

# DSP Lect 6

(1)

## Frequency response

$$Y(t) = x(t) * h(t)$$

$$Y(\omega) = X(\omega)H(\omega)$$

why its true

$$Y(t) = \int_{-\infty}^{\infty} x(\tau) h(t-\tau) d\tau$$

$$\begin{aligned} Y(\omega) &= \int_{-\infty}^{\infty} y(t) e^{-j\omega t} dt = \int_{-\infty}^{\infty} \left( \int_{-\infty}^{\infty} x(\tau) h(t-\tau) d\tau \right) e^{-j\omega t} dt \\ &= \int_{-\infty}^{\infty} x(\tau) \left[ \int_{-\infty}^{\infty} h(t-\tau) e^{-j\omega t} dt \right] d\tau \end{aligned}$$

This looks like the FT of  $h(t-\tau)$

$$= \int_{-\infty}^{\infty} x(\tau) \tilde{f}(h(t-\tau)) d\tau = \int_{-\infty}^{\infty} x(\tau) H(\omega) e^{-j\omega \tau} d\tau$$

for  $h(t-\tau)$

$$\int_{-\infty}^{\infty} h(t-\tau) e^{-j\omega t} dt$$

$$= \int_{-\infty}^{\infty} h(x) e^{-j\omega(x+\tau)} dx = e^{-j\omega \tau} H(\omega)$$

Note! for  $F(k) = \int_{-\infty}^{\infty} f(x) e^{ikx} dx$ ,  $f(x) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(k) e^{-ikx} dk$

translation  $\Leftrightarrow F(k) e^{ik\tau}$  for above convention

Continuing,

$$H(\omega) \int_{-\infty}^{\infty} x(\tau) e^{-j\omega \tau} d\tau = H(\omega) X(\omega)$$

② Note: when using the convention, I learned in class  
the translation is opposite the sign

→ which works out beautifully for convolution

when  $F(k) = \int_{-\infty}^{\infty} f(x) e^{ikx} dx$

recall

$$f(t) \rightarrow \boxed{\begin{matrix} \text{LTI} \\ \text{System} \end{matrix}} \rightarrow h(t)$$

Impulse  
Response

$$F(h(t)) = H(\omega) \quad \begin{matrix} \text{Frequency} \\ \text{Response} \end{matrix}$$

Sometimes a system is written like

$$x(t) \rightarrow \boxed{h(t)} \rightarrow y(t)$$

$$x(t) \rightarrow \boxed{H(\omega)} \rightarrow y(t)$$

$$x(t) \rightarrow \boxed{h_1(t)} \rightarrow \boxed{h_2(t)} \rightarrow y(t)$$

$$x(t) \rightarrow \boxed{H_1(\omega)} \rightarrow \boxed{H_2(\omega)} \rightarrow y(t)$$

$$Y(\omega) = X(\omega) H_1(\omega) H_2(\omega) = X(\omega) H_2(\omega) H_1(\omega)$$

→ "Legal"

$$x(t) \rightarrow \boxed{H_2(\omega)} \rightarrow \boxed{H_1(\omega)} \rightarrow y(t)$$

changing order of  
LTI systems doesn't  
change result

$$x(t) \rightarrow \boxed{h_2(t)} \rightarrow \boxed{h_1(t)} \rightarrow y(t)$$

→ So what does the frequency response mean?

(3)

$$X(t) = e^{j\omega_0 t} \quad (\text{phase shift of } 1)$$

$$X(\omega) = 2\pi S(\omega - \omega_0) \quad \begin{array}{l} \text{phase shifted into the domain} \\ \rightarrow \text{time shift in frequency} \\ \text{domain} \end{array}$$

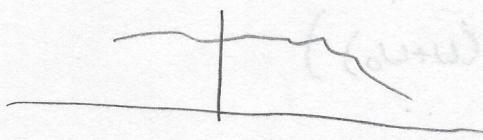
As a phase shift in the frequency domain is a time shift in the time domain.

So now

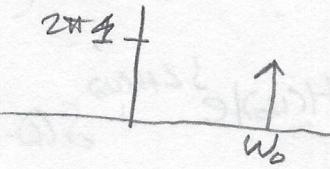
$$Y(\omega) = H(\omega) X(\omega) = H(\omega) 2\pi S(\omega - \omega_0)$$

freq  
response

$H(\omega)$



So then



$$H(\omega) 2\pi S(\omega - \omega_0) = H(\omega_0) 2\pi S(\omega - \omega_0)$$

And so

$$\mathcal{F} \{ Y(\omega) \} = y(t) = H(\omega_0) e^{j\omega_0 t}$$

some complex  
scalar

↳ original input  
signal

→ The LTI system cannot produce new frequencies that weren't present in the input

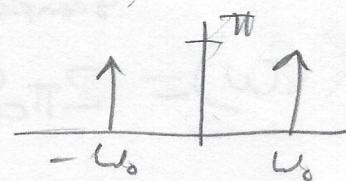
(4)

Suppose  $h(t)$  is real

$$X(t) = \cos(\omega_0 t)$$

$$\text{So then, } H(\omega) = (H(-\omega))^*$$

$$Y(\omega) = X(\omega)H(\omega)$$



$$= \pi (\delta(\omega - \omega_0) + \delta(\omega + \omega_0)) H(\omega)$$

$$= \pi (H(\omega_0) \delta(\omega - \omega_0) + H(-\omega_0) \delta(\omega + \omega_0))$$

$$= \pi (H(\omega_0) \delta(\omega - \omega_0) + (H(\omega_0))^* \delta(\omega + \omega_0))$$

$$= \pi (|H(\omega_0)| e^{j\angle H(\omega_0)} \delta(\omega - \omega_0) + |H(\omega_0)| e^{-j\angle H(\omega_0)} \delta(\omega + \omega_0))$$

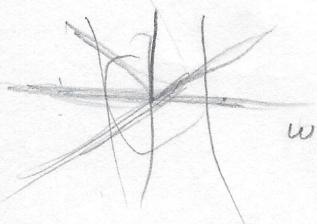
$$\Rightarrow Y(t) = |H(\omega_0)| \cos(\omega_0 t + \angle H(\omega_0))$$

Same cosine affected by amplitude and a phase

$\cos(3t) \rightarrow \square \rightarrow \cos \omega t$  Not an LTI system and

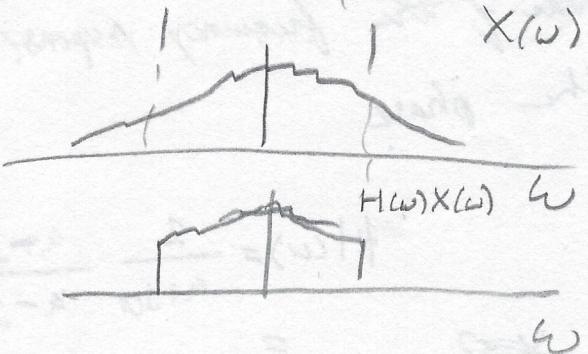
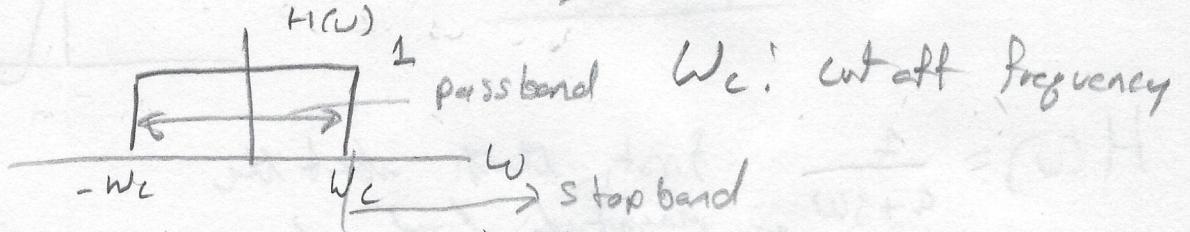
There is a different frequency  
Not from the original signal

To note a note



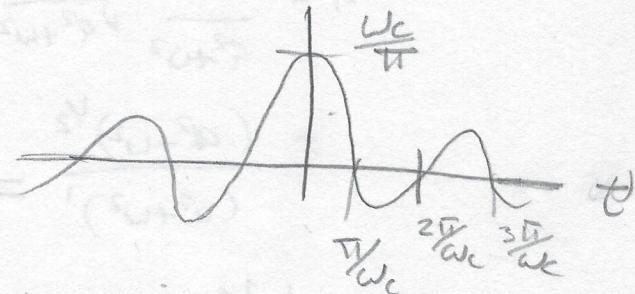
We often/usually interpret  $H(\omega)$  as what the system does to frequencies of the input signal "Filter" (5)

Important one: Low Pass Filter



So we can see that

$$h(t) = \frac{\omega_c}{\pi} \sin(\omega t)$$



There are some issues with  $h(t) = \frac{\omega_c}{\pi} \sin(\omega t)$

→ It's not causal. We are looking into the future to filter the signal (existing signal  $x(-t)$ ) which corresponds to the impulse response centered to the left of the y-axis.

→ The signal extends outward infinitely from the origin, so trying to create a huge delay ~~causes severe problems~~ to capture thousands of samples for the filter is a lot for precision. (Gotta stop somewhere)

→ The ripples of the sinc function will leak out in the output which is unwanted.

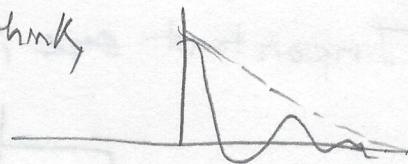
\* We will need to sacrifice in the frequency domain for a better time-domain filter.

(6) So what a good approximation?

Consider  $h(t) = e^{-at} u(t)$   $a > 0$



and think

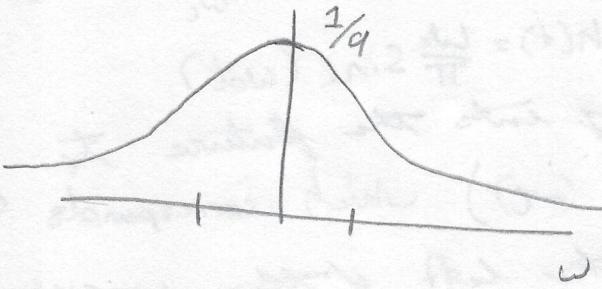


$$H(\omega) = \frac{1}{a + j\omega}$$

first, think about the magnitude of the frequency response  
also the phase

$$|H(\omega)| = \frac{1}{\sqrt{a^2 + \omega^2}} = \frac{\sqrt{a^2 + \omega^2}}{(a^2 + \omega^2)^{1/2}}$$

$$H(\omega) = \frac{1}{a + j\omega} = \frac{a - j\omega}{|a^2 + \omega^2|}$$



$H(\omega) \rightarrow$  a complex #

so look at  $|H(\omega)|$

→ This is how the input  $\rightarrow$   
affected by the magnitude!  
→ Essence of LPF

The width depends  
on  $a$

1) compute  $X(\omega)$  from  $x(t)$

2) multiply  $X(\omega)H(\omega) = Y(\omega)$

3) Take inverse FT to get  $y(t)$

(7)

$$X(t) = e^{-st} u(t), \quad h(t) = e^{-3t} u(t)$$

$$X(\omega) = \frac{1}{s+j\omega}$$

$$H(\omega) = \frac{1}{3+j\omega}$$

$$Y(\omega) = \frac{1}{(s+j\omega)(3+j\omega)}$$

$$H(\omega) = \frac{1}{3+j\omega}$$

$$Y(\omega) = \frac{A(3+j\omega) + B(s+j\omega)}{(s+j\omega)(3+j\omega)} = \frac{(3A+5B) + (A+D)j\omega}{(s+j\omega)(3+j\omega)}$$

$$3A + 5B = 1$$

$$A + B = 0$$

$$2B = 1 \quad B = \frac{1}{2} \quad A = -\frac{1}{2}$$

$$B = -A$$

$$Y(\omega) = \frac{-\frac{1}{2}}{s+j\omega} + \frac{\frac{1}{2}}{3+j\omega}$$

$$Y(t) = -\frac{1}{2} e^{-st} u(t) + \frac{1}{2} e^{-3t} u(t)$$

$$X(t) = e^{-t} u(t)$$

$$H(\omega) = \frac{2+j\omega}{(1+j\omega)(3+j\omega)}$$

$$X(\omega) = \frac{1}{1+j\omega}$$

$$\text{so } Y(\omega) = \frac{2+j\omega}{(1+j\omega)^2(3+j\omega)}$$

$$Y(\omega) = \frac{A}{(1+j\omega)^2} + \frac{B}{1+j\omega} + \frac{C}{3+j\omega}$$

$$\rightarrow \frac{4(3+j\omega) + B(1+j\omega)(3+j\omega) + C(1+j\omega)^2}{(1+j\omega)^2(3+j\omega)}$$

$$= \frac{(3A+3B+C) + (A+4B+2C)j\omega + (B+C)\omega^2}{(1+j\omega)^2(3+j\omega)}$$

$$3A + 3B + C = 2 \quad A + 4B + 2C = 1$$

$$B + C = 0$$

$$C = -B$$

$$A = \frac{1}{2}$$

$$B = \frac{1}{4}$$

$$C = -\frac{1}{4}$$

$$\rightarrow 3A + 2B = 2, \quad A + 2D = 1 \quad 2A = 1$$

so 
$$Y(\omega) = \frac{Y_2}{(1+j\omega)^2} + \frac{Y_4}{(1+j\omega)} + \frac{-Y_4}{(3+j\omega)}$$

$$Y(t) = Y_2 t e^{-t} u(t) + \frac{1}{4} e^{-t} u(t) - \frac{1}{4} e^{-3t} u(t)$$

$$Y(t) = \frac{d}{dt} X(t)$$

$$Y(\omega) = j\omega X(\omega)$$

$$\frac{d^2}{dt^2} Y(t) + 4 \frac{dY(t)}{dt} + 3Y(t) = \frac{d}{dt} X(t) + 2X(t)$$

$$(j\omega)^2 Y(\omega) + 4j\omega Y(\omega) + 3Y(\omega) = j\omega X(\omega) + 2X(\omega)$$

$$H(\omega) = \frac{Y(\omega)}{X(\omega)} = \frac{2 + j\omega}{(1 + j\omega)(3 + j\omega)}$$

Note multiplication in the time domain  $\leftrightarrow$   
convolution in the frequency domain

$$Z(t) = X(t)Y(t) \rightarrow Z(\omega) = \frac{1}{2\pi} X(\omega) * Y(\omega)$$

$$X(t) \cos(\omega_0 t)$$

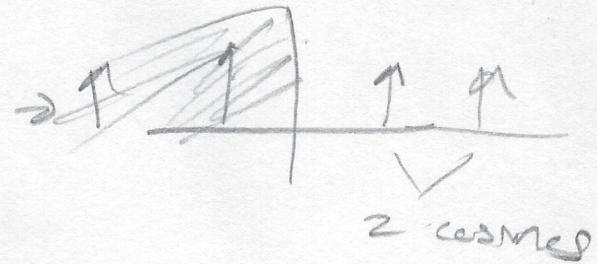
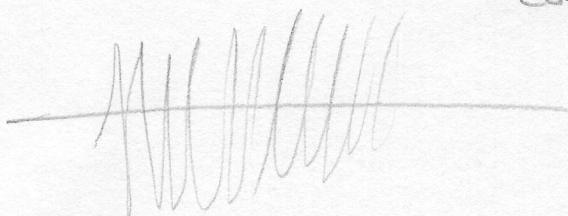
modulation  
Property

$$\overline{\text{---}} * \overline{1/1}$$

$$\overline{\text{---}} + \overline{\text{---}}$$

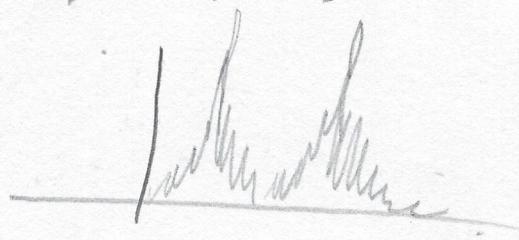
⑨

2 cosines



→ Low pass filter to get rid of one of the cosines

Since 2 cosines multiplied by 2 pulses



Sinc functions convolved  
with the impulses

A musical instrument gives you resonant frequencies → strong frequency peaks in the frequency domain

FT operates on  $\infty$  long continuous signal

→ Do long discrete the signal

→ finite long discrete signal

→ use filters and Notches to  
get rid of unwanted noise

→ to clean up the signal, there may need to be  
compression.