# Analog IC Design – Cadence Tools

Lab 03

Cascode Amplifier

# **Part 1: Sizing Chart**

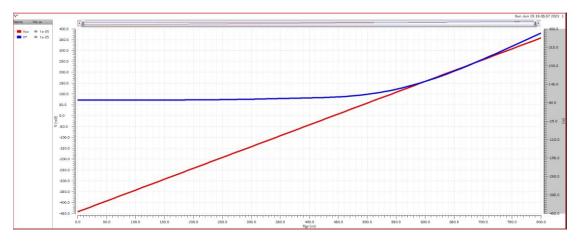


Figure 1 V\* and Vov VS VGS

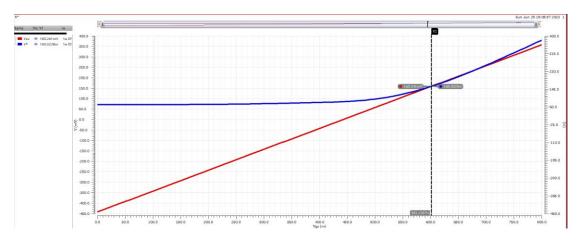


Figure 2 V\* =160m v

The corresponding VovQ = 160.241 m v and VGSQ = 601.235 m v

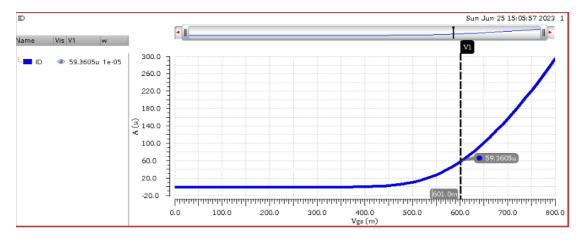


Figure 3 ID VS VGS

The corresponding ID = IDx = 59.3605u

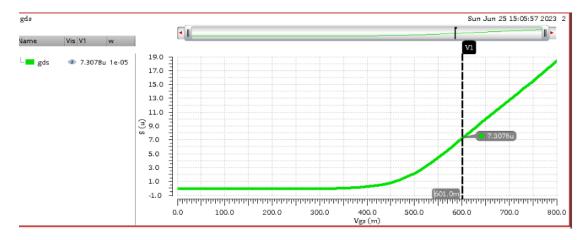


Figure 4 gds VS VGS

The corresponding gds = gdsx = 7.3078u

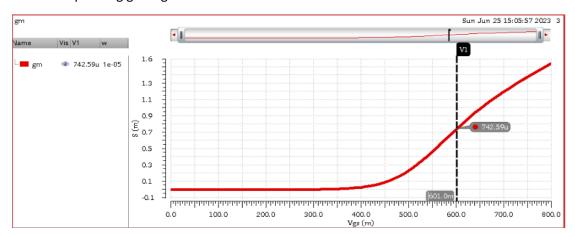


Figure 5 gm VS VGS

The corresponding gm = gmx = 742.59u

W	ID	
10u	59.3605u	
2.52693u	15 u	

W=2.52693u

gm	ID
742.59u	59.3605u
187.6475u	15 u

gmQ = 187.6475u

gds	ID
7.3078u	59.3605u
1.846632u	15 u

gdsQ=1.846632u

# **PART 2: Cascode for Gain**

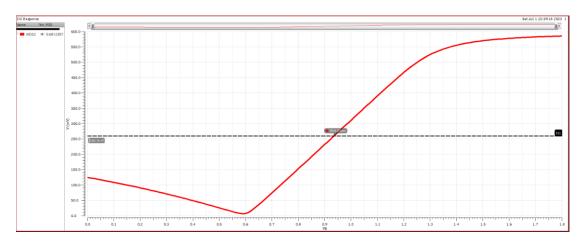


Figure 6 VDS2 VS VB

VB = 934m v

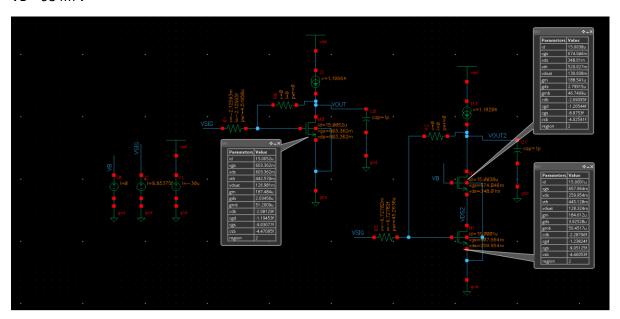


Figure 7 OP points

All transistors are in saturations (region = 2)

	Actual for CS	Designed for CS	
gm	187.484u	187.6475u	
gds	2.0346u	1.846632u	

#### Vth for M1 & M2 & M3

$$V_{TH} = V_{THo} + \gamma \left( \sqrt{2\varphi_F + V_{SB}} - \sqrt{|2\varphi_F|} \right)$$

Transistors have the different  $V_{th}$ , because Vth depend on the value of  $V_{SB}$  and as  $V_B$  is grounded, so the value of  $V_{th}$  will depend only on  $V_S$ , so as shown  $V_{th1}$  and  $V_{th2}$  are equal because  $V_S$  is equal and  $V_{th3}$  is different from them because its value of  $V_S$  is different.

( Note that all transistors are identical)

gm >> gds

gm > gmb

cgs > cgd

csb > cdb

gm	187.484u
gds	2.03456u
gmb	51.2009u
cdb	-2.08129f
cgd	-1.19453f
cgs	-9.03077f
csb	-4.47095f

# 2. AC Analysis

Test	Output	Nominal
Lab_1:LAB_3:1	Vout_dB	<u>L</u>
Lab_1:LAB_3:1	max_Vout_dB	39.29
Lab_1:LAB_3:1	max_Vout_mag	92.15
Lab_1:LAB_3:1	BW_Vout	322.4k
Lab_1:LAB_3:1	GBW1	29.78M
Lab_1:LAB_3:1	UGF1	30.03M
Lab_1:LAB_3:1	Vout2_dB	<u>L</u>
Lab_1:LAB_3:1	max_Vout2_dB	72.04
Lab_1:LAB_3:1	max_Vout 2_mag	4k
Lab_1:LAB_3:1	BW_Vout2	7.206k
Lab_1:LAB_3:1	GBW2	28.9M
Lab_1:LAB_3:1	UGF2	29.16M

Figure 8 circuit parameters

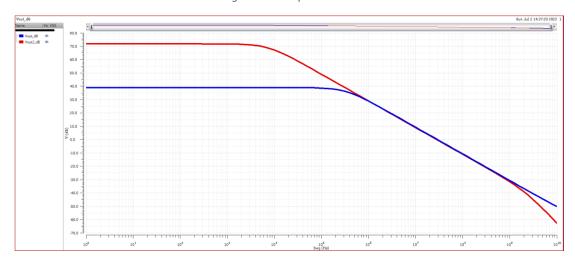


Figure 9 Bode plot (magnitude) of CS and cascode

## **Hand analysis:**

C (out) =1P, as all parasitic capacitances << 1P, and in parallel with it.

$$r_o = \frac{1}{g_{ds}}$$

DC gain (CS) = 
$$-g_m * r_o = \frac{-g_{m1}}{g_{ds1}} = \frac{-187.5}{2.035} = -92.137$$

$$r_{o2t} = (r_{o1} + r_{o2} + (g_{m2} + g_{mb2}) * r_{o1} * r_{o2})$$

$$r_{o2t} = \left(\frac{1}{3.9528u} + \frac{1}{2.79915u} + (188.5u + 46.75u) * \frac{1}{3.9528u} * \frac{1}{2.8u}\right) = 21.9M$$

$$\textit{DC gain (Cascode)} = -g_{m1} * r_{o2t} = -184.612u * 21.9M = -4240.65 = -4.039K$$

$$BW(CS) = \frac{1}{2*\pi*r_o*C} = \frac{2.035u}{2\pi*1p} = 323.88K$$

$$BW(Cascode) = \frac{1}{2*\pi*r_{o2t}*C} = \frac{1}{2\pi*21.9M*1p} = 7.267K$$

$$GBW(CS) = BW1 * DC gain 1 = 29.84133M$$

$$GBW(Cascode) = BW2 * DC gain 2 = 29.3514M$$

GPW analytically is UGF (unity gain frequency)

Lab_1:LAB_3:1	UGF1	30.03M
-		
Lab_1:LAB_3:1	UGF2	29.16M

## **Comments:**

The Cascode amplifier Gain is higher than the common-source amplifier Gain, as The Cascode amplifier has higher Rout and  $DC gain = -g_m * r_o$ .

The Cascode amplifier Bandwidth is lower than the common-source amplifier Bandwidth, as The Cascode amplifier has higher Rout and  $BW = \frac{1}{2*\pi*r_o*C}$ .