

Audio Math

Fundamental Signal RMS Voltage

The RMS voltage at the fundamental frequency is simply the height of the fundamental frequency's bin in the FFT.

V @ Frequency

Signal RMS Voltage

The RMS voltage is calculated one of two ways. For time domain data it's just the RMS definition

$$V_{RMS} = \frac{\sqrt{\left(\sum_{t=0}^T V_t^2\right)}}{n}$$

For bandlimited frequency data it's a bit different since frequencies values are like densities.

$$V_{RMS} = \frac{\sqrt{\left(\sum_{fmin}^{fmax} V_f^2\right)}}{ENBW(windowing)}$$

ENBW is the equivalent noise bandwidth of the fft windowing method. In some ways it's a measure of how much the signal is smeared into adjacent channels. It can be calculated by

$$ENBW = \frac{\sqrt{\left(\sum_{t=0}^T W_t^2\right)}}{\sum_{t=0}^T W_t}$$

Where W_t is the fft weight at time t . Note this is scale-independent of the weights.

Harmonic Distortion

Using the frequency domain results the distortion voltage, in VRMS, of each harmonic is simply the height of the harmonic bin, V @ Harmonic Frequency.

The total harmonic distortion (THD) is the RMS total distortion divided by fundamental.

$$THD = \frac{\sqrt{\left(\sum_{t=2}^N V_{Ft}^2\right)}}{V_F}$$

Currently QA40xPlot uses N=7. Note that distortion spectra are clearly in-phase but the above approximation is good enough.

Intermodulation Distortion

CCIF style math for IMD

When close together fundamentals ($f_H/f_L < 2$) use the 2nd order CCIF2 or 3rd order CCIF3. QA40xPlot uses CCIF3.

CCIF2 uses a single value

$$CCIF2 \text{ IMD} = \frac{V_{f_H-f_L}}{V_{f_H}+V_{f_L}}$$

CCIF3 uses a different single value

$$CCIF3 \text{ IMD} = \frac{\sqrt{V_{f_H-f_L}^2 + (V_{2f_L-f_H} + V_{2f_H-f_L})^2}}{V_{f_H}+V_{f_L}}$$

SMPTE/DIN IMD (or MOD IMD)

When the fundamentals are far apart ($f_H/f_L > 7$) use SMPTE/DIN math

$$SMPTE/DIN \text{ IMD} = \frac{\sqrt{(V_{f_H-f_L} + V_{f_H+f_L})^2 + (V_{f_H-2f_L} + V_{f_H+2f_L})^2}}{V_{f_H}}$$

RMS Power IMD

Finally, when $2 < f_H/f_L < 7$ use IMD RMS power methods using RMS addition

$$POWER \text{ IMD} = \frac{\sqrt{V_{f_H-f_L}^2 + V_{f_H+f_L}^2 + V_{f_L-2f_H}^2 + V_{f_L+2f_H}^2 + V_{f_H-2f_L}^2 + V_{f_H+2f_L}^2}}{\sqrt{V_{f_H}^2 + V_{f_L}^2}}$$

Noise Weighting Curves

From [A-weighting - Wikipedia](#)

The function(f) for C weighting is:

$$W_c(f) = \frac{12194^2 * f^2}{(f^2 + 20.6^2)(f^2 + 12194^2)}$$

Adding two real-axis poles to the C-weighting transfer function gives us A-weighting:

$$W_A(f) = \frac{12194^2 * f^4}{(f^2 + 20.6^2)(f^2 + 1219^2) \sqrt{(f^2 + 107.7^2)(f^2 + 73.9^2)}}$$

And unweighted effectively is

$$W_z(f) = 1.0$$

The weights are normalized to 1.0 at 1KHz.