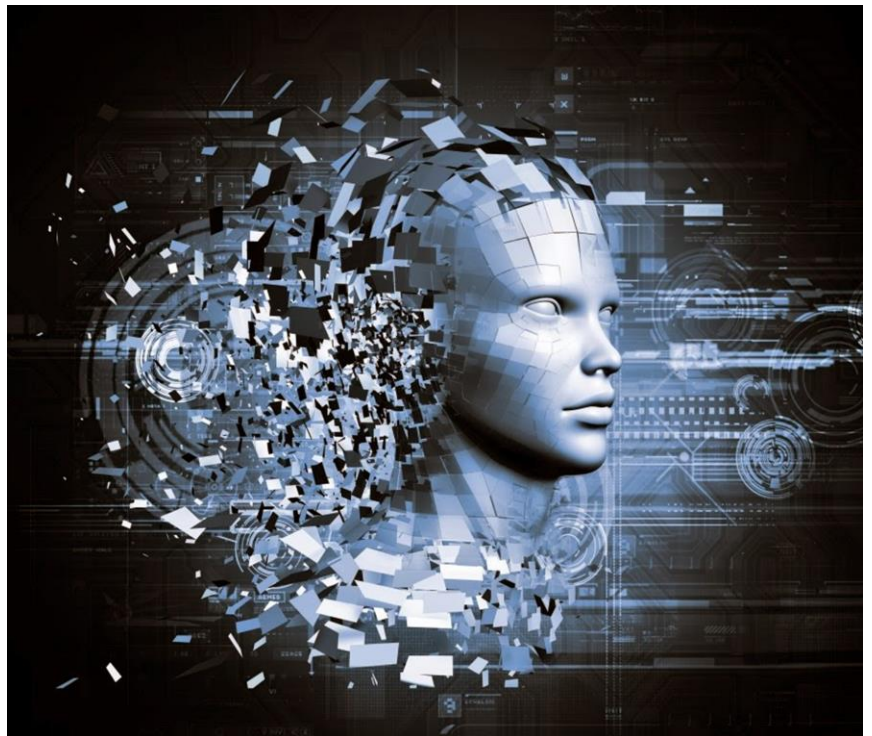


5/15/2018

Control System-I Lab - MCT-333L

Lab Reports



Submitted By:

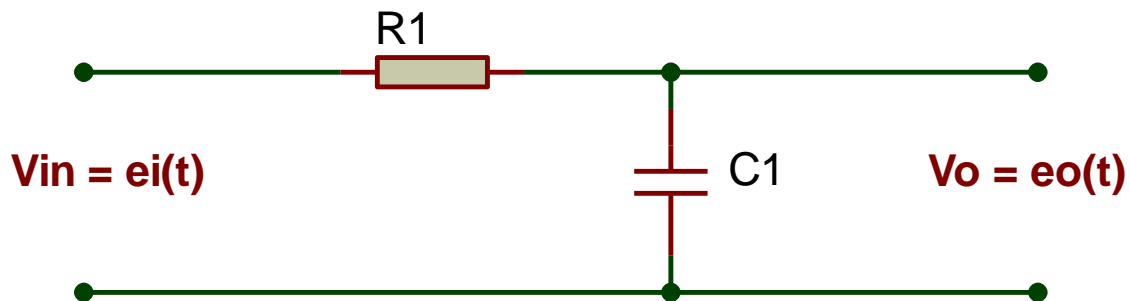
Muhammad Waqar Nawaz
(2015-MC-167)

Submitted To:

Engr. Abdullah Tahir

Lab # 1**First Order System****Objectives:**

1. To model the following circuit and also select the components for maximum $T_s = 0.8s$ and maximum $T_r = 0.06s$

**Theory:****Modeling:**

$$R \frac{dq}{dt}(t) + \frac{1}{C} q(t) = e_i(t)$$

$$\diamond q(t) = C e_o(t)$$

$$RC s E_o(s) + E_o(s) = E_i(s)$$

$$\frac{E_o(s)}{E_i(s)} = \frac{1}{RCs + 1}$$

$$\frac{E_o(s)}{E_i(s)} = \frac{\frac{1}{RC}}{(s + \frac{1}{RC})}$$

Compare it with General T.F of 1st order equation $T.F = \frac{a}{s+a}$

$$a = 1/RC$$

$$T_s = 3.91/a$$

$$T_r = 2.195/a$$

Required:

$$a = 3.91/0.8$$

$$a = 1/RC = 4.8875$$

$$a = 2.195/0.06$$

$$a = 1/RC = 36.58$$

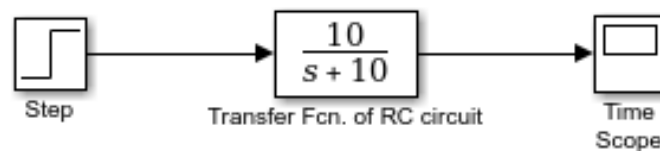
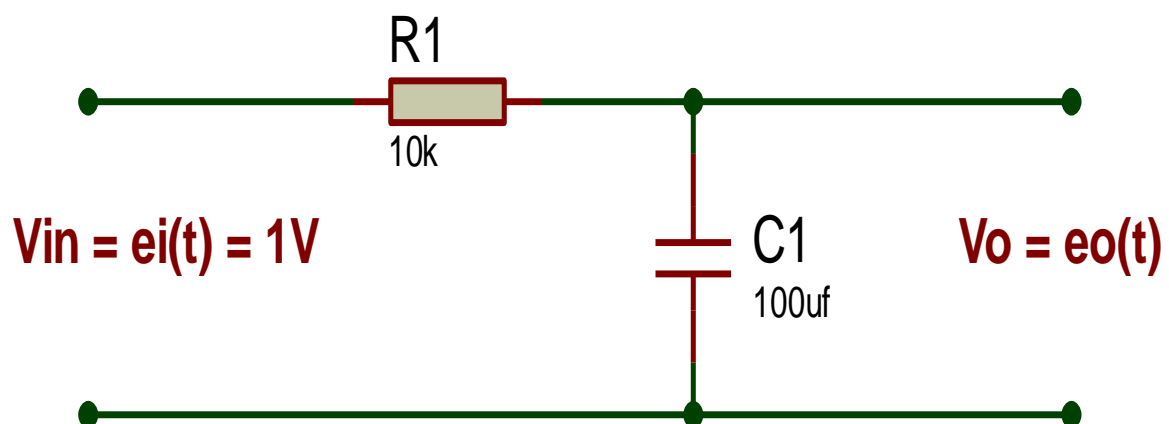
$$4.8875 < a < 36.58$$

Let $a = 10$ then,

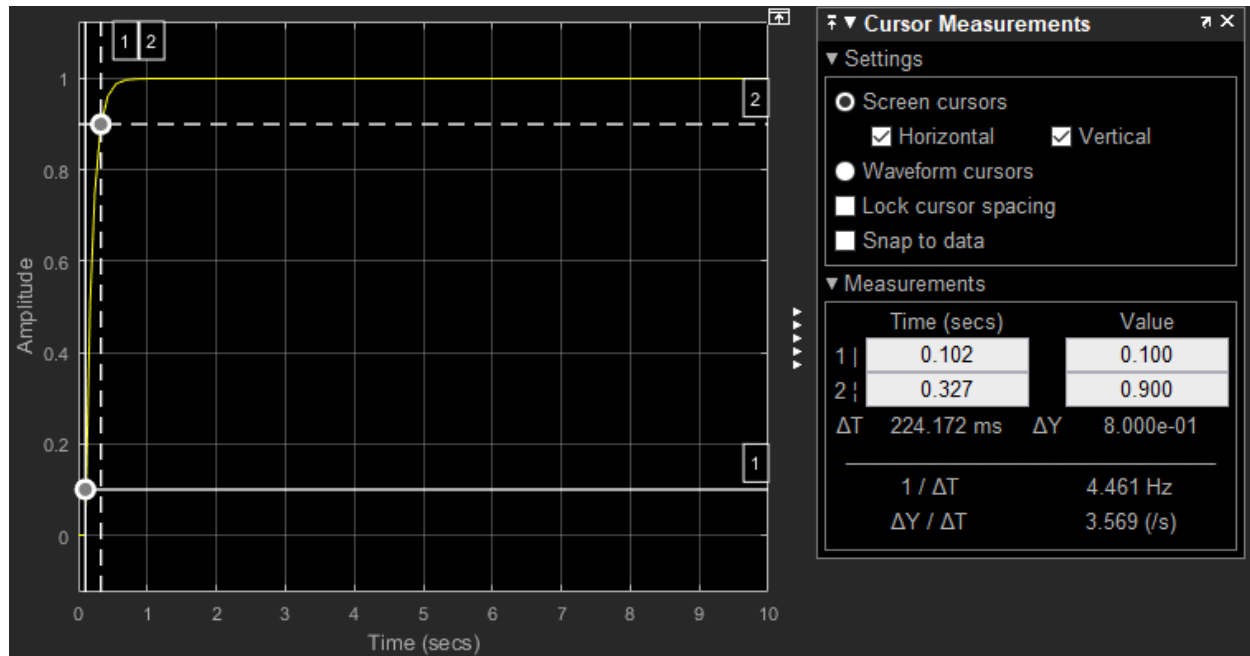
$$R = 1K(\text{ohm})$$

$$C = 100 \times 10^{-6} f$$

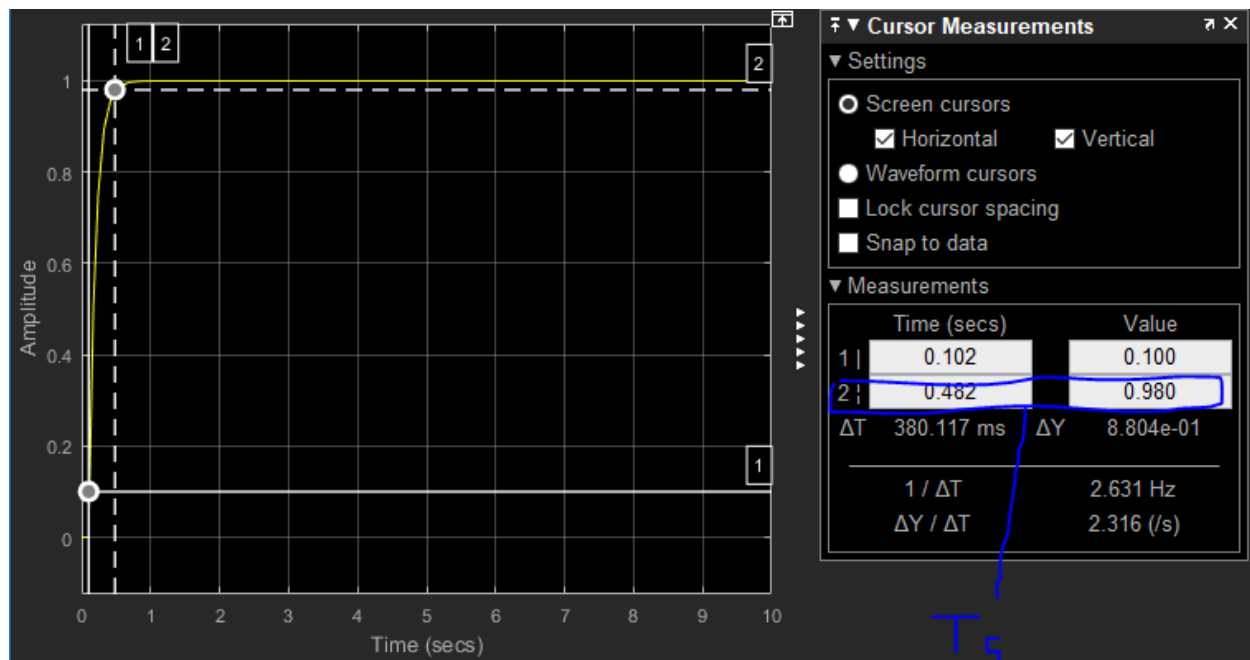
$$\text{Step input} = e_i(t) = 1V$$

Simulation:**Hardware Schematic:**

Result:

Rise Time (T_r):

$$T_r = 0.327 - 0.102 = 0.225s$$

Settling Time (T_s):

$$T_s = 0.482s$$

Comments:

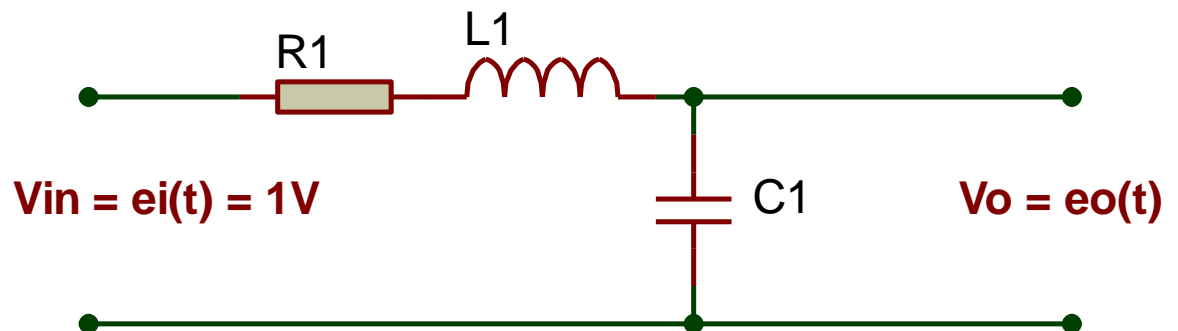
- System settling time less than 0.8s.

Lab # 2

Second Order System

Objectives:

- To model the following circuit and also select the components for
 - Under-damped
 - Over damped
 - Critically damped
 - Un-damped



Theory:

Modeling:

$$L \left(\frac{d^2 q}{dt^2} \right) + R \frac{dq}{dt} + \frac{1}{C} q(t) = e_i(t)$$

$$\diamond q(t) = C e_o(t)$$

$$L C s^2 E_o(s) + R C s E_o(s) + E_o(s) = E_i(s)$$

$$\frac{E_o(s)}{E_i(s)} = \frac{1}{(L C s + R C) s + 1}$$

$$\frac{E_o(s)}{E_i(s)} = \frac{\frac{1}{L C}}{\left(\left(s + \frac{R}{L} \right) s + \frac{1}{L C} \right)}$$

Compare it with General T.F of 2nd order equation T.F = $\omega_n^2 / (s^2 + 2\rho\omega_n s + \omega_n^2)$

$$a = R/L = 2\rho\omega_n$$

$$\rho = a/(2\omega_n)$$

$$b = 1/(LC) = \omega_n^2$$

Required:

- Under-damped

$$0 < \rho < 1$$

$$R = 40 \text{ (ohm)}; C = 510 \times 10^{-6} \text{ F}; L = 1 \text{ H}; e_i = 1 \text{ volt}$$

$$\rho = 0.452$$

- Over damped

$$\rho < 0$$

$$R = 100 \text{ (ohm)}; C = 510 \times 10^{-6} \text{ F}; L = 1 \text{ H}; e_i = 1 \text{ volt}$$

$$\rho = 1.129$$

- Critically damped

$$\rho = 1$$

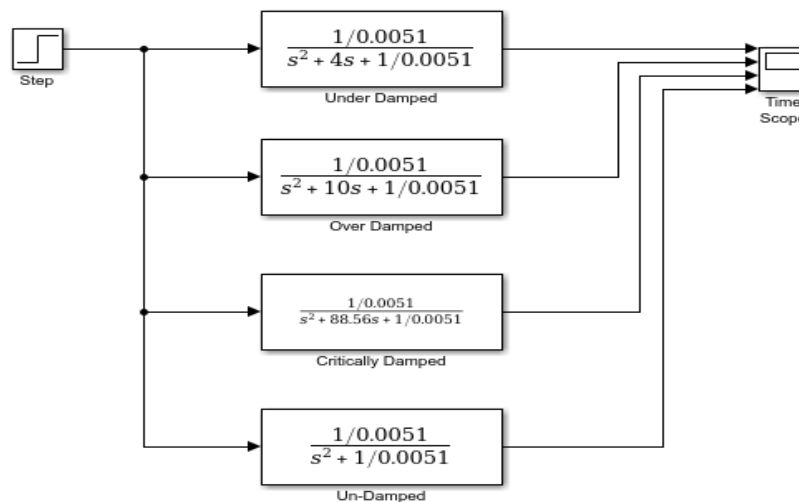
$$R = 885.6 \text{ (ohm)}; C = 510 \times 10^{-6} \text{ F}; L = 1 \text{ H}; e_i = 1 \text{ volt}$$

$$\rho \approx 1$$

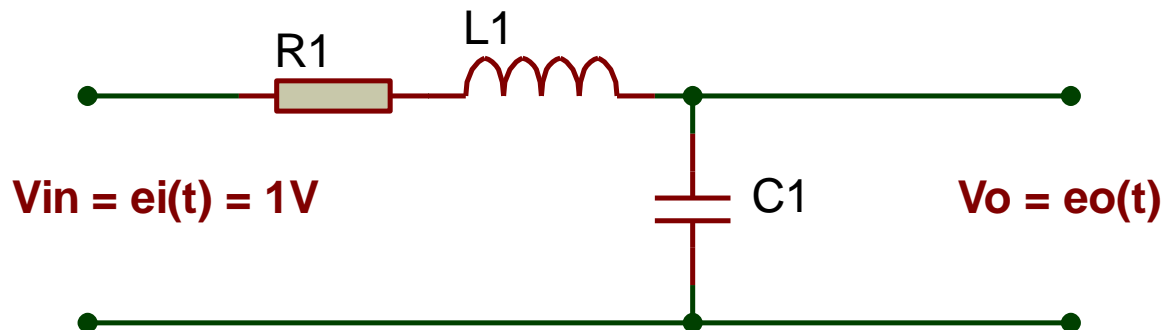
- Un-damped

$$\rho = 0$$

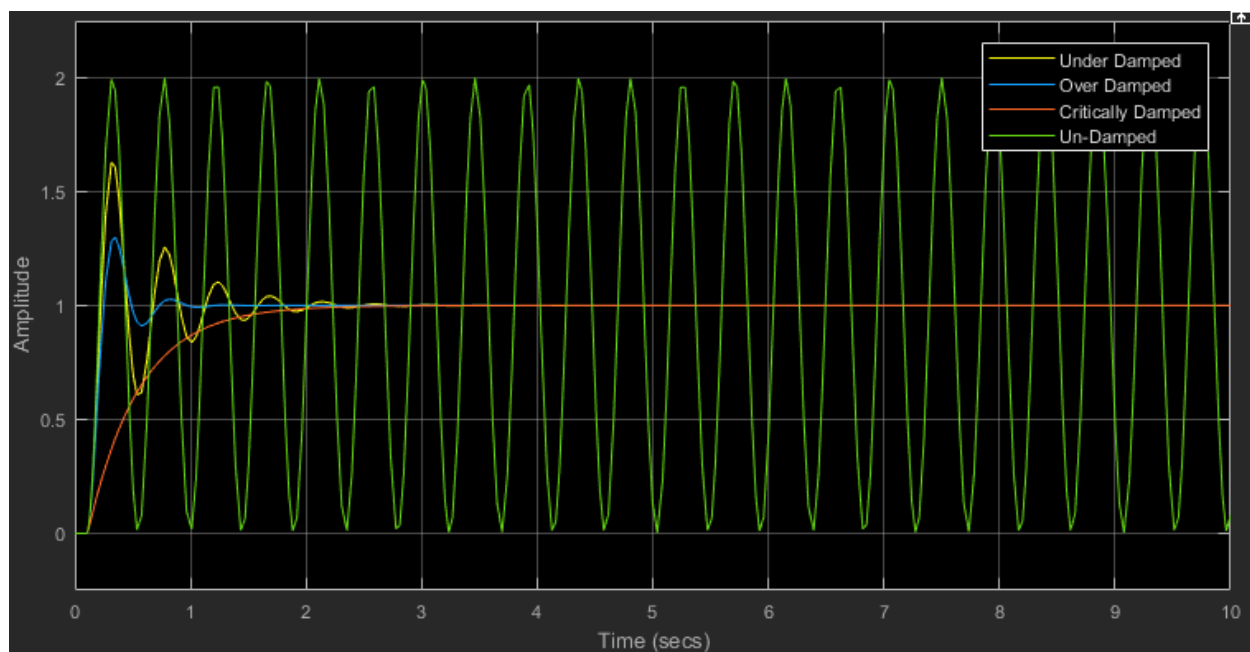
$$R = 0 \text{ (ohm)}; C = 510 \times 10^{-6} \text{ F}; L = 1 \text{ H}; e_i = 1 \text{ volt}$$

Simulation:

Hardware Schematic:



Result:

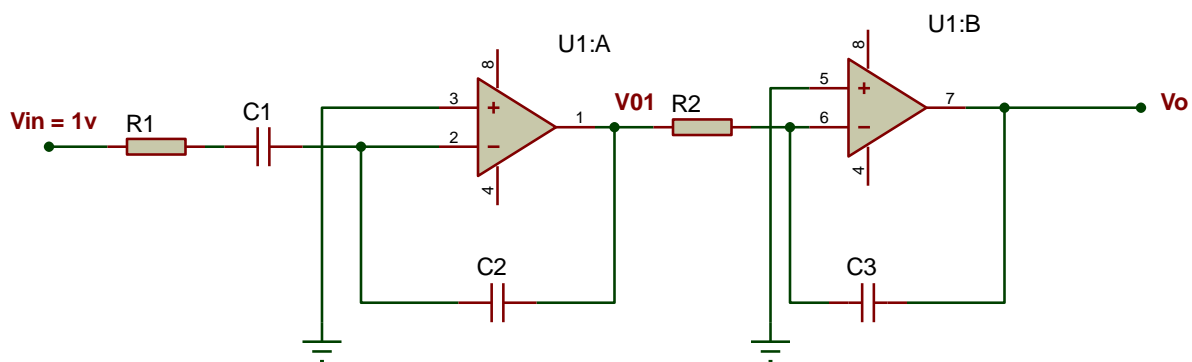


Comments:

- In 1st order system value starts from zero of the graph but in Over damped system value starts after zero of the graph.

Lab # 3**Operational Amplifier****Objectives:**

1. Design the following circuit for maximum OS% = 10%, maximum $T_p = 0.2s$ and maximum $T_s = 0.6s$.

**Theory:****Modeling:**

$$\frac{V_{o1}}{V_{in}} = - \frac{Z_2(s)}{Z_1(s)}$$

$$Z_1(s) = (1/C_1S) + R_1 = (R_1C_1S + 1) / (C_1S)$$

$$Z_2(s) = (1/C_2S)$$

$$\frac{V_{o1}}{V_{in}} = - C_1 / (R_1C_2C_1S + C_2)$$

$$\frac{V_o}{V_{o1}} = - \frac{Z_4(s)}{Z_3(s)}$$

$$\frac{V_o}{V_{o1}} = -1 / (R_2C_3S)$$

$$\frac{V_o}{V_{in}} = ((1 / R_1R_2C_2C_3) / (S^2 + (1 / (R_1C_1))))$$

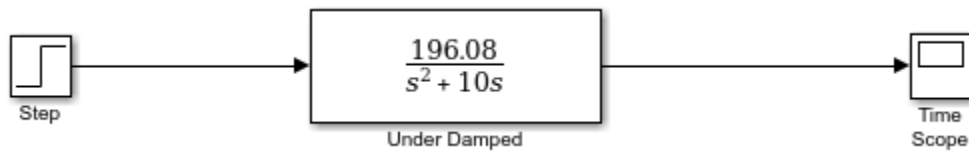
Required:

- Under-damped

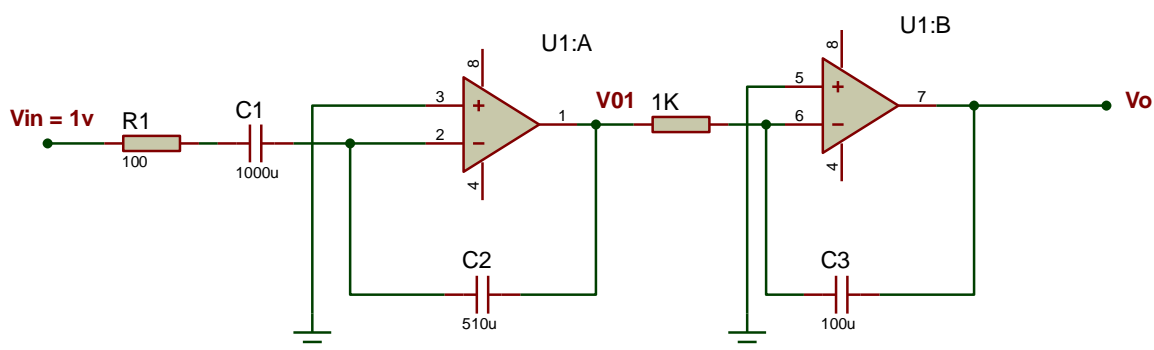
$$0 < \rho < 1$$

$R_1 = 100 \text{ (ohm)}$; $R_2 = 1000 \text{ (ohm)}$; $C_2 = 510 \times 10^{-6} \text{ F}$; $C_3 = 100 \mu\text{F}$; $C_1 = 1000 \mu\text{F}$; $e_i = 1 \text{ volt}$

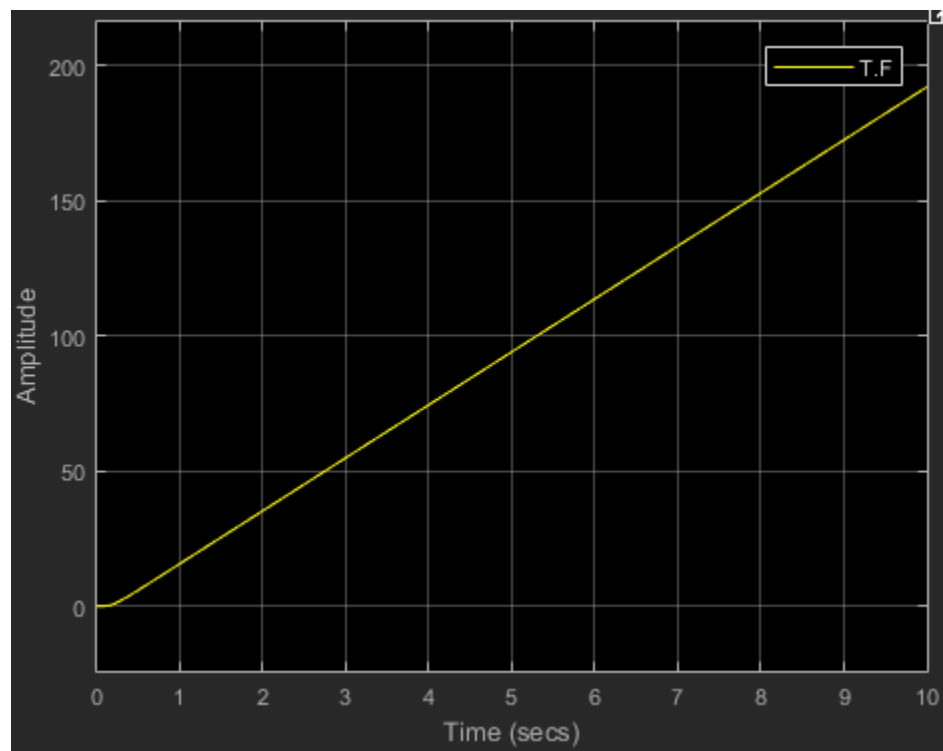
Simulation:



Hardware Schematic:

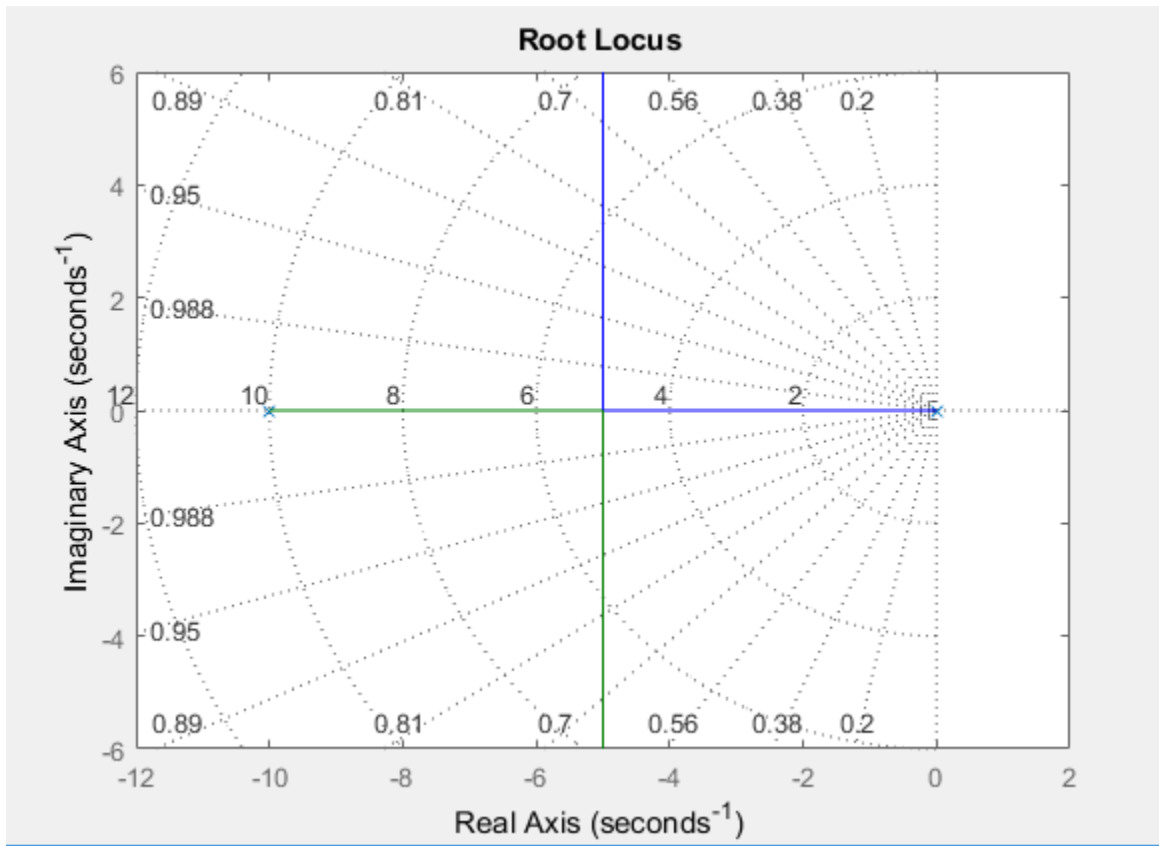


Result:



Comments:

- According to root locus diagram its %OS didn't reached 10%.



Lab # 4

Stability Design via Routh-Hurwitz

Objectives:

1. Find out the range of gain in which system is stable.

$$G(s) = \frac{0.25K(s+0.435)}{s^4 + 3.456s^3 + 3.457s^2 + 0.719s + 0.0416}$$

Theory:

$$\begin{aligned}
 T(s) &= \frac{G(s)}{1+G(s)} \\
 &= \frac{\frac{0.25K(s+0.435)}{s^4 + 3.456s^3 + 3.457s^2 + 0.719s + 0.0416}}{1 + \frac{0.25K(s+0.435)}{s^4 + 3.456s^3 + 3.457s^2 + 0.719s + 0.0416}} \\
 &= \frac{0.25K(s+0.435)}{s^4 + 3.456s^3 + 3.457s^2 + (0.719 + 0.25K)s + (0.0416 + 0.109K)}
 \end{aligned}$$

s^4	1	3.457	$0.0416 + 0.109K_1$
s^3	3.456	$0.719 + 0.25K_1$	
s^2	$11.228 - 0.25K_1$	$0.144 + 0.377K_1$	
s^1	$\frac{-0.0625K_1^2 + 1.324K_1 + 7.575}{11.228 - 0.25K_1}$		
s^0	$0.144 + 0.377K_1$		

From s^2 the value of K , where over-all answer should be in +ve

$$11.228 - 0.25K = 0$$

$$K = 44.91$$

$$-\infty < K < 44.91$$

From s^1 the value of K , where over-all answer should be in +ve

Quadratic equation so, $K = -4.685$ and 25.87

For +ve numerator $-4.685 < K < 25.87$

From s^0 the value of K , where over-all answer should be in +ve

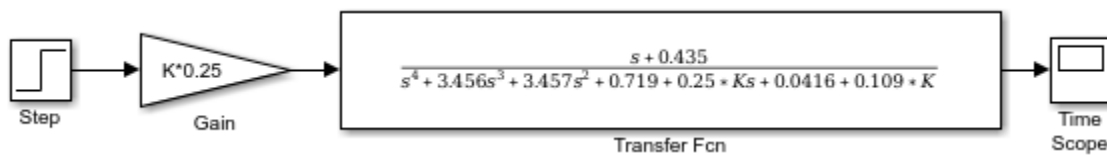
$$0.144 + 0.377K = 0$$

$$K = -0.3819$$

$$-0.3819 < K < \infty$$

Over-all System Stability lies b/w – **0.3819 < K < 25.87**

Simulation:

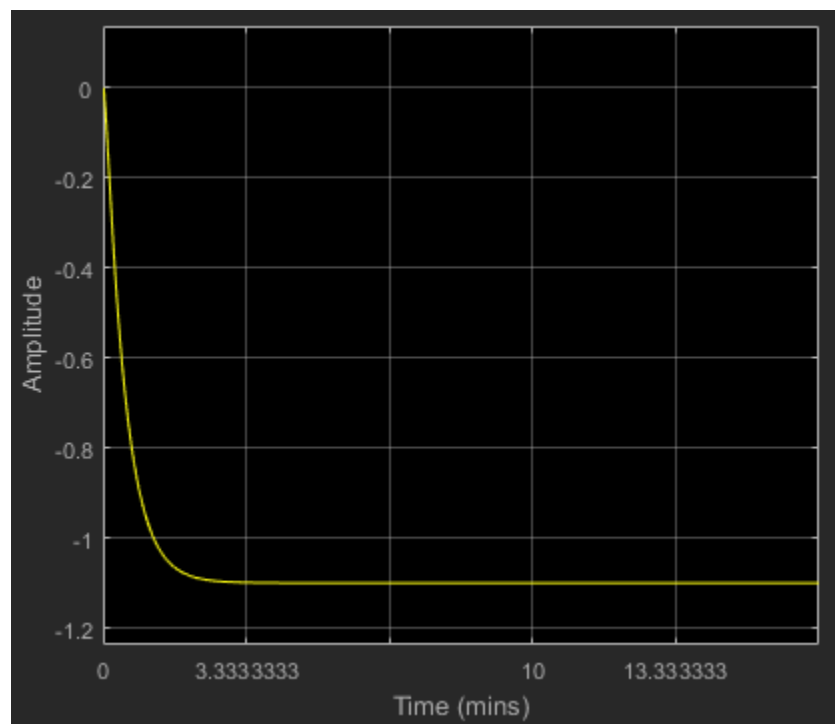


Hardware Schematic:

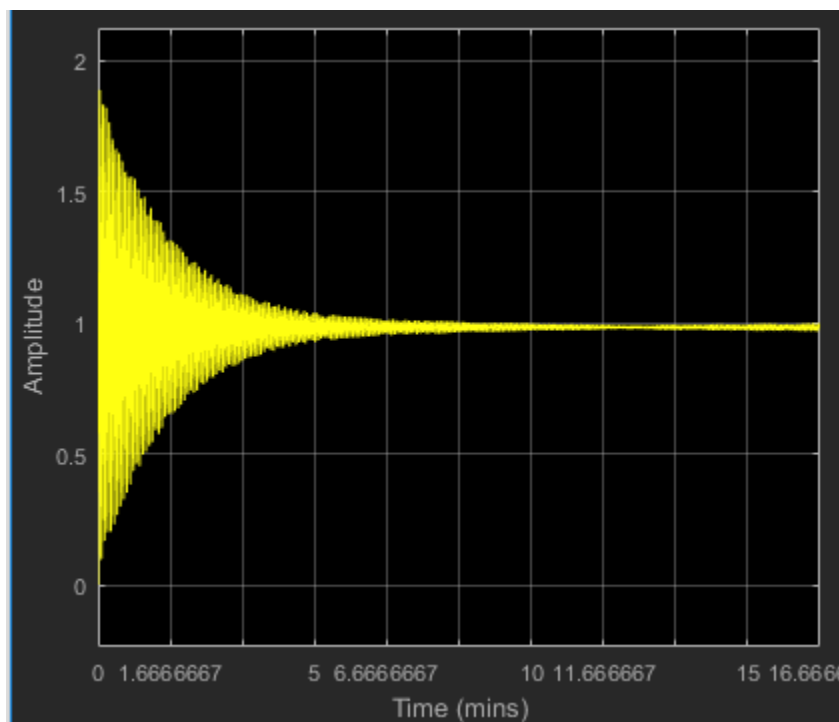
No hardware for this lab.

Result:

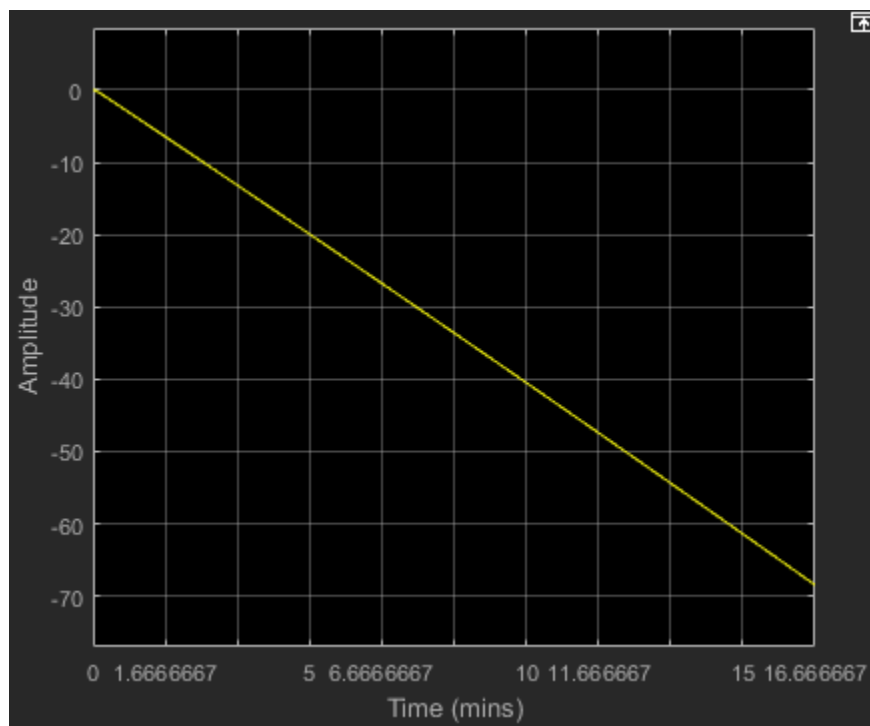
$K = -0.2$:



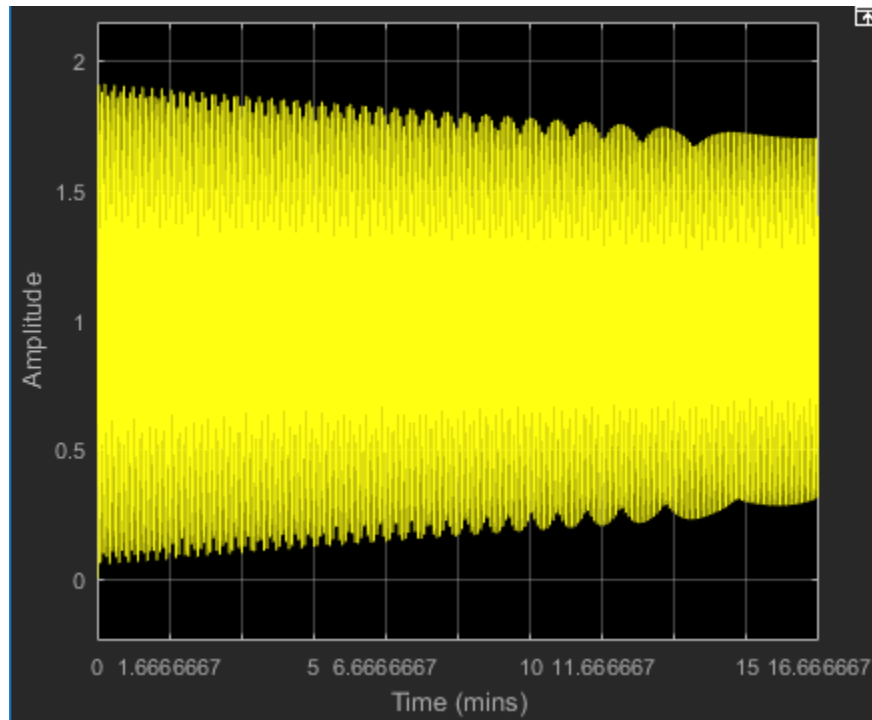
$K = 25$:



$K = -0.382$:



$K = 25.87$:

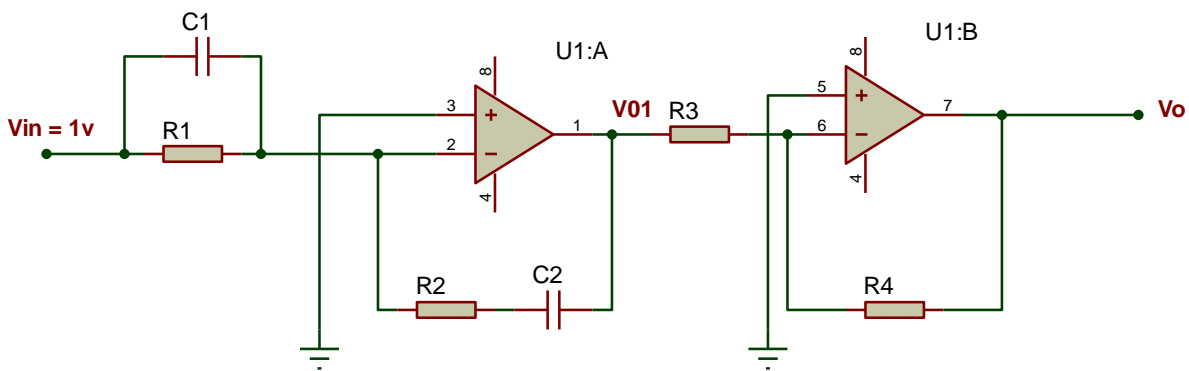


Comments:

- System was stable when K value lie b/w -0.382 to 25.87 .
- When K value is less than or equal to -0.382 and great than or equal to 25.87 then system became unstable.

Lab # 5**Operational Amplifier****Objectives:**

1. Design the following circuit for maximum DC gain =20, $K_p = 5$, $K_i = 0.9$ & $K_d = 1.6$.

**Theory:****Modeling:**

$$\frac{V_{o1}}{V_{in}} = - \frac{Z_2(s)}{Z_1(s)}$$

$$1 / Z_1(s) = C_1 s + 1 / R_1 = (1/C_2 s)$$

$$Z_1(s) = R_1 / (1 + R_1 C_1 s)$$

$$Z_2(s) = (1 + R_2 C_2 s) / C_2 s$$

$$\frac{V_{o1}}{V_{in}} = - (R_1 R_2 C_1 C_2 s^2 + (R_1 C_1 + R_2 C_2) s + 1) / (R_1 C_2 s)$$

$$\frac{V_o}{V_{o1}} = - \frac{Z_4(s)}{Z_3(s)}$$

$$\frac{V_o}{V_{o1}} = -R_4 / R_3$$

$$\frac{V_o}{V_{in}} = (R_1 R_2 R_4 C_1 C_2 s^2 + (R_1 C_1 + R_2 C_2) R_4 s + R_4) / (R_3 R_1 C_2 s)$$

In form of K_p, K_i, K_d

$$T.F = \text{Gain} (K_p + K_i/S + K_dS)$$

$$\text{Dc gain} = R_4$$

$$K_p = (R_1 C_1 + R_2 C_2) / (R_3 R_1 C_2) \quad \text{eq. (a)}$$

$$K_i/S = 1 / (R_3 R_1 C_2 S) \quad \text{eq. (b)}$$

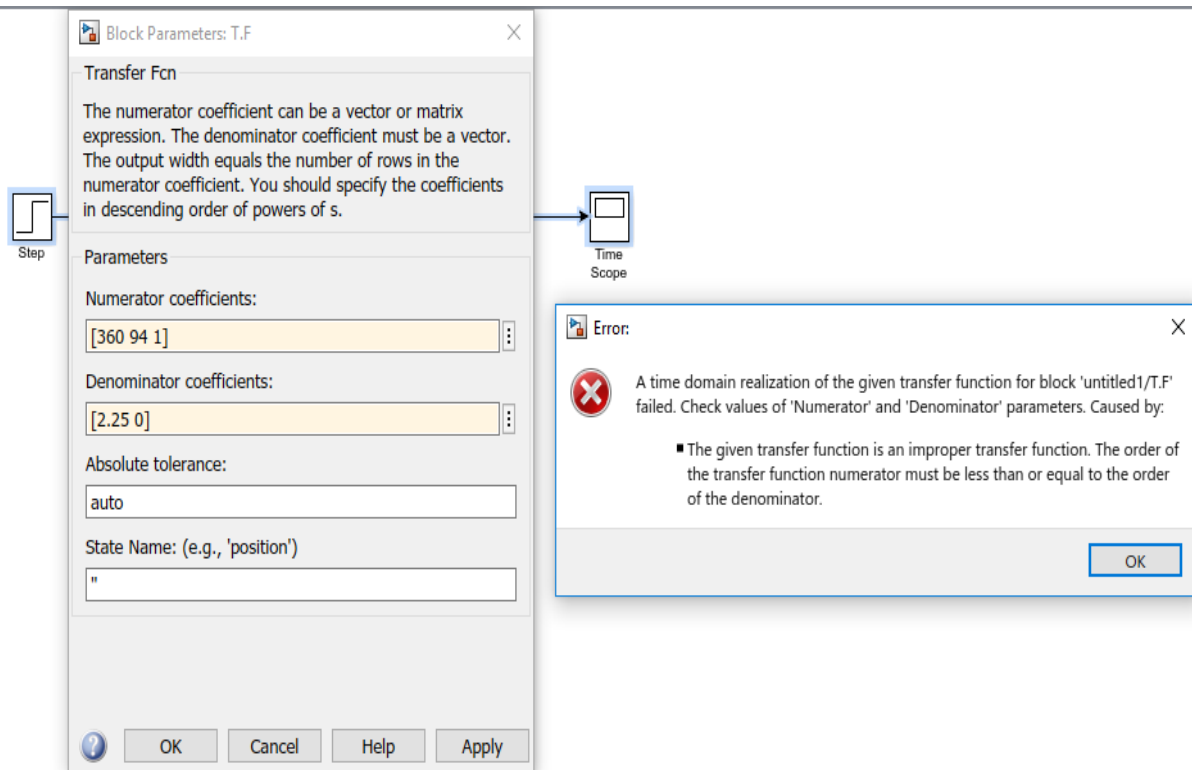
$$K_d S = (R_2 C_1 S) / R_3 \quad \text{eq. (c)}$$

Required:

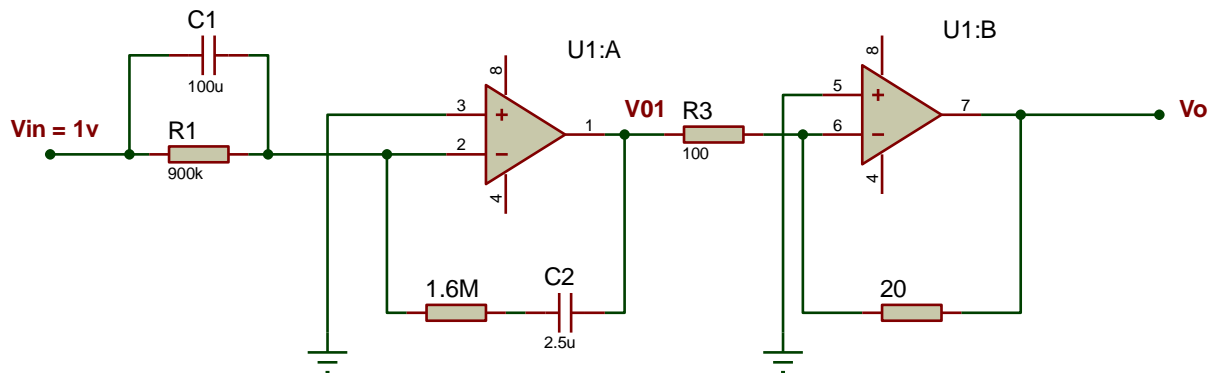
- Dc Gain = 20
- $K_p = 5$
- $K_i = 0.9$
- $K_d = 1.6$

$R_1 = 10k \text{ (ohm)}$; $R_2 = 1.6M \text{ (ohm)}$; $R_3 = 100 \text{ (ohm)}$; $R_4 = 20 \text{ (ohm)}$; $C_1 = 100 \times 10^{-6}F$; $C_2 = 2.5\mu F$; $e_i = 1\text{volt}$

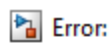
Simulation:



Hardware Schematic:



Result:



A time domain realization of the given transfer function for block 'untitled1/T.F' failed. Check values of 'Numerator' and 'Denominator' parameters. Caused by:

- The given transfer function is an improper transfer function. The order of the transfer function numerator must be less than or equal to the order of the denominator.

OK

Comments:

- According to equation a, b and c different values are required for R_1 , C_2 etc. This logic is wronged.

Lab # 6**Steady-State Error****Objectives:**

- Find the steady-state error for the inputs of $5u(t)$ (Step Input), $5tu(t)$ (Ramp Input).

$$G(s) = \frac{120(s+2)}{(s+3)(s+4)}$$

Theory:**SSE for Step Input:**

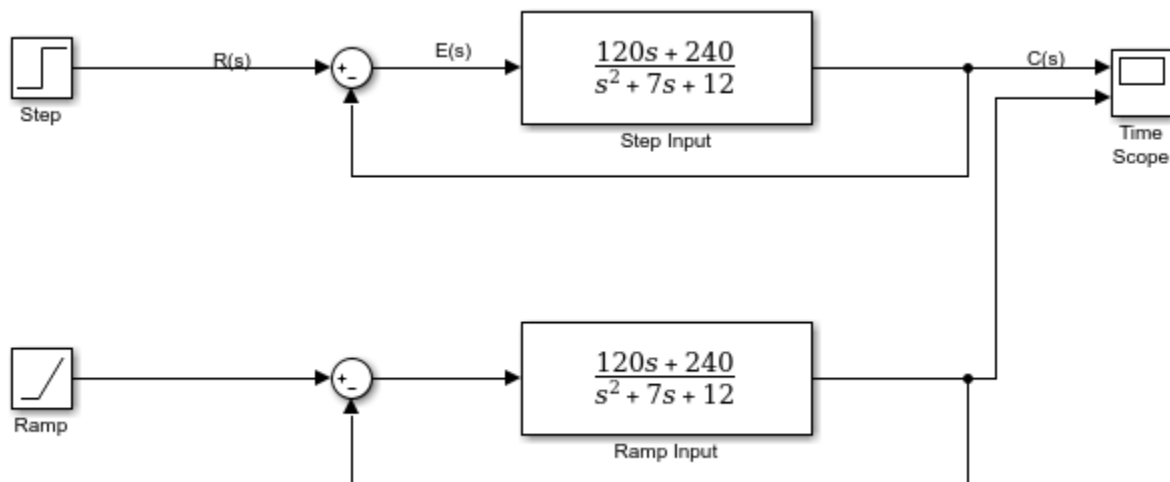
$$e(\infty) = e_{\text{step}}(\infty) = 5 / (1 + \lim_{s \rightarrow 0} G(s))$$

$$e_{\text{step}}(\infty) = e(\infty) = 5/21$$

SSE for Ramp Input:

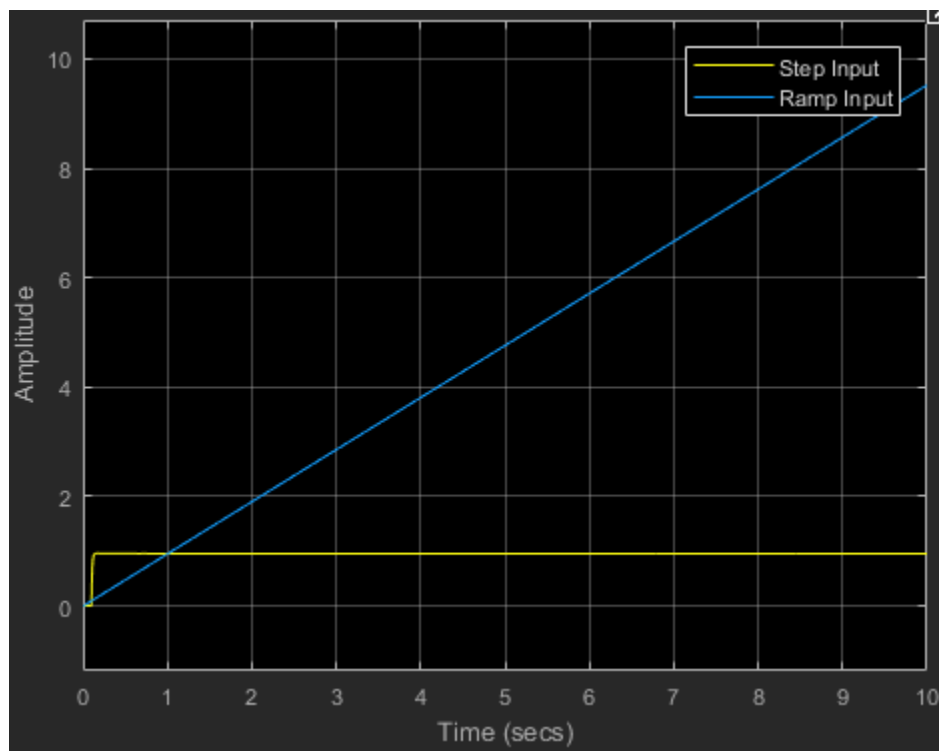
$$e(\infty) = e_{\text{ramp}}(\infty) = 5 / (\lim_{s \rightarrow 0} sG(s))$$

$$e_{\text{step}}(\infty) = e(\infty) = 5/0 = \infty$$

Simulation:**Hardware Schematic:**

No hardware for this lab.

Result:



Comments:

- For ramp Input SSE of T.F approaches to infinity.

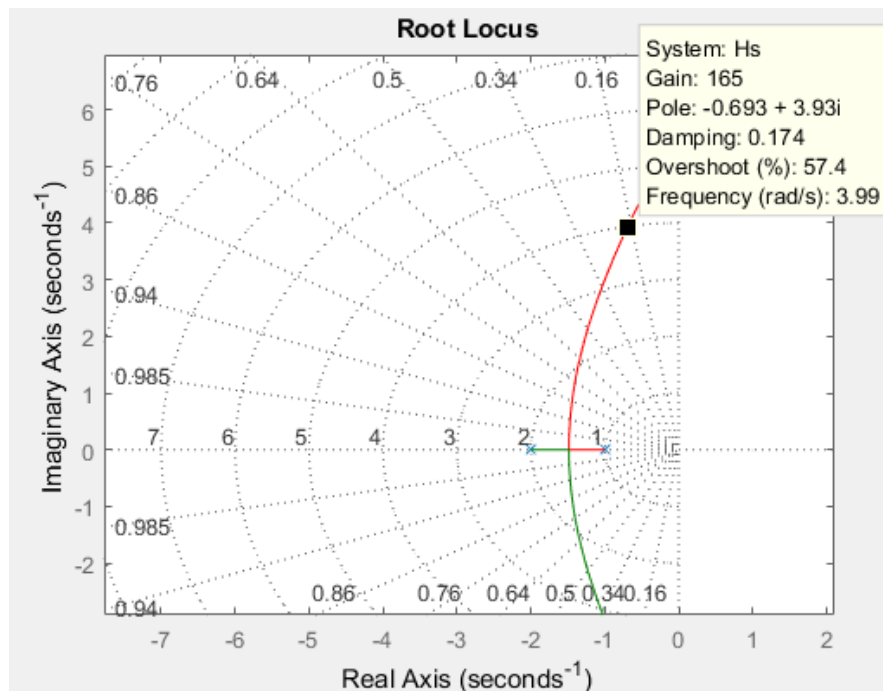
Lab # 7**Design a Lag Compensator****Objectives:**

1. Improve SSE by a factor of 10 if system is operating with damping ratio of 0.174.

$$G(s) = \frac{1}{(s+1)(s+2)(s+10)}$$

Theory:**Root Locus:**

```
>> num=[1];
>> den=[1 13 32 20];
>> Hs=tf(num,den)
>> rlocus(Hs)
```



$$K_p = 165 / ((1)(10)(2))$$

$$K_p = 8.25$$

$$SSE = e(\infty) = 1 / (1 + K_p)$$

$$e(\infty) = 0.108$$

Required SSE:

$$SSE_{req.} = e(\infty) / 10 = 0.0108$$

$$K_p = 91.6$$

Compensator:

$$K_{comp.} / K_{uncomp.} = z_c / p_c = 91.6 / 8.25 = 11.1$$

Let $p_c = 0.001$

$$Z_c = (0.001)(11.1) = 0.0111$$

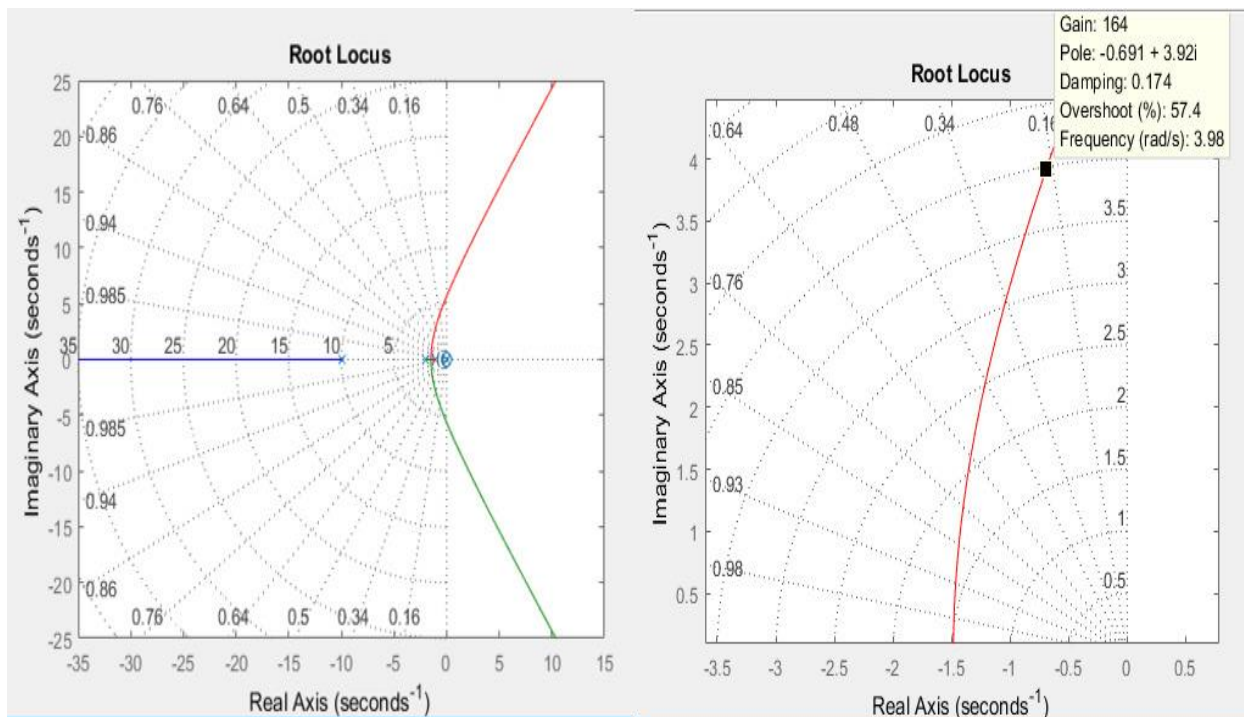
Root Locus:

```
>> num=[1 0.011];
```

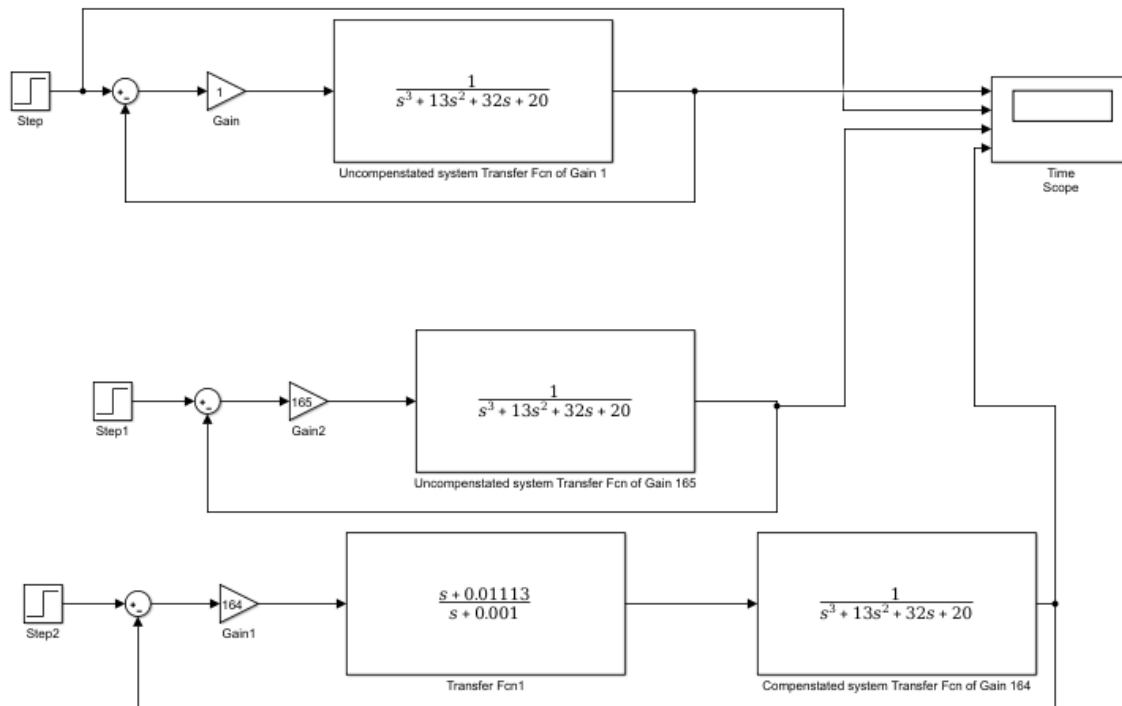
```
>> den=[ 1 13.001 32.013 20.032 0.0200];
```

```
>> Hs=tf(num,den)
```

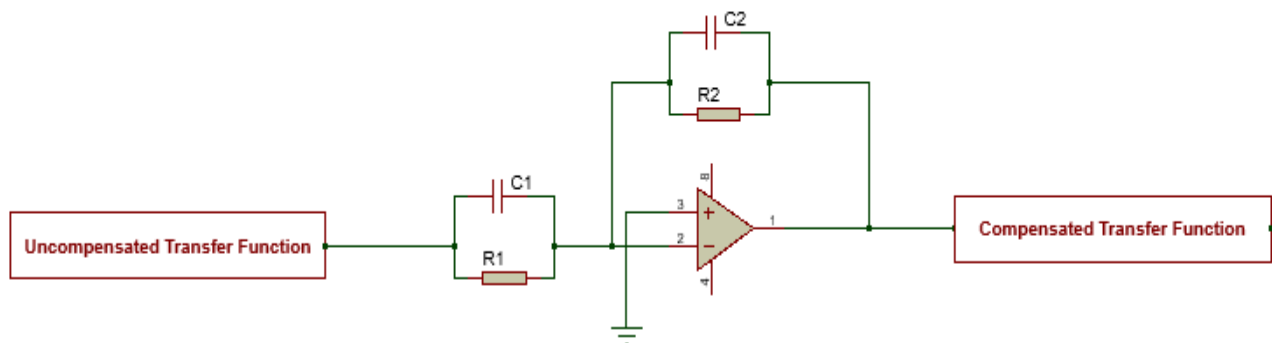
```
>> rlocus(Hs)
```



Simulation:



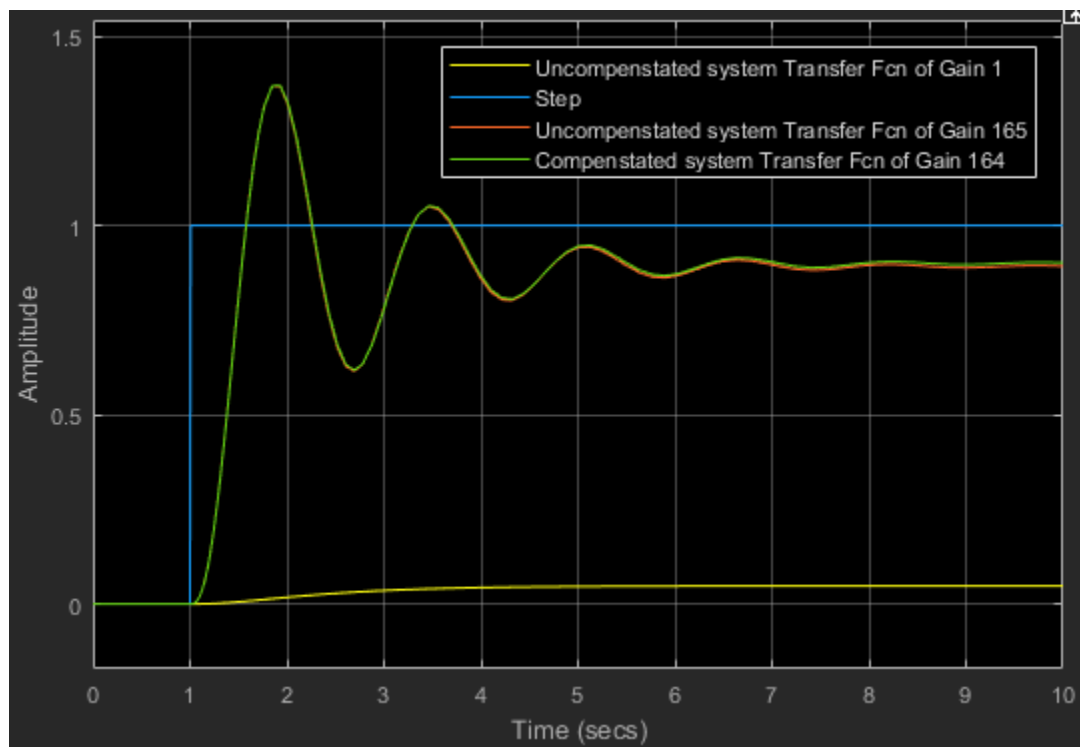
Hardware Schematic:



$$R_1 C_1 < R_2 C_2$$

$$\text{Gain} = K = -C_1 / C_2$$

Result:



Comments:

- Root locus diagram remain unchanged in Lag Compensation.
- Lag compensator didn't effect on transient response of any transfer function.
- It is used to improve SSE.

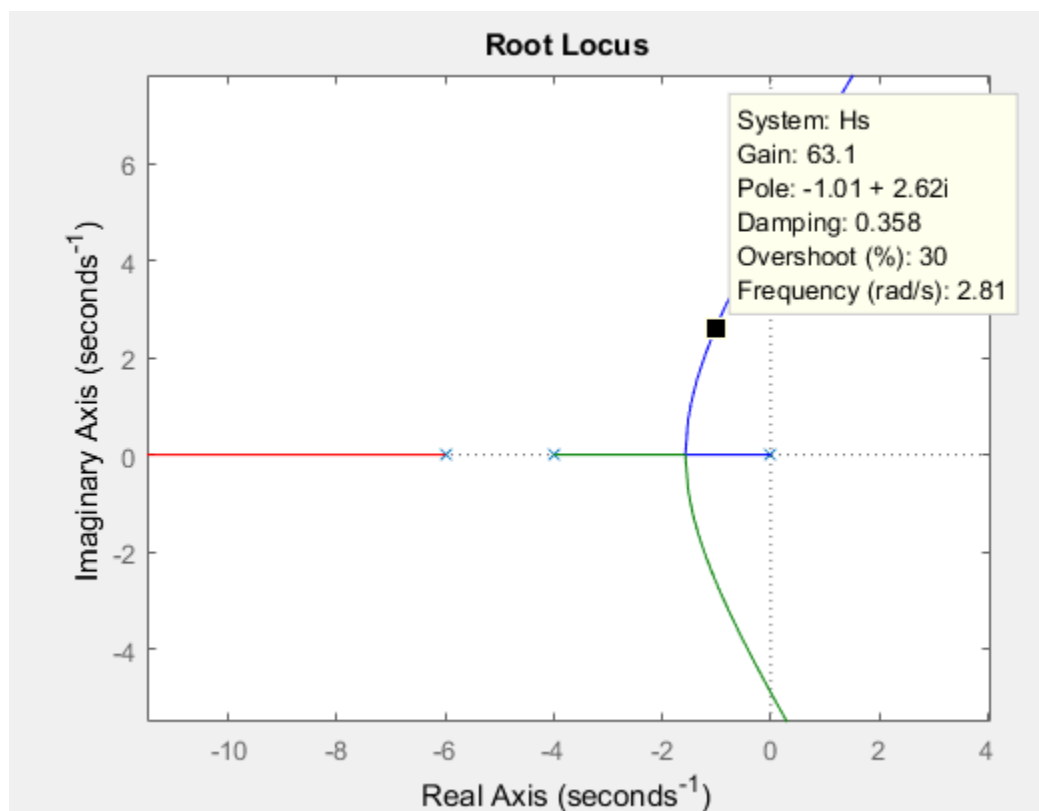
Lab # 8**Design a Lead Compensator****Objectives:**

1. Improve transient response by a factor of 2 if system is operating at 30% overshoot.

$$G(s) = \frac{k}{s(s+4)(s+6)}$$

Theory:**Root Locus:**

```
>> num=[1];  
>> den=[1 10 24 0];  
>> Hs=tf(num,den)  
>> rlocus(Hs)
```



$$\zeta = \cos \theta$$

$$\theta = \cos^{-1}(\zeta)$$

$$\theta = 110.98$$

$$\text{Pole} = -1.01 + 2.62j$$

$$T_s = 4/1.01 = 3.96$$

Required T_s :

$$(\text{Transient Resposne})_{\text{req.}} = T_s / 2 = 1.98$$

$$\text{Real part} = \zeta_d = 2.02$$

$$\text{Img. Part} = -2.02 (\tan (110.98)) = 5.3$$

Compensator:

$$\text{Let } z_c = 5$$

$$p_c = 42.96$$

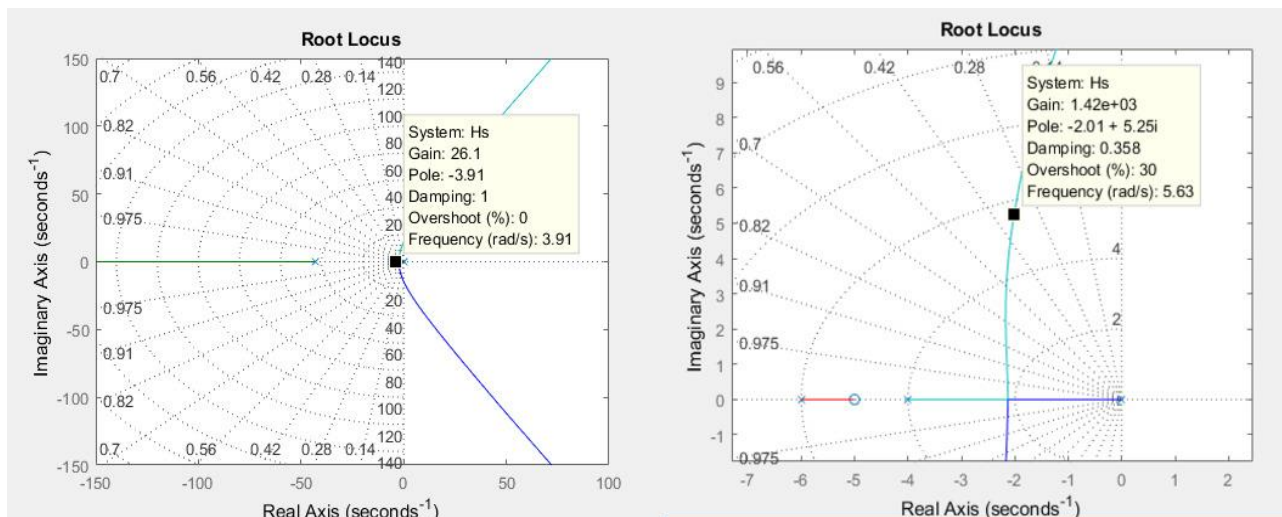
Root Locus:

```
>> num=[1 5];
```

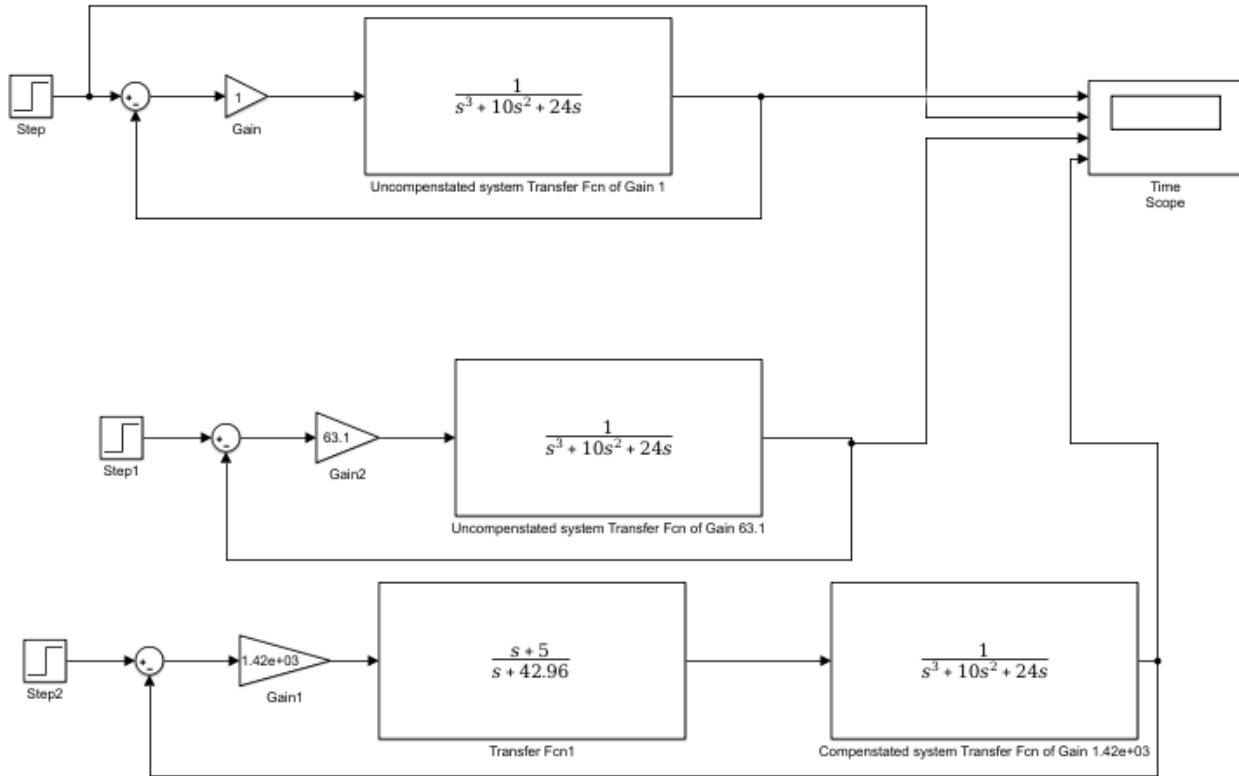
```
>> den=[ 1 52.96 453.6 1031.04 0];
```

```
>> Hs=tf(num,den)
```

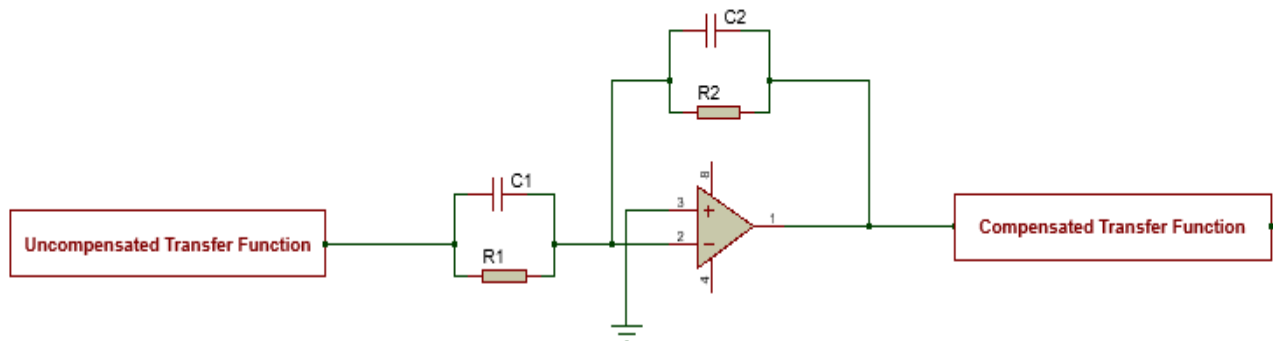
```
>> rlocus(Hs)
```



Simulation:



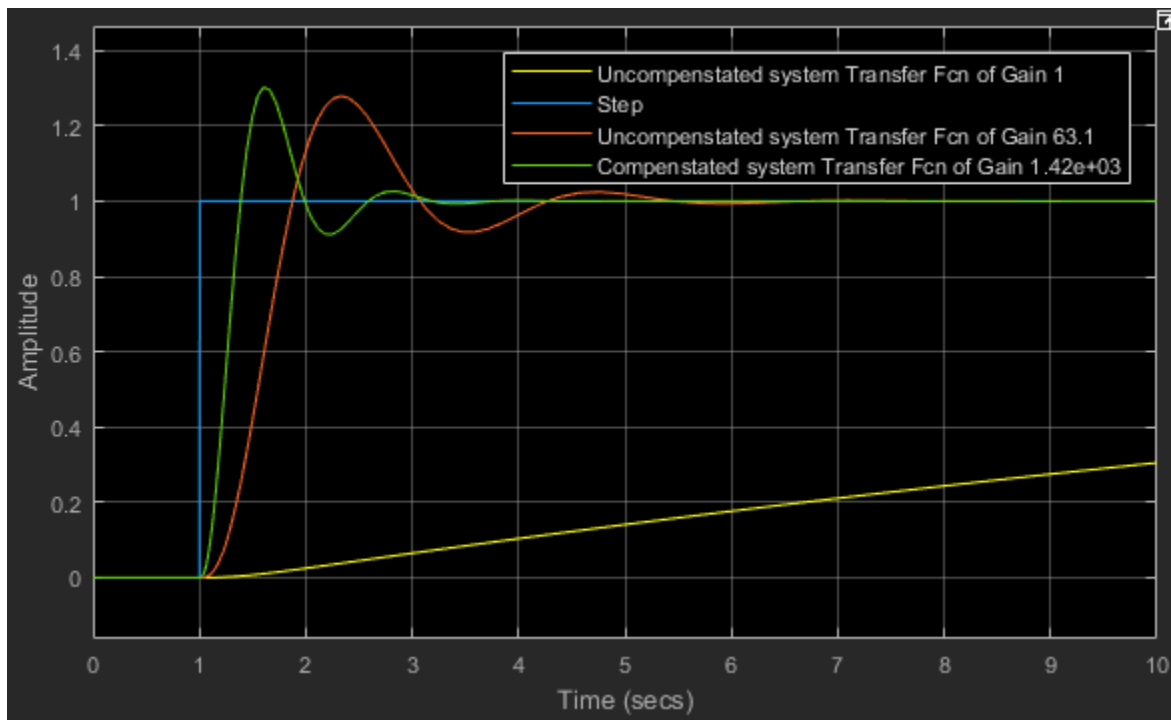
Hardware Schematic:



$$R_1 C_1 > R_2 C_2$$

$$\text{Gain} = K = -C_1 / C_2$$

Result:



Comments:

- Root locus diagram changed in Lead Compensation.
- Lead compensator didn't effect on SSE of any transfer function.
- It is used to improve transient response of any transfer function.

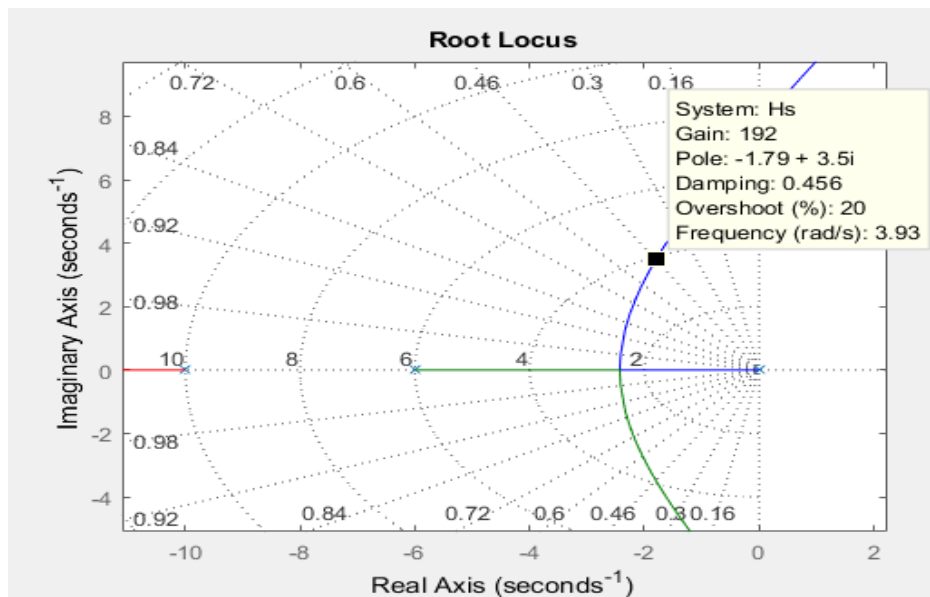
Lab # 9**Design a Lead-Lag Compensator****Objectives:**

1. Improve transient response and SSE by a factor of 2 and 10 respectively if system is operating at 20% overshoot.

$$G(s) = \frac{k}{s(s+10)(s+6)}$$

Theory:**Lead Compensation****Root Locus:**

```
>> num=[1];
>> den=[1 16 60 0];
>> Hs=tf(num,den)
>> rlocus(Hs)
```



$$\zeta = \cos \theta$$

$$\theta = \cos^{-1}(0.456)$$

$$\theta = 62.87$$

$$\text{Pole} = -1.79 + 3.5j$$

$$T_s = 4/1.79 = 2.23$$

Required T_s :

$$(\text{Transient Resposne})_{\text{req.}} = T_s / 2 = 1.117$$

$$\text{Real part} = \zeta_d = 3.58$$

$$\text{Img. Part} = 3.58 (\tan (62.87)) = 6.987$$

$$S = -3.58 + 6.987j$$

Compensator:

Let $z_c = -6$

$$p_c = -29.03$$

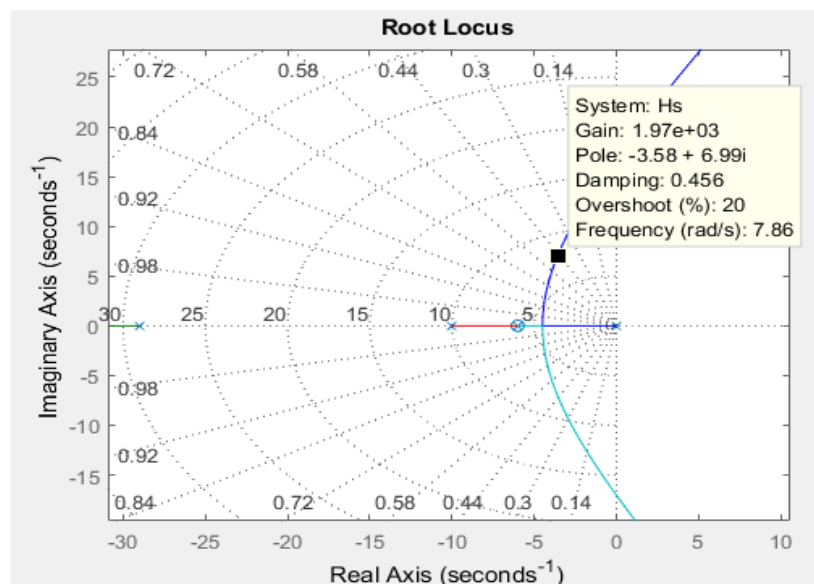
Root Locus:

```
>> num=[1 6];
```

```
>> den=[1 45.03 524.485 1741.8 0];
```

```
>> Hs=tf(num,den)
```

```
>> rlocus(Hs)
```



Lead Compensation

$$SSE = e(\infty) = 1 / K_v$$

$$K_v = 192 / 6(10) = 3.2$$

$$SSE = e(\infty) = 1 / 3.2 = 0.3125$$

Required SSE:

$$SSE_{req.} = e(\infty) / 10 = 0.03125 \text{ (overall)}$$

$$K_v \text{ (lead compensator)} = 1977(6) / ((29.03)(10)(6)) = 6.8$$

$$SSE = e(\infty) = 1/6.8 = 0.147$$

$$\frac{K(lead)}{K(uncomp)} = \frac{6.8}{3.2} = 2.12$$

Compensator:

$$SSE_{req.} = 10 / 2.12 = 4.716 \text{ (After Lead Compensation)}$$

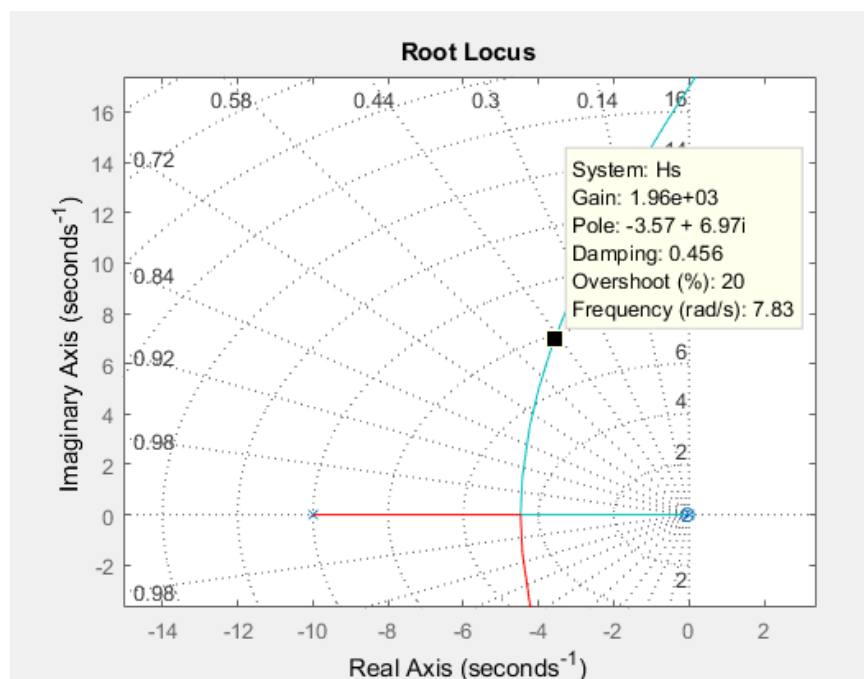
$$z_c / p_c = 4.716$$

Let $p_c = 0.01$

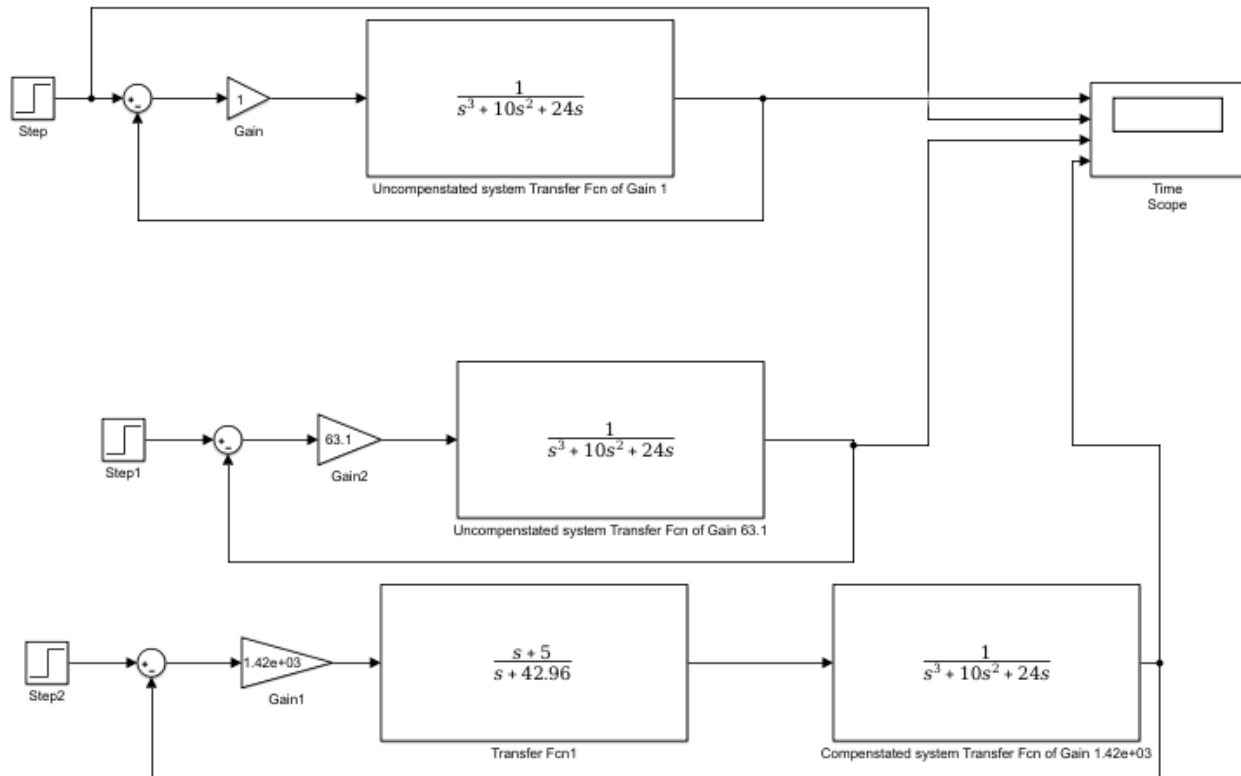
$$z_c = 0.04716$$

Root Locus:

```
>> num=[1 0.04716];
>> den=[1 39.04 290.69 2.903 0];
>> Hs=tf(num,den)
>> rlocus(Hs)
```

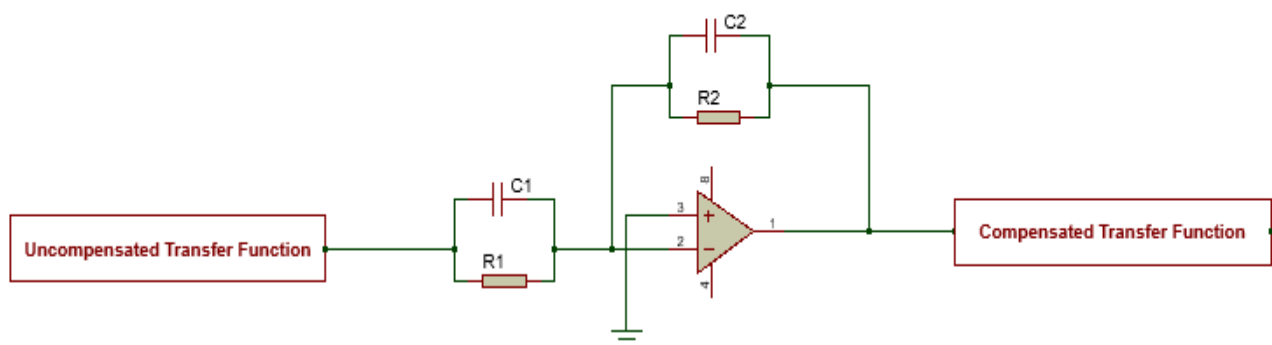


Simulation:



Hardware Schematic:

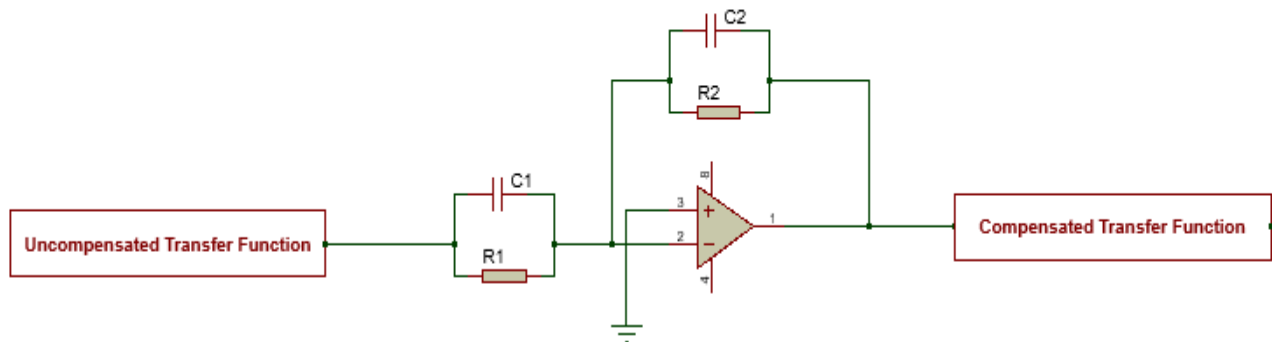
Lead Compensation:



$$R_1 C_1 > R_2 C_2$$

$$\text{Gain} = K = -C_1 / C_2$$

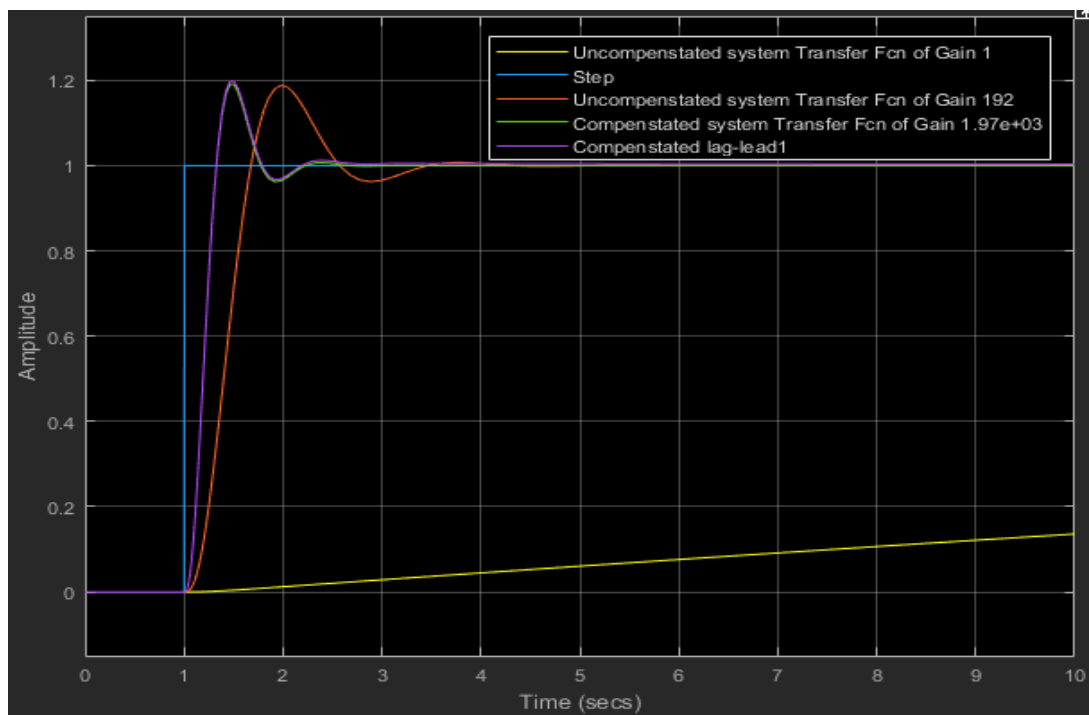
Lag Compensation:



$$R_1 C_1 < R_2 C_2$$

$$\text{Gain} = K = -C_1 / C_2$$

Result:



Comments:

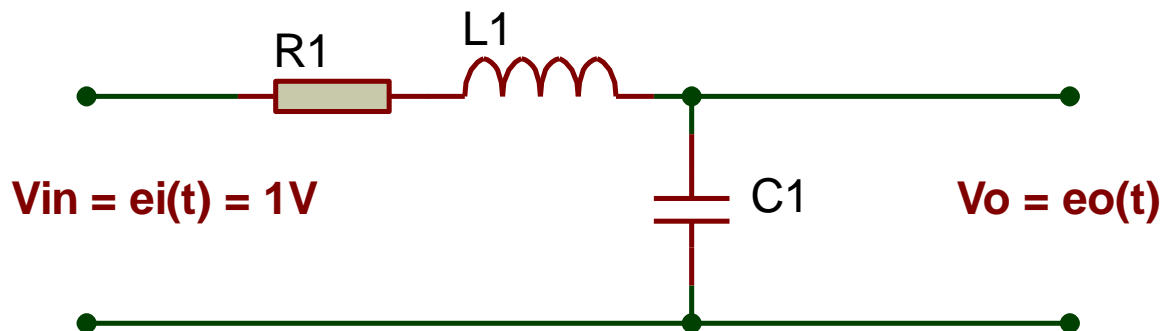
- Root locus diagram changed in Lead Compensation.
- Lead compensator didn't effect on SSE of any transfer function.
- It is used to improve transient response of any transfer function.
- Root locus diagram remain unchanged in Lag Compensation.
- Lag compensator didn't effect on transient response of any transfer function.
- It is used to improve SSE.
- By lead-lag compensation we improved both transient response and SSE.

Lab # 10

PID Controller

Objectives:

1. To model the following circuit and also use the PID controller for Under-Damped system



Theory:

Modeling:

$$L \left(\frac{d^2 q}{dt^2} \right) + R \frac{dq}{dt} + \frac{1}{C} q(t) = e_i(t)$$

$$\diamond q(t) = C e_o(t)$$

$$L C S^2 E_o(s) + R C S E_o(s) + E_o(s) = E_i(s)$$

$$\frac{E_o(s)}{E_i(s)} = \frac{1}{(L C S + R C) S + 1}$$

$$\frac{E_o(s)}{E_i(s)} = \frac{\frac{1}{L C}}{\left(\left(S + \frac{R}{L} \right) S + \frac{1}{L C} \right)}$$

Compare it with General T.F of 2st order equation T.F = $\omega_n^2 / (s^2 + 2\rho\omega_n s + \omega_n^2)$

$$a = R/L = 2\rho\omega_n$$

$$\rho = a/(2\omega_n)$$

$$b = 1/(L C) = \omega_n^2$$

$$0 < \rho < 1$$

$R = 40 \text{ (ohm)}; C = 510 \times 10^{-6} \text{ F}; L = 1 \text{ H}; e_i = 1 \text{ volt}$

$$\rho = 0.452$$

$$\omega_n = 44.28 \text{ rad/s}$$

$$T_p = \frac{\pi}{\omega \sqrt{1-\rho^2}} = 0.0795 \text{ s}$$

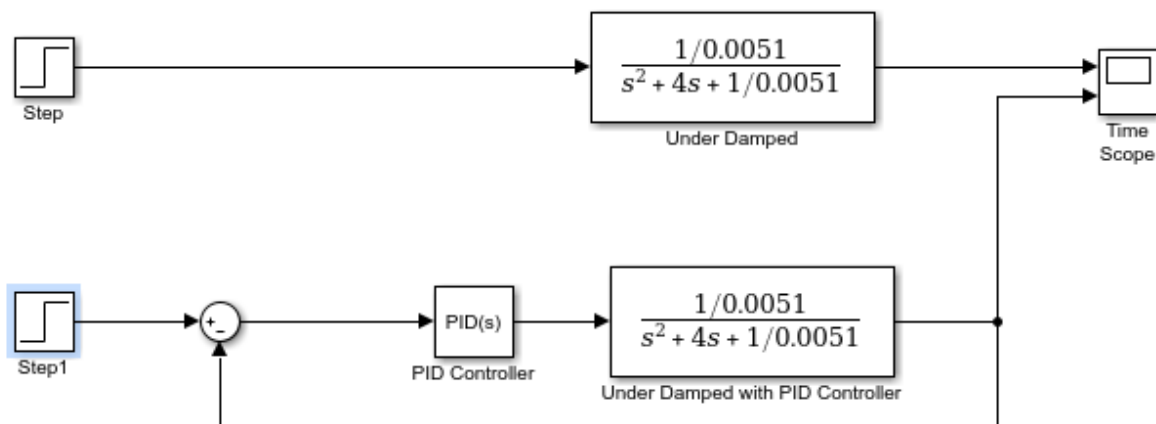
$$\%OS = e^{-\frac{\rho\pi}{\sqrt{1-\rho^2}}} \times 100 = 20.4\%$$

Required:

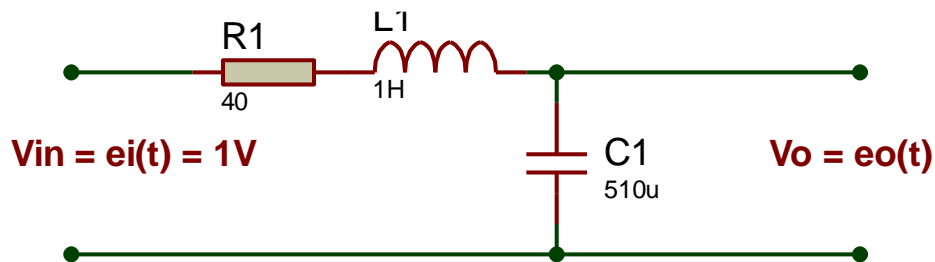
$$T_p = \frac{T_p}{5.3} = 0.015 \text{ s}$$

$$\%OS = e^{-\frac{\rho\pi}{\sqrt{1-\rho^2}}} \times 100 = 20.4\%$$

Simulation:

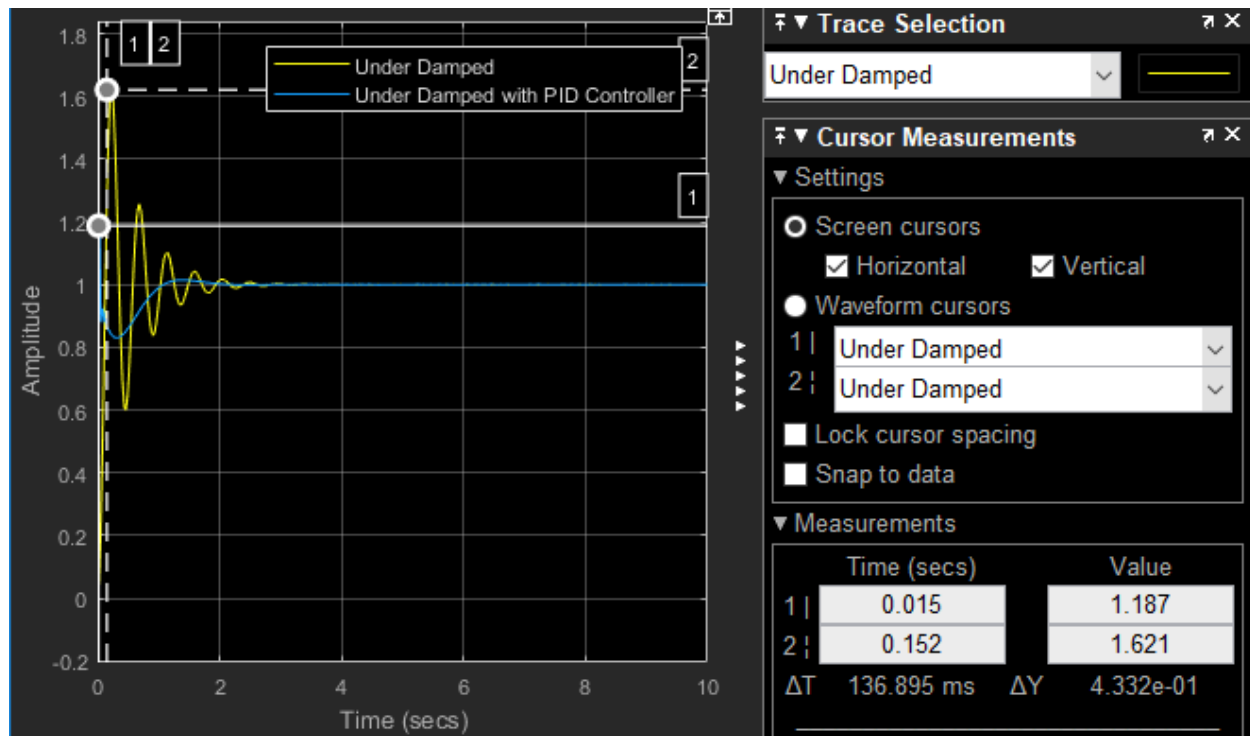


Hardware Schematic:



Result:

at $K_p = 2.3$, $K_i = 10$ & $K_d = 0.7$



Comments:

- By PID controller we can control the transient response as well as SSE, Tr, Ts etc.