

## Lesson 3

Writing  $\ell(Q)$  was through the dimensionlessisation of the Euler equation, and allowed us to find dimensionless terms.

Result of last lesson:

$$\ell = u_2 v_{2t} - u_1 v_{1t}$$

$$\ell = \ell(Q, n, D, \text{SHAPE})$$

$\hookrightarrow$  becomes dimensionless

$$\lambda = \lambda(Q, \text{SHAPE})$$

Using:

$n$  = time scale

$D$  = length scale

We find:

$$\left\{ \begin{array}{l} \varphi = \frac{Q}{nD^2} \\ \lambda = \frac{\ell}{n^2 D^2} \end{array} \right.$$

Abstract approach to return to  $H(Q)$

$$H = H(Q) ? \rightarrow \boxed{gH} = \ell - \ell_w = \ell(Q, n, D, \text{SHAPE}) - \ell_w(n, D_f, \rho, \mu, \text{SHAPE})$$

What is  $\ell_w$ ?

$$\Rightarrow \boxed{H(Q, n, D, \rho, \mu, \text{SHAPE})}$$

$$y \rightarrow \xi = \frac{y}{\sqrt{2}} = \xi(\text{Re, SHAPE})$$

$\hookrightarrow$  Dimensionless loss

"Tsi"  $\rightarrow$  zeta

$$\ell_w \rightarrow \xi = \ell_w / n^2 D^2 = \xi(\text{Re, SHAPE}); \text{Re} = \frac{\rho D w}{\mu}$$

$\hookrightarrow$  Physically it's the same a  $y$ , but occurs inside the machine

$\hookrightarrow$  To make dimensionless it's best to use the easiest thing to

determine.

$$\Rightarrow \bar{h}\omega = \bar{h}\omega(n, D, \varphi, \mu, \text{SHAPE})$$

↳ We are taking this for granted without much demonstration

→ Head dimensionless coefficient:

$$\bar{\psi} = \frac{g H}{n^2 D^2}$$

$$\Rightarrow \bar{\psi} = \bar{\psi}(\varphi, \text{Re}, \text{SHAPE})$$

In this course we always consider  $\text{Re}$  such that we have a fully-turbulent flow.  $\Rightarrow \frac{\partial \bar{\psi}}{\partial \text{Re}} = 0 \rightarrow \bar{\psi} = \bar{\psi}(\varphi, \text{SHAPE})$

$$\text{and } g H = g^{+}(\bar{Q}, n, D, \text{SHAPE})$$

Hydraulic similarity

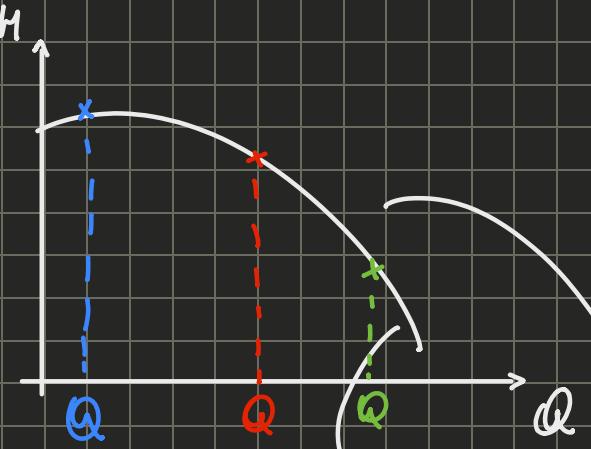
$\Rightarrow$  Incompressible flows

$\Rightarrow$  Fully-turbulent flow (dynamic  $\rightarrow$  kinematic)

SHAPE ASSIGNED  $\rightarrow$  we focus on a family of geometrically similar machines.

D assigned  $\Rightarrow$  size of the machine defined, since we have already given SHAPE, everything else is defined

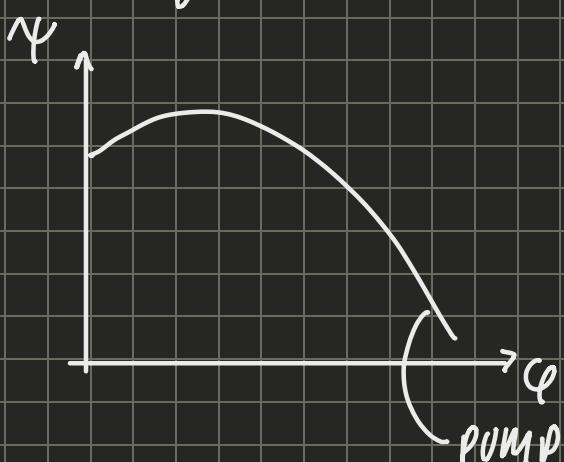
$\bar{Q}, n \rightarrow$  represent the operating condition of the machine



SHAPE, D and n are fixed  
=> only once have done this  
will we have a dimensional  
relationship

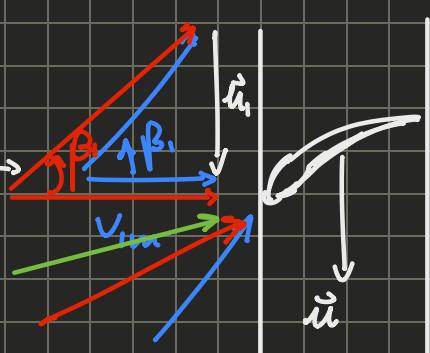
PUMP at given  $n$ ,  $D$ ,  $\beta_1$   
and  $\beta_2$ .  
=> valid for specific machine,  
of shape and size and  
operating condition.

In dimensionless term only the SHAPE needs to be  
arranged since  $H - \dot{V}(\varphi, \text{SHAPE})$



=> These curves are true for a  
family of machines, independent  
of size and operating condition

This is very useful for us.



Once we know  $Q$  and the  
size - we know  $V_{ii}$

We only design the blade to one  
 $\beta_1$ , so if we change  $Q$ , there will  
only one condition (correct condition)  
that works.

$\beta_2$  is constructive. The more we have to deflect the flow,  
the more energy do we have spent. So varying  $Q$ , the  
head also changes.

Off the nominal point, the hydraulics, and performances.

Using  $h_w$  to define efficiency.

### Hydrodynamic efficiency of pump

$$\eta_p = \frac{g H}{\ell} = \frac{\ell - h_w}{\ell} = 1 - \frac{h_w}{\ell}$$

$$\eta_p = \frac{\psi}{\lambda} = \eta_p(\varphi, \text{SHAPE})$$

since both  
are three dimensional  
terms divided by  
 $n^2 D^2$ .

IF NOT FULLY-TURBOLENT FLOW:  $\eta_p(\varphi, Re, \text{SHAPE})$

Result of dimensionless analysis:

$$\lambda = \lambda(\varphi, \text{SHAPE})$$

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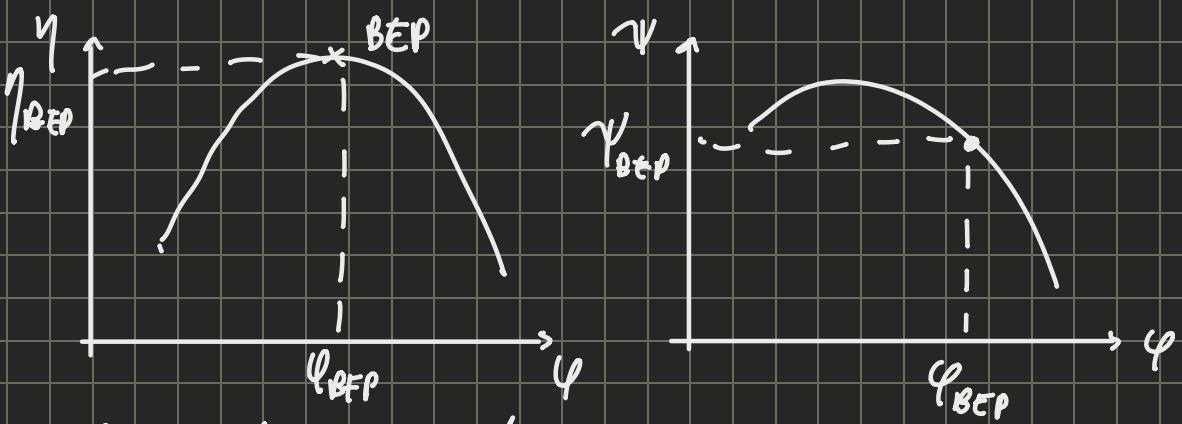
$$\psi = \psi(\varphi, \cancel{\lambda}, \text{SHAPE}) \rightarrow \text{if } Re \text{ is low we need to add corrective term.}$$

$$\eta = \eta(\varphi, \cancel{\lambda}, \text{SHAPE})$$

$\psi = \psi(\lambda, \text{SHAPE}) \rightarrow$  we can do this as long as we only have 2-dimensional terms.

$\eta = \eta(\lambda, \text{SHAPE})$  or  $\eta = \eta(\psi, \text{SHAPE})$   $\rightarrow$  independent

We can represent the relationships:



B.E.P = efficiency point

We typically try to design a machine to its BEP.

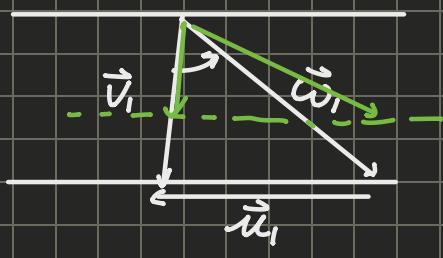
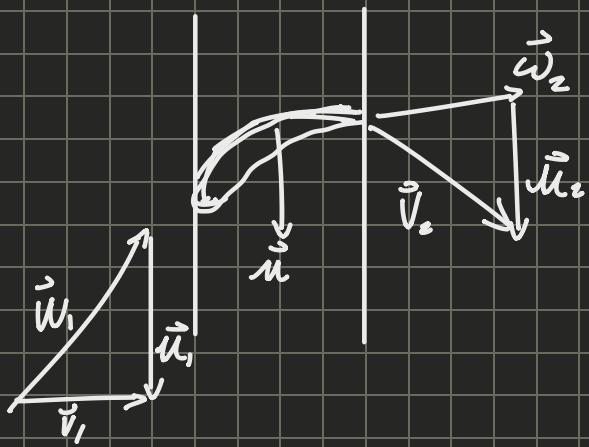
Given a machine for which  $H = H(Q, n, D, \text{SHAPE})$   
 $\Psi = \Psi(\varphi, \text{SHAPE})$

Is it possible to change  $Q, n, D$  such that they change but  $\Psi$  doesn't?

Yes. If true these conditions are called similarity / corresponding conditions.

$$\left\{ \begin{array}{l} \varphi, \varphi' \\ \Psi, \Psi' \end{array} \right. \text{ such that } \left\{ \begin{array}{l} \varphi = \varphi' \\ \Psi = \Psi' \end{array} \right. \Rightarrow \text{similarity or corresponding conditions}$$

Example to help understand

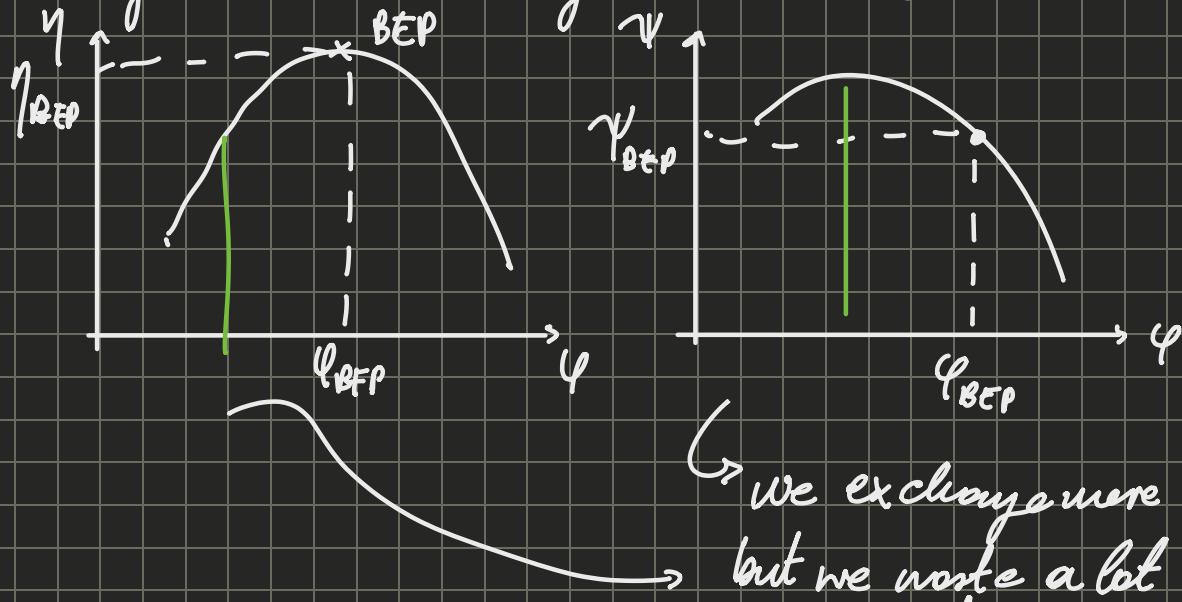


$\alpha_1$  &  $\beta_2$

do not change since they are constructive

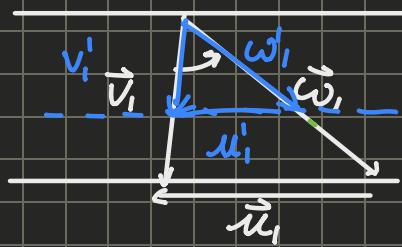
What happens if  $Q' = Q/2$

keeping the machine as is, without changing D or n, everything changes as we have changed conditions.

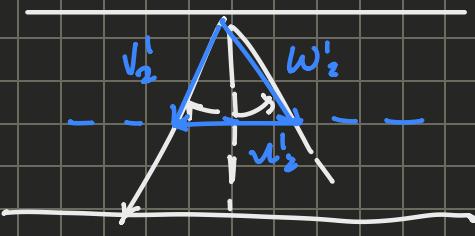


$Q' = Q/2$ ,  $D' = D$  → we want to find n  
we keep the same machine  
so we don't have to get another one.

$$\text{if similarity: } \varphi' = \varphi \Rightarrow \frac{Q'}{n' \cancel{\varphi}} = \frac{Q}{n \cancel{\varphi}} \Rightarrow \frac{n'}{n} = \frac{Q'}{Q} \Rightarrow n' = n/2$$



to have similarity we need to halve the speed.



The  $\beta_1$  &  $\alpha_2$  are the same  
⇒ through similarity conditions,

$$\beta'_i = \beta_i \text{ & } \alpha'_z = x_z$$

We can guarantee that our non-constrictive angles are conserved.

Conserving the shape of the triangles, we also conserve performance parameters ( $\varphi' = \varphi$  &  $\psi' = \psi$ )

The velocity triangles are different, meaning the work is lower since the factor was 2, the work will be 4 times lower.

The head is proportional to the work only if the efficiency is constant  $\Rightarrow$  since  $\frac{\ell'}{\ell} = \frac{1}{4} \Rightarrow \frac{H'}{H} = \frac{1}{4}$

In this case

In this case.

Other approach

$$Q' = Q/2 ; D' = D, \text{ and } \underline{\text{shape assigned.}}$$

$$\left. \begin{array}{l} \varphi' = \varphi \\ \psi = \psi(\varphi, \text{SHAPE}) \\ \psi' = \psi'(\varphi', \text{SHAPE}) \end{array} \right\} \Rightarrow \psi' = \psi \Rightarrow H' = \left( \frac{n'}{n} \right) H$$

quicker derivation

since  $\varphi' = \varphi$  and the shape is assigned.

Similarity condition  $\Rightarrow$  similarity in the velocity triangles.

Once again, everything will become more complicated with other fluid machines where  $\rho \neq \text{const.}$

The next 2 hours we will be using an approach  
which isn't very rigorous, but the result works.