

"Unit 1"

Coordinate system:-

- ① Cartesian
- ② spherical
- ③ cylindrical

① Cartesian:-

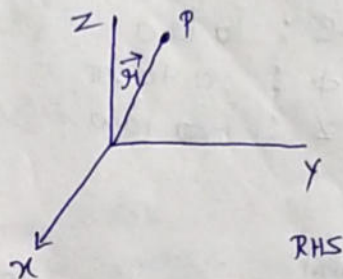
$$\vec{r} = x\hat{i} + y\hat{j} + z\hat{k}$$

★ limits:-

$$x: -\infty \text{ to } \infty$$

$$y: -\infty \text{ to } \infty$$

$$z: -\infty \text{ to } \infty$$



★ length element:-

$$dx = dx \hat{i}$$

$$dy = dy \hat{j}$$

$$dz = dz \hat{k}$$

★ Surface element:-

$$ds_x = dy \hat{j} \times dz \hat{k} = dy dz \hat{i}$$

$$ds_y = dx dz \hat{j}$$

$$ds_z = dx dy \hat{k}$$

★ Volume element:-

$$dV = \vec{dx} \cdot (\vec{dy} \times \vec{dz})$$

$$dV = dx dy dz$$

② spherical:- (r, θ, ϕ)

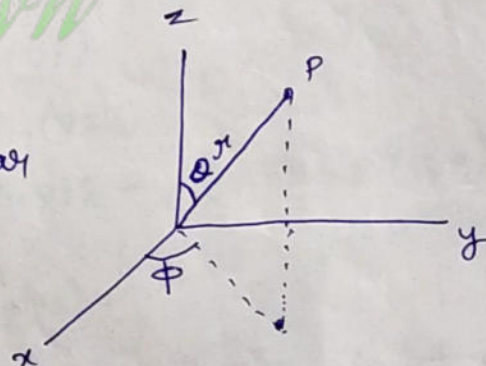
r, θ, ϕ will be mutually perpendicular

$$x = r \sin \theta \cos \phi$$

$$y = r \sin \theta \sin \phi$$

$$z = r \cos \theta$$

$$\vec{r} = r \sin \theta \cos \phi \hat{i} + r \sin \theta \sin \phi \hat{j} + r \cos \theta \hat{k}$$



★ limit:-

$$r: 0 \rightarrow \infty$$

$$\theta: 0 \rightarrow \pi$$

$$\phi: 0 \rightarrow 2\pi$$

★ length element:-

$$dr = dr \hat{r}, d\theta = r d\theta \hat{\theta}, d\phi = r \sin \theta d\phi \hat{\phi}$$

$$d\phi = r \sin \theta d\phi \hat{\phi}$$

★ Surface element:-

$$(r \rightarrow \text{fix}) ds_r = r^2 \sin \theta d\theta d\phi \hat{r}$$

$$(\theta \rightarrow \text{fix}) ds_\theta = r \sin \theta dr d\phi \hat{\theta}$$

$$(\phi \rightarrow \text{fix}) ds_\phi = r dr d\theta \hat{\phi}$$

★ Volume element:-

$$dV = r^2 \sin \theta dr d\theta d\phi$$

③ Cylindrical coordinate system :- (ρ, ϕ, z) or (s, ϕ, z)

$$x = \rho \cos \phi$$

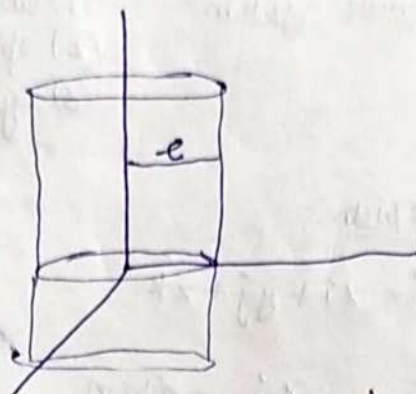
$$y = \rho \sin \phi$$

$$z = z$$

limit:- $\rho : 0 \text{ to } \infty$

$$\phi : 0 \text{ to } 2\pi$$

$$z : -\infty \text{ to } \infty$$



length element:-

$$d\rho = d\rho \hat{\rho}$$

$$d\phi = \rho d\phi \hat{\phi}$$

$$dz = dz \hat{z}$$

surface element:-

$$ds_{\rho} = d\phi \times dz$$

$$ds_{\phi} = \rho d\phi dz \hat{\phi}$$

$$ds_z = dz d\rho \hat{z}$$

$$ds_z = \rho d\rho d\phi \hat{z}$$

volume element:-

$$dv = \rho d\rho d\phi dz$$

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Gradient!- ① The gradient ∇T points in direction of max^m increase of function T .
 $\& |\nabla T|$ gives slope along this direction.

② $\nabla T = 0$ for max^m point, min point or a saddle point.
 (highest) (lowest)

③ scalar \rightarrow vector

Divergence!- $\nabla \cdot \vec{v}$ ① vector \rightarrow scalar
 ② point with +ve divergence = source
 " " -ve " = sink

Curl!- ① It is measure of how much a vector \vec{v} swirls around a point.

Imp. Rules!-

$$① \nabla(fg) = f\nabla g + g\nabla f$$

$$② \nabla(A \cdot B) = A \times (\nabla \times B) + B \times (\nabla \times A) + (A \cdot \nabla)B + (B \cdot \nabla)A$$

$$③ \nabla \cdot (fA) = f(\nabla \cdot A) + A \cdot (\nabla f)$$

$$④ \nabla \cdot (A \times B) = B \cdot (\nabla \times A) - A \cdot (\nabla \times B)$$

$$⑤ \nabla \times (A \times B) = (B \cdot \nabla)A - (A \cdot \nabla)B + A(\nabla \cdot B) - B(\nabla \cdot A)$$

for second derivatives (5 possibilities):-

$$① \text{Divergence of gradient} = \nabla \cdot (\nabla T) = \nabla^2 T \text{ (called as Laplacian of scalar } T)$$

for vector \vec{v} ,

$$\nabla^2 \vec{v} = (\nabla^2 v_x)\hat{i} + (\nabla^2 v_y)\hat{j} + (\nabla^2 v_z)\hat{k} \text{ (To calculate Laplacian of a vector)}$$

$$\text{where } \nabla^2 v_x = \left(\frac{d^2 v_x}{dx^2} + \frac{d^2 v_x}{dy^2} + \frac{d^2 v_x}{dz^2} \right)$$

$$\nabla^2 v_y = \frac{d^2 v_y}{dx^2} + \frac{d^2 v_y}{dy^2} + \frac{d^2 v_y}{dz^2}$$

$$\nabla^2 v_z = \frac{d^2 v_z}{dx^2} + \frac{d^2 v_z}{dy^2} + \frac{d^2 v_z}{dz^2}$$

② Curl of gradient:-

$$\nabla \times (\nabla T) = 0$$

③ Gradient of divergence:-

$$\nabla (\nabla \cdot \mathbf{v}) \neq \nabla^2 \mathbf{v}$$

④ Divergence of curl:-

$$\nabla \cdot (\nabla \times \mathbf{v}) = 0$$

⑤ Curl of curl:-

$$\nabla \times (\nabla \times \mathbf{v}) = \nabla (\nabla \cdot \mathbf{v}) - \nabla^2 \mathbf{v}$$

Integral Calculus:-

① Line integral:-

$$\int_a^b \mathbf{v} \cdot d\mathbf{l}$$

(Line integral is independent of path so called as conservative.)

$$(d\mathbf{l} = dx \hat{i} + dy \hat{j} + dz \hat{k})$$

② Surface integral:-

$$\oint_a^b \mathbf{v} \cdot d\mathbf{a}$$

(represents total mass per unit time passing through surface) called as flux.

$$d\mathbf{a} \hat{x} = dy dz \hat{i}$$

$$d\mathbf{a} \hat{j} = dx dz \hat{j}$$

$$d\mathbf{a} \hat{k} = dx dy \hat{k}$$

③ Volume integral:-

$$\int_V T d\tau$$

$$, (d\tau = dx dy dz)$$

Fundamental Theorem of Calculus:-

① $\int_a^b f(x) dx = f(b) - f(a)$

② Theorem for Gradients:-
for a function T

$$\int_a^b (\nabla T) \cdot d\mathbf{l} = T(b) - T(a)$$

① It is independent of path taken

② if $a=b \Rightarrow T(b) - T(a) = 0$

③ Theorem of divergence:-

$$\int_V (\nabla \cdot \mathbf{v}) d\tau = \oint_S \mathbf{v} \cdot d\mathbf{a}$$

Gauss' theorem
Green theorem
divergence theorem

$$d\tau = dx dy dz$$

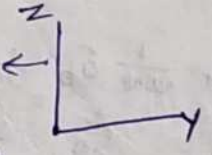
④ Theorem of curls:-

$$\int_S (\nabla \times \mathbf{v}) \cdot d\mathbf{a} = \oint_P \mathbf{v} \cdot d\mathbf{l}$$

Stoke's theorem

① $\int (\nabla \times \mathbf{v}) \cdot d\mathbf{a}$ depends only on the boundary line not on particular surface used

② $\oint (\nabla \times \mathbf{v}) \cdot d\mathbf{a} = 0$ for any closed surface

$$\begin{aligned} d\mathbf{a} &= dy dz \hat{i} & (\text{for } y-z \text{ plane}) \\ d\mathbf{a} &= dx dy \hat{k} & (\text{for } x-y \text{ plane}) \\ d\mathbf{a} &= dx dz \hat{j} & (\text{for } x-z \text{ plane}) \end{aligned}$$


② Spherical coordinates:-

$$x = r \sin \theta \cos \phi$$

$$y = r \sin \theta \sin \phi$$

$$z = r \cos \theta$$

$$\hat{r} = \sin \theta \cos \phi \hat{i} + \sin \theta \sin \phi \hat{j} + \cos \theta \hat{k}$$

$$\hat{\theta} = \cos \theta \cos \phi \hat{i} + \cos \theta \sin \phi \hat{j} - \sin \theta \hat{k}$$

$$\hat{\phi} = -\sin \phi \hat{i} + \cos \phi \hat{j}$$

$$dr = dr$$

$$d\theta = r d\theta$$

$$d\phi = r \sin \theta d\phi$$

$$dl = dr \hat{r} + r d\theta \hat{\theta} + r \sin \theta d\phi \hat{\phi}$$

① Gradient:-

$$\nabla T = \frac{\partial T}{\partial r} \hat{r} + \frac{1}{r} \frac{\partial T}{\partial \theta} \hat{\theta} + \frac{1}{r \sin \theta} \frac{\partial T}{\partial \phi} \hat{\phi}$$

② Divergence:-

$$\nabla \cdot \mathbf{V} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 V_r) + \frac{1}{(r \sin \theta)} \frac{\partial}{\partial \theta} (\sin \theta V_\theta) + \frac{1}{r \sin \theta} \frac{\partial V_\phi}{\partial \phi}$$

③ Curl:-

$$\nabla \times \mathbf{V} = \frac{1}{r \sin \theta} \left[\frac{\partial}{\partial \theta} (\sin \theta V_\phi) - \frac{\partial V_\theta}{\partial \phi} \right] \hat{r} + \frac{1}{r} \left[\frac{1}{\sin \theta} \frac{\partial V_r}{\partial \phi} - \frac{\partial}{\partial r} (r V_\phi) \right] \hat{\theta} + \frac{1}{r} \left[\frac{\partial}{\partial r} (r V_\theta) - \frac{\partial V_r}{\partial \theta} \right] \hat{\phi}$$

OR

$$\nabla \times \mathbf{A} = \begin{vmatrix} \frac{1}{r \sin \theta} \hat{r} & \frac{1}{r \sin \theta} \hat{\theta} & \frac{1}{r} \hat{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ 1 \cdot A_r & r A_\theta & r \sin \theta A_\phi \end{vmatrix}$$

$$\nabla \times \mathbf{V} = \begin{vmatrix} \hat{r} & \hat{\theta} & \hat{\phi} \\ \frac{1}{r^2 \sin \theta} & \frac{1}{r \sin \theta} & \frac{1}{r} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ r V_r & r V_\theta & r \sin \theta V_\phi \end{vmatrix}$$

$$= \frac{1}{r^2 \sin \theta} \hat{r} \left(\frac{\partial}{\partial \theta} (r \sin \theta V_\phi) - \frac{\partial}{\partial \phi} (r V_\theta) \right) - \frac{1}{r \sin \theta} \hat{\theta} \left(\frac{\partial}{\partial r} (r V_\phi) - \frac{\partial}{\partial \phi} (r V_r) \right) + \frac{1}{r} \hat{\phi} \left(\frac{\partial}{\partial r} (r V_\theta) - \frac{\partial}{\partial \theta} (r V_r) \right)$$

$$= \frac{1}{r \sin \theta} \left(\frac{\partial}{\partial \theta} (\sin \theta V_\phi) - \frac{\partial V_\theta}{\partial \phi} \right) \hat{r} + \frac{1}{r} \left(\frac{1}{\sin \theta} \frac{\partial V_r}{\partial \phi} - \frac{\partial}{\partial r} (r V_\phi) \right) \hat{\theta} + \frac{1}{r} \left(\frac{\partial}{\partial r} (r V_\theta) - \frac{\partial V_r}{\partial \theta} \right) \hat{\phi}$$

④ Laplacian:-

$$\nabla^2 T = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2}$$

Trick: from divergence again multiply ∇^2 by 1, r , $r \sin \theta$

③ Cylindrical Coordinate :- $(\hat{s}, \hat{\phi}, \hat{z})$

$$\begin{aligned} x &= s \cos \phi \\ y &= s \sin \phi \\ z &= z \end{aligned}$$

$$\left. \begin{aligned} ds &= ds \\ d\phi &= s d\phi \\ dz &= dz \end{aligned} \right\} \boxed{dl = ds \hat{s} + s d\phi \hat{\phi} + dz \hat{z}}$$

① Gradient :-

$$\boxed{\nabla T = \frac{\partial T}{\partial s} \hat{s} + \frac{1}{s} \frac{\partial T}{\partial \phi} \hat{\phi} + \frac{\partial T}{\partial z} \hat{z}}$$

② Divergence :-

$$\boxed{\nabla \cdot \mathbf{V} = \frac{1}{s} \frac{\partial}{\partial s} (s V_s) + \frac{1}{s} \frac{\partial V_\phi}{\partial \phi} + \frac{\partial V_z}{\partial z}}$$

③ Curl :-

$$\vec{\nabla} \times \mathbf{V} = \begin{vmatrix} \frac{1}{s} \hat{s} & \frac{1}{s} \hat{\phi} & \frac{1}{s} \hat{z} \\ \frac{\partial}{\partial s} & \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ V_s & s V_\phi & V_z \end{vmatrix}$$

$$= \frac{1}{s} \hat{s} \left(\frac{\partial V_z}{\partial \phi} - \frac{\partial (s V_\phi)}{\partial z} \right) + \hat{\phi} \left(\frac{\partial V_z}{\partial s} - \frac{\partial V_s}{\partial z} \right) + \frac{1}{s} \hat{z} \left(\frac{\partial}{\partial s} (s V_\phi) - \frac{\partial V_s}{\partial \phi} \right)$$

$$\vec{\nabla} \times \mathbf{V} = \hat{s} \left(\frac{1}{s} \frac{\partial V_z}{\partial \phi} - \frac{\partial V_\phi}{\partial z} \right) + \hat{\phi} \left(\frac{\partial V_z}{\partial z} - \frac{\partial V_s}{\partial s} \right) + \frac{1}{s} \hat{z} \left(\frac{\partial}{\partial s} (s V_\phi) - \frac{\partial V_s}{\partial \phi} \right)$$

④ Laplacian:-

$$\nabla^2 T = \frac{1}{s} \frac{\partial}{\partial s} \left(s \frac{\partial T}{\partial s} \right) + \frac{1}{s^2} \frac{\partial^2 T}{\partial T^2} + \frac{\partial^2 T}{\partial z^2}$$



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① Maxwell's Equations :- (4 eqn) for

① $\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$ (Gauss law of electrostatics)

② $\nabla \cdot \vec{B} = 0$ (" " of magnetostatics)

③ $\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$ (Faraday law of Mutual Induction)

④ $\nabla \times \vec{B} = \mu_0 \left(\vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right)$ (Modified Ampere's Circuital law)
 correction factor (displacement current)

Notations :-
 $\vec{D} = \epsilon_0 \vec{E}$ (displacement density)
 $\vec{H} = \frac{1}{\mu_0} \vec{B}$ (magnetic field intensity)
 $\vec{J} = \frac{1}{\mu_0} \vec{B}$ (current density)
 $B = \mu_0 H$

② In Integral form of these 4 eqn is -

① $\oint_S \vec{E} \cdot d\vec{s} = \frac{q}{\epsilon_0} = \frac{1}{\epsilon_0} \int_V \rho dv$ [Gauss Law]

② $\oint_S \vec{B} \cdot d\vec{s} = 0$

③ $\int_l \vec{E} \cdot d\vec{l} = -\frac{d}{dt} \int_S \vec{B} \cdot d\vec{s}$ [Faraday law]

④ $\int_l \vec{B} \cdot d\vec{l} = \mu_0 \oint_S \left(\vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right) \cdot d\vec{s}$

③ Derivation of Maxwell's equations -

$$\textcircled{1} \oint_s \vec{E} \cdot d\vec{s} = \frac{1}{\epsilon_0} \int_V \rho dv$$

Proof:

we know that

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon_0}$$

apply volume integral both sides

$$\int_V (\vec{\nabla} \cdot \vec{E}) dv = \frac{1}{\epsilon_0} \int_V \rho dv$$

apply gauss divergence Theorem -

$$\boxed{\oint_s \vec{E} \cdot d\vec{s} = \frac{1}{\epsilon_0} \int_V \rho dv} \quad \text{h.p.}$$

$$\textcircled{2} \oint_s \vec{B} \cdot d\vec{s} = 0$$

Proof:

$$\vec{\nabla} \cdot \vec{B} = 0$$

apply .VI both sides

$$\int_V (\vec{\nabla} \cdot \vec{B}) dv = 0$$

$$\boxed{\oint_s \vec{B} \cdot d\vec{s} = 0} \quad \text{h.p.}$$

$$\textcircled{3} \int_L \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \oint_s \vec{B} \cdot d\vec{s}$$

Proof:

we know that

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

apply surface integral -

$$\oint_s \vec{\nabla} \times \vec{E} \cdot d\vec{s} = -\frac{\partial}{\partial t} \oint_s \vec{B} \cdot d\vec{s}$$

apply stoke's theorem -

$$\boxed{\oint_L \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \oint_s \vec{B} \cdot d\vec{s}} \quad \text{h.p.}$$

$$\textcircled{4} \int_L \vec{B} \cdot d\vec{l} = \oint_s \left(\vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right) \cdot d\vec{s}$$

Proof:

$$\vec{\nabla} \times \vec{B} = \vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

apply s.o

$$\oint_S \vec{\nabla} \times \vec{B} \cdot d\vec{s} = \oint_S \left(\vec{J} + \frac{\partial \vec{P}}{\partial t} \right) \cdot d\vec{s}$$

$$\boxed{\int_L \vec{B} \cdot d\vec{l} = \oint_S \left(\vec{J} + \frac{\partial \vec{E}}{\partial t} \right) \cdot d\vec{s}}$$

④ Maxwell's 3rd eqn in differential form $\boxed{\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}}$

Proof: we know that by faraday's law of mutual induction

$$\boxed{\text{emf} = -\frac{d}{dt} \Phi_B} \quad \text{--- (i)}$$

also $\text{emf} = \oint_L \vec{E} \cdot d\vec{l}$ --- (ii)

using eqn (i) & (ii)

$$\oint_L \vec{E} \cdot d\vec{l} = -\frac{d}{dt} (\Phi_B) \quad \text{--- (iii)}$$

mag flux = $B \cdot A$

$$\Phi_B = \oint_S \vec{B} \cdot d\vec{s}$$

putting in eqn (iii)

$$\oint_L \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \left(\oint_S \vec{B} \cdot d\vec{s} \right)$$

by stoke's theorem

$$\oint_S (\vec{\nabla} \times \vec{E}) \cdot d\vec{s} = -\frac{\partial}{\partial t} \left(\oint_S \vec{B} \cdot d\vec{s} \right)$$

$$\oint_S \left[\vec{\nabla} \times \vec{E} + \frac{\partial}{\partial t} (\vec{B}) \right] \cdot d\vec{s} = 0$$

$$\boxed{\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}}$$

⑤ Maxwell's 4th eqn :- $\nabla \times \vec{B} = \mu_0 \left(\vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right)$

Proof: by ampere ckt law

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I$$

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 \int_S \vec{J} \cdot d\vec{s}$$

using stoke's theorem to LHS

$$\oint_S (\nabla \times \vec{B}) \cdot d\vec{s} = \mu_0 \int_S \vec{J} \cdot d\vec{s}$$

$$\oint_S [\nabla \times \vec{B} - \mu_0 \vec{J}] \cdot d\vec{s} = 0$$

$$\boxed{\nabla \times \vec{B} = \mu_0 \vec{J}} \text{ ---- (i)}$$

Now checking validity of eqn (i) -

using eqn of continuity i.e. $\nabla \cdot \vec{J} = -\frac{\partial \rho}{\partial t}$ ---- (ii)

Taking divergence of eqn (i)

$$\nabla \cdot (\nabla \times \vec{B}) = \mu_0 (\nabla \cdot \vec{J})$$

but from vector identity $\text{div}(\text{curl } \vec{B}) = 0$

so $\boxed{\nabla \cdot \vec{J} = 0}$ but eqn of continuity state that $\text{div}(\vec{J}) \neq 0$

hence we can say eqn (i) is not a valid eqn.

hence ~~the~~ maxwell modified the ampere's ckt law \rightarrow

maxwell introduced the concept of disp. current

$$\boxed{\nabla \times \vec{B} = \mu_0 (\vec{J} + \vec{J}_d)} \text{ ---- (ii)}$$

disp. current density

Now ~~test~~ checking validity of eqn -

$$\text{Div}(\text{curl } \vec{B}) = \mu_0 (\vec{\nabla} \cdot \vec{J} + \vec{\nabla} \cdot \vec{J}_d)$$

$$0 = \mu_0 (\vec{\nabla} \cdot \vec{J} + \vec{\nabla} \cdot \vec{J}_d)$$

$$\boxed{\vec{\nabla} \cdot \vec{J} = -\vec{\nabla} \cdot \vec{J}_d} \text{ ----}$$

that means $\vec{\nabla} \times \vec{J} \neq 0$ for eqn (ii)

hence eqn (ii) is a valid eqn.

$$** \boxed{\vec{\nabla} \times \vec{B} = \mu_0 (\vec{J} + \vec{J}_d)} **$$

⑥ Now maxwell modified the eqn as -

~~by eqn of continuity~~

$$\vec{\nabla} \cdot \vec{J} = -\vec{\nabla} \cdot \vec{J}_d$$

(by eqn of continuity)

$$-\frac{\partial e}{\partial t} = -\vec{\nabla} \cdot \vec{J}_d$$

$$\vec{\nabla} \cdot \vec{J}_d = \frac{\partial e}{\partial t}$$

$$\vec{\nabla} \cdot \vec{J}_d = \frac{\partial}{\partial t} (\vec{\nabla} \cdot \vec{E})$$

$$\left(\text{using maxwell 1st eqn} \right. \\ \left. \vec{\nabla} \cdot \vec{E} = \frac{e}{\epsilon_0} \right)$$

$$\vec{\nabla} \cdot \vec{J}_d = \epsilon_0 \frac{\partial}{\partial t} (\vec{\nabla} \cdot \vec{E})$$

$$\vec{\nabla} \cdot \vec{J}_d = \epsilon_0 \vec{\nabla} \cdot \frac{\partial \vec{E}}{\partial t}$$

$$\vec{\nabla} \cdot \left(\vec{J}_d - \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right) = 0$$

$$\boxed{\vec{J}_d = \epsilon_0 \frac{\partial \vec{E}}{\partial t}}$$

Putting value of \vec{J}_d in eqn (ii)

$$\boxed{\vec{\nabla} \times \vec{B} = \mu_0 \left(\vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right)}$$

hence proved

"Electrostatics"

Coulomb's law:-

$$F = \frac{1}{4\pi\epsilon_0} \frac{q_1 q_2}{r^2} \hat{r}_{12}$$

$$\epsilon_0 = 8.85 \times 10^{-12} \frac{C^2}{N \cdot m^2}$$

$$\frac{1}{4\pi\epsilon_0} = 9 \times 10^9 \frac{Nm^2}{C^2}$$

Electric field:-

$$F = QE$$

$$E(\mathbf{r}) = \frac{1}{4\pi\epsilon_0} \sum_{i=1}^n \frac{q_i}{r_i^2} \hat{r}_i$$

For continuous charge distributions:-

① for a line charge:- $dq = \lambda dl$

$$E(\mathbf{r}) = \frac{1}{4\pi\epsilon_0} \int \frac{\lambda(\mathbf{r}')}{r^2} \hat{r} dl$$

② for a surface charge:- $dq = \sigma da$

$$E(\mathbf{r}) = \frac{1}{4\pi\epsilon_0} \int \frac{\sigma(\mathbf{r}')}{r^2} \hat{r} da$$

③ for a volume charge:- $dq = \rho d\tau$

$$E(\mathbf{r}) = \frac{1}{4\pi\epsilon_0} \int \frac{\rho(\mathbf{r}')}{r^2} \hat{r} d\tau$$

① Gauss law:- / divergence of E:-

$$\textcircled{1} \oint E \cdot da = \frac{1}{\epsilon_0} Q_{\text{enclosed}}$$

and

$$\oint_V (\nabla \cdot E) d\tau = \int E \cdot da \quad (\text{Gauss law})$$

so in differential form

$$\oint_V (\nabla \cdot E) d\tau = \frac{1}{\epsilon_0} Q_{\text{enclosed}} = \frac{1}{\epsilon_0} \int_V \rho d\tau$$

$$(\nabla \cdot E) - \frac{\rho}{\epsilon_0} = 0$$

$$\star\star \quad \nabla \cdot E = \frac{1}{\epsilon_0} \rho$$

(divergence of E = $\frac{1}{\epsilon_0}$ (volume charge density))

② Curl of E:-

$$\nabla \times E = 0$$

Note! if $\nabla \times E \neq 0$
 \rightarrow impossible electric field

③ Potential:-

$$V(x) = - \int_0^x E \cdot dl$$

$$V_b - V_a = - \int_a^b E \cdot dl$$

from theorem of gradient

$$\int_a^b (\nabla V) \cdot dl = - \int_a^b E \cdot dl$$

$$\star\star \quad E = - \nabla V$$

④

$$E = -\nabla V$$

$$\nabla \cdot E = \frac{\rho}{\epsilon_0}$$

$$\nabla \times E = 0$$

using these 2 eqns $\nabla \cdot (-\nabla V) = \frac{\rho}{\epsilon_0}$

$$\nabla^2 V = -\frac{\rho}{\epsilon_0}$$

Poisson's equation:-

$$\nabla^2 V = -\frac{\rho}{\epsilon_0}$$

Laplace equation:-

for there is no charge

$$\nabla^2 V = 0$$

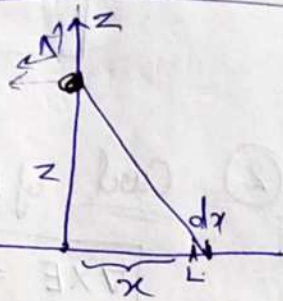
St. wire of $l=2L$

$$E = \frac{1}{4\pi\epsilon_0} \int_{-L}^L \frac{\lambda d\mathbf{l}}{(z^2+x^2)^{3/2}} = k\lambda \int_{-L}^L \frac{z\hat{z} - x\hat{x}}{(z^2+x^2)^{3/2}} dx$$

$$E = k\lambda \left[z\hat{z} \int_{-L}^L \frac{1}{(z^2+x^2)^{3/2}} dx - \hat{x} \int_{-L}^L \frac{x}{(z^2+x^2)^{3/2}} dx \right]$$

$$= k\lambda \left[\frac{z \cdot x}{z^2 \sqrt{z^2+x^2}} \Big|_{-L}^L - \hat{x} \left(\frac{-1}{\sqrt{z^2+x^2}} \right) \Big|_{-L}^L \right]$$

$$E = \frac{1}{4\pi\epsilon_0} \frac{2\lambda L}{z \sqrt{z^2+L^2}}$$



$$d\mathbf{l} = (z\hat{z} - x\hat{x}) dx$$

"Magnetostatics"

① Magnetic force =

$$F_{\text{mag}} = Q(\mathbf{v} \times \mathbf{B})$$

② Lorentz force :-

$$\mathbf{F} = Q(\mathbf{E} + (\mathbf{v} \times \mathbf{B}))$$

③ Cyclotron formula :-

$$P = QBR$$

$$R = \frac{mv}{QB}$$

④ Magnetic forces do not work !

$$W_{\text{mag}} = F_{\text{mag}} \cdot d\mathbf{l} = Q(\mathbf{v} \times \mathbf{B}) \cdot \mathbf{v} dt = \underline{\underline{0}}$$

⑤ Currents :-

A line charge λ travelling down a wire at speed v constitutes a current

$$I = \lambda v$$

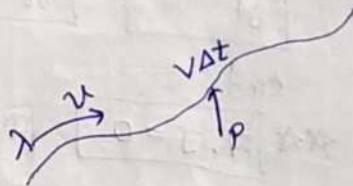
~~Region~~

The magnetic force on segment of current carrying wire is -

$$F_{\text{mag}} = \int (\mathbf{v} \times \mathbf{B}) dq = \int (\mathbf{v} \times \mathbf{B}) \lambda dl = \int (I \times \mathbf{B}) dl$$

when $I = \text{constant}$

$$F_{\text{mag}} = I \int (d\mathbf{l} \times \mathbf{B})$$



$$\lambda = \frac{q}{l}$$
$$I = \frac{q}{t} = \lambda v$$

⑥ (a) Mag. force due to line current:-

$$F_{\text{mag}} = I \int d\vec{l} \times \vec{B}$$

(b) Mag. force on surface current -

$$F_{\text{mag}} = \int (K \times B) da$$

where $K = \sigma v$
 (σ = charge density)
 (v = velocity)

(c) Mag. force on a volume current -

$$F_{\text{mag}} = \int (J \times B) d\tau = \int (J \times B) d\tau$$

J = current per unit area

⑦ Biot-Savart Law:-

for steady currents, \Rightarrow Constant mag. fields : magnetostatics.

$$\frac{\partial E}{\partial t} = 0, \quad \frac{\partial J}{\partial t} = 0$$

and

$$\nabla \cdot J = 0 \quad \text{for steady currents}$$

$$B(r) = \frac{\mu_0}{4\pi} \int \frac{J \times \hat{r}}{r^2} dl' = \frac{\mu_0}{4\pi} I \int \frac{dl \times \hat{r}}{r^2}$$

$$\left[\frac{\mu_0}{4\pi} = 10^{-7} \text{ N/A}^2 \right]$$

$$\text{unit of } B = \text{Tesla (T)}$$

⑧ Mag. field due to wire:

due to finite wire -

$$B(P) = \frac{\mu_0}{4\pi} I \int \frac{dl \times \hat{r}}{r^2}$$

$$= \frac{\mu_0 I}{4\pi} \int_{\theta_1}^{\theta_2} \left(\frac{\cos^2 \theta}{s^2} \right) \left(\frac{s}{\cos^2 \theta} \right) \cos \theta d\theta$$

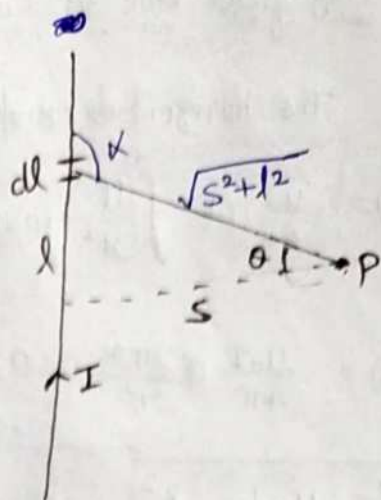
$$B = \frac{\mu_0 I}{4\pi s} \int_{\theta_1}^{\theta_2} \cos \theta d\theta$$

$$B = \frac{\mu_0 I}{4\pi s} (\sin \theta_2 - \sin \theta_1)$$

for infinite wire:

$$\theta_1 = \pi/2, \theta_2 = -\pi/2$$

$$B = \frac{2\mu_0 I}{4\pi s} \uparrow$$



$$l = s \tan \theta$$

$$dl = \frac{s}{\cos^2 \theta} d\theta$$

$$s = r \cos \theta$$

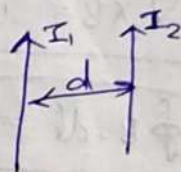
$$\frac{1}{r^2} = \frac{\cos^2 \theta}{s^2}$$

$$dl \sin \theta = dl \cos \theta$$

⑨ Force b/w 2 infinite parallel wires:-

$$F_{12} = I B dl$$

$$\frac{F}{l} = \frac{\mu_0}{4\pi} \frac{2I_1 I_2}{d}$$



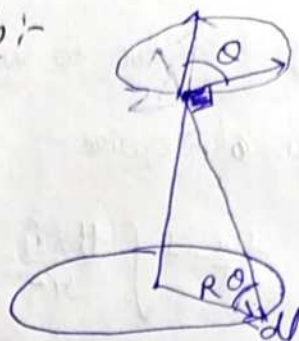
⑩ mag. field due to current carrying loop:-

The horizontal components cancel and

$$B(z) = \frac{\mu_0}{4\pi} I \int \frac{dl}{r^2} \cos\theta$$

$$B(z) = \frac{\mu_0 I}{4\pi} \times \frac{2\pi R}{R^2} \cos\theta = \frac{\mu_0 I}{2} \frac{R^2}{(R^2+z^2)^{3/2}}$$

$$B(z) = \frac{\mu_0 I}{2} \frac{R^2}{(R^2+z^2)^{3/2}}$$



as $\vec{dl} \times \hat{r} = dl$ as $\vec{dl} \perp \hat{r}$
 $\oint dl = 2\pi R$

At centre of loop = $\frac{\mu_0 I}{2} \left(\frac{R^2}{R^3} \right)$

$$B_c = \frac{\mu_0 I}{2R}$$

⑪ Ampere's Law:-

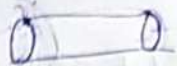
★ $\nabla \times B = \mu_0 J$ is called ampere's law (in differential form)

★ $\oint B \cdot dl = \mu_0 I_{enc}$

Proof: $\left[\int (\nabla \times B) \cdot da = \int B \cdot dl = \mu_0 \int J \cdot da \right]$

(14) vector potential of an infinite solenoid with n turns per unit length

$$\oint \mathbf{A} \cdot d\mathbf{l} = \int (\nabla \times \mathbf{A}) \cdot d\mathbf{a} = \int \mathbf{B} \cdot d\mathbf{a} = \Phi$$



$$\oint \mathbf{A} \cdot d\mathbf{l} = A(2\pi s) = \oint \mathbf{B} \cdot d\mathbf{a} = \mu_0 n I (\pi s^2)$$

$$A = \frac{\mu_0 n I \pi s^2}{2\pi s} = \frac{\mu_0 n I}{2} s \hat{\phi} \quad \text{for } s \leq R$$

for outside loop, $\oint \mathbf{B} \cdot d\mathbf{a} = \mu_0 n I (\pi R^2)$

$$\cancel{\oint \mathbf{A} \cdot d\mathbf{l}} \quad A = \frac{\mu_0 n I R^2}{2s} \hat{\phi} \quad \text{for } s \geq R$$

so

$$\begin{aligned} \mathbf{A} &\rightarrow \frac{\mu_0 n I s}{2} \hat{\phi}, \quad s \leq R \\ &\rightarrow \frac{\mu_0 n I R^2}{2s} \hat{\phi}, \quad s \geq R \end{aligned}$$