



IIT ROORKEE



NPTEL ONLINE
CERTIFICATION COURSE

Charging Infrastructure

Lecture-13

Closed Loop Control of Single-phase Boost PFC Converter

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Recap

$$d(t) = 1 - \frac{|V_{s, pk} \sin \omega t|}{V_o}$$

$$L = \frac{V_o}{4 \Delta i_{L, max} f_{sw}}$$

$$C = \frac{P_L}{2\pi f_s \Delta V_o \cdot V_o}$$

→ 2nd line harmonic component

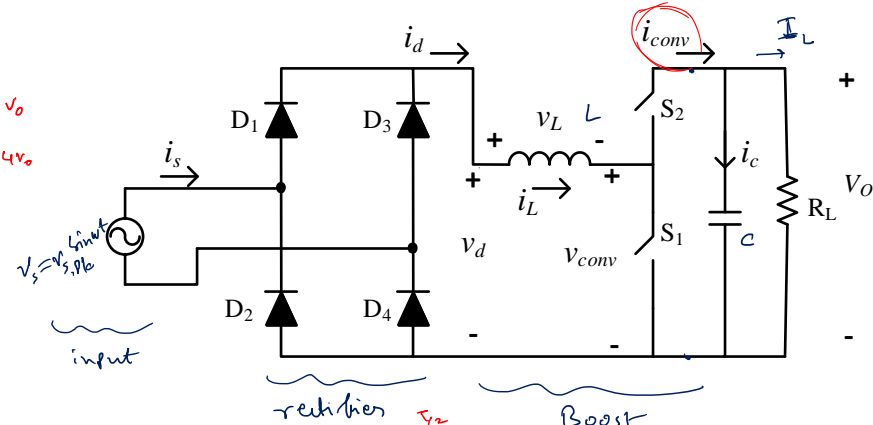
voltage rating of $S_1, S_2 = V_o$

≈ 14V_o

$$P_1, P_2, P_3, P_4 \rightarrow V_{RRM} = V_{s, pk}$$

$$I_{avg} = \frac{I_{s, pk}}{\pi}$$

$$I_{rms} = \frac{I_{s, pk}}{2}$$



$$I_{avg, s2} = \frac{1}{T_{12}} \int_0^{T_{12}} (i_s(t) (1-d(t))) \cdot dt \rightarrow I_{avg, s1} = \frac{1}{T_{12}} \int_0^{T_{12}} (i_s(t) d(t)) \cdot dt$$

$$I_{s1, rms} = \sqrt{\frac{1}{T_{12}} \int_0^{T_{12}} (i_s(t))^2 \cdot d(t) \cdot dt}$$

$$I_{L, rms} = \frac{I_{s, pk}}{\sqrt{2}}$$

$$I_{s, pk} = \frac{2 P_{in}}{V_{s, pk}}$$

$$I_{rms, s2} = \sqrt{\frac{1}{T_{12}} \int_0^{T_{12}} ((i_s(t))^2 \cdot (1-d(t))) \cdot dt}$$

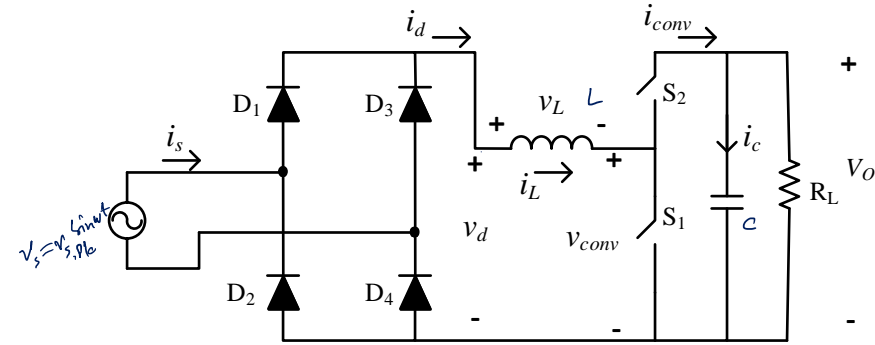
$$I_{rms, c} = \sqrt{I_{rms, conv}^2 - I_L^2}$$

$$I_{rms, conv} = \frac{V_o}{R_L}$$

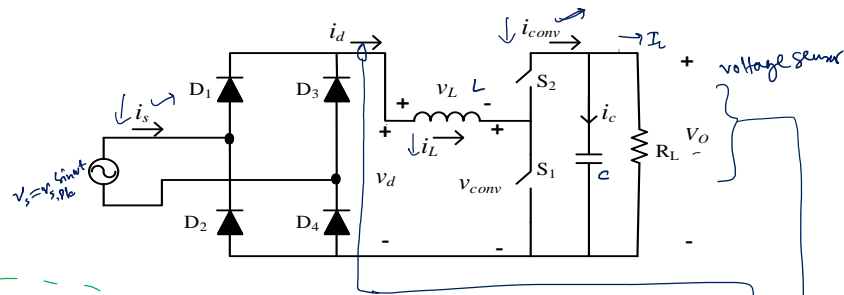
Closed Loop Control

Control objective

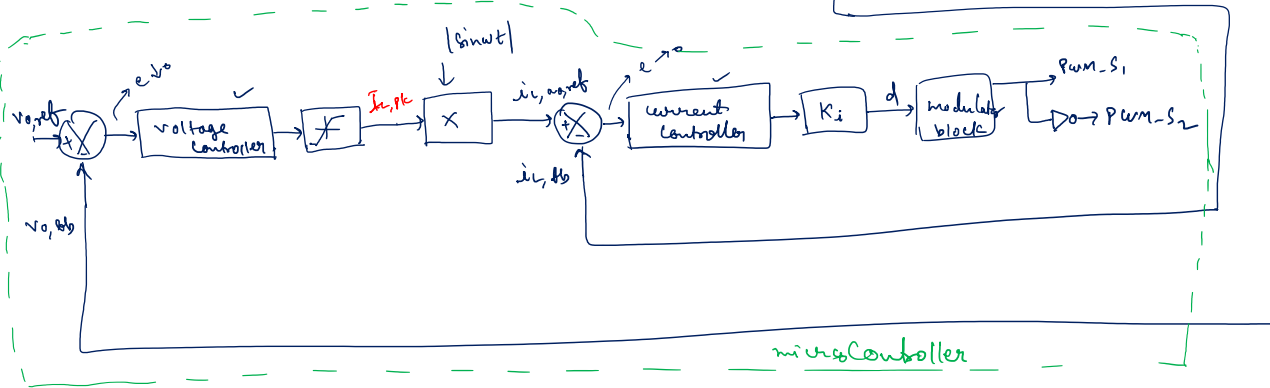
- ① The regulation or controlling of output DC voltage at its desired ($V_o > V_{s, pk}$)
- ② The acb current is being drawn from the input AC source or grid

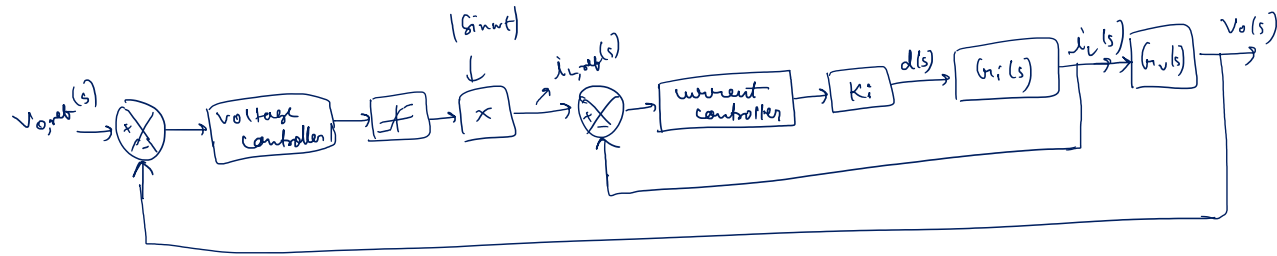


$$T_s = \frac{1}{\omega} \approx \frac{1}{2\pi f_s}$$



$V_o, t_b > V_o, ref \Rightarrow$ the capacitor need to discharge
 $i_{conv} \downarrow \rightarrow i_L \downarrow \rightarrow i_s \downarrow$
 $V_o, t_b < V_o, ref \Rightarrow$ the capacitor need to charge
 $i_{conv} \uparrow \rightarrow i_L \uparrow \rightarrow i_s \uparrow$





$$G_i(s) = \frac{i_L(s)}{d(s)}$$

$$G_v(s) = \frac{V_o(s)}{i_L(s)}$$

$$V_o(s) = V_c(s)$$

Small Signal Model

Average large signal model using state equations

↓
perturbation

↓
linearize the state equation around the operating point

↓
time-domain to s-domain

Thank You

