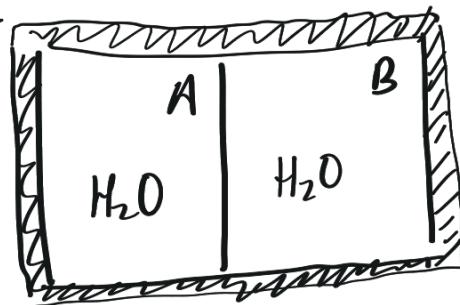


# Esercitazione 5 - Sistemi Chiusi

Esercitazione 4) Esercizio 4)

4.



H.p. Sistema Isolato

Liquido Incompressibile

$$M^A = M^B = 1 \text{ kg}$$

$$C^A = C^B = 4186 \frac{\text{J}}{\text{kg K}}$$

Ma meno interessante

$$T_1^A = 353,15 \text{ K}$$

Stato finale 2 di equilibrio

$$T_2^B = 293,15 \text{ K}$$

$$? T_2^A ? T_2^B ? S_{\text{rea}}$$

$$\mathcal{E} = A \cup B$$

$$\Delta U^A \stackrel{\substack{\text{P.A.} \\ \text{additivo}}}{=} \Delta U^A + \Delta U^B$$

Proprietà additiva

$\Delta U^B \stackrel{\substack{\text{P.A.} \\ \text{additivo}}}{=} \Delta U^B$

$Q \xrightarrow{\text{adiabatico}} 0$

$= 0$

$$\Delta S_{\text{rea}} \stackrel{\substack{\text{P.A.} \\ \text{additivo}}}{=} \Delta S^A + \Delta S^B = S^A + S_{\text{rea}}$$

$$\Delta U^A \stackrel{\text{L.I.}}{=} M^A c (T_2^A - T_1^A)$$

$$\textcircled{2} \quad T_2^A = T_2^B = T_2$$

$$\Delta U^B \stackrel{\text{L.I.}}{=} M^B c (T_2^B - T_1^B)$$

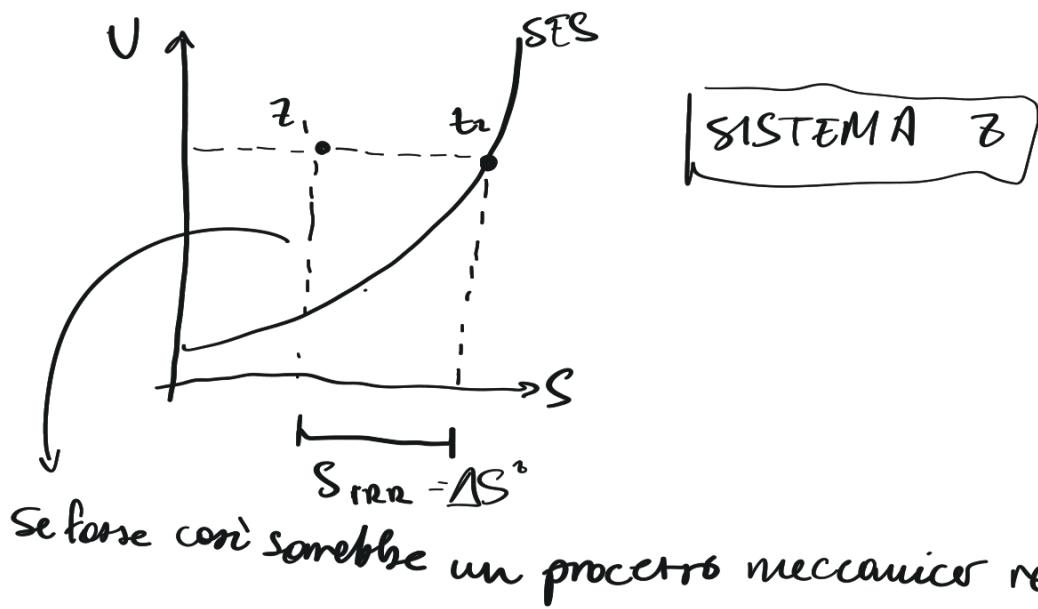
$$\Delta U^A + \Delta U^B = 0$$

$$M_A (T_2 - T_1^A) + M_B (T_2 - T_1^B)$$

$$T_2 = \frac{T_1^A + T_1^B}{2} = 323,15 \text{ K}$$

$$\Delta S^{\circ} = S_{\text{irr}} = \Delta S^{\circ A} + \Delta S^{\circ B} \stackrel{L^{\circ}}{=} M_C \left( \ln \frac{T_2}{T_1^A} + \ln \frac{T_2}{T_1^B} \right) =$$

$= 36,23 \frac{J}{K \cdot mol}$  → possibile irreversibile



Se fosse così sarebbe un processo meccanico reversibile

Per trovare processo reversibile

$$\begin{cases} (V_2 - V_1)^{\circ} = Q^{\circ} - L^{\circ} \\ (S_2 - S_1)^{\circ} = S^{\circ} + S_{\text{irr}} \end{cases} \xrightarrow{\text{processo reversibile}}$$

$$\Delta U = 0$$

$$\Delta S = 36,23 \frac{J}{K}$$

Dati qualsiasi punti 1 e 2 <sup>in un sistema TD</sup> esiste un processo reversibile se posso fare quello che voglio

Serbatoi

$$\Delta U = T \Delta S$$

Gli scambi con serbatoi occorrono anche con  $\Delta T$  infinitesime

$$ds^{\leftarrow} = \frac{dQ^{\leftarrow}}{T}$$

$$T_0 = 293,15 \text{ K}$$

$$S^{\leftarrow} = \frac{Q_0}{T_0}$$

da cui l'aria scambiata è la  $Q$  scambiata con il serbatoio diviso per la  $T$  del serbatoio

$$\begin{cases} Q_0^{\leftarrow} - L^{\rightarrow} = 0 \rightarrow Q_0^{\leftarrow} = L^{\rightarrow} \\ \Delta S^{\leftarrow} - S^{\leftarrow} = \frac{Q_0^{\leftarrow}}{T_0} \rightarrow \frac{Q_0^{\leftarrow}}{293,15} = 36,25 \frac{\text{J}}{\text{K}} \end{cases}$$

$$Q_0^{\leftarrow} = 10633 \text{ J} \rightarrow L^{\rightarrow} = 10623 \text{ J}$$



ha senso perdere  
 $\Delta S$  ora  $> 0$   
 quindi stiamo  
 parlando calore



$$\Psi_{10}^2 = (L_{Z1 \rightarrow 0})_{PMR}$$

↳ Processo  
 Meccanico  
 Reversibile

$$Q^{\leftarrow} = 0 \wedge S^{\leftarrow} = 0$$

$$\begin{cases} (V_0 - V_1)^A + (V_0 - V_1)^B = Q_{10}^P \\ (S_0 - S_1)^A + (S_0 - S_1)^B = S_{10}^P + S_{122} \end{cases}$$

processo meccanico  
reversibile

$$\begin{cases} \Psi_{10}^2 = \Delta_{10 \max}^P = M_C \left( T_1^A + T_1^B - 2 \bar{T}_0 \right) = 11,69 \text{ kJ} \\ M_C \ln \frac{\bar{T}_0^2}{T_1^A T_1^B} = 0 \rightarrow \bar{T}_0 = \sqrt{T_1^A T_1^B} = 321,6 \text{ K} \end{cases}$$

Esercitazione 6 → servono tabelle dell'acqua

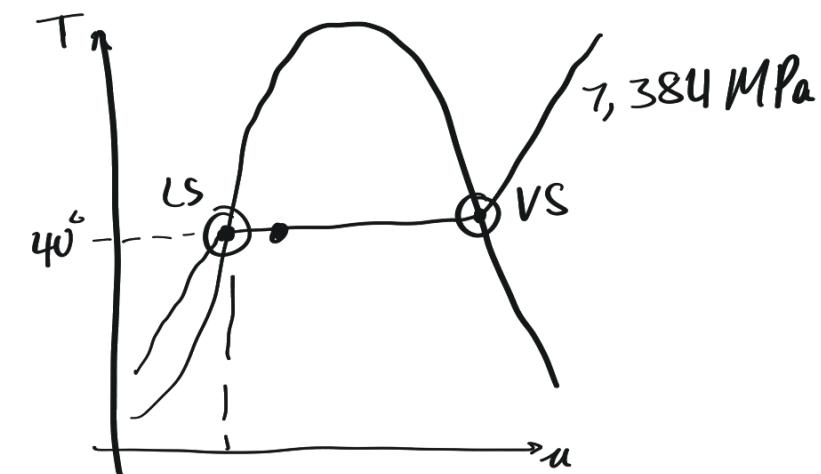
⑤  $M = 0,6 \text{ kg H}_2\text{O}$

$T = 40^\circ\text{C} = 313,15 \text{ K}$

$U = 320 \text{ kJ}$

?V

Bifase / Miscelle → Tabelle a singola entrata  
 Vapore Sovraccollato → Tabelle a doppia entrata



$$u = \frac{U}{M} = \frac{320 \text{ kJ}}{0,6} = 533 \frac{\text{kJ}}{\text{kg}}$$

$$u_f = 167,53 \frac{\text{kJ}}{\text{kg}}$$

$$M_f = M_w = 2421,4 \frac{\text{kJ}}{\text{kg}}$$

$u_f < u < u_g \Rightarrow$  siamo in stato bifase a  $T = 110^\circ\text{C}$

$$\text{Titolo } X = \frac{u - u_2}{M_w - u_2}$$

$= \frac{533,3 - 167,56}{2430,1 - 167,56} = 0,1524$ 

$\downarrow$   
 $\% \text{ di vapore}$

$\hookrightarrow$  già in tabella

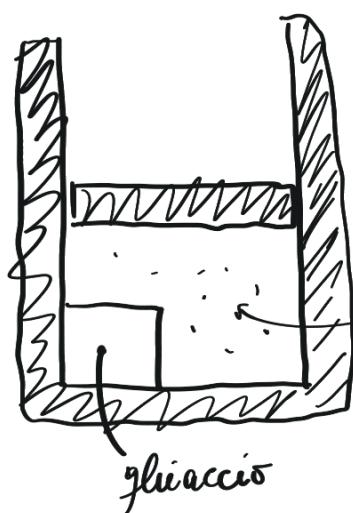
$$? V \quad V = M \cdot v^+ = M \left[ (1-X) v_L + X v_v \right] = 1,785 \text{ m}^3$$

$$v_L = 1007,8 \quad 1,0078 \quad 0,0010078 \frac{\text{m}^3}{\text{kg}}$$

$$v_g = 19,523 \frac{\text{m}^3}{\text{kg}}$$

~, perché  
dovevano  
dividere per  
1000 non moltiplicare,  
in ciascun numero  
non sommare  
moltiplicazioni

3)



$$P = 2 \text{ MPa}$$

$$M_{V_1} = 7 \text{ kg} \quad M_{S_1} = 3 \text{ kg}$$

vapore

$$T_{V_1} = 623,15 \text{ K}$$

$$T_{S_1} = 243,15 \text{ K}$$

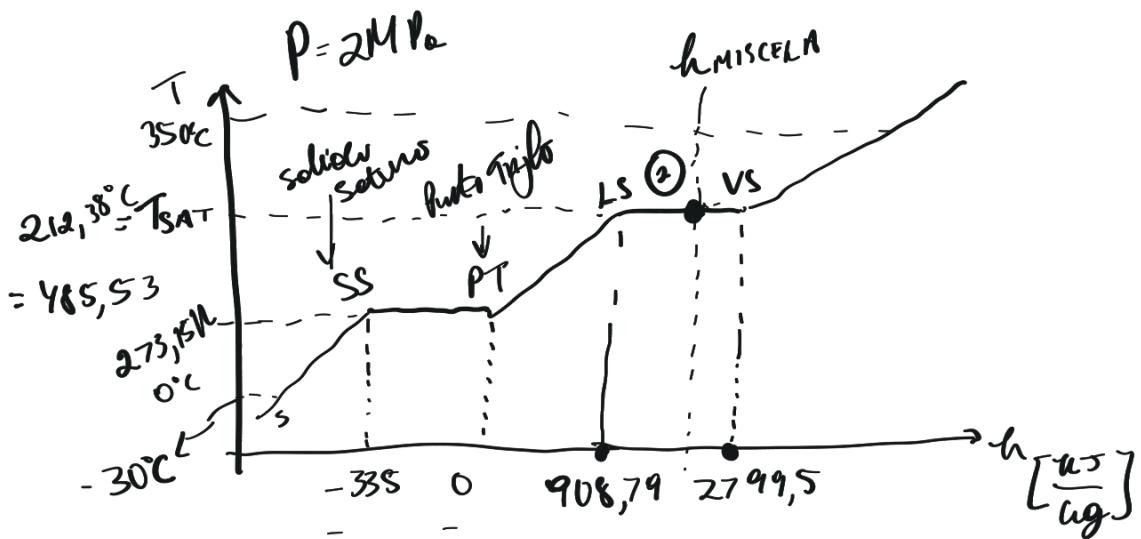
CONDIZIONI STATO FINALE

$$? M_{S_2} \quad ? M_{L_2} \quad ? M_{V_2}$$

? TITOLO

MISCELAZIONE ADIABATICA DI VAPORE + GHIACCIO

$$\Delta H = 0 \Rightarrow H_1 = H_2$$



$$M_{\text{TOT}} \cdot h_{\text{TOT}2} = M_{V_1} \cdot h_{V_1} + M_{S_1} \cdot h_{S_1}$$

?      ?      ?

$M_{\text{TOT}} = 10 \text{ kg}$

da tabelle vapore suriscaldato

$$h_{V_1} = 3137 \frac{\text{kJ}}{\text{kg}}$$

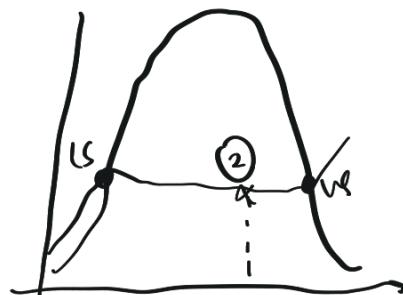
$$h_{s_1} = -335 + c_s (\Delta T) = -335 \frac{kJ}{kg} + 2,0934 \frac{kJ}{kg \cdot K} \cdot (-30 K)$$

$$= -397,8 \frac{kJ}{kg}$$

$$h_{\text{TOT2}} = \frac{M_{v_1} \cdot h_{v_1} + M_{s_1} \cdot h_{s_1}}{M_{\text{TOT}}} = 2076,86 \frac{kJ}{kg}$$

$h_{ls} < h_{\text{TOT2}} < h_{vs} \Rightarrow \text{Before}$

$$h_{\text{TOT2}} = (1-x) h_{ls} + x h_{vs}$$

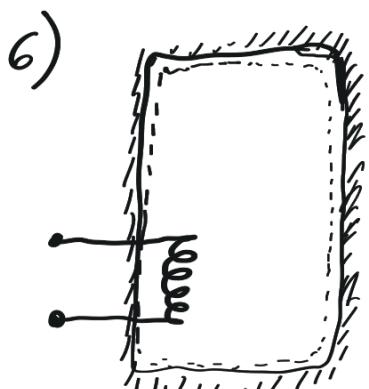


$$X = \frac{h_{\text{TOT2}} - h_{ls}}{h_{vs} - h_{ls}} = 0,62$$

$$M_{v_2} = X M_{\text{TOT}} = 6,2 \text{ kg}$$

$$M_{l_2} = (1-X) \cdot M_{\text{TOT}} = 3,8 \text{ kg}$$

6 e 7)



$$V = 0,06 \text{ m}^3$$

$$M = 0,3 \text{ kg} \quad H_2O$$

$$T = 333,15 \text{ K}$$

$$L = 1 \text{ kW}$$

$$f = 15' = 900 \text{ s}$$

$$\begin{matrix} ? P_2 \\ ? T_2 \end{matrix}$$

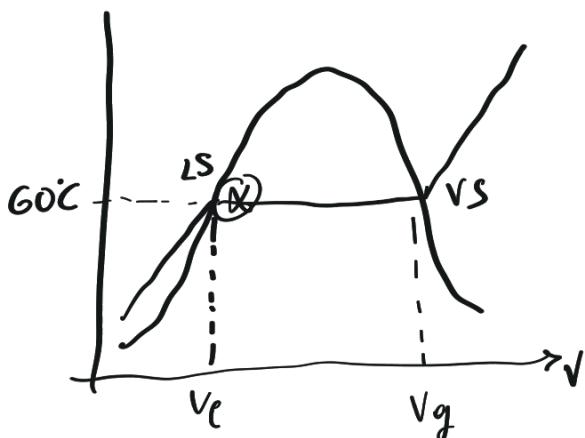
2. c  
Stando  
Fluode

Adiabatico L non Q ← considerando resistenze come parte del sistema adiabatico

$$U_2 - U_1 = \underbrace{Q}_{0 \text{ adiabatico}} - \vec{L} \quad \vec{L} = -\vec{L}_{el} = \int_0^t W_{el} dt = \vec{Z} \cdot t = 900 \text{ kJ}$$

$$\Delta U = U_2 - U_1 = \vec{L}_{el} = 900 \text{ MJ}$$

Veniamo a fare



$$V = v \cdot M \Rightarrow v = 0,2 \frac{\text{m}^3}{\text{kg}} \quad V_1 = 0,2$$

$$V_f = 0,001072 \frac{\text{m}^3}{\text{kg}} \quad V_f < V_1 < V_g \Rightarrow \text{BIFASE}$$

$$V_g = 7,671 \frac{\text{m}^3}{\text{kg}}$$

$$U_1 = M u_1 = M(u_{e1} + \chi_1 u_{lg}) \approx 2,58$$

$\underbrace{\text{percentuale}}_{\text{differenza tra } u_e \text{ e } u_{lg}} \cdot \text{differenza tra } u_e \text{ e } u_{lg}$

$$U_2 = U_1 + \vec{L}_{el} = 992,58 \text{ kJ}$$

$$u_2 = \frac{V_2}{M} = 3308,6 \frac{\text{kJ}}{\text{kg}}$$

sappiamo  $V$  perché non varia

$$\text{A } 180^\circ \rightarrow v_g \approx 0,2 \quad V_2$$

$$v_g = 2583,7 \frac{\text{kJ}}{\text{kg}}$$

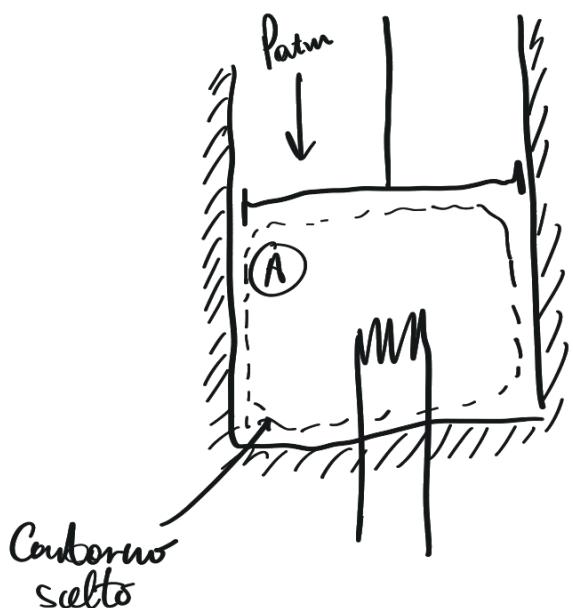
Non possono avere  
tutte e due  
nelle miscele  
Lo spazio che questo  
è fornito dalle  
muscole

Nel tabella <sup>di VS</sup> cerchiamo  $P_2$  e  $T_2$  che soddisfano

$$V_2 \in u_2 \rightarrow P_i = 2 \text{ MPa} \leftarrow$$

$$T_2 = 600^\circ\text{C} \leftarrow$$

### Esercizio 7



$$V_1 = 0,02 \text{ m}^3$$

$$T_1 = 10^\circ\text{C}$$

$$P_1 = P_{ATM} = 101325 \text{ Pa} - P_i = P$$

$$\lambda_2 = 0,1 \quad ? h_2, v_2, s_2$$

( $\hookrightarrow$  Titolo finale)

$\rightarrow$  Titolo  $\leftrightarrow$  Bifore



$$? L'ee \quad ? Me_2$$

$$\Delta U_B = U_{2B} - U_{1B} = L' - L'_{ee}$$

$$h_1 = 419,04 \quad h_2 = 2676,1$$

$$h_2 = X \cdot h_2 + (1-X) \cdot h_1 = 0,1 \cdot 2676,1 \frac{kJ}{kg} + 0,9 \cdot 419,04 \frac{kJ}{kg} = \\ = 644,7 \frac{kJ}{kg}$$

$$v_2 = 0,168 \frac{m^3}{kg}$$

$$s_2 = 1,9 \frac{kJ}{kgK}$$

$$(V_2 - V_1)^* = Q^* - L^* = Q^* - L_{ee}^* - L_{esp}^*$$

(Adiabatic)

$$L_{esp}^* = \int_1^2 P dV \stackrel{\text{isobaric}}{=} P(V_2 - V_1) =$$

$$V_2 - V_1 = L_{ee}^* - (P V_2 - P V_1)$$

$$L_{ee}^* - (V_2 - PV_2) - (V_1 - PV_1) = H_2 - H_1$$

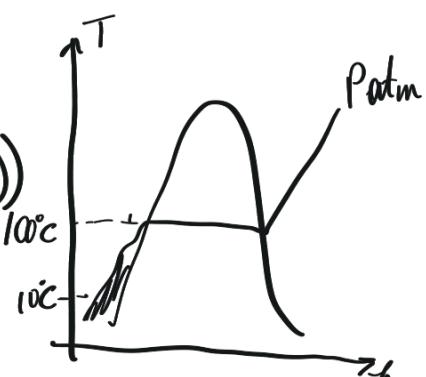
*Come debba tempo se si potrebbero scegliere le \**

$$L_{ee}^* = M_{\text{air}} (h_2^* - h_1^*)$$

$$M = \rho \cdot V = \frac{V}{r} = \frac{0,002 \text{ m}^3}{0,001 \text{ m}^3/\text{kg}} = 2 \text{ kg}$$

$$h_e(p, T) = h_{1s}(10^\circ\text{C}) + v_{es}(p - p_{80^\circ\text{C}}(10^\circ\text{C}))$$

*Patin 10°C*



$$= 41990 \boxed{\frac{J}{kg}} + 0,01 \frac{m^3}{kg} \cdot (101325 Pa - 1236 Pa) = 42,090 \frac{J}{kg}$$

$$L_{ee}^* = M (h_2^* - h_1^*) = 1202 \text{ kJ}$$

$$M_{el2} = (1 - \chi_e) M = 0,9 \cdot 2 \text{ kg} = 1,8 \text{ kg}$$

Fine sistemi diurni