with white background while the rest of input parameters are calculated automatically by MCAT tool engine. These parameters are read-only and shadowed, see Figure 5.
- Expert all inputs parameters are accessible and freely editable by a user. However, their setting requires a certain level of expertise in motor control theory, see Figure 6.

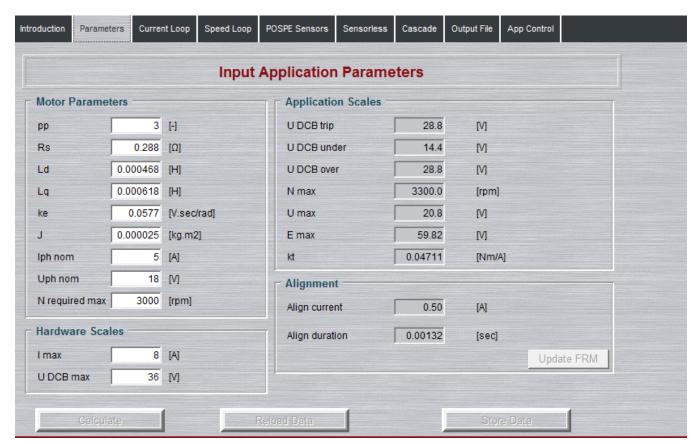


Figure 5. Parameters tab – Basic mode



#### IVICAT tool for 3-phase PMSM

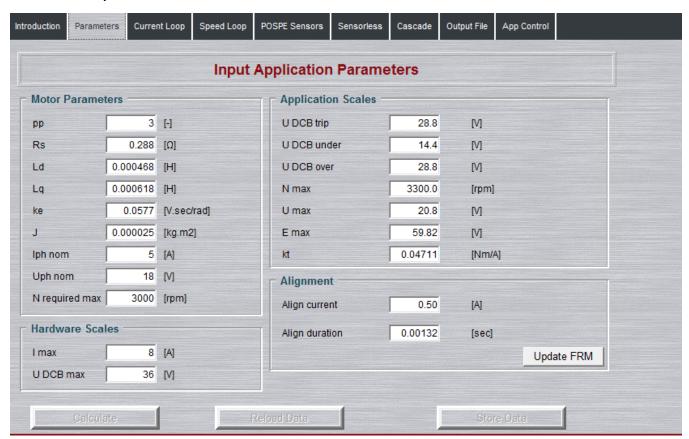


Figure 6. Parameters tab – Expert mode

The Table 1 shows the list of the MCAT tool input parameters with their physical units, brief description, the impacted algorithms and accessibility status in basic mode.

Table 1. Inputs of the Parameter tab

Parameter Name	Units	Description	Use in constant calculation	Basic mode accessibility
рр	[-]	Motor pole pairs	Speed and Position module	Yes
Rs	[Ω]	Resistance of one motor phase	Current PI controller BEMF Observer	Yes
Ld	[H]	Direct Inductance of one motor phase	Current PI controller BEMF Observer	Yes
Lq	[H]	Quadrature Inductance of one motor phase	Current PI controller BEMF Observer	Yes
ke	[V.sec/rad]	Back-EMF constant	BEMF Observers	Yes
J	[Kg.m <sup>2</sup> ]	Drive Inertia	Speed PI controller	Yes
Iph nom	[A]	Nominal phase current	Current scale calculation	Yes
Uph nom	[V]	Nominal phase voltage	Voltage scale calculation	Yes

Table continues on the next page...



Table 1. Inputs of the Parameter tab (continued)

Parameter Name	Units	Description	Use in constant calculation	Basic mode accessibility
N required max	[rpm]	Maximal required speed in the application. It is not a speed scale!	Speed scale calculation	Yes
Imax	[A]	HW current sensing scale	Current PI controller  BEMF Observer Speed Controller	No
U DCB max	[V]	HW DC-Bus voltage scale	Current PI controller BEMF Observer Speed Controller	No
U DCB trip	[V]	Trigger value that switches an external DC-Bus braking resistor on	Fault protection	No
U DCB under	[V]	Voltage value that generates DC-Bus UNDER VOLTAGE fault	Fault protection	No
U DCB over	[V]	Voltage value that generates DC-Bus OVER VOLTAGE fault	Fault protection	No
N max	[rpm]	Speed scale – maximal value of electrical angular velocity	Speed and position BEMF Observer Tracking Observer	No
U max	[V]	Voltage scale – maximal value of FOC	Current PI Controller BEMF Observer	No
E max	[V]	Back-EMF voltage scale	BEMF Observer	No
kt	[Nm/A]	Torque constant	Speed PI controller	No
Align current / voltage	[A] / [V]	DC value of current or voltage for rotor alignment	Rotor alignment	No
Align duration	[sec]	Duration of rotor alignment	Rotor alignment	No

The parameters of the controlled motor can be acquired from a motor datasheet provided by motor manufacturer or from laboratory measurement.

#### 6.2.1 Parameter modification

All parameter cells are filled automatically with predefined data downloaded from an external file. The input parameter cells are freely accessible for editing in accordance to the selected tuning mode, as it is shown in Table 1. There are four user buttons on the page with the following functionality:

• Update FRM – the DC voltage or current and the duration of applied alignment state can be updated by using this button. The button is disabled in basic tuning mode.

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#### WUAT tool for 3-phase PMSM

- Calculate the button is disabled by default. In case that the tuning mode has changed from an expert to a basic mode and at least one of the input application parameters has changed as well, a new set of application scales have to be recalculated. The Calculate button provides calculation and update of application scales values.
- Reload Data the button is disabled by default. If the value in a particular field has changed, the background of the cell
  is changed from white to pink color for the purpose of signalization the changes and the button becomes enabled. By
  pressing the Reload Data button all modified cells will be filled with original values taken from the file. After
  successful data reload, the background of the cells becomes white and the button gets disabled
- Store Data the button is disabled by default. If the value in a particular field has changed, the background of the cell
  is changed from white to pink color for the purpose of signalization the changes and the button becomes enabled. By
  pressing the Store Data button all new values from modified cells will be saved into the file. After successful data
  saving, the background of the cells becomes white and the button gets disabled.

The editing fields accept only numeric characters. The parameter values are fully under a user responsibility and no additional checking is applied to those items. The typical range of the parameter value appears when the mouse pointer is in a parameter name focus.

## 6.3 Current Loop tab

The Current Loop (CL) is a tab designed for tuning of the current control loop. The current control loop is the most inner loop in the cascade control structure of vector controlled PMSM. One of the FOC features is separate controlling of the flux (d axis) and torque (q axis) components of the current, Figure 2. Due to this, PMSM control structure has two current loops and each of them consists of a PI controller and an optional zero-cancellation block.

The CL tab is logically divided into two parts. The first part represents an input data field with required control loop parameters needed for PI controller parameter calculation. The second one is an output data field which displays the calculated parameters of PI controllers in both d and q axis. All PI controller constants are calculated from the motor parameters, application scales and current loop parameters.

Application tuning modes available in Current Loop tab:

- Basic highly recommended for users who are not experienced enough in motor control theory. There are no input
  parameters required in this mode. All input parameters of the CL are estimated from the motor and application
  parameters automatically by MCAT tool engine. The cells requiring these parameters are shadowed with the status
  read-only, Figure 7.
- Expert all input parameters cells of the CL are accessible and freely editable by the user, as given in Figure 8. However, their setting requires a certain level of expertise in motor control theory.



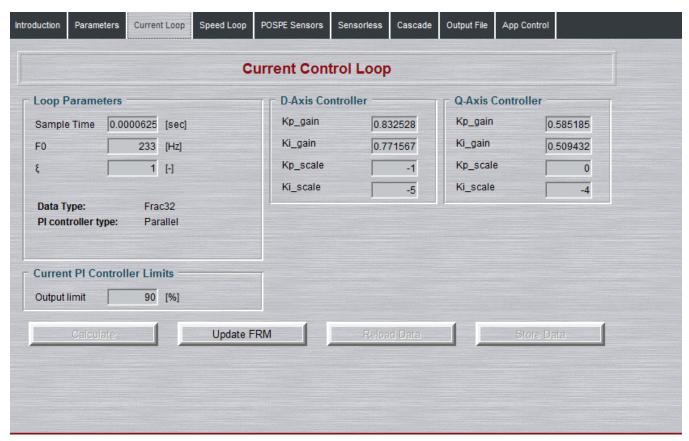


Figure 7. Current Loop tab - Basic mode



#### IVICAT tool for 3-phase PMSM

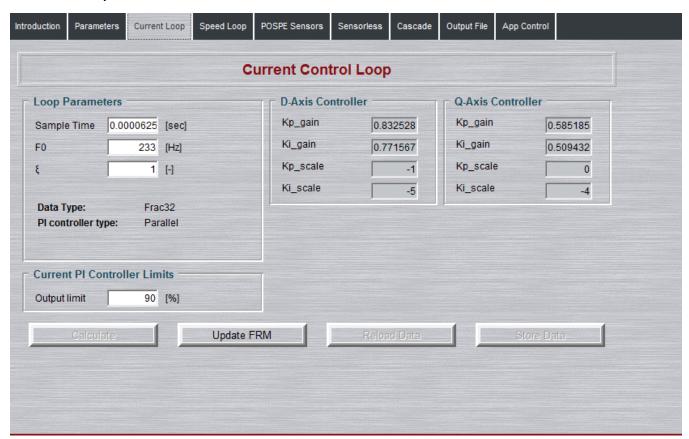


Figure 8. Current Loop tab – Expert mode

The Table 2 shows the list of the current loop input parameters with their physical units, brief description, the impacted algorithms and accessibility status in basic mode.

Table 2. Inputs of the Current Loop tab

Parameter Name	Units	Description	Use in Constant Calculation	Basic Mode Accessibility
Sample Time	[sec]	CL sampling time	Current PI controller Zero-compensator	NO
F0	[Hz]	Current loop bandwidth	Current PI controller Zero-compensator	NO
ξ	[-]	Current loop attenuation	Current PI controller Zero-compensator	NO
Output limit	[%]	Limit of the current PI controllers		NO

## 6.3.1 Current Loop Setting Variability

Two types of PI controllers and optional zero-cancellation blocks (Figure 2 )lead to several variations of current control loop structure.



The MCAT tool covers both options, it means it supports both types of PI controllers and offers an opportunity to use the optional zero-cancellation blocks. Moreover, including the variability of data type representation, there are several modes available that are required to be supported by the current loop tab, see Table 3.

Table 3. Summary of Current Loop setting modes

The control loop available mode	Applicable changes
PI controllers	Parallel / Recurrent form
Zero-cancellation blocks	Allowed / Non allowed
Data type representation	FIX, FLOAT arithmetic

#### NOTE

All settings shown in Table 3 will be predefined by Freescale developer according to the MC reference application.

## 6.3.2 Current loop parameters calculation

The parameters of the PI controllers in current loop are calculated by exploiting the pole placement (PP) method. Pole placement method is an approach of the feedback control system theory to place the closed-loop poles of a plant in predetermined locations. The PP method applied to the closed-loop system leads to desired controlled system behavior.

A simplified closed current control loop shown in Figure 9, is used for deriving the PI controller parameters calculation process.

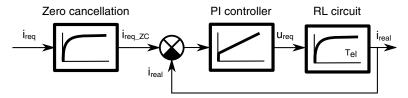


Figure 9. Simplified current control loop

Considering a general form of closed loop with RL model as a plant of first order and PI controller:

$$G_{PI}(s) = \frac{K_{P_{-}I}s + K_{I_{-}I}}{s}$$

#### Equation 1.

$$G_{\text{RL}}(s) = \frac{1}{Ls+R}$$

#### Equation 2.

where L is the stator inductance and R is a stator resistance. The closed loop transfer function is derived in Laplace domain as follows:

$$G_{I}(s) = \frac{i_{\text{rea}I}(s)}{i_{\text{req}\_ZC}(s)} = \frac{G_{\text{Pl}\_I}(s)G_{\text{RL}}(s)}{1+G_{\text{Pl}\_I}(s)G_{\text{RL}}(s)} = \frac{\frac{K_{P\_I}}{L}s + \frac{K_{I\_I}}{L}}{s^{2} + \left(\frac{K_{P\_I} + R}{L}\right)s + \frac{K_{I\_I}}{L}} = \frac{\frac{K_{I\_I}(k_{P\_I} + R)}{L}s + \frac{K_{I\_I}}{L}}{s^{2} + \left(\frac{K_{P\_I} + R}{L}\right)s + \frac{K_{I\_I}}{L}}$$

#### Equation 3.

The PI controller however, introduced a zero to the closed loop transfer function for command changes, located at  $-K_{I\_I}/K_{P\_I}$ . This derivative characteristic of the loop increases the system overshoot, lowering the potential closed loop bandwidth. Due to this, the zero of the PI controller must be compensated. This can be done by introducing a zero-cancellation block in the feed-forward path, which has the following transfer function:

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#### IVICAT tool for 3-phase PMSM

$$G_{\text{ZC\_I}}(s) = \frac{1}{\left(\frac{K_{P\_I}}{K_{I}} s + 1\right)}$$

#### Equation 4.

The current loop transfer function with the zero-cancellation block in feed-forward is then:

$$G_{\mathbf{I}}(s) = \frac{i_{\text{real}}(s)}{i_{\text{req}}(s)} = G_{ZC\_f}(s) \frac{G_{PI\_f}(s)G_{RL}(s)}{1 + G_{PI\_f}(s)G_{RL}(s)} = \frac{\frac{K_{I\_f}}{L}}{s^{2} + \left(\frac{K_{P\_f} + R}{L}\right)s + \frac{K_{I\_f}}{L}}$$

#### Equation 5.

Having the closed loop with canceled zero (Equation 5 on page 14), the PI controller can be designed by comparing the closed loop characteristic polynomial with that of a standard second order system as:

$$s^{2} + \left(\frac{K_{P_{\underline{I}}} + R}{L}\right) s + \frac{K_{\underline{I}} - I}{L} = s^{2} + 2\xi \omega_{0} s + \omega_{0}^{2}$$

#### Equation 6.

where  $\omega_0$  is the natural frequency of the closed loop system (loop bandwidth) and  $\xi$  is the loop attenuation. The proportional and integral gains of the PI controller can be therefore calculated from (Equation 6 on page 14) as:

$$K_{P}I = 2\xi\omega_0 L - R$$

#### Equation 7.

$$K_{I} = L\omega_0^2$$

#### Equation 8.

(Equation 7 on page 14, Equation 8 on page 14) describe a PI controller design in continuous time domain. Considering the discrete domain the expressions (Equation 7 on page 14, Equation 8 on page 14) will change as follows:

$$K_P I(z) = K_P I(s)$$

#### Equation 9.

$$K_{I\_I}(z) = K_{I\_I}(s)T_S$$

## Equation 10.

where  $T_S$  is sampling period of the current loop.

The form of PI controller (Equation 1 on page 13) implementation which allows the user to define the proportional and integration components independently without interaction is called parallel PI controller. Another type of PI controller implementation is recurrent form that can be reached by transforming (Equation 1 on page 13) into a discrete domain as follows:

$$u_{(k)} = u_{(k-1)} + e_{(k)}CC_1 + e_{(k-1)}CC_2$$

#### Equation 11.

where u(k) is the controller output, e(k) is the controller input error signal, CC1 and CC2 are controller coefficients calculated using Trapezoidal method:

$$CC_{1\_I} = K_{P\_I} + K_{I\_I} \frac{T_S}{2}$$

## Equation 12.



$$CC_{2} I = -K_{P} I + K_{I} I \frac{T_{S}}{2}$$

#### Equation 13.

The zero cancellation transfer function (Equation 4 on page 14) can be also transformed into Z domain using Backward Euler method. Then the discrete implementation is therefore given by:

$$y_{(k)} = \frac{K_{I\_I}T_S}{K_{P\_I}+K_{I\_I}T_S} x_{(k)} + \frac{K_{P\_I}}{K_{P\_I}+K_{I\_I}T_S} y_{(k-1)}$$

#### Equation 14.

It is clear that (Equation 14 on page 15) is a simplified form of 1<sup>st</sup> order Butterworth LP filter in IIR implementation. So the zero cancellation block physically behaves as a low pass filter, smoothing the input command. It therefore allows increasing of the loop gain, achieving higher bandwidth.

In depends on the PI controller implementation, the controller constants (Equation 9 on page 14, Equation 10 on page 14) or (Equation 12 on page 14, Equation 13 on page 15) are used in case of floating point data representation. The discrete implementation of PI controllers in the fixed point arithmetic platform requires the scaling approach to keep all signals in the range <-1, 1). Detailed description of proper PI controller's parameters scaling is in [3], [4].

#### 6.3.3 Parameter modification

All parameter cells are filled automatically with predefined data downloaded from an external file. The parameter cells are freely accessible for editing according to the selected tuning mode, as shown in Table 2. There are four user buttons on the page with the following functionality:

- Calculate the button is disabled by default. The button becomes enabled as soon as one of the input Loop Parameters is changed. The background of the cell is changed from white to pink color for the purpose of change signalization. By pressing the Calculate button all PI controller parameters are recalculated according to the Current loop parameters calculation.
- Update FRM the button is enabled by default. By pressing the button, the application PI controller parameters on the embedded side are updated with the ones displayed in output field data.
- Reload Data the button is disabled by default. The button becomes enabled as soon as one of the input Loop
  Parameters is changed. The background of the cell is changed from white to pink color for the purpose of change
  signalization. By pressing the Reload Data button all the modified cells will be rewritten with original values taken
  from the file. After successful data reload, the background of the cells becomes again white and the button gets
  disabled.
- Store Data the button is disabled by default. The button becomes enabled as soon as one of the input Loop Parameters is changed. The background of the cell is changed from white to pink color for the purpose of change signalization. By pressing the Store Data button all new values from modified cells will be saved into the file. After successful data saving, the background of the cells becomes white and the button gets disabled.

The editing fields accept only numeric characters. The parameter values are fully under user responsibility and no additional checking is applied to those items. The typical range of the parameter value appears when the mouse pointer is in a parameter name focus.

## 6.4 Speed Loop Tab

The Speed Loop (SL) is a tab designed for tuning the speed control loop. The speed control loop is an outer loop in the cascade control structure of vector controlled PMSM. Speed loop consists of a PI controller and optional blocks like zero-cancellation or ramp function.



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The SL tab is logically divided into two parts. The first part represents input data fields with required control loop parameters needed for PI controller parameter calculation. The second one is an output data field which displays the calculated parameters of the speed controller. The PI controller constants are calculated from the motor parameters, application scales and speed loop parameters.

Application tuning modes available in Speed Loop tab are as follows:

- Basic highly recommended for users which are not enough experienced in motor control theory. There are no input parameters required in this mode. All input parameters of the SL are estimated from the motor and application parameters automatically by MCAT tool engine. The cells requiring these parameters are shadowed with the status read-only, as in Figure 10.
- Expert all input parameters cells of the SL are accessible and freely editable by an user, as in Figure 11. However, their setting requires a certain level of expertise in motor control theory.

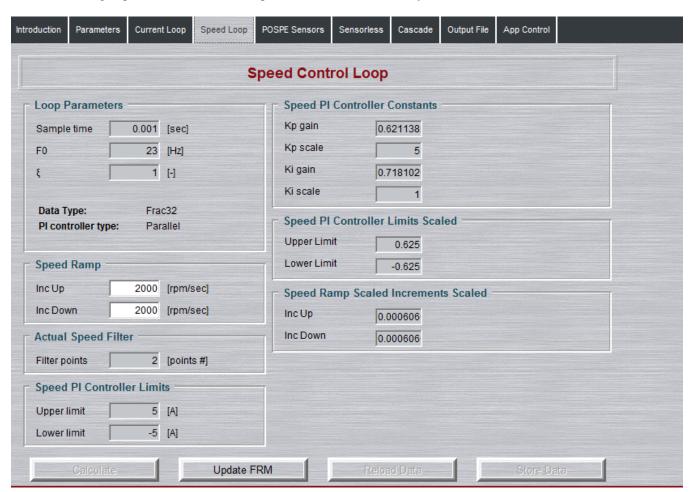


Figure 10. Speed Loop tab - Basic mode



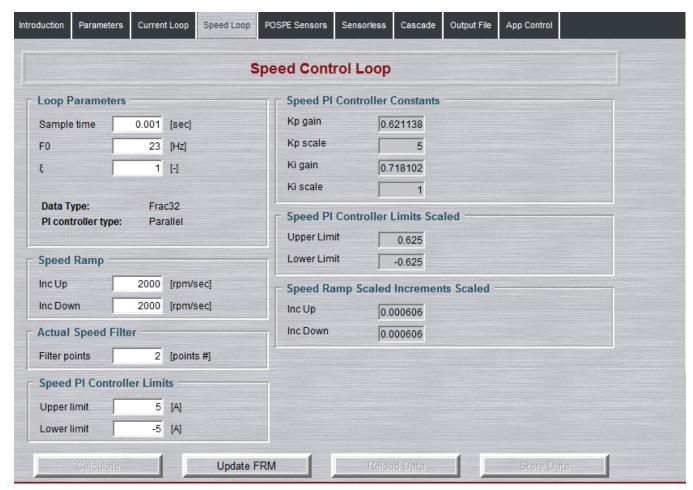


Figure 11. Speed Loop tab - Expert mode

The Table 4 shows the list of the speed loop input parameters with their physical units, brief description, the impacted algorithms and accessibility status in basic mode.

Table 4. Input of the Speed Loop tab

Parameter Name	Units	Description	Use in constant calculation	Basic mode accessibility
Sample time	[sec]	CL sampling time	Current PI controller Zero-compensator	NO
F0	[Hz]	Current loop bandwidth	Current PI controller Zero-compensator	NO
ξ	[-]	Current loop attenuation	Current PI controller Zero-compensator	NO
Inc Up	[rpm/sec]	Speed increasing with the increment	Ramp function	NO
Inc Down	[rpm/sec]	Speed decreasing with the increment	Ramp function	NO
Filter points	[points #]	Moving Average Filter Samples		NO

Table continues on the next page...



#### INICAT tool for 3-phase PMSM

Table 4. Input of the Speed Loop tab (continued)

Parameter Name	Units	Description	Use in constant calculation	Basic mode accessibility
Upper Limit	[A]	Required current upper limit		NO
Lower limit	[A]	Required current lower limit		NO

## 6.4.1 Speed Loop Setting Variability

Two types of speed PI controller and optional blocks as zero-cancellation block or ramp function (Figure 2) lead to the several variations of speed control loop structure.

The MCAT tool covers all above mentioned options, it means it supports both types of PI controllers and offers an opportunity to use different approach in speed feed-forward path as the optional zero-cancellation blocks or ramp function. Moreover, including the variability of data type representation, there are available several modes that are required to be supported by the speed loop tab, see Table 5.

Table 5. Summary of Speed Loop setting modes

The control loop available mode	Applicable changes
PI controllers	Parallel / Recurrent form
Zero-cancellation blocks	Allowed / Non allowed
Ramp function	Allowed / Non allowed
Ramp function	FIX, FLOAT arithmetic

#### **NOTE**

All settings shown in Table 5 will be predefined by Freescale developer according to the MC reference application.

## 6.4.2 Speed loop parameters calculation

Again the pole placement approach is used for parameters calculation of all speed loop control elements. A simplified closed speed control loop, shown in Figure 12, is used for deriving the parameters of all blocks of speed control loop.

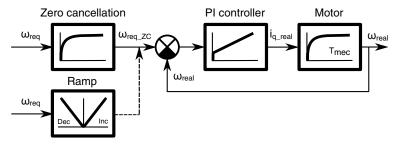


Figure 12. Simplified speed control loop



In most cases the electrical time constant of the RL circuit  $T_{el}$  is much smaller than the mechanical time constant of the motor Tmec. Small  $T_{el}$  requires the current control loop running at higher sampling frequency, hence the name fast loop. On the contrary, the speed loop regarding the higher time constant can run in slower control loop with lower sampling frequency. Such approach gives enough time to control the current between two speed samples. Based on this, the behavior of the current loop can be considered as a torque gain from speed loop perspective.

The speed loop is closed by a PI controller, which enables speed control with zero steady state error. Considering a general form of closed loop with a first order plant and PI controller:

$$G_{PI}(s) = \frac{K_{P_{-}\omega}s + K_{I_{-}\omega}}{s}$$

#### Equation 15.

$$G_{\mathbf{M}}(s) = \frac{K_T}{J_{s+B}}$$

#### Equation 16.

where  $K_T$  represents torque constant, J is a moment of inertia and B is a friction. Then the speed closed loop transfer function is derived in Laplace domain as follows:

$$G_{\omega}(s) = \frac{\omega_{\text{real}}(s)}{\omega_{\text{req\_ZC}}(s)} = \frac{G_{\text{Pl\_}\omega}(s)G_{M}(s)}{1 + G_{\text{Pl\_}\omega}(s)G_{M}(s)} = \frac{\frac{K_{T}K_{P\_\omega}}{J}_{s+\frac{K_{T}K_{P\_\omega}}{J}}}{s^{2+\left(\frac{K_{T}K_{P\_\omega}+B}{J}\right)s+\frac{K_{T}K_{I\_\omega}}{J}}} = \frac{\frac{K_{T}K_{I\_\omega}}{J}_{s+\frac{K_{T}K_{I_\omega}}{J}}}{s^{2+\left(\frac{K_{T}K_{P_\omega}+B}{J}\right)s+\frac{K_{T}K_{I_\omega}}{J}}} = \frac{\frac{K_{T}K_{I_\omega}}{J}_{s+\frac{K_{T}K_{I_\omega}}{J}}}{s^{2+\left(\frac{K_{T}K_{P_\omega}+B}{J}\right)s+\frac{K_{T}K_{I_\omega}}{J}}} = \frac{\frac{K_{T}K_{I_\omega}}{J}_{s+\frac{K_{T}K_{I_\omega}}{J}}}{s^{2+\left(\frac{K_{T}K_{P_\omega}+B}{J}\right)s+\frac{K_{T}K_{I_\omega}}{J}}} = \frac{\frac{K_{T}K_{I_\omega}}{J}_{s+\frac{K_{T}K_{I_\omega}}{J}}}{s^{2+\left(\frac{K_{T}K_{P_\omega}+B}{J}\right)s+\frac{K_{T}K_{I_\omega}}{J}}} = \frac{\frac{K_{T}K_{I_\omega}}{J}_{s+\frac{K_{T}K_{I_\omega}}{J}}}{s^{2+\left(\frac{K_{T}K_{P_\omega}+B}{J}\right)s+\frac{K_{T}K_{I_\omega}}{J}}} = \frac{\frac{K_{T}K_{I_\omega}}{J}_{s+\frac{K_{T}K_{I_\omega}}{J}}}{s^{2+\left(\frac{K_{T}K_{P_\omega}+B}{J}\right)s+\frac{K_{T}K_{I_\omega}}{J}}} = \frac{\frac{K_{T}K_{I_\omega}}{J}_{s+\frac{K_{T}K_{I_\omega}+B}{J}}}{s^{2+\left(\frac{K_{T}K_{P_\omega}+B}{J}\right)s+\frac{K_{T}K_{I_\omega}+B}{J}}} = \frac{\frac{K_{T}K_{I_\omega}+B}{J}_{s+\frac{K_{T}K_{I_\omega}+B}{J}}}{s^{2+\left(\frac{K_{T}K_{P_\omega}+B}{J}\right)s+\frac{K_{T}K_{I_\omega}+B}{J}}} = \frac{\frac{K_{T}K_{I_\omega}+B}{J}}{s^{2+\left(\frac{K_{T}K_{I_\omega}+B}{J}\right)s+\frac{K_{T}K_{I_\omega}+B}{J}}} = \frac{\frac{K_{T}K_{I_\omega}+B}{J}}{s^{2+\left(\frac{K_{T}K_{I_\omega}+B}{J}\right)s+\frac{K_{T}K_{I_\omega}+B}{J}}} = \frac{\frac{K_{T}K_{I_\omega}+B}{J}}{s^{2+\left(\frac{K_{T}K_{I_\omega}+B}{J}\right)s+\frac{K_{T}K_{I_\omega}+B}{J}}} = \frac{\frac{K_{T}K_{I_\omega}+B}{J}}{s^{2+\left(\frac{K_{T}K_{I_\omega}+B}{J}\right)s+\frac{K_{T}K$$

#### Equation 17.

Similar to the approach described in the current loop parameters calculation (Current loop parameters calculation), the speed PI controller introduces a zero to the closed loop transfer function. The zero can be compensated by introducing a zero cancellation block into the speed feed-forward path, which has the following transfer function:

$$G_{\text{ZC}_{-}\omega}(s) = \frac{1}{\left(\frac{K_{P_{-}\omega}}{K_{I_{-}\omega}}s+1\right)}$$

## Equation 18.

The speed loop transfer function with the zero-cancellation block in feed-forward path is then:

$$G_{\omega}(s) = \frac{\omega_{\text{real}}(s)}{\omega_{\text{req}}(s)} = G_{\text{ZC}\_\omega}\left(s\right) \frac{G_{\text{Pl}\_\omega}(s)G_{M}(s)}{1 + G_{\text{Pl}\_\omega}(s)G_{M}(s)} = \frac{\frac{K_{T}K_{I\_\omega}}{J}}{s^{2} + \left(\frac{K_{T}K_{P\_\omega}+B}{J}\right)s + \frac{K_{T}K_{I\_\omega}}{J}}$$

#### Equation 19.

Then the proportional and integral gains of the PI controller as well as the zero-cancellation block parameters can be derived as follows:

$$K_{P_{-}\omega}(z) = K_{P_{-}\omega}(s) = \frac{2\xi\omega_0^{J-B}}{K_T}$$

#### Equation 20.

$$K_{I\_\omega}(z) = K_{I\_\omega}(s)T_S = \frac{J}{K_T}\omega_0^2T_S$$

#### Equation 21.

where  $T_S$  is sampling period of the speed loop,  $\omega_0$  is the natural frequency of the closed loop system (loop bandwidth) and  $\xi$  is the speed loop attenuation. The constants (Equation 20 on page 19, Equation 21 on page 19) represent a parallel form of PI controller, whereas the recurrent type of PI controller utilizes CC1 and CC2 constants:



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$$CC_{1 \omega} = K_{P_{\omega}} + K_{I_{\omega}} \frac{T_S}{2}$$

## Equation 22.

$$CC_{2\omega} = -K_{P\omega} + K_{I\omega} \frac{T_S}{2}$$

#### Equation 23.

The zero cancellation transfer function (Equation 18 on page 19) can be also transformed into Z domain using Backward Euler method. Then the discrete implementation is therefore given by:

$$y_{(k)} = \frac{K_{I_{-}\omega}T_{S}}{K_{P_{-}\omega} + K_{I_{-}\omega}T_{S}} x_{(k)} + \frac{K_{P_{-}\omega}}{K_{P_{-}\omega} + K_{I_{-}\omega}T_{S}} y_{(k-1)}$$

#### Equation 24.

The discrete implementation of speed zero-cancellation block represents a simplified form of 1st order Butterworth LP filter in IIR implementation.

It depends on the PI controller implementation, the controller constants (Equation 20 on page 19, Equation 21 on page 19, Equation 22 on page 20, Equation 23 on page 20) are used in case of floating point data representation. The discrete implementation of PI controllers in the fixed point arithmetic platform requires the scaling approach to keep all signals in the range <-1, 1). Detailed description of proper PI controller's parameters scaling is in [3] [4].

As can be seen, to get the constants of the speed loop a very sensitive parameter – moment of inertia is required. However, there is plenty of motor control applications where this parameter is either completely unknown or rapidly changed during the operation in depends on the load torque behavior. In such case, the ramp function placed in the speed feed-forward path can be used instead of zero-cancellation block. The ramp behavior of the required speed can partly suppress the impact of the inaccurate calculated PI controller parameters caused by a difference in estimated moment of inertia. More details about ramp function can be found in [3] [4].

## 6.4.3 Parameter modification

All parameter cells are filled automatically with predefined data downloaded from an external file. The parameter cells are freely accessible for editing according to the selected tuning mode, as shown in Table 4. There are four user buttons on the page with the following functionality:

- Calculate the button is disabled by default. The button becomes enabled as soon as one of the input Loop Parameters
  is changed. The background of the cell is changed from white to pink color for the purpose of changes signalization. By
  pressing the Calculate button all PI controller parameters are recalculated according to the Speed loop parameters
  calculation
- Update FRM the button is enabled by default. By pressing the button, the application PI controllers on the embedded side are updated with the ones displayed in output field data.
- Reload Data the button is disabled by default. The button becomes enabled as soon as one of the input Loop
  Parameters is changed. The background of the cell is changed from white to pink color for the purpose of change
  signalization. By pressing the Reload Data button all the modified cells will be rewritten with original values taken
  from the file. After successful data reload, the background of the cells becomes white again and the button gets
  disabled.
- Store Data the button is disabled by default. The button becomes enabled as soon as one of the input Loop Parameters is changed. The background of the cell is changed from white to pink color for the purpose of change signalization. By pressing the Store Data button all new values from modified cells will be saved into the file. After successful data saving, the background of the cells becomes white and the button gets disabled.

The editing fields accept only numeric characters. The parameter values are fully under user responsibility and no additional checking is applied to those items. The typical range of the parameter value appears when the mouse pointer is in a parameter name focus.



#### 6.5 POSPE sensors tab

The most important signals in the PMSM FOC control scheme are speed and position feedbacks. The POSPE sensors (PS) tab deals with the algorithm for the speed and position signals estimation. An angle tracking observer (ATO) represents a Freescale SW solution for obtaining the actual angle and speed of the resolver and encoder sensors.

Similar to previous tabs, the PS tab is also divided into two parts. The first part represents an input data field with required sensor parameters and ATO loop parameters needed for ATO PI controller parameters calculation. The second one is an output data field displaying the calculated parameters of the ATO algorithm. The ATO PI controller constants are calculated from the application scales and ATO loop parameters.

Application tuning modes available in POSPE sensors tab:

- Basic highly recommended for users who are not enough experienced in motor control theory. Only sensor parameters are required as an input in this mode. Position observer input parameters of the PS tab are estimated from the motor and application parameters automatically by MCAT tool engine. The cells requiring these parameters are shadowed with the status read-only, as shown in Figure 13.
- Expert all input parameter cells of the PS tab are accessible and freely editable by a user, as shown in Figure 14. However, their setting requires a certain level of expertise in motor control theory.

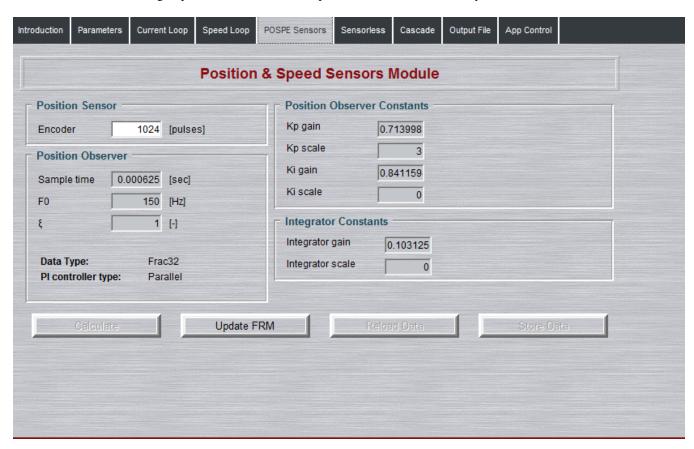


Figure 13. POSPE sensor tab - Basic mode



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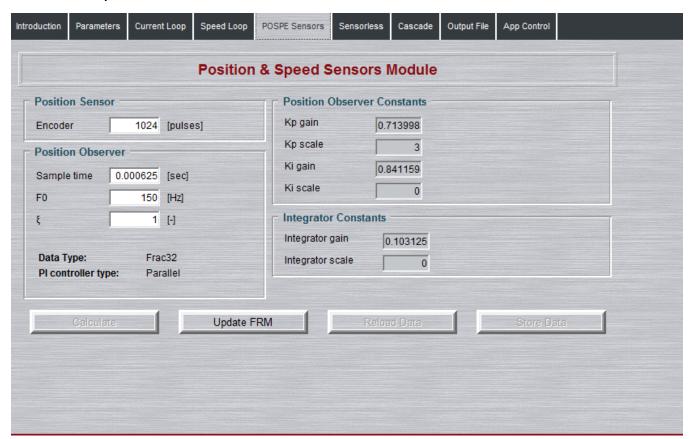


Figure 14. POSPE sensor tab - Expert mode

Table 6 shows the list of the POSPE Sensors tab inputs with their physical units, brief description, the impacted algorithms and accessibility status in basic mode.

Table 6. Inputs of the POSPE Sensors tab

Parameter Name	Units	Description	Use in Constant calculation	Basic mode accessibility
Encoder	[pulses]	Pulses of an encoder	ATO PI controller	YES
Resolver	[-]	Pole pairs of resolver	ATO PI controller	YES
Sample Time	[sec]	Observer sampling time	ATO PI controller	NO
F0	[Hz]	Observer bandwidth	ATO PI controller	NO
ξ	[-]	Observer attenuation	ATO PI controller	NO



## 6.5.1 POSPE sensors setting variability

The PI controller within an ATO algorithm can be implemented by both parallel and recurrent way. The MCAT tool supports both types of PI controllers as well as respects the variability of data type representation. The available setting modes supported by the POSPE sensors tab can be seen in Table 7.

Table 7. Summary of POSPE sensors setting modes

Position and Speed Sensor module	Applicable changes
PI controllers	Parallel/Recurrent form
Data type representation	FIX, FLOAT arithmetic

#### NOTE

All settings shown in Table 7 will be predefined by Freescale developer according to the MC reference application.

## 6.5.2 POSPE sensors parameter calculation

Angle Tracking Observer algorithm is used for the estimation of the rotor angle and the angular speed. The ATO approach yields smooth and accurate estimations. As in any common closed-loop systems, the intent is to minimize observer error. The observer error is given here by subtraction of the estimated resolver rotor angle  $\Theta_{est}$  from the actual rotor angle  $\Theta_{r}$ , see Figure 15.

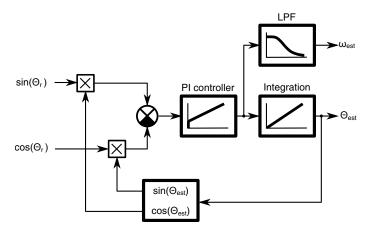


Figure 15. Block scheme of the Angle Tracking Observer

The position tracking structure according to the scheme Figure 15 can be expressed by the following transfer function:

$$G_{\text{ATO}}(s) = \frac{\theta_{\text{est}}(s)}{\theta_{\text{err}}(s)} = \frac{K_{P\_\text{ATO}}s + K_{I\_\text{ATO}}}{s^2 + K_{P\_\text{ATO}}s + K_{I\_\text{ATO}}}$$

#### Equation 25.

The observer error corresponds to the formula of the difference of two angles:

$$\sin(\theta_r)\cos(\theta_{est}) - \cos(\theta_r)\sin(\theta_{est}) = \sin(\theta_r - \theta_{est})$$

#### Equation 26.

The ATO PI controller can be designed by comparing the closed loop characteristic polynomial (Equation 25 on page 23) with that of a standard second order system and the angle tracking observer coefficients  $K_{P\_ATO}$  and  $K_{I\_ATO}$  can by calculated using:



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$$K_{P\_ATO}(z) = K_{P\_ATO}(s) = 4\pi\xi f_0$$

## Equation 27.

$$K_{I\_ATO}(z) = K_{I\_ATO}(s)T_S = (2\pi f_0)^2 T_S$$

#### Equation 28.

where  $\xi$  is the required attenuation,  $f_0$  required bandwidth (in Hz) and  $T_S$  is sampling time. The constants (Equation 27 on page 23, Equation 28 on page 24) represent a parallel form of PI controller, whereas the recurrent type of PI controller utilizes CC1 and CC2 constants:

$$CC_{1 \text{ ATO}} = K_{P \text{ ATO}} + K_{I \text{ ATO}} \frac{T_S}{2}$$

#### Equation 29.

$$CC_{2 \text{ ATO}} = -K_{P\_ATO} + K_{I\_ATO} \frac{T_S}{2}$$

## Equation 30.

The PI controller coefficients (Equation 27 on page 23, Equation 28 on page 24, Equation 29 on page 24, Equation 30 on page 24) are used in case of floating point data representation. The discrete fixed point arithmetic implementation of PI controllers requires the scaling approach to keep all signals in the range <-1, 1). Detailed description of proper PI controller's parameters scaling is in [3], [4].

#### 6.5.3 Parameter modification

All parameter cells are filled automatically with predefined data downloaded from an external file. The parameter cells are freely accessible for editing in accordance to the selected tuning mode, as it is shown in Table 6. There are four user buttons on the page with the following functionality:

- Calculate the button is disabled by default. The button becomes enabled as soon as one of the input sensor or observer parameters is changed. The background of the cell is changed from white to pink color for the purpose of changes signalization. By pressing the Calculate button PI controller parameters and integral coefficient are recalculated according to the POSPE sensors parameter calculation.
- Update FRM the button is enabled by default. By pressing the button, the application PI controllers on the embedded side are updated with those ones displayed in output field data.
- Reload Data the button is disabled by default. The button becomes enabled as soon as one of the input sensor or
  observer parameters is changed. The background of the cell is changed from white to pink color for the purpose of
  changes signalization. By pressing the Reload Data button the all modified cells will be rewritten with original values
  taken from the file. After successful data reload, the background of the cells becomes again white and the button gets
  disabled
- Store Data the button is disabled by default. The button becomes enabled as soon as one of the input sensor or observer parameters is changed. The background of the cell is changed from white to pink color for the purpose of changes signalization. By pressing the Store Data button all new values from modified cells will be saved into the file. After successful data saving, the background of the cells becomes white and the button gets disabled.

The editing fields accept only numeric characters. The parameter values are fully under a user responsibility and no additional checking is applied to those items. The typical range of the parameter value appears when the mouse pointer is in a parameter name focus.



## 6.6 Sensorless tab

As it has been mentioned, the most important signals in the PMSM FOC control scheme are speed and position feedbacks. They can be acquired from either physical speed sensors or some advanced observer algorithms. The Sensorless (SLS) tab deals with a Back Emf (BEMF) observer as a sensorless algorithm for the speed and position signals estimation.

Similar to previous tabs, the SLS tab is also divided into two parts. The first part represents an input data field with required sensorless parameters and parameters for open loop start-up. The second one is an output data field displaying the calculated parameters of BEMF observer, tracking observer (TO) and open loop start-up.

Application tuning modes available in Sensorless tab:

- Basic highly recommended for users who are not enough experienced in motor control theory. Only open loop startup parameters are required as an input in this mode. The BEMF observer and tracking observer input parameters are estimated from the motor and application parameters automatically by MCAT tool engine. The cells requiring these parameters are shadowed with the status read-only, as in Figure 16.
- Expert all input parameter cells of the SLS tab are accessible and freely editable by an user, as in Figure 17. However, their setting requires a certain level of expertise in motor control theory.

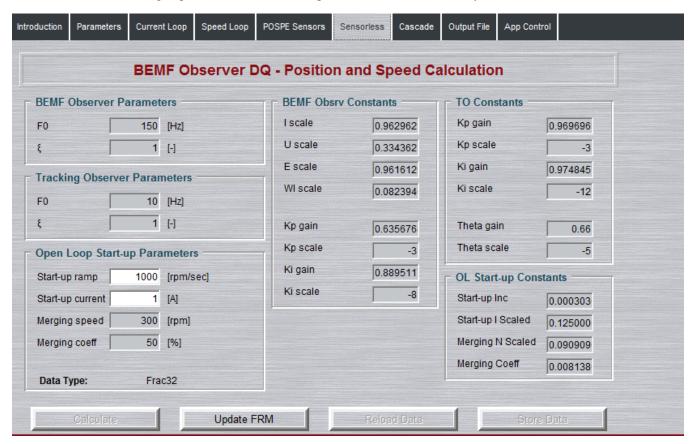


Figure 16. Sensorless tab – Basic mode



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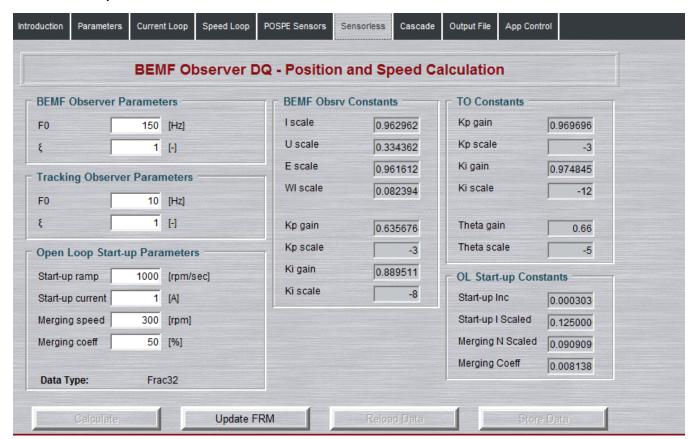


Figure 17. Sensorless tab - Expert mode

The Table 8 shows the list of the Sensorless tab inputs with their physical units, brief description, the impacted algorithms and accessibility status in basic mode.

Table 8. Inputs of the Sensorless tab

Parameter Name	Units	Description	Use in Constant calculation	Basic mode accessibility
F0	[Hz]	BEMF loop natural frequency	BEMF observer	NO
ξ	[-]	BEMF loop attenuation	BEMF observer	NO
F0	[Hz]	TO loop natural frequency	Tracking observer	NO
ξ	[-]	TO loop attenuation	Tracking observer	NO
Start-up ramp	[rpm/sec]	The slope of risen current	Open loop start-up	YES
Start-up current	[A]	Current limit for start-up process	Open loop start-up	YES
Merging speed	[rpm]	Switch open– to closed loop at given speed	Open loop start-up	NO
Merging speed	[%]	How fast switch open – to closed loop position	Open loop start-up	NO



## 6.6.1 Sensorless setting variability

The only variability within the Sensorless tab is given by a different data type representation, as in Table 9.

#### Table 9. Summary of Sensorless setting modes

Position and Speed Sensor module	Applicable changes
Data type representation	FIX32, FIX16

#### NOTE

All settings shown in Table 9 will be predefined by Freescale developer according to the MC reference application.

## 6.6.2 Sensorless algorithm parameter calculation

Detailed overview describing the coefficient calculation of Back EMF observer and Tracking observer is shown in [4].

#### 6.6.3 Parameter modification

All parameter cells are filled automatically with predefined data downloaded from an external file. The parameter cells are freely accessible for editing in accordance to the selected tuning mode, as it is shown in Table 8. There are four user buttons on the page with the following functionality:

- Calculate the button is disabled by default. The button becomes enabled as soon as one of the input sensor or observer parameters is changed. The background of the cell is changed from white to pink color for the purpose of change signalization. By pressing the Calculate button PI controller parameters and integral coefficient are recalculated according to the Sensorless algorithm parameter calculation.
- Update FRM the button is enabled by default. By pressing the button, the application algorithms on the embedded side are updated with the ones displayed in output field data.
- Reload Data the button is disabled by default. The button becomes enabled as soon as one of the input BEMF, TO or
  open loop start-up parameter is changed. The background of the cell is changed from white to pink color for the
  purpose of changes signalization. By pressing the Reload Data button the all modified cells will be rewritten with
  original values taken from the file. After successful data reload, the background of the cells becomes again white and
  the button gets disabled.
- Store Data the button is disabled by default. The button becomes enabled as soon as one of the input sensor or observer parameters is changed. The background of the cell is changed from white to pink color for the purpose of change signalization. By pressing the Store Data button all new values from modified cells will be saved into the file. After successful data saving, the background of the cells becomes white and the button gets disabled.

The editing fields accept only numeric characters. The parameter values are fully under user responsibility and no additional checking is applied to those items. The typical range of the parameter value appears when the mouse pointer is in a parameter name focus.

## 6.7 Output file tab

Previous tabs are mainly dedicated to tuning the motor control applications. Once the application is tuned according to the requirements, it might be useful to store the coefficients that correspond to the overall electrical drive. For this purpose, an Output File tab has been designed and it is a part of tab menu.

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The Output File (OF) tab serves a preview of the application coefficients that correspond to the tuned motor control application, as in Figure 18. The coefficients are thematically divided into the groups according to selected control tabs as follows:

- Application scales
- · Mechanical alignment
- Current loop parameters
- Speed loop parameters
- Position and Speed Sensors module parameters (if required)
- Sensorless BEMF DQ observer (if required)
- Cascade control structure parameters (if required)
- FreeMASTER scale variables

There are no application tuning modes available for this tab.



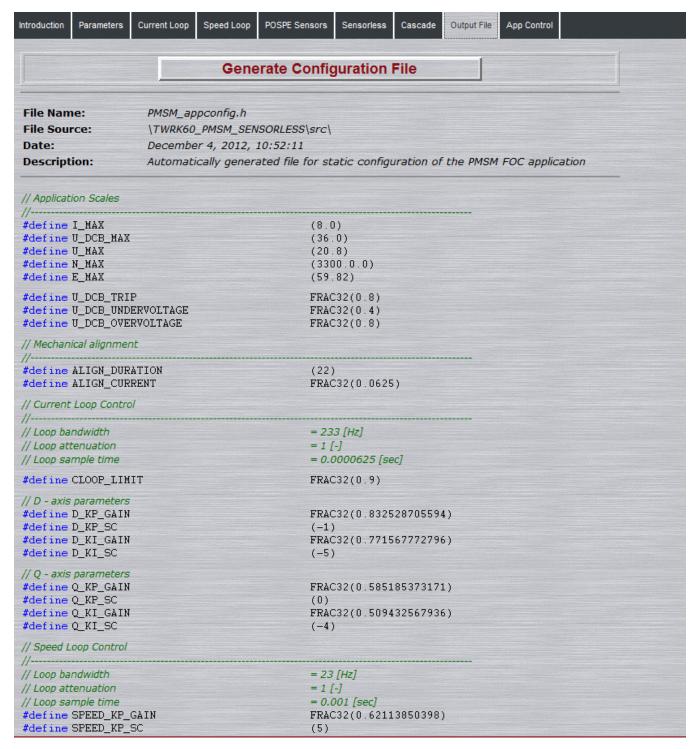


Figure 18. Output File tab example

In other words, the Output File tab shows a content of the file that can be generated by MCAT tool. The coefficients that correspond to the tuned application represent the static configuration of the PMSM FOC application. Static configuration file is a part of the S/W package, as seen in Figure 1, and it is linked with the application source code as a header file.



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## 6.7.1 Output file generation

To generate the content of the Output File tab, Generate Configuration File button needs to be pressed. The header file PMSM\_appconfig.h is generated and will be saved to the default path.

## 6.8 Cascade tab

Cascade tab deals with the control structure of the PMSM motor. Assuming that the embedded application is based on the cascade control structure, depicted in Figure 2, the Cascade tab might be very helpful. Connecting and tuning new electric drive setup becomes easier because the MCAT tool via Cascade tab offers a possibility to split the control structure and consequently to control the motor at various levels of cascade control structure. Such cascade control loops arrangement results to four optional control modes:

- scalar control mode
- · voltage FOC control
- · current FOC control
- speed FOC control

The Cascade tab contains ON/OFF switch that can run the application, a window for displaying the current application state, Update FRM button that provides an update of reference variables on embedded application side and finally the window with separately distributed control buttons for each available level of control structure. The functionality of each control mode will be described in the following topics.

Application tuning modes available in Cascade tab:

- Basic highly recommended for users who are not enough experienced in motor control theory, as in Figure 19. The inputs availability in basic mode depends on the selected control mode and will be described in the related topics.
- Expert all input parameter cells of the Cascade tab are accessible and freely editable by an user, as in Figure 20. However, their setting requires a certain level of expertise in motor control theory.



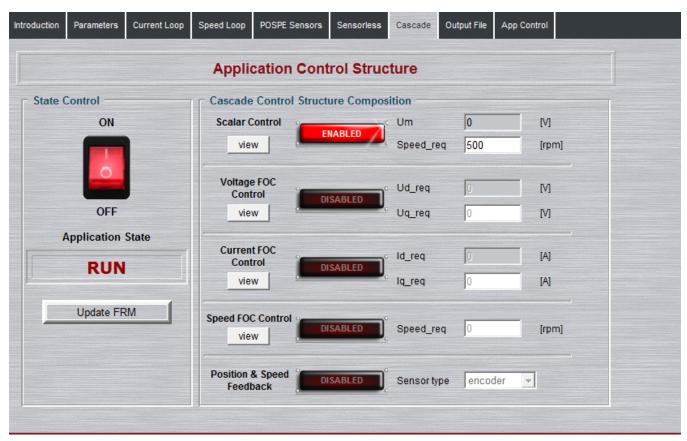


Figure 19. Cascade tab - Basic mode



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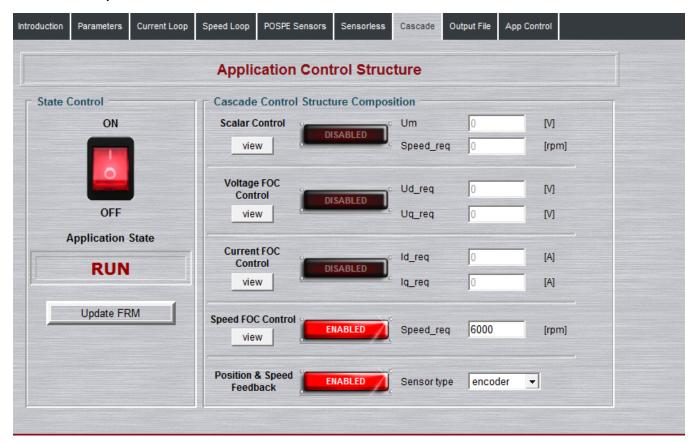


Figure 20. Cascade tab – Expert mode

Despite the tool deals with the common cascade control structure, getting a full support of Cascade tab requires software switches in the embedded FOC implementation. Such modification will be an integral part of Freescale reference source code. Then the toggling control mode can be used.

#### 6.8.1 Scalar Control

It is the simplest type of electric drives control strategy. The motor is supplied with the set of voltages given by the following expression:

$$U_{\rm abc} = U_m \sin(\theta_e \pm \frac{2}{3}\pi)$$

## **Equation 31**

$$\theta_e = \int \left(\frac{2\pi}{60} N_{\text{req}}\right) dt$$

## **Equation 32**

The ratio between the magnitude of the voltage and the frequency (frequency information is hidden in the Nreq) has to be kept at the nominal ratio. Therefore, attention must be paid during entering required voltage and speed in expert tuning mode. The ratio will be automatically kept constant in basic tuning mode and user does not have to take care about that. The only required input will be required speed.

As can be seen from the Figure 21, there is no feedback in the control structure hence the name open loop control.



Figure 21. Scalar control mode

In fact, it is not very common to use scalar control for PMSM motors. Such control approach can be used just for initial application tuning. Since there are no any feedbacks, it is the easiest way to get the motor run just hooked with new inverter. Once the motor rotates, sensor/estimator signals can be evaluated and aligned with the direction of rotation and so on.

If it is done, the control loop can be closed with the rotor position signal by toggling Voltage FOC Control method.

## 6.8.2 Voltage FOC control

If the direction of the rotor spinning is according to the user demand and the measured/estimated position gives also correct direction, the Voltage FOC control can be chosen. There are two reference variables available for motor controlling, as in Figure 22. Required voltage in d axis  $U_{d\_req}$  is actually not enabled in basic tuning mode. The q-component of the voltage  $U_{q\_req}$  represents a torque component and by its application the motor will run.

Once the motor runs, few tests should be provided in order to verify the conditions needed for successful torque and consequently speed control. If positive  $U_{q\_req}$  voltage is applied to the motor, rotor should rotate to the positive direction and vice versa. Consequently the currents have to be checked. The correct phases order and polarity of the currents have to be checked.

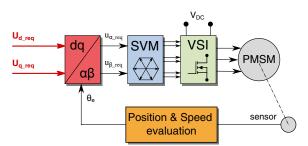


Figure 22. Voltage FOC control mode

If it is done, a control loop can be then closed with the current feedback signals by toggling the Current FOC Control.

## 6.8.3 Current FOC control

Current control or also called torque control requires rotor position feedback as well as the currents transformed into the dq-synchronous frame. There are two reference variables available for motor controlling, as in Figure 23. Required current in d axis  $I_{d\_req}$  is actually not enabled in basic tuning mode and is kept at zero by default. The q-component of the current  $I_{q\_req}$  represents a torque component and by its application the motor will run. By changing the polarity of the current  $I_{q\_req}$  the motor will change the direction of the rotation.

Supposing the Position and Speed evaluation algorithms are tuned correctly, the current PI controllers can be tuned using Current Loop tab.



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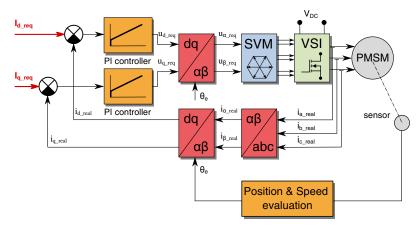


Figure 23. Current (torque) control mode

If the motor runs correctly and the Position/Speed evaluation algorithm provides correct information about the speed, the current control loop can be then closed with an outer speed loop by toggling the Speed FOC Control.

## 6.8.4 Speed FOC control

Speed control loop requires information about the actual rotor speed. This can be provided by physical sensor or sensorless algorithm.

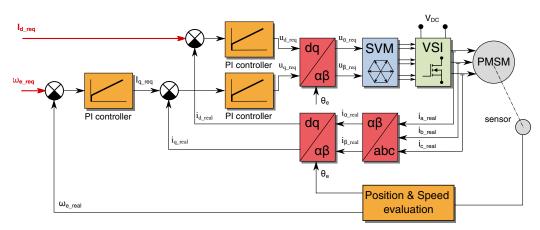


Figure 24. Speed FOC control mode

Supposing the current controllers are tuned correctly, the speed PI controller can be tuned using Speed Loop tab.

## 6.8.5 Cascade control structure controlling

The variables are entered to the white boxes of the selected control method. The cells disabled due to the basic tuning mode are shadowed. Selected method is marked with a red colored button with a title ENABLED. To change the control structure safety the application must be OFF. Toggling the control strategy the related red colored button has to be pressed.

Each change of reference value has to be confirmed by a button Update FRM.

If there is more than one source of the position/speed information, the proper sensor type can be selected from the list Sensor type.



## 6.9 Application control tab

The last tab available from the menu is App Control tab. It is a voluntary tab that offers a possibility to display an optional application control HTML-based page. This option will be fully supported by a Freescale developer and will depend on the application type as well as the target MCU.

As an example of possible application control pages can be found [5] [6].

## 7 References

- 1. FreeMASTER user's manual, freescale.com/FreeMASTER
- 2. AN4518, Dual 3-Phase PMSM Development Kit with MPC5643L, freescale.com/AutoMCDevKits
- 3. Automotive Math and Motor Control Library Set, fixed-point arithmetic, freescale.com/AutoMCLib
- 4. Embedded Software and Motor Control Libraries
- 5. AN4561, 3-Phase PMSM Motor Control Kit with the MPC5604P, page 24
- 6. DRM110, Sensorless PMSM Control for an H-axis Washing Machine Drive, page 6-65



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