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Charging Infrastructure

Lecture-26

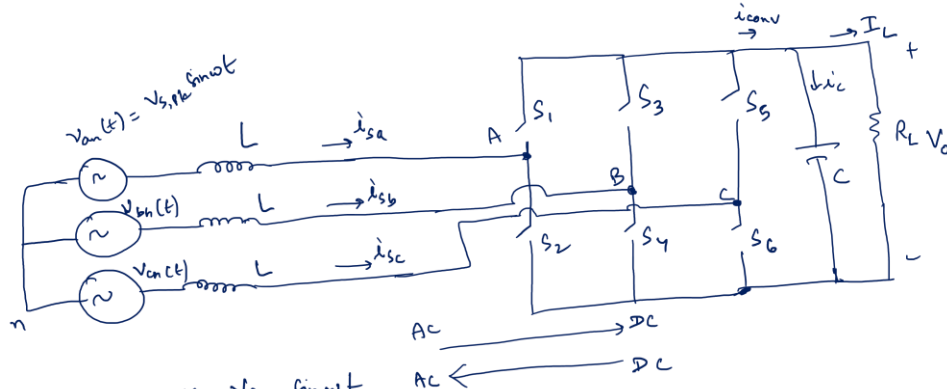
Closed loop control of three-phase AC-DC converter-I

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Recap



$$V_{an}(t) = V_{s,PK} \sin \omega t$$

$$V_{bn}(t) = V_{s,PK} \sin (\omega t - 120^\circ)$$

$$V_{cn}(t) = V_{s,PK} \sin (\omega t - 240^\circ)$$

$$\Rightarrow (\omega L \cdot I_{s,PK}) < 10\% \text{ of } V_{s,PK}$$

Assumed

$$L = \sqrt{\frac{\left(\frac{m V_o}{2}\right)^2 - V_{s,PK}^2}{(2\pi f_s \cdot I_{s,PK})^2}}$$

\Rightarrow the voltage drop across inductor (corresponding to fundamental) must be less than 10% of the $V_{s,PK}$

FEC

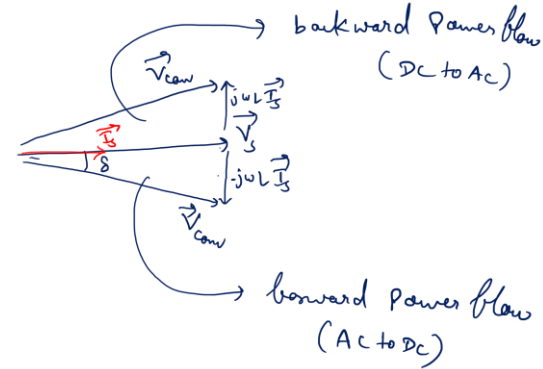
\Rightarrow modulation index $\xrightarrow{\text{designer's choice}}$ (0.8 to 0.9)

$V_{s,PK} \rightarrow$ specification

$V_o \rightarrow$ specification

$f_s \rightarrow$ line frequency given in specification

$$I_{s,PK} \rightarrow \frac{P_L \times \sqrt{2}}{3V_{ph,ns}} \leftarrow \text{assuming no loss in the power converter}$$



Recap

$$C_{min} \geq \frac{\Delta P_{max} T_d}{2 V_o \cdot \Delta V_o}$$

ΔP_{max} → specification
 T_d → designer choice
 ΔV_o → specification
 V_o → specification

there is no 2nd line harmonic voltage ripple on output Capacitance

where ΔP_{max} → maximum power variation of the converter

T_d → response time of closed loop

ΔV_o → the permissible voltage ripple

V_o → output voltage

$$i_{c,ms} = I_{s,plc} \sqrt{\left(\frac{\sqrt{3}}{\pi} m \sin \phi\right)^2 - \frac{9}{16} m^2}$$

$$I_{s,plc} = \frac{\sqrt{2} P_L}{3 V_{ph,ms}} \quad \text{(converter is lossless)}$$

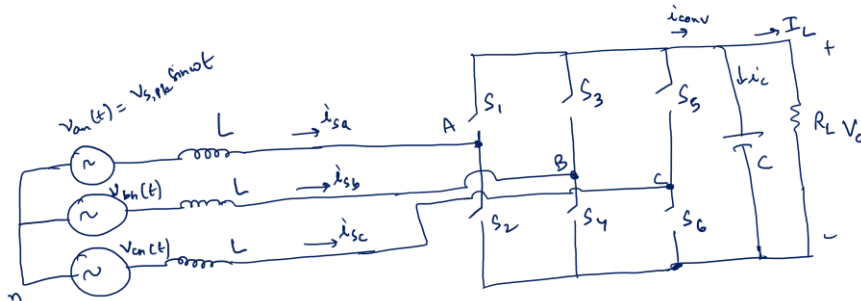
$$I_{s,plc} = \frac{\sqrt{2} P_L}{h \cdot 3 V_{ph,ms}} \quad \left[h \rightarrow \text{efficiency of 3-}\phi \text{ AC-DC Converter} \right]$$

∴ the voltage rating of Capacitance $> V_o + \frac{\Delta V_o}{2}$

Closed Loop Control

Control objectives

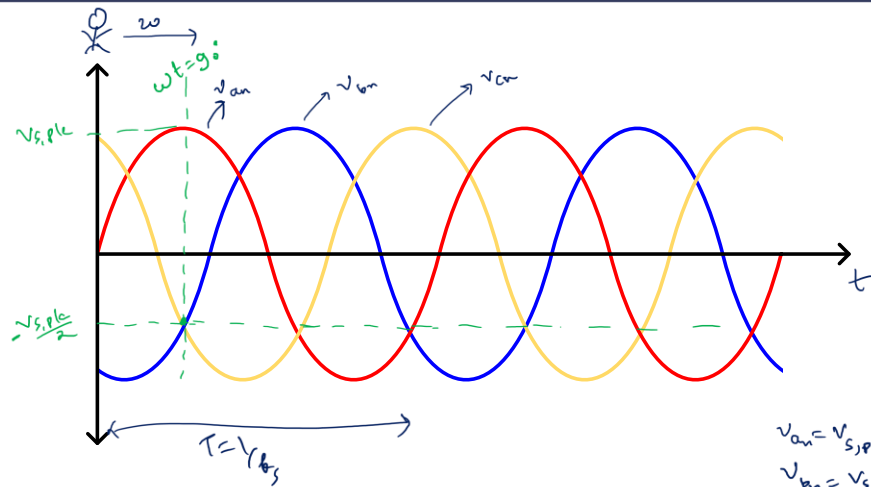
- ① To regulate the output voltage to a desired value. ($> \sqrt{2} V_{L-L}$)
 $\approx 565 \text{ V} \times 1.1$
 $> 625 \text{ V}$
- ② The current drawn should have unity power factor (upf) operation



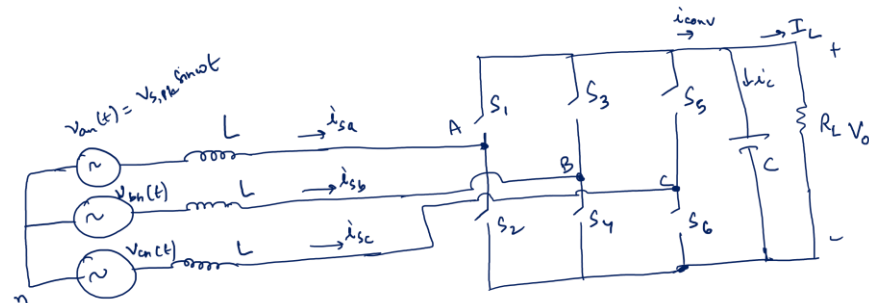
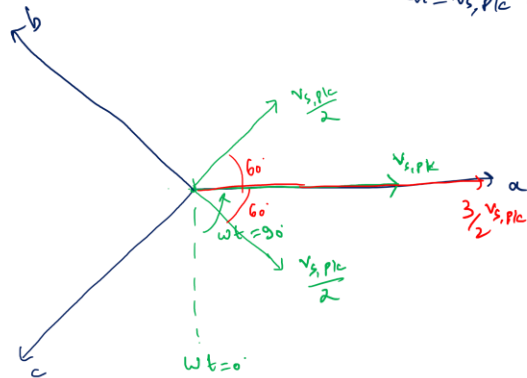
we have balanced three-phase operation,

$$\Rightarrow i_{sa} + i_{sb} + i_{sc} = 0$$

\Rightarrow the three-phase currents are dependent on each other

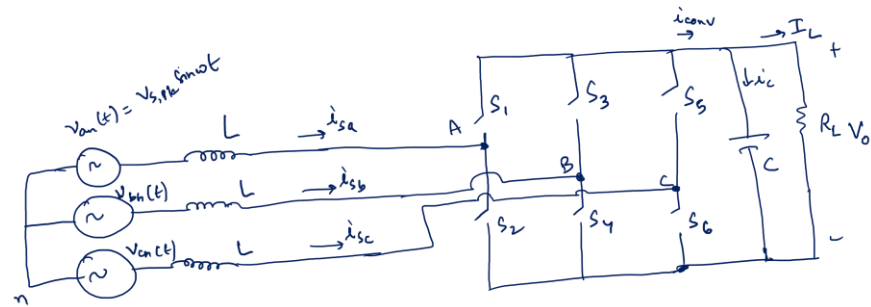
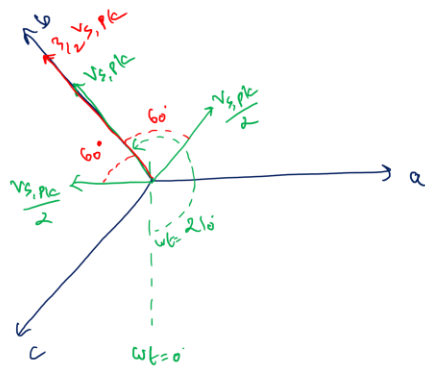
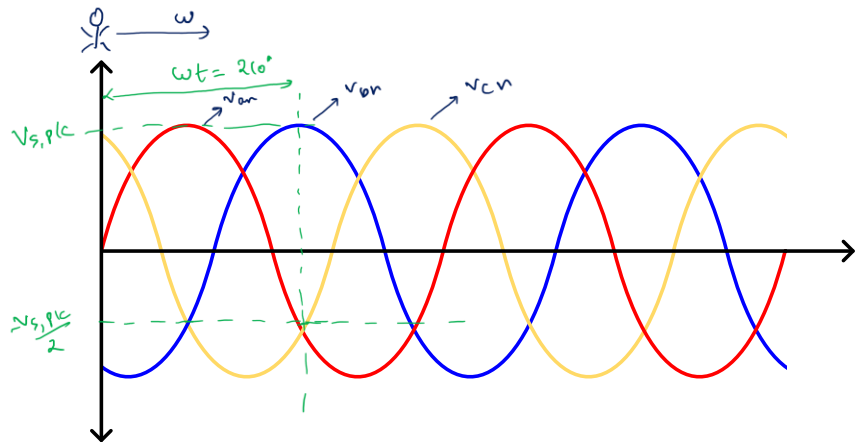


$$\omega = 2\pi f_s = \frac{2\pi}{T}$$



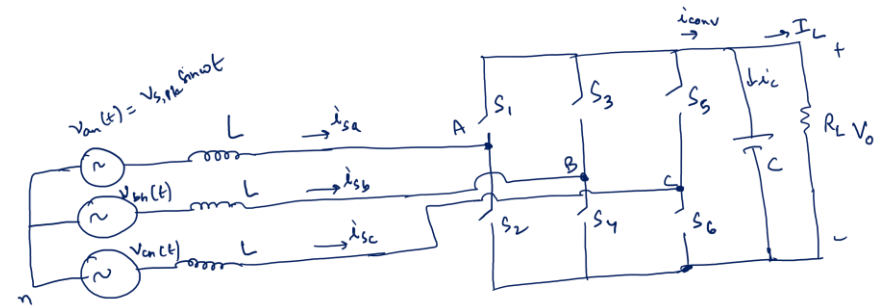
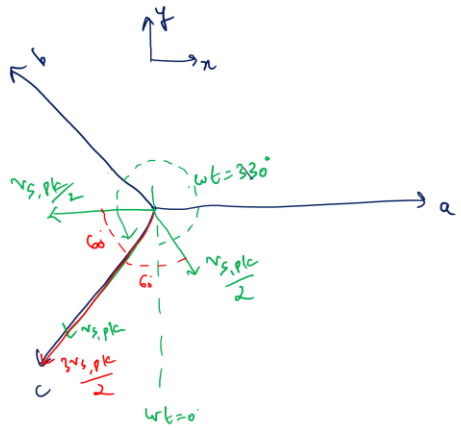
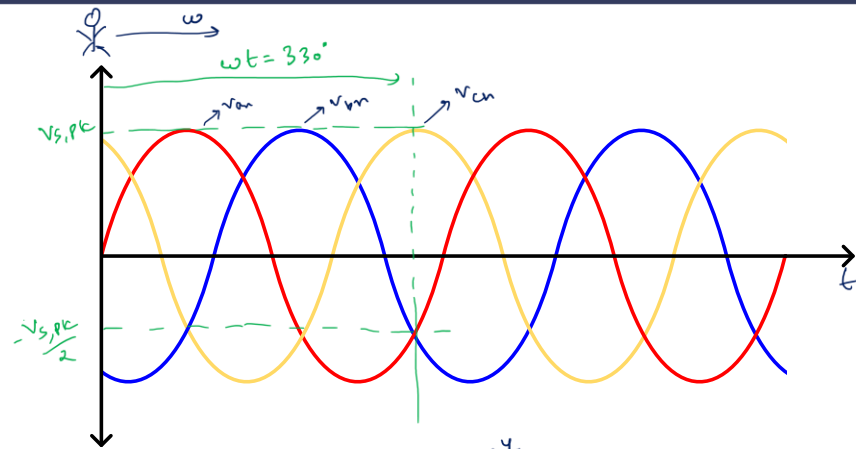
$$\begin{aligned} v_{an} &= V_{s,plc} \sin \omega t \\ v_{bn} &= V_{s,plc} \sin (\omega t - 120^\circ) \\ v_{cn} &= V_{s,plc} \sin (\omega t - 240^\circ) \end{aligned}$$

$$V_{s,resultant} = V_{s,plc} + \frac{V_{s,plc}}{2} \cos 60^\circ + \frac{V_{s,plc}}{2} \cos 60^\circ = \frac{3}{2} V_{s,plc}$$



$$V_{s, \text{resultant}} = V_{s, pk} + \frac{V_{s, pk}}{2} \cos 60^\circ + \frac{V_{s, pk}}{2} \cos 60^\circ$$

$$= \frac{3}{2} V_{s, pk}$$

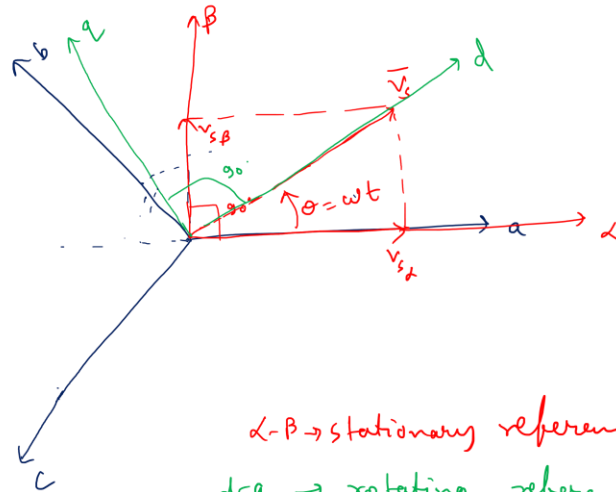


$$\Rightarrow V_{s, \text{resultant}} = V_{s, \text{pk}} + \frac{V_{s, \text{pk}}}{2} \cos 60^\circ + \frac{V_{s, \text{pk}}}{2} \cos 60^\circ$$

$$= \frac{3}{2} V_{s, \text{pk}}$$

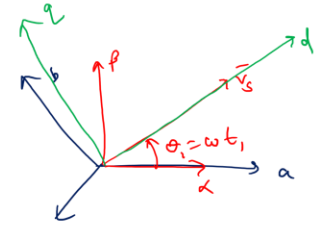
The resultant is a vector quantity, whose magnitude = $\frac{3}{2} V_{s,plc}$ and it is rotating with the speed = ω ($\omega = 2\pi f_s$)

⇒ the vector is rotating in a 2-D space, in order to obtain the independent component of vector, the representative axis has to be 90° apart from each other



$$V_{s\alpha}, V_{s\beta}$$

$$\text{at } \theta_0 = 0$$



$\alpha-\beta \rightarrow$ stationary reference frame

$d-q \rightarrow$ rotating reference frame

at one instant 't'

$a, b, c \rightarrow$ sampled quantity

$$\Rightarrow \alpha = a - \frac{b}{2} - \frac{c}{2} \Rightarrow \alpha = \frac{3a}{2}$$

$$\beta = a \cos 90^\circ + b \cos 30^\circ - c \cos 30^\circ \Rightarrow \beta = \frac{\sqrt{3}}{2} b - \frac{\sqrt{3}}{2} c$$

$$\Rightarrow d = \alpha \cos \theta + \beta \sin \theta$$

$$q = -\alpha \sin \theta + \beta \cos \theta$$

Thank You

