

Esercitazione 7 -

dark practical lesson with full exercise for multiple dof system.
From next only the matrices

Continuing exercise from last time

L EOM:

$$\frac{d}{dt} \frac{\partial E_c}{\partial \ddot{\theta}} - \frac{\partial E_c}{\partial \dot{\theta}} + \frac{\partial D}{\partial \theta} + \frac{\partial V}{\partial \theta} = Q$$

we usually partition
(free and constrained
dof.)

By skipping the theoretical passages we end up with:

$$[M]\ddot{q} + [R]\dot{q} + [k]q \quad \text{with } q = \begin{bmatrix} \theta \\ z \end{bmatrix}$$

↑ free (unconstraint)
↓ constrained

$$[M]\ddot{q} + [R]\dot{q} + [k]q = [Q_u]$$

can be a matrix, or just an element

In 3dof system with 1constrained:

e.g.

$$\begin{bmatrix} m_{uu} & m_{uv} & m_{uw} \\ m_{vu} & m_{vv} & m_{vw} \\ m_{wu} & m_{wv} & m_{ww} \end{bmatrix} \begin{bmatrix} \ddot{q}_u \\ \ddot{q}_v \\ \ddot{q}_w \end{bmatrix}$$

we split the matrix in the same way.

$$\begin{aligned} I &= \begin{bmatrix} [m_{uu}] & [m_{lu}] \\ [m_{lu}] & [m_{ll}] \end{bmatrix} \begin{bmatrix} \ddot{q}_l \\ \ddot{q}_u \end{bmatrix} + \begin{bmatrix} [R_{lu}] & [R_{ll}] \\ [R_{lu}] & [R_{ll}] \end{bmatrix} \begin{bmatrix} \dot{q}_l \\ \dot{q}_u \end{bmatrix} + \begin{bmatrix} [k_{lu}] & [k_{ll}] \\ [k_{lu}] & [k_{ll}] \end{bmatrix} \begin{bmatrix} q_l \\ q_u \end{bmatrix} = [Q_l] \\ II &= \begin{bmatrix} [m_{uu}] & [m_{lu}] \\ [m_{lu}] & [m_{ll}] \end{bmatrix} \begin{bmatrix} \ddot{q}_l \\ \ddot{q}_u \end{bmatrix} + \begin{bmatrix} [R_{lu}] & [R_{ll}] \\ [R_{lu}] & [R_{ll}] \end{bmatrix} \begin{bmatrix} \dot{q}_l \\ \dot{q}_u \end{bmatrix} + \begin{bmatrix} [k_{lu}] & [k_{ll}] \\ [k_{lu}] & [k_{ll}] \end{bmatrix} \begin{bmatrix} q_l \\ q_u \end{bmatrix} = [Q_u] \end{aligned}$$

$L \rightarrow \text{libero}$ $V \rightarrow \text{vincato}$
 (not V)

→ We have split the contributions of the free and constrained effects.

q_L and Q_V can be scalar or vectors.

q_V is known, Q_L is unknown

but q_L and Q_V are unknown

We need to solve the two rows, one is an ODE, the second is an algebraic equation.

$$(ODE) \text{ I Row } [M_{LL}] \ddot{q}_L + [R_{LL}] \dot{q}_L + [k_{LL}] q_L = -([M_{LV}] \ddot{q}_V + [R_{LV}] \dot{q}_V + [k_{LV}] q_V) + Q_L$$

known

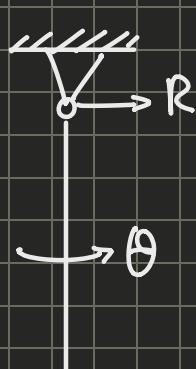
? ? ?

→ Solving we find q_L

II. Row (Algebraic equation)

$$Q_V = \underbrace{[M_{VL}] \ddot{q}_L}_{\text{we have found these}} + \underbrace{[R_{VL}] \dot{q}_L}_{\text{we have found these}} + \underbrace{[k_{VL}] q_L}_{\text{unknown}} + \underbrace{[M_{VV}] \ddot{q}_V}_{\text{unknown}} + \underbrace{[R_{VV}] \dot{q}_V}_{\text{unknown}} + \underbrace{[k_{VV}] q_V}_{\text{unknown}}$$

→ we get Q_V → this is how we get the reaction forces where the degrees of freedom are constrained.

 How to calculate R ?

→ Solve the system for t
or change the system to:

in this case $z=0$



imposing a motion of z ,
we get the reaction
forces of the system.

$$z(t) = z_0 \cos(\sqrt{t})$$

L6OM → FRF

From L6OM we can write FRF for a degree of freedom

$$z \rightarrow \theta$$

$$F_L$$

INPUT → $\boxed{\text{FRF}}$ → θ
(can be z ,
or some force.)

OUTPUT is
always θ for us.

$$q_v = \bar{q}_{v0} \cos(\sqrt{t}) \xrightarrow{[A]} q_L = \bar{q}_{L0} \cos(\sqrt{t})$$

→ use first row of system, substitute and calculate FRF

$$\left[\begin{array}{l} -\sqrt{z} [M_{L1}] + i\sqrt{z} [R_{L1}] + [k_{L1}] \\ \vdots \end{array} \right] \bar{q}_{L0} e^{i\sqrt{t}} = \left[\begin{array}{l} -\sqrt{z} [M_{L1}] + i\sqrt{z} [R_{L1}] + [k_{L1}] \\ \vdots \end{array} \right] \bar{q}_{v0} e^{i\sqrt{t}}$$

[A] → complex since i
[B] → we don't care for t , since we
are interested in the steady state

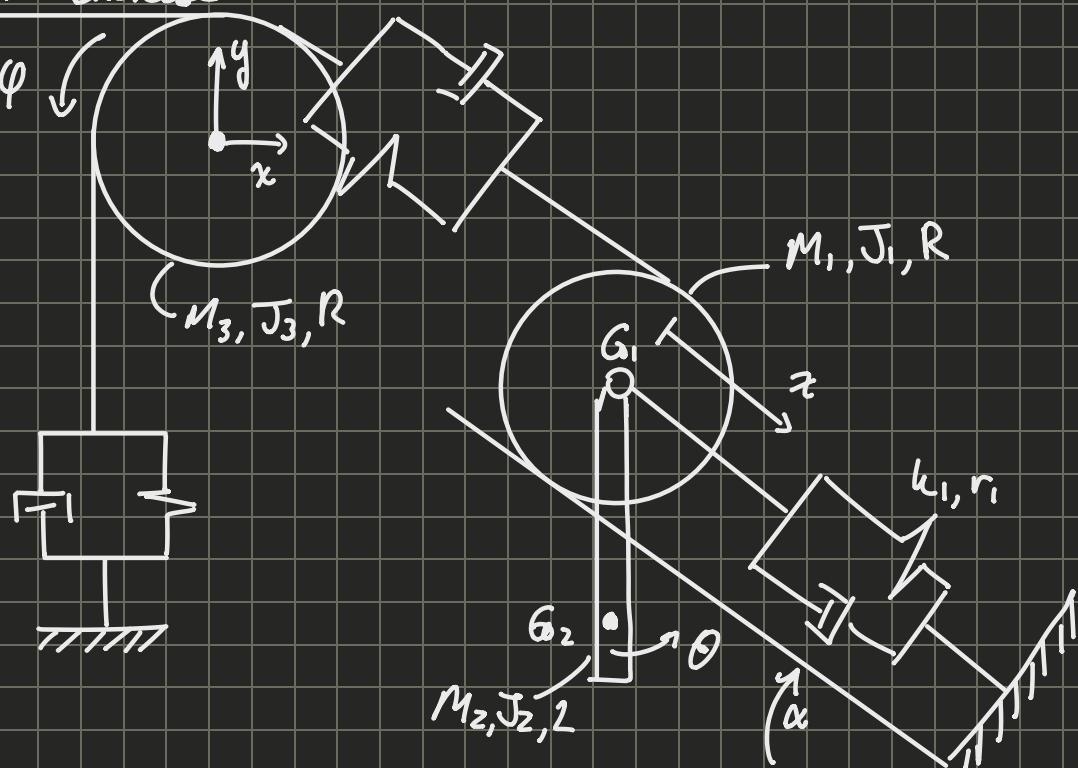
[A] depends on the system

[B] depends on the position of the input

sum of all FRF between inputs and / outputs

$$[A] q_{lo} = [B] q_{vo} \rightarrow q_{lo} = [A]^{-1} [B] q_{vo} = \underbrace{[G(v)]}_{\substack{\text{mechanical} \\ \text{impedance matrix} \\ \text{of system}}} q_{vo}$$

Other exercise



$$q = [x, \theta, \varphi]^T$$

↳ constrained variable \rightarrow just for practice, nothing changes.

$$\varphi = \varphi_0 \cos(\sqrt{2}t)$$

Step 3 dof

3 bodies 3×3 9 dof

2 hinges 2×2 -4

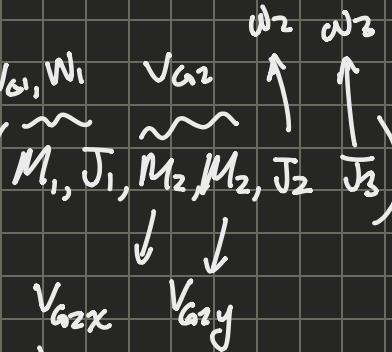
1 roll w/slide 1×2 -2

3 dof

Step 2

$$\cdot \underline{\underline{\boldsymbol{\delta}_c}} = \frac{1}{2} \dot{\underline{\underline{\boldsymbol{y}_m}}}^T \begin{bmatrix} m_1 \\ m_2 \\ m_3 \end{bmatrix} \dot{\underline{\underline{\boldsymbol{y}_m}}}$$

$$\begin{bmatrix} m_1 \\ m_2 \\ m_3 \end{bmatrix} = \text{diag} \left(\begin{bmatrix} M_1, J_1 \\ M_2, J_2 \\ M_3, J_3 \end{bmatrix} \right)$$



since v_{Gz} has a complex trajectory it's easier to split the motion in two directions.

$$\cdot \underline{\underline{\boldsymbol{D}}} = \frac{1}{2} \dot{\underline{\underline{\boldsymbol{\Delta l}}}}^T \begin{bmatrix} r_1 \\ r_2 \\ r_3 \end{bmatrix} \dot{\underline{\underline{\boldsymbol{\Delta l}}}}$$

$$\cdot \underline{\underline{\boldsymbol{V_u}}} = \frac{1}{2} \dot{\underline{\underline{\boldsymbol{\Delta l}}}}^T \begin{bmatrix} h_1 \\ h_2 \\ h_3 \end{bmatrix} \dot{\underline{\underline{\boldsymbol{\Delta l}}}}$$

$$\cdot \underline{\underline{\boldsymbol{V_g}}} = \underline{\underline{\boldsymbol{f}}}^T \cdot \underline{\underline{\boldsymbol{h}}}_c$$

$$\cdot \dot{\underline{\underline{\boldsymbol{\delta}}}} \dot{\underline{\underline{\boldsymbol{\alpha}}}} = \underline{\underline{\boldsymbol{F}}}^T \cdot \underline{\underline{\boldsymbol{S_y}}}_{\underline{\underline{\boldsymbol{F}}}}$$

$$\underline{\underline{\boldsymbol{r}}}_1 = \text{diag} \begin{bmatrix} r_1, r_2, r_3 \end{bmatrix}$$

$$\underline{\underline{\boldsymbol{h}}}_1 = \text{diag} \begin{bmatrix} h_1, h_2, h_3 \end{bmatrix}$$

$$\underline{\underline{\boldsymbol{f}}}^T = [M_1 g, M_2 g, M_3 g]^T$$

$$\dot{\underline{\underline{\boldsymbol{\Delta l}}}} = [\dot{\Delta l}_1, \dot{\Delta l}_2, \dot{\Delta l}_3]^T$$

$$\ddot{\underline{\underline{\boldsymbol{\Delta l}}}} = [\ddot{\Delta l}_1, \ddot{\Delta l}_2, \ddot{\Delta l}_3]^T$$

$$\underline{\underline{\boldsymbol{h}}} = [h_1, h_2, h_3]^T$$

Always vertical vectors

Step 3

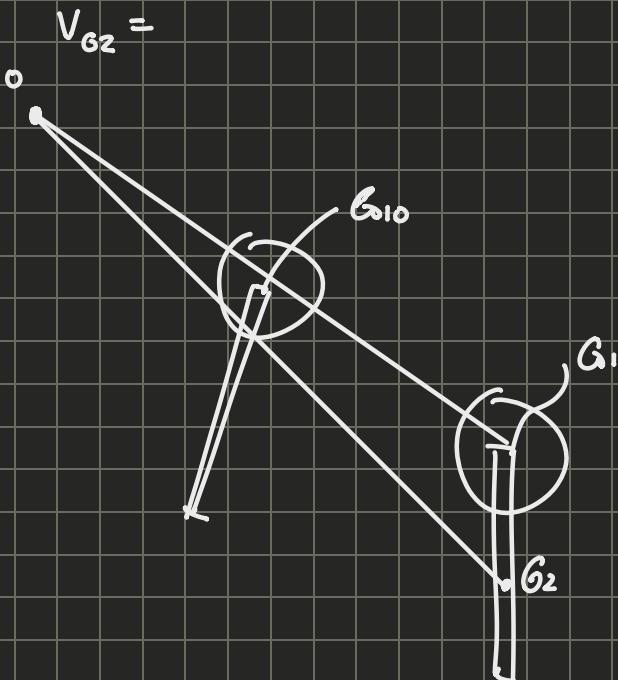
$$- V_{G1} = \dot{x}$$

$$- \omega_1 = -\frac{\dot{x}}{R}$$

$$- \omega_2 = \dot{\theta}$$

$$- \omega_3 = \dot{\phi}$$

$$V_{G2} = ?$$



(NL) Vektorial Closing

$$(G_{10} - O) = (\tilde{x} \hat{i} + \tilde{y} \hat{j})$$

$$(G_1 - G_{10}) = x \cos \alpha \hat{i} - x \sin \alpha \hat{j}$$

↳ constant, shown in diagram

$$(G_2 - G_1) = \frac{L}{2} \sin \Theta \hat{i} - \frac{L}{2} \cos \Theta \hat{j}$$

$$(G_2 - O) = (G_{10} - O) + (G_1 - G_{10}) + (G_2 - G_1)$$

$$= \left(\tilde{\tau}_x + x \cos \alpha + \frac{L}{2} \sin \theta \right) \hat{i} + \left(\tilde{\tau}_y - x \sin \alpha - \frac{L}{2} \cos \theta \right) \hat{j}$$

$$V_{Gz} = \frac{d}{dt} (G_z - 0) = \left(x \cos \alpha + \frac{L}{2} \cos \theta + \dot{\theta} \right) \hat{i} + \underbrace{\left(-x \sin \alpha + \frac{L}{2} \sin \theta \cdot \dot{\theta} \right)}_{\downarrow h_2} \hat{j}$$

$[\Lambda_m]$	\dot{x}	$\dot{\theta}$	$\dot{\varphi}$
V_{G1}	1	0	0
ω_1	$-1/R$	0	0
V_{G2x}	$\cos \alpha$	$\frac{L}{2} \cos \theta$	0
V_{G2y}	$-\sin \alpha$	$\frac{L}{2} \sin \theta$	0
ω_2	0	1	0
ω_3	0	0	1

\downarrow linearize

$[\Lambda_m]_0$	\dot{x}	$\dot{\theta}$	$\dot{\varphi}$
\sim	1	0	0
\sim	$-1/R$	0	0
\sim	$\cos \alpha$	$\frac{L}{2}$	0
\sim	$-\sin \alpha$	0	0
\sim	0	1	0
\sim	0	0	1

since α is a constant, it's already linear

$$\theta_0 = 0$$

$$\Delta l = ?$$

since x compresses l_1

$$\Delta l_1 = \Delta l_{01} \downarrow x$$

$$\Delta l_2 = \Delta l_{02} + 2x + \varphi R$$

$$\Delta l_3 = \Delta l_{03} - R\varphi$$

Δ_u	x	θ	φ
Δl_1	-1	0	0
Δl_2	2	0	R
Δl_3	0	0	$-R$

$$\left[\Delta_u \right]_o = \left[\Delta_k \right]_o$$

is evaluated at equilibrium

because l_i and r_i are all in parallel sets

$$- h_{G1} = \tau_2 - x \sin \alpha \rightarrow [H_{G1}] = \phi = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$- h_{G2} = \tau_2 - x \sin \alpha - \frac{L}{2} \cos \theta \rightarrow [H_{G2}] = \begin{bmatrix} \frac{\partial^2 h_2}{\partial x^2} & \frac{\partial^2 h_2}{\partial x \partial \theta} & \frac{\partial^2 h_2}{\partial x \partial \varphi} \\ \frac{\partial^2 h_2}{\partial \theta \partial x} & \frac{\partial^2 h_2}{\partial \theta^2} & \frac{\partial^2 h_2}{\partial \theta \partial \varphi} \\ \frac{\partial^2 h_2}{\partial \varphi \partial x} & \frac{\partial^2 h_2}{\partial \varphi \partial \theta} & \frac{\partial^2 h_2}{\partial \varphi^2} \end{bmatrix}$$

$$- h_{G3} = \text{const} \rightarrow [H_{G3}] = \phi$$

Hessian of h_{G2}

$$[H_{G2}] = \begin{bmatrix} 0 & 0 & 0 \\ 0 & L/2 \cos \theta & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

Eval. at Equilibrium

$$\bar{q}_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$[H_{G2}]_o = \begin{bmatrix} 0 & 0 & 0 \\ 0 & L/2 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\delta \ddot{x}^F = \underline{F}^T S y_F = \underbrace{\underline{F}^T}_{Q^T} \left[\Delta_F \right]_o \delta \bar{q}$$

$Q^T \sim$ Lagrangian component of external forces.

$\begin{bmatrix} \Lambda_F \end{bmatrix}$	x	θ	φ
δy_3	0	0	1

$$E_c = \frac{1}{2} \dot{q}^T [M] \dot{q} \quad \text{with } [M] = [\Lambda_{m_0}]^T [\Lambda_{m_1}] [\Lambda_{m_0}]$$

$$D = \frac{1}{2} \ddot{q}^T [R] \ddot{q} \quad \text{with } [R] = [\Lambda_{r_0}] [\Lambda_{r_1}] [\Lambda_{r_0}]$$

$$V_u = \frac{1}{2} \dot{q}^T [h] \dot{q} \quad \text{with } [h] = [\Lambda_{u_0}] [\Lambda_{u_1}] [\Lambda_{u_0}]$$

$$V_g = F^T h$$

$$V = V(q_0) + \frac{\partial V}{\partial q} \Big|_{q_0} (q - q_0) + \frac{1}{2} q^T [\Lambda_{u_0}]^T [\Lambda_{u_1}] [\Lambda_{u_0}] \cdot q$$

$\underbrace{\phantom{q^T [\Lambda_{u_0}]^T [\Lambda_{u_1}] [\Lambda_{u_0}] \cdot q}_{q_0}}$

$$+ \frac{1}{2} q^T \left[\sum_{i=1}^{Nq} M_i g [H_{k_i}] \right] \Big|_{q_0} \quad q \rightarrow \begin{bmatrix} h_I \\ h_{II} \end{bmatrix}$$

$$+ \frac{1}{2} q^T \left[\sum_{i=1}^{Nq} h_i \Delta \ell_{0i} [H \Delta \ell_i] \right] \Big|_{q_0}$$

$\hookrightarrow \begin{bmatrix} h_{III} \end{bmatrix}$

Hessian for $\Delta \ell_i$

$$Q^T = F^T [\Lambda_F]$$

we didn't calculate since they were all linear, so it would be a null matrix.