

**Analog IC Design****Lab 04****Common Drain Frequency Response****Intended Learning Objectives**

In this lab you will:

- Design and simulate a common-drain amplifier.
- Learn how to generate and use design charts.
- Learn how to do ac, DC, and transient simulations of a CD amplifier.
- Investigate the ringing and peaking problem in a capacitive-loaded CD amplifier with a large signal source resistance ( $R_{sig}$ ) and learn how to solve it.
- Use PMOS input transistor to avoid body effect in a CD amplifier.

**Part 1: Sizing Chart**

- 1) We can show that the intrinsic gain of a MOSFET is given by

$$|A_v| \approx g_m r_o = \frac{2I_D}{V_{ov}} \times \frac{V_A}{I_D} = \frac{2V_A}{V_{ov}}$$

Interestingly, the gain only depends on  $\lambda$  and  $V_{ov}$ . However, to derive this expression we used  $g_m = \frac{2I_D}{V_{ov}}$  which is based on the square-law. For a real MOSFET, if we compute  $V_{ov}$  and  $\frac{2I_D}{g_m}$  they will not be equal. Let's define a new parameter called V-star ( $V^*$ ) which is calculated from actual simulation data using the formula

$$V^* = \frac{2I_D}{g_m} \leftrightarrow g_m = \frac{2I_D}{V^*}$$

For a square-law device,  $V^* = V_{ov}$ , however, for a real MOSFET they are not equal. The actual gain is now given by

$$|A_v| \approx \frac{2V_A}{V^*}$$

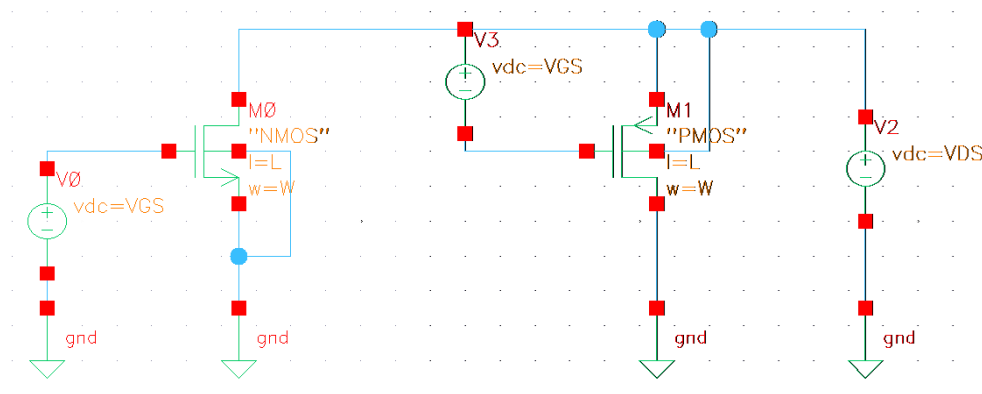
The lower the  $V^*$  the higher the gain, but the larger the area and the lower the speed. An often used sweet-spot that provides good compromise between different trade-offs is  $V^* = 200mV$ .

- 2) We want to design a CD amplifier with the parameters below.

Parameter	0.13um CMOS	0.18um CMOS
Input transistor	PMOS	PMOS
$L$	$1\mu m$	$1\mu m$
$V^*$	$200mV$	$200mV$
Supply	$1.2V$	$1.8V$
Current consumption	$10\mu A$	$10\mu A$

- 3) The remaining variable in the design is to calculate  $W$ . Since the square-law is not accurate, we cannot use it to determine the sizing. Instead, we will use a sizing chart generated from simulation.

Create a testbench for PMOS transistor as shown below (we will use PMOS only in this lab). Use  $W = 10\mu m$  (we will understand why shortly) and  $L = 1\mu m$  (the same  $L$  selected before).



- 4) Sweep  $V_{GS}$  from 0 to  $\approx V_{TH} + 0.4V$  with 10mV step. Set  $V_{DS} = V_{DD}/2$ .
- 5) We want to compare  $V^* = 2I_D/g_m$  and  $V_{ov} = V_{GS} - V_{TH}$  by plotting them overlaid. Use the calculator to create expressions for  $V^*$  and  $V_{ov}$ . You can save the expressions to reuse them later.
- 6) Plot  $V^*$  and  $V_{ov}$  overlaid vs  $V_{GS}$ . Make sure the y-axis of both curves has the same range. You will notice that at the beginning of the strong inversion region,  $V^*$  and  $V_{ov}$  are relatively close to each other (i.e., square-law is relatively valid). For deep strong inversion (large  $V_{ov}$ : velocity saturation and mobility degradation) or weak inversion (near-threshold and subthreshold operation) the behavior is quite far from the square-law.
- 7) An often used sweet-spot that provides good compromise between different trade-offs is  $V^* = 200mV$ . On the  $V^*$  and  $V_{ov}$  chart locate the point at which  $V^* = 200mV$ . Find the corresponding  $V_{ovQ}$  and  $V_{GSQ}$ .
- 8) Plot  $I_D$ ,  $g_m$ , and  $g_{ds}$  vs  $V_{GS}$ . Find their values at  $V_{GSQ}$ . Let's name these values  $I_{DX}$ ,  $g_{mX}$ , and  $g_{dsX}$ .
- 9) Now back to the assumption that we made that  $W = 10\mu m$ . This is not the actual value that we will use for our design. But the good news is that  $I_D$  is always proportional to  $W$  irrespective of the operating region and the model of the MOSFET (regardless square-law is valid or no). Thus, we can use ratio and proportion (cross-multiplication) to determine the correct width at which the current will be  $I_{DQ} = 10\mu A$  as given in the specs. Calculate  $W$  as shown below.

$W$	$I_D$
$10\mu m$	$I_{DX} @ V_Q^*$ (from the chart)
?	$I_{DQ} = 10\mu A$ (from the specs)

- 10) Now we are almost done with the design of the amplifier. Note that  $g_m$  is also proportional to  $W$  as long as  $V_{ov}$  is constant. On the other hand,  $r_o = 1/g_{ds}$  is **inversely** proportional to  $W$  ( $I_D$ ) as long as  $L$  is constant. Before leaving this part, calculate  $g_{mQ}$  and  $g_{dsQ}$  using ratio and proportion (cross-multiplication).

## PART 2: CD Amplifier

### 1. OP (Operating Point) Analysis

- 1) Create a new schematic for the CD amplifier (the schematic is not included in the lab document and is left for the student as an exercise). Use a PMOS and use a  $10\mu A$  ideal current source for biasing (note that the current source will be connected to the source terminal). Connect the source to the bulk. Use  $L = 1\mu m$  and  $W$  as determined in Part 1. Use  $C_L = 2pF$ ,  $R_{sig} = 2M\Omega$ , and a DC input voltage = 0V.

- 2) Simulate the OP point. Report a snapshot clearly showing the following parameters (add a filter to your monitor).

ID
VGS
VDS
VTH
VDSAT
GM
GDS
GMB
CDB
CGD
CGS
CSB
Region

- 3) Check that the transistor operates in saturation.

## 2. AC Analysis

- 1) Perform AC analysis (1Hz:10GHz, logarithmic, 20points/decade) to investigate the frequency domain peaking.
- 2) Report the Bode plot magnitude.
- 3) Do you notice frequency domain peaking?  
→ Cadence Hint: Use the following expression to calculate the peaking in dB:  
`ymax(dB20(VF("/vout")))`
- 4) Analytically calculate quality factor (use approximate expressions). Is the system underdamped or overdamped?
- 5) (Optional) Perform parametric sweep: CL = 2p, 4p, 8p.
  - Report Bode plot magnitude overlaid on same plot.
  - Report the peaking vs CL.
  - Comment.
- 6) (Optional) Perform parametric sweep: R<sub>sig</sub> = 20k, 200k, 2M.
  - Report Bode plot magnitude overlaid on same plot.
  - Report the peaking vs R<sub>sig</sub>.
  - Comment.

## 3. Transient Analysis

- 1) Use a pulse source (pulse\_v\_source) as your transient stimulus and set it as follows (delay = 2us, initial = 0V, period = 8us, pulse\_value = 100mV, t<sub>fall</sub> = 1ns, t<sub>rise</sub> = 1ns, width = 4us). Run transient analysis (max step = 10n) for 10us to investigate the time domain ringing.
- 2) Report Vin and Vout overlaid vs time.
- 3) Calculate the DC voltage difference (DC shift) between Vin and Vout.
  - What is the relation between the DC shift and VGS?
  - How to shift the signal down instead of shifting it up?
- 4) Do you notice time domain ringing?  
→ Cadence Hint: Use the overshoot function to calculate the maximum overshoot as a percentage
- 5) (Optional) Perform parametric sweep: CL = 2p, 4p, 8p.
  - Report Vout vs time overlaid on same plot.
  - Report the overshoot vs CL.
  - Comment.
- 6) (Optional) Perform parametric sweep: R<sub>sig</sub> = 20k, 200k, 2M.
  - Report Vout vs time overlaid on same plot.

- Report the overshoot vs  $R_{sig}$ .
- Comment.

#### 4. $Z_{out}$ (Inductive Rise) (optional)

- 1) We want to simulate the CD amplifier output impedance. Replace CL with an AC current source with magnitude = 1. Remove the AC input signal.
- 2) Perform AC analysis (1Hz:10GHz, logarithmic, 10points/decade). The voltage across the AC current source is itself the output impedance.
- 3) Plot the output impedance (magnitude and phase) vs frequency. Do you notice an inductive rise? Why?
- 4) Does  $Z_{out}$  fall at high frequency? Why?  
Hint:  $C_{gd}$  appears in parallel with  $R_{sig}$ .
- 5) Analytically calculate the zeros, poles, and magnitude at low/high frequency for  $Z_{out}$ . Compare with simulation results in a table.

#### 5. How to solve the peaking/ringing problem? (optional)

- 1) Place the input/output poles away from each other (as we did when we swept CL and  $R_{sig}$ ).
- 2) (This part is optional) A compensation network can be used to compensate for the negative input impedance and prevent overshoots. Read [Johns and Martin, 2012] Section 4.4 and try to implement the compensation network.

## Lab Summary

In Part 1 you learned:

- How to generate and use design charts for NMOS and PMOS transistors.
- How to design a PMOS common-drain amplifier.
- How the overdrive voltage of a MOS transistor deviates from the square law in different regions of operation.

In Part 2 you learned:

- How to do ac, DC and transient simulations of a CD amplifier.
- How the peaking in the frequency response of a CD amplifier changes with the load capacitor and source resistance.
- How the ringing in the transient response of a CD amplifier changes with the load capacitor and source resistance.
- How the output impedance of a CD amplifier shows inductive behavior.

## Acknowledgements

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