

# Adjoint Computational Electromagnetics

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The adjoint method is used to inverse design linear and nonlinear photonic devices. The purpose of this handout is give the reader an introduction to the topic.

## Motivation

In normal electromagnetic simulation, we are given a material distribution represented by  $(\epsilon(x, y, z), \mu(x, y, z))$  and a current density source  $\mathbf{J}(\mathbf{x}, \mathbf{y}, \mathbf{z})$ . Maxwell's equations are then solved using one of the computational techniques (FD, FEM, MoM) for the excited electromagnetic field  $(\mathbf{H}, \mathbf{E})$ . For linear, isotropic, non magnetic and stationary media <sup>1</sup>  $\mathbf{B} = \mu_0 \mathbf{H}$  and  $\mathbf{D} = \epsilon \mathbf{E}$ . Maxwell's equations take the form

$$\nabla \times \mathbf{E} = -\mu_0 \frac{\partial \mathbf{H}}{\partial t} \quad (1a)$$

$$\nabla \times \mathbf{H} = \mathbf{J} + \epsilon \frac{\partial \mathbf{E}}{\partial t} \quad (1b)$$

<sup>1</sup> In general  $\epsilon$  and  $\mu$  may be nonlinear anisotropic tensors. We restricted ourselves to linear isotropic media for simplicity and most material are nearly the case.

We are asked to maximize the scalar quantity  $G(\mathbf{E}, \mathbf{H})$  by varying the dielectric structure  $\epsilon(x, y, z)$ .  $G$  is often a measure of device performance: for example, the power flowing in certain direction or mode conversion efficiency. This is an inverse design problem, we start by defining an objective  $G$  and ask for the best material distribution to achieve this objective.

The gradient quantity  $\frac{dG}{d\epsilon}$  is useful to compute. It could be used as a measure of robustness and sensitivity to any structure deformations like fabrication imperfections. In inverse design, it is the major quantity needed as it points in the direction of steepest ascent, from which we have an informed decision of how to update the dielectric structure.

$$\epsilon \leftarrow \epsilon + \alpha \frac{dG}{d\epsilon} \quad (2)$$

Where  $\alpha$  is the step size in the gradient direction<sup>2</sup>.

Assuming we have  $n$  number of design points, to calculate the sensitivity  $\frac{dG}{d\epsilon}$  there are different approaches which vary in complexity and accuracy. One way is by using a finite difference approximation  $\frac{dG}{d\epsilon} \approx \frac{\Delta G}{\Delta \epsilon}$ . In this approach we need to carry  $n$  number of forward simulations. For a typical  $100 \times 100 \times 100$  3D finite difference grid,

<sup>2</sup> Some algorithms attempt to optimize the step size so that the step maximally increases  $G$

this means 1000000 simulations!. This approach also suffers from numerical discretization errors and the need to determine how small or large is  $\Delta\epsilon$ . Automatic differentiation can be used to get the derivative exactly. However, there are two modes in automatic differentiation. The automatic forward mode, like finite difference, needs  $n$  number of forward simulations. In the automatic adjoint or reverse mode, two simulations are only needed regardless of the number of the design points. So, the adjoint method is by far much better in accuracy than finite difference and computational cost than automatic forward differentiation.

### Problem Formulation

Before driving the adjoint equation, lets put Maxwell's in a matrix form:

$$\begin{bmatrix} \mu_0 & 0 \\ 0 & -\epsilon \end{bmatrix} \begin{bmatrix} \frac{\partial \mathbf{H}}{\partial t} \\ \frac{\partial \mathbf{E}}{\partial t} \end{bmatrix} + \begin{bmatrix} 0 & \nabla \times \\ \nabla \times & 0 \end{bmatrix} \begin{bmatrix} \mathbf{H} \\ \mathbf{E} \end{bmatrix} = \begin{bmatrix} 0 \\ \mathbf{J} \end{bmatrix} \quad (3)$$

Which could be written as

$$[C] \frac{d\mathbf{X}}{dt} + [D]\mathbf{X} = \mathbf{S} \quad (4)$$

if the following definitions have been made  $\mathbf{X} = \begin{bmatrix} \mathbf{H} \\ \mathbf{E} \end{bmatrix}$ ,  $[C] =$

$$\begin{bmatrix} \mu_0 & 0 \\ 0 & -\epsilon \end{bmatrix}, [D] = \begin{bmatrix} 0 & \nabla \times \\ \nabla \times & 0 \end{bmatrix} \text{ and } \mathbf{S} = \begin{bmatrix} 0 \\ \mathbf{J} \end{bmatrix}$$

The initial condition for equation(4) is

$$I(\mathbf{X}(0), \epsilon) = \mathbf{0} \quad (5)$$

Our optimization problem can be then formulated as

$$\begin{aligned} \max_{\epsilon} \quad & G(\epsilon) = \int_0^T g(\mathbf{X}, \epsilon, t) dt \\ \text{s.t.} \quad & [C] \frac{d\mathbf{X}}{dt} + [D]\mathbf{X} - \mathbf{S} = 0 \\ & I(\mathbf{X}(0), \epsilon) = \mathbf{0} \end{aligned} \quad (6)$$

Where we have assumed our objective function can be written in this integral form  $\int_0^T g(\mathbf{X}, \epsilon, t) dt$ .

Equation (4) is commonly solved by discretization in space first and then solving the resulting system of Ordinary Differential Equations (ODEs). We can either start by replacing time derivatives with finite differences to arrive at a recursive set of spatial problems to be discretized. The discretization in space could be in done in real or spectral domains. Maxwell's equation could even be expanded in the natural complete eigen-basis of the problem in a coupled-mode-like

fashion and inverse design could be done with very low dimensional matrices. Among the numerical methods, the finite difference method, the finite element method, and the method of moments form the core of computational electromagnetics. One of our goals is to show a simple one dimensional example with code for each method along with its adjoint formulation. Interested readers can directly add an adjoint solver on top their EM solvers very easily and start doing inverse design.

### Adjoint Method

In gradient based inverse design, we start with an initial dielectric profile  $\epsilon^0(x, y, z)$  and then use local gradient of the objective function to guide the search in device space <sup>3</sup>. The gradient of the objective function  $G$  in equation (6)

$$\frac{dG}{d\epsilon} = \int_0^T \left[ \frac{\partial g}{\partial \epsilon} + \frac{\partial g}{\partial \mathbf{X}} \frac{\partial \mathbf{X}}{\partial \epsilon} \right] dt \quad (7)$$

To evaluate the last integral, we need to calculate the term  $\frac{\partial \mathbf{X}}{\partial \epsilon}$ . If the vector  $\epsilon$  is  $n$  dimensional, we need to repeat the simulation  $n$  number of times. For each, we change the component  $\epsilon_i$  by  $\Delta \epsilon_i$ , then the change in the objective function is determined. Finally, the slope is calculated by dividing the change in the objective function by  $\Delta \epsilon_i$ . The whole point of adjoint method is to avoid calculating the derivative term  $\frac{\partial \mathbf{X}}{\partial \epsilon}$ . Soon, we will discover that the adjoint method can magically determine the gradient at all design points with an additional cost of one extra simulation. The remaining terms inside the objective integral are not really problematic.  $\frac{\partial g}{\partial \mathbf{X}}$  and  $\frac{\partial g}{\partial \mathbf{X}}$  can be evaluated (efficiently and exactly) with a reverse mode automatic differentiation package <sup>4</sup>. In Julia, the package "Nabla.jl" does a pretty good job in calculating these gradients.

To eliminate the term  $\frac{\partial \mathbf{X}}{\partial \epsilon}$ , the first step is to add multiples of 0 to the objective function.

$$G = \int_0^T g(\mathbf{X}, \epsilon, t) + \lambda^T \left( [C(\epsilon)] \frac{d\mathbf{X}}{dt} + [D]\mathbf{X} - \mathbf{S} \right) + \kappa^T (I(\mathbf{X}(0), \epsilon)) dt \quad (8)$$

The vector  $\lambda$  is time dependent.  $\kappa$  is another vector associated with the initial conditions. The objective function has not changed after this modification, the equation is also the same for any choice of  $\lambda$  and  $\kappa$ . We will choose them in a way that eliminate the need for the term  $\frac{\partial \mathbf{X}}{\partial \epsilon}$  in the objective function gradient  $\frac{dG}{d\epsilon}$ . The vectors  $\lambda$  and  $\kappa$  are commonly called Lagrange multipliers and the modified objective function is the system Lagrangian that we seek to maximize.

<sup>3</sup> Additional constraints should be added to guarantee robustness and easy fabrication of the final discovered devices. Fabrication constraints play a key role in inverse design and we will talk about it more in a future separate handout.

<sup>4</sup> There are two levels of reverse mode differentiation (1) Differentiation of scalar function with respect to large dimensional vectors. (2) Efficient evaluation of PDE constrained objective function gradients using adjoint method.

Taking the total derivative of the Lagrangian,

$$\begin{aligned} \frac{dG}{d\epsilon} = \int_0^T \left( \left[ \frac{\partial g}{\partial \epsilon} + \frac{\partial g}{\partial \mathbf{X}} \frac{\partial \mathbf{X}}{\partial \epsilon} \right] + \lambda^T \left[ \frac{dC}{d\epsilon} \frac{d\mathbf{X}}{dt} + C \frac{\partial}{\partial \epsilon} \frac{d\mathbf{X}}{dt} + D \frac{\partial \mathbf{X}}{\partial \epsilon} \right] \right) dt \\ + \kappa^T \left[ \frac{\partial I}{\partial \mathbf{X}(0)} \frac{\partial \mathbf{X}(0)}{\partial \epsilon} + \frac{\partial I}{\partial \epsilon} \right] \end{aligned} \quad (9)$$

The problematic term  $\frac{\partial \mathbf{X}}{\partial \epsilon}$  is what we want to get rid of, however we have now its time derivative added. Integration by parts can help us reduce the time derivative to zero order.

$$\int_0^T \left( \lambda^T C \frac{\partial}{\partial \epsilon} \frac{d\mathbf{X}}{dt} \right) dt = \lambda^T C \frac{\partial \mathbf{X}}{\partial \epsilon} \Big|_0^T - \int_0^T \frac{d(\lambda^T C)}{dt} \frac{\partial \mathbf{X}}{\partial \epsilon} dt \quad (10)$$

Substituting (10) into (9) and collecting terms in  $\frac{\partial \mathbf{X}}{\partial \epsilon}$  and  $\frac{\partial \mathbf{X}(0)}{\partial \epsilon}$  yield

$$\begin{aligned} \frac{dG}{d\epsilon} = \int_0^T \left( \left[ \frac{\partial g}{\partial \epsilon} + \lambda^T \frac{dC}{d\epsilon} \frac{d\mathbf{X}}{dt} \right] + \left[ \frac{\partial g}{\partial \mathbf{X}} + \lambda^T D - \frac{d(\lambda^T C)}{dt} \right] \frac{\partial \mathbf{X}}{\partial \epsilon} \right) dt + \\ \left[ \kappa^T \frac{\partial I}{\partial \mathbf{X}(0)} - \lambda^T C \right] \frac{\partial \mathbf{X}(0)}{\partial \epsilon} + \lambda^T C \frac{\partial \mathbf{X}(T)}{\partial \epsilon} + \kappa^T \frac{\partial I}{\partial \epsilon} \end{aligned} \quad (11)$$

We can get rid of  $\frac{\partial \mathbf{X}}{\partial \epsilon}$  by choosing  $\lambda^T$  to satisfy the following differential equation

$$\frac{\partial g}{\partial \mathbf{X}} + \lambda^T D - \frac{d(\lambda^T C)}{dt} = 0 \quad (12)$$

We can get rid of  $\frac{\partial \mathbf{X}(0)}{\partial \epsilon}$  by choosing  $\kappa^T = \lambda^T C \left[ \frac{\partial I}{\partial \mathbf{X}(0)} \right]^{-1}$

If we also imposed the terminal condition  $\lambda^T(T)C = 0$ , the objective function gradient is

$$\frac{dG}{d\epsilon} = \int_0^T \left[ \frac{\partial g}{\partial \epsilon} + \lambda^T \frac{dC}{d\epsilon} \frac{d\mathbf{X}}{dt} \right] dt + \kappa^T \frac{\partial I}{\partial \epsilon} \quad (13)$$