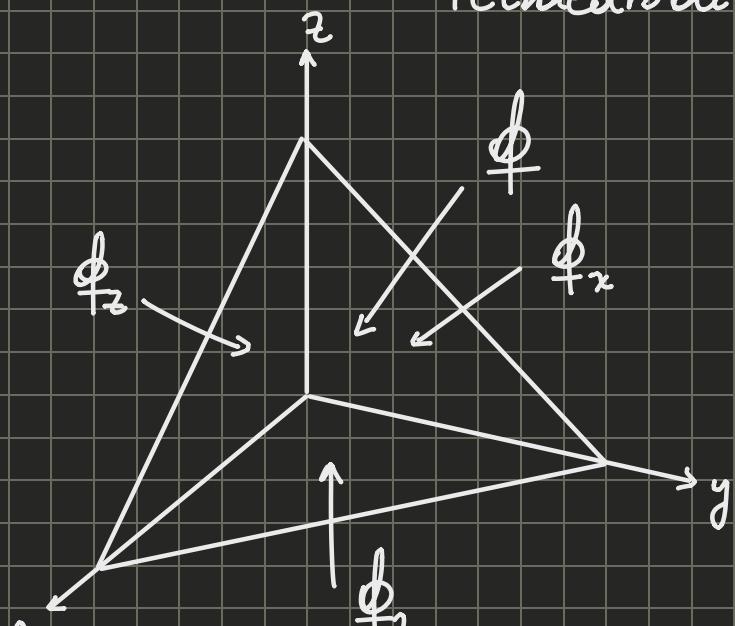


## Tetraedro di Cauchy



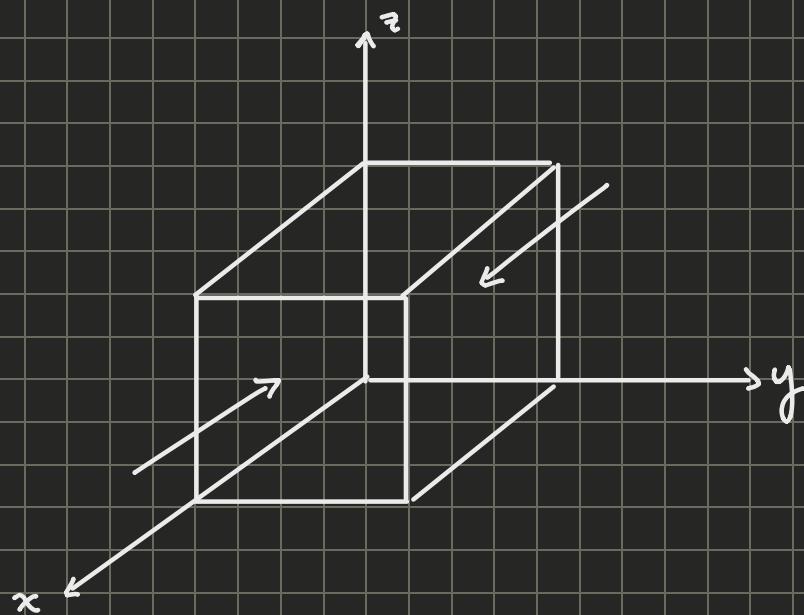
$$\phi A = \phi_x A_x + \phi_y A_y + \phi_z A_z$$

$$\phi = \phi_x \frac{A_x}{A} + \phi_y \frac{A_y}{A} + \phi_z \frac{A_z}{A}$$

$$= \phi_x u_x + \phi_y u_y + \phi_z u_z$$

$$\phi = \phi u$$

Equilibrio Statico indefinito e legge di Stevino



~~$\rho dy dz i - (p + \frac{\partial p}{\partial x} dx) dy dz i$~~  per ogni direzione

$$-\frac{\partial p}{\partial x} dW - \frac{\partial p}{\partial y} dW - \frac{\partial p}{\partial z} dW = -\text{grad } p dW$$

L'azione di massa è:

$$\rho \underline{f} d\Omega$$

L'equilibrio dei due è:

$$\rho \underline{f} d\Omega - \text{grad } p d\Omega = 0$$

$$\rho \underline{f} - \text{grad } p = 0$$

Stevino

Essendo:  $\underline{f} = \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix}$  grad z, troviamo

$$-\rho g \text{ grad } z = \text{grad } p$$

Abbiamo allora che:  $\text{grad} \left( z + \frac{p}{\rho g} \right) = 0$

$$\Rightarrow z + \frac{p}{\rho g} = \text{costante}$$

Sposta su superficie piana

$$\vec{S} = \int_A \rho \vec{n} dA = \int_A \gamma s \vec{n} dA = \int_A \gamma x \cos \alpha \vec{n} dA$$

$$= \gamma \cos \alpha \vec{n} \int_A x dA = \gamma \cos \alpha \vec{n} x_G A = \gamma \vec{n} z_G A = \vec{n} p_G A$$

$$\vec{S}_b = \int_A \rho x \vec{n} dA$$

$$\cancel{\gamma \cos \alpha n} \int_A x dA = \cancel{\gamma \cos \alpha n} \int_A x^2 dA$$

$$G = \frac{\int_A x^2 dA}{\int_A x dA}$$

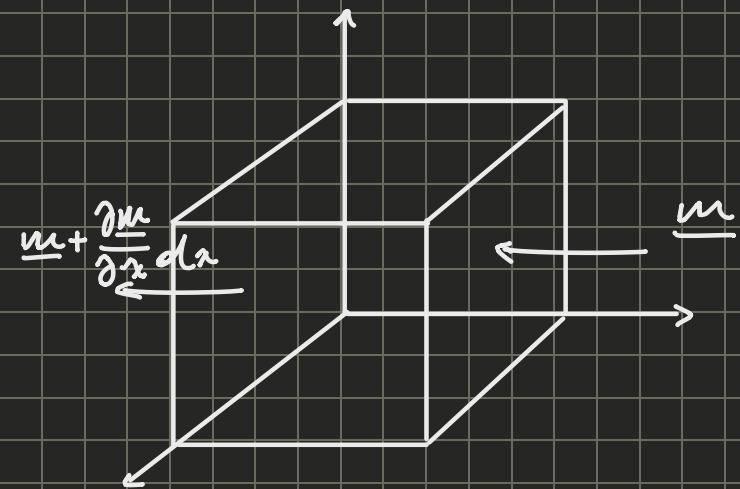
## Equilibrio Statico Globale

$$\int_W \rho \vec{f} dW = \int_W \text{grad } \rho dW$$

$\underline{\omega}$        $-\underline{\Pi}$

$$\underline{\omega} + \underline{\Pi} = 0$$

## Equazione inolfinità di continuità



Massa Entrante nel tempo  $\partial t$ :

$$\rho u dy dz dt + \rho v dx dz dt + \rho w dx dy dt$$

Massa Uscente in  $\partial t$

$$\left( \rho u + \frac{\partial \rho u}{\partial x} dx \right) dy dz dt + \left( \rho v + \frac{\partial \rho v}{\partial y} dy \right) dx dz dt + \left( \rho w + \frac{\partial \rho w}{\partial z} dz \right) dx dy dt$$

La massa accumulata è:

$$\frac{\partial \rho}{\partial t} dx dy dz dt$$

Semplificando tutto si trova:

$$-\cancel{\frac{\partial \rho u}{\partial x} dx dy dz dt} - \cancel{\frac{\partial \rho v}{\partial y} dx dy dz dt} - \cancel{\frac{\partial \rho w}{\partial z} dx dy dz dt} = \frac{\partial \rho}{\partial t}$$

$$-\frac{\partial \rho u}{\partial x} - \frac{\partial \rho v}{\partial y} - \frac{\partial \rho w}{\partial z} = \frac{\partial \rho}{\partial t}$$

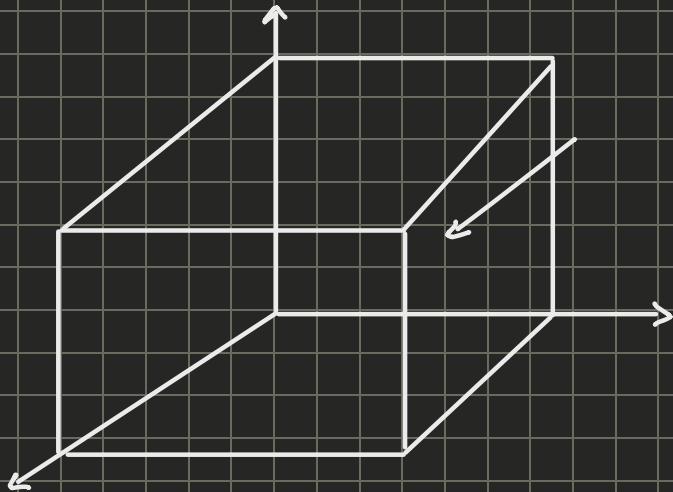
$$-\operatorname{div}(\vec{\rho v}) = \frac{\partial \rho}{\partial t} \Rightarrow \frac{\partial \rho}{\partial t} + \operatorname{div}(\vec{\rho v}) = 0$$

Equazione Globale Continuità

$$\int_W \underbrace{\frac{\partial \rho}{\partial t}}_{\sim} dW = - \int_W \underbrace{\operatorname{div}(\vec{\rho v})}_{\sim} dW$$

$$\frac{\partial M}{\partial t} = \int_A \rho \vec{v} \cdot \vec{n} dA = \rho Q$$

Equazione indefinita dell'equilibrio dinamico



Equilibrio di azioni di massa e superficie

$$\rho \vec{f} dx dy dz - \rho \vec{a} dx dy dz + \underbrace{\left( -\frac{\partial \phi_x}{\partial x} - \frac{\partial \phi_y}{\partial y} - \frac{\partial \phi_z}{\partial z} \right) dx dy dz}_\text{Azione di inerzia} = 0$$

Azione di inerzia

$$\rho(\vec{f} - \vec{a}) = \operatorname{div}(\phi)$$

Teorema di Bernoulli

↳ Tante ipotesi, incluso fluido incomprensibile e stazionario

$$\rho(\vec{f} - \vec{a}) = \operatorname{div}(\phi) \quad \phi = \rho \pm$$

$$\Rightarrow \rho(\vec{f} - \vec{a}) = \operatorname{grad} p$$

Rispetto alla terza intuiscibile ( $s, u, b$ ):

$$\left\{ \begin{array}{l} -\rho g \frac{\partial z}{\partial s} - \rho \frac{dV}{dt} = \frac{\partial p}{\partial s} \quad (\cancel{*}) \\ -\rho g \frac{\partial z}{\partial u} - \rho \frac{V^2}{R} = \frac{\partial p}{\partial u} \\ -\rho g \frac{\partial z}{\partial b} = \frac{\partial p}{\partial b} \end{array} \right.$$

$$-\rho g \frac{\partial z}{\partial s} - \rho \frac{\partial \overset{\circ}{x}}{\partial t} - V \frac{\partial v}{\partial s} - \cancel{\circ \frac{\partial v}{\partial u}} - \cancel{\circ \frac{\partial v}{\partial b}} = \frac{\partial p}{\partial s}$$

$$-\frac{\partial z}{\partial s} - \frac{\partial}{\partial s} \frac{V^2}{2g} = \frac{\partial}{\partial s} \left( \frac{p}{\gamma} \right)$$

$$\underbrace{\frac{\partial}{\partial s} \left( z + \frac{p}{\gamma} + \frac{V^2}{2g} \right)}_{H} = 0 \Rightarrow z + \frac{p}{\gamma} + \frac{V^2}{2g} = \text{costante}$$

Essendo  $H$  costante troviamo che un fluido ideale non dissipà energia quando è in flusso. Questo è vero perché  $H$  può essere visto come energia però quindi troviamo che la sua energia non cambia in flusso.

# Velocità di Defor mazione

$$\text{grad } v = \begin{bmatrix} \frac{\partial u}{\partial x} & \frac{\partial v}{\partial x} & \frac{\partial w}{\partial x} \\ \frac{\partial u}{\partial y} & \frac{\partial v}{\partial y} & \frac{\partial w}{\partial y} \\ \frac{\partial u}{\partial z} & \frac{\partial v}{\partial z} & \frac{\partial w}{\partial z} \end{bmatrix} = D + \nabla$$

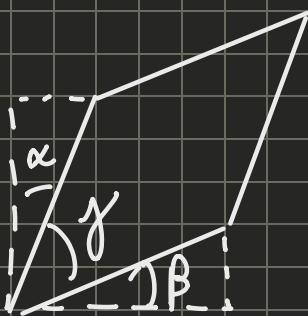
$$D = \begin{bmatrix} \frac{\partial u}{\partial x} - \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) & \frac{1}{2} \left( \frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right) & \\ \frac{\partial v}{\partial y} & \frac{1}{2} \left( \frac{\partial w}{\partial y} + \frac{\partial v}{\partial z} \right) & \\ \frac{\partial w}{\partial z} & & \end{bmatrix}$$

SYMM.

$$\overrightarrow{dx} \quad \overrightarrow{dx'}$$

$$\varepsilon = \frac{dx' - dx}{dx} = \frac{1}{dx} (u_2 - u_1) dt$$

$$\frac{d\varepsilon}{dt} = \frac{\partial u}{\partial x}$$



$$\alpha = \frac{v_2 - v_1}{dx} dt$$

$$\beta = \frac{u_2 - u_1}{dy} dt$$

$$\frac{dy}{dt} = - \frac{d\alpha}{dt} - \frac{d\beta}{dt} = - \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right)$$

## Navier Stokes

Prendiamo  $\phi = p \mathbb{I} + \phi_D$

$$\phi_D = \phi - p \mathbb{I} = -\mu' \operatorname{div}(v) \mathbb{I} - 2\mu D \mathbb{D}$$

Usando l'equazione indeterminata dell'equilibrio dinamico

$$\int \rho(\vec{f} - \vec{a}) = \operatorname{div} \phi$$

$$\left( \underbrace{\phi - p \mathbb{I}}_{\text{incompressibile}} = -\mu' \operatorname{div}(v) \mathbb{I} - 2\mu D \mathbb{D} \right)$$

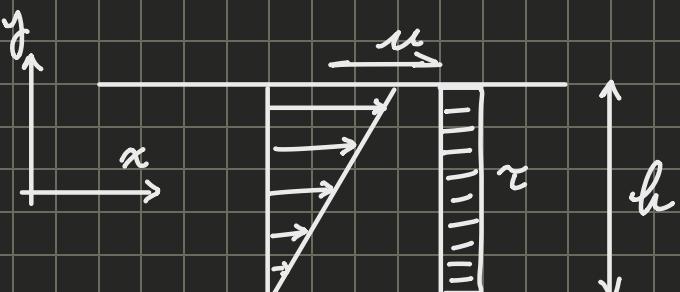
$$\rightarrow \rho(\vec{f} - \vec{a}) = \operatorname{grad} p - \operatorname{grad}(\mu' \operatorname{div}(v)) - \operatorname{div}(2\mu D)$$

$$= \operatorname{grad} p - \mu \nabla^2 v$$

Flusso incompressibile.

$$\rho(\vec{f} - \vec{a}) = \operatorname{grad} p - \mu \nabla^2 v$$

## Couette



$$\rho \left( \cancel{f_x} - \frac{\partial p}{\partial t} - \mu \cancel{\frac{\partial u}{\partial x}} - \cancel{\lambda \frac{\partial u}{\partial y}} \right) = \frac{\partial p}{\partial x} - \left( \frac{\partial^2 p}{\partial x^2} - \frac{\partial^2 u}{\partial y^2} \right) \mu$$

$$\mu \frac{\partial^2 u}{\partial y^2} = 0 \rightarrow \mu \frac{\partial u}{\partial y} = A \rightarrow \mu u(y) = Ay + B$$

da velocità prende forma lineare

$$u(0) = 0 \rightarrow B = 0$$

$$u(h) = U \rightarrow Ah = U \rightarrow A = \frac{U}{h}$$

$$u(y) = U \frac{y}{h} \quad y \in [0, h]$$

### Poiseuille



$$\rho \left( \cancel{f_x} - \frac{\partial u}{\partial t} - \mu \cancel{\frac{\partial u}{\partial x}} - \cancel{\lambda \frac{\partial u}{\partial y}} \right) = \frac{\partial p}{\partial x} - \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) \mu$$

$$\frac{1}{\mu} \frac{\partial p}{\partial x} = \frac{\partial^2 u}{\partial y^2}$$

$$\frac{\partial u}{\partial y} = \frac{1}{\mu} \frac{\partial p}{\partial x} y + C$$

$$u(y) = \frac{1}{\mu} \frac{\partial p}{\partial x} \frac{y^2}{2} + Cy + D$$

$$u(0) = 0 \Rightarrow D = 0$$

$$u(\partial h) = 0 \Rightarrow C = -\frac{1}{\mu} \frac{\partial f}{\partial x} h$$

$$\rightarrow u(y) = \frac{1}{\mu} \frac{\partial p}{\partial x} \left( \frac{y^2}{2} - hy \right)$$

Equazione Globale dell'equilibrio dinamico:

$$\int_{\omega} \rho \vec{f} dW - \int_{\omega} \rho \vec{a} dW = \int_{\omega} \operatorname{div}(\phi) dW$$

$$\underbrace{\underline{\rho}}_{G} \underbrace{\underline{\vec{I}} + \underline{\vec{M}}}_{Sforzo per la accelerazione}$$

$$-\bar{T}\vec{r}$$

locale e convettiva      Ideale

Reale

$$\phi_f = \rho \underline{\vec{I}}$$

$$\phi = \rho \underline{\vec{I}} - \phi_0$$

$$- (\bar{\tau}_p)$$

$$- (\bar{\tau}_p + \bar{T})$$

Termino di pressione

Termino di Sforzo di Attrito dato dalla viscosità

Reynolds

La media di Reynolds è usata per analizzare flumi turbolenti, per mettendoci da parte

variazioni dalla media, poi permane  
 lavorare  $\overline{\quad}$  media e aggiungendo  
 sul flusso  
 poi le deviazioni.

Navier-Stokes:

$$\rho(\vec{f} - \vec{\alpha}) = \text{grad } p - \mu \nabla^2 \vec{v}$$

Reynolds:

$$\rho \left( \vec{f}_m - \frac{\partial \underline{v}_m}{\partial t} - \underline{\mu}_m \frac{\partial \underline{v}_m}{\partial t} - \underline{v}_m \frac{\partial \underline{v}_m}{\partial y} - \underline{w}_m \frac{\partial \underline{w}_m}{\partial z} \right) = \text{grad } p_m - \mu \nabla^2 \underline{v}_m + \text{div } \underline{\phi}_R$$

$$\underline{\phi}_R = \begin{bmatrix} (u'u')_m & (u'v')_m & (u'w')_m \\ (v'v')_m & (v'w')_m & \\ \text{sym} & & (w'w')_m \end{bmatrix}$$