

# STEEL DESIGN

**CODE:** NF EN 1993-1:2005/NA:2007/AC:2009, Eurocode 3: Design of steel structures.

**ANALYSIS TYPE:** Member Verification

## CODE GROUP:

**MEMBER:** 40 號 H 鋼

**POINT:** 7

**COORDINATE:** x = 1.00 L = 4.50 m

## LOADS:

*Governing Load Case:* 16 ULS /105/ 1\*1.35 + 2\*1.35 + 3\*1.35 + 4\*1.35 + 5\*1.35 + 6\*1.35 + 7\*1.05 + 8\*1.05 + 9\*1.05 + 14\*1.50

## MATERIAL:

ACIER  $f_y = 235.00$  MPa



## SECTION PARAMETERS: HEA 180

h=17.1 cm	gM0=1.00	gM1=1.00	
b=18.0 cm	Ay=37.93 cm <sup>2</sup>	Az=14.47 cm <sup>2</sup>	Ax=45.25 cm <sup>2</sup>
tw=0.6 cm	Iy=2510.29 cm <sup>4</sup>	Iz=924.61 cm <sup>4</sup>	Ix=14.86 cm <sup>4</sup>
tf=0.9 cm	Wply=324.85 cm <sup>3</sup>	Wplz=156.49 cm <sup>3</sup>	

## INTERNAL FORCES AND CAPACITIES:

N <sub>Ed</sub> = 43.17 kN	My <sub>Ed</sub> = -58.29 kN*m	Mz <sub>Ed</sub> = -0.00 kN*m	Vy <sub>Ed</sub> = 0.00 kN
Nc <sub>Rd</sub> = 1063.38 kN	My <sub>Ed,max</sub> = -58.29 kN*m		Mz <sub>Ed,max</sub> = -0.00 kN*m
	Vy <sub>T,Rd</sub> = 514.61 kN		
Nb <sub>Rd</sub> = 742.80 kN	My <sub>c,Rd</sub> = 76.34 kN*m	Mz <sub>c,Rd</sub> = 36.78 kN*m	Vz <sub>Ed</sub> = -22.21 kN
	MN <sub>y,Rd</sub> = 76.34 kN*m	MN <sub>z,Rd</sub> = 36.78 kN*m	Vz <sub>T,Rd</sub> = 196.32 kN
	Mb <sub>Rd</sub> = 76.34 kN*m		Tt <sub>Ed</sub> = -0.00 kN*m
			Class of section = 1



## LATERAL BUCKLING PARAMETERS:

z = 0.00	Mcr = 825.93 kN*m	Curve,LT -	XLT = 1.00
Lcr,low=2.25 m	Lam_LT = 0.30	fi,LT = 0.55	XLT,mod = 1.00

## BUCKLING PARAMETERS:



About y axis:

Ly = 4.50 m	Lam_y = 0.68
Lcr,y = 4.76 m	Xy = 0.79
Lamy = 63.91	ky = 0.63



About z axis:

Lz = 4.50 m	Lam_z = 0.74
Lcr,z = 3.15 m	Xz = 0.70
Lamz = 69.69	kyz = 0.59

## Torsional buckling:

Curve,T=c	alfa,T=0.49
Lt=2.25 m	fi,T=0.68
Ncr,T=4832.77 kN	X,T=0.86
Lam_T=0.47	Nb,T,Rd=914.63 kN

## Flexural-torsional buckling

Curve,TF=c	alfa,TF=0.49
Ncr,y=2295.96 kN	fi,TF=0.85
Ncr,TF=2295.96 kN	X,TF=0.74
Lam_TF=0.68	Nb,TF,Rd=783.38 kN

## VERIFICATION FORMULAS:

### Section strength check:

N<sub>Ed</sub>/N<sub>c,Rd</sub> = 0.04 < 1.00 (6.2.4.(1))

My<sub>Ed</sub>/MN<sub>y,Rd</sub> = 0.76 < 1.00 (6.2.9.1.(2))

$$M_{z,Ed}/M_{N,z,Rd} = 0.00 < 1.00 \quad (6.2.9.1.(2))$$

$$(M_{y,Ed}/M_{N,y,Rd})^2 + (M_{z,Ed}/M_{N,z,Rd}) = 0.58 < 1.00 \quad (6.2.9.1.(6))$$

$$V_{y,Ed}/V_{y,T,Rd} = 0.00 < 1.00 \quad (6.2.6-7)$$

$$V_{z,Ed}/V_{z,T,Rd} = 0.11 < 1.00 \quad (6.2.6-7)$$

$$\tau_{xy,Ed}/(f_y/(\sqrt{3} \cdot g_{M0})) = 0.00 < 1.00 \quad (6.2.6)$$

$$\tau_{xz,Ed}/(f_y/(\sqrt{3} \cdot g_{M0})) = 0.00 < 1.00 \quad (6.2.6)$$

**Global stability check of member:**

$$\lambda_y = 63.91 < \lambda_{max} = 210.00 \quad \lambda_z = 69.69 < \lambda_{max} = 210.00 \quad \text{STABLE}$$

$$N_{Ed}/\min(N_{b,Rd}, N_{t,Rd}, N_{TF,Rd}) = 0.06 < 1.00 \quad (6.3.1)$$

$$M_{y,Ed,max}/M_{b,Rd} = 0.76 < 1.00 \quad (6.3.2.1.(1))$$

$$N_{Ed}/(X_y \cdot N_{Rk}/g_{M1}) + k_{yy} \cdot M_{y,Ed,max}/(X_{LT} \cdot M_{y,Rk}/g_{M1}) + k_{yz} \cdot M_{z,Ed,max}/(M_{z,Rk}/g_{M1}) = 0.53 < 1.00 \quad (6.3.3.(4))$$

$$N_{Ed}/(X_z \cdot N_{Rk}/g_{M1}) + k_{zy} \cdot M_{y,Ed,max}/(X_{LT} \cdot M_{y,Rk}/g_{M1}) + k_{zz} \cdot M_{z,Ed,max}/(M_{z,Rk}/g_{M1}) = 0.31 < 1.00 \quad (6.3.3.(4))$$

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**Section OK !!!**