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systems at equilibrium are poised to undergo reversible change

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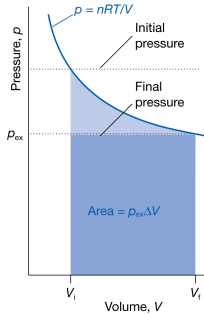
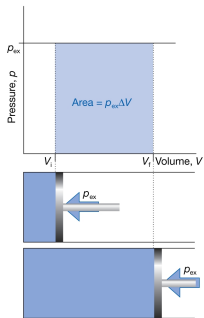
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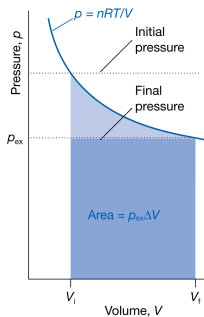
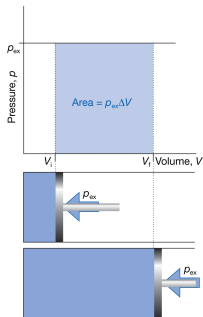
Such a system is **not** in mechanical equilibrium

Calculating work :



For a perfect gas, reversible work of expansion =

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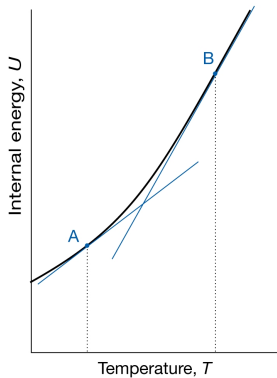
For a perfect gas, reversible work of expansion =

$$\begin{aligned}
 - \int_{V_i}^{V_f} p_{\text{ext}} dV &= - \int_{V_i}^{V_f} p dV \\
 &= -nRT \ln \frac{V_f}{V_i}
 \end{aligned}$$

for spontaneous expansion :

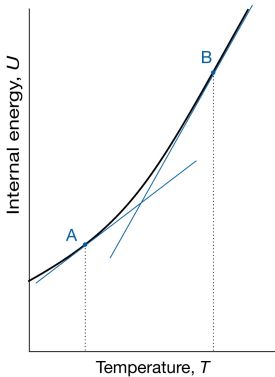
$$\text{work} = -p_{\text{ext}} (V_f - V_i)$$

Internal energy (U) as a function of temperature : $U(V, T)$



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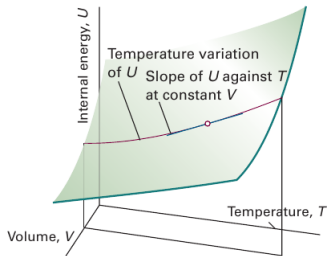


internal energy of a system
increases as temperature is raised
slope of tangent at any
temperature = heat capacity, C

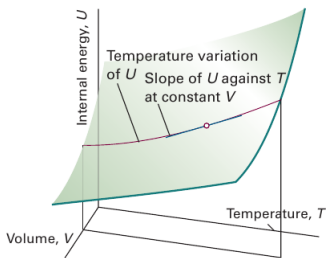
in the Fig.,

$$C \text{ at A} < C \text{ at B}$$

$$U(V, T)$$

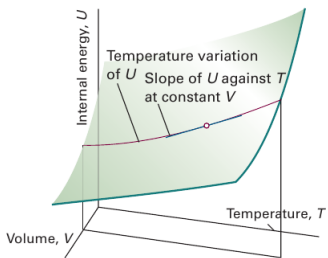


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$$C_V = \left(\frac{dq}{dT} \right)_V = \left(\frac{\partial U}{\partial T} \right)_V$$

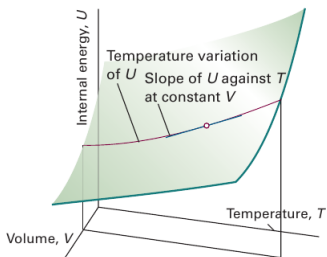
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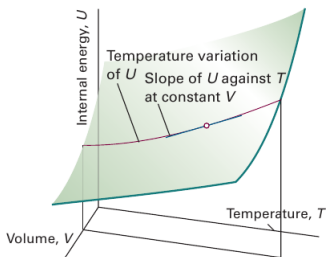


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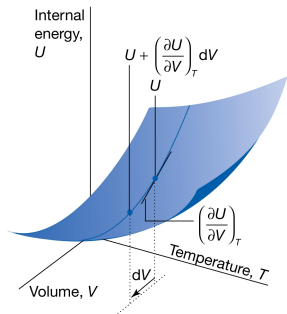
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then $\Delta U = C_V \Delta T$

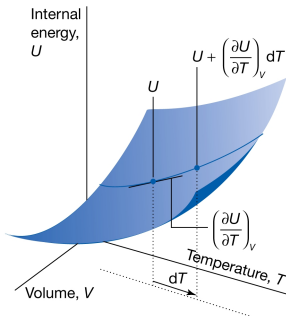
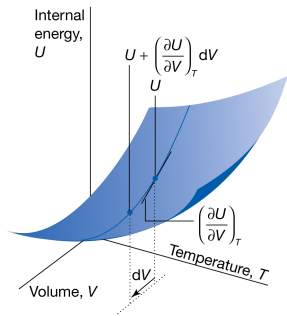
for $f \equiv f(x, y)$

$$df = \left(\frac{\partial f}{\partial x}\right)_y dx + \left(\frac{\partial f}{\partial y}\right)_x dy$$



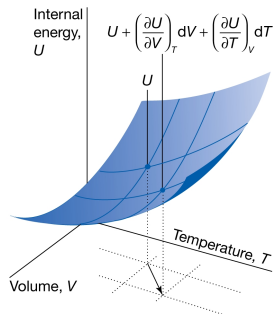
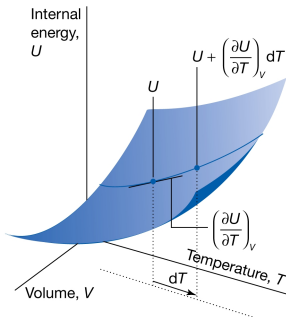
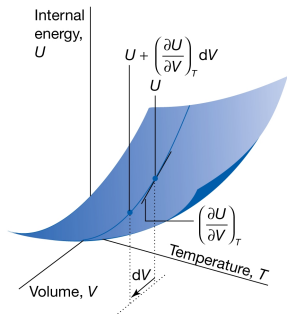
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e.g., for CO_2 , $U_m(T) = U_m(0) + \frac{3}{2}RT + RT + \dots$

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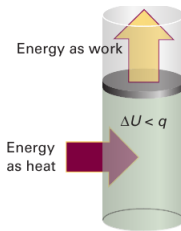
⇒ internal energy of a perfect gas is independent of the volume it occupies

$$\left(\frac{\partial U}{\partial V}\right)_T = 0$$

Enthalpy

$\Delta \text{energy} \neq$ energy transferred as heat
when system is free to change its volume

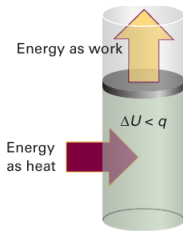
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def. $H = U + pV$, a state function

$$dH = d(U + pV) = dU + pdV + Vdp = dq + Vdp \implies dq_p = dH$$

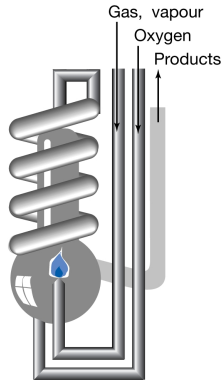
$$\text{def. } c_p = \left(\frac{dq}{dT} \right)_p = \left(\frac{\partial H}{\partial T} \right)_p \implies dH = C_p dT$$

$$\overbrace{\int_i^f dH}^{H_f - H_i} = \overbrace{\int_i^f dq_p}^{q_p}$$

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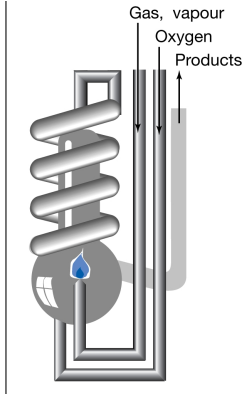


$$\underbrace{H_f - H_i}_f = \underbrace{q_p}_f$$

$$\int_i^f dH = \int_i^f dq_p$$

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Combustion occurs as a known amount of reactant is passed through to fuel the flame, and the rise of temperature is monitored.

solved problem :

when 1.0 mol CaCO_3 as calcite converts to aragonite, $\Delta U = 0.21 \text{ kJ}$

Calculate $\Delta H - \Delta U$ when $p = 1 \text{ bar}$ given densities of solids : 2.71 g cm^{-3} and 2.93 g cm^{-3} respectively

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\blacktriangleright usually justifiable to ignore $\Delta H - \Delta U$ for condensed phases, except at very high pressures, when pV is no longer negligible

Ex. Calculate $\Delta H - \Delta U$ when 1.0 mol Sn(s, grey) of density 5.75 g cm^{-3} changes to Sn(s, white) of density 7.31 g cm^{-3} at 10.0 bar. At 298 K, $\Delta H = 2.1 \text{ kJ}$

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$$\blacktriangleright \therefore \Delta H - \Delta U = -0.44 \text{ J } (\approx 0.2\% \text{ of } \Delta U)$$

enthalpy of a perfect gas:

$$H = U + pV = U + nRT \quad \Rightarrow \quad \Delta H = \Delta U + \Delta nRT$$

solved problem :

Water is heated to boiling under $p = 1.0$ atm. When an electric current of 0.50 A from a 12 V supply is passed for 300 s through a resistance in thermal contact with it,

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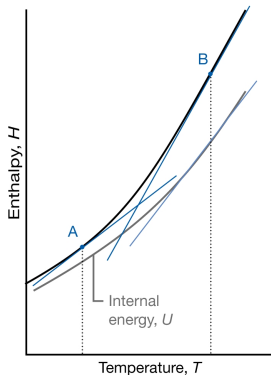
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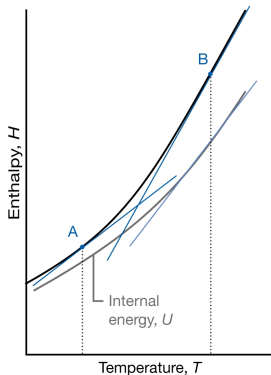
Notice $\Delta U_m < \Delta H_m$ because energy has been used to drive back surrounding atmosphere to make room for vapour

Enthalpy (H) as a function of temperature :



internal energy and enthalpy of system increase as temperature is raised

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at constant pressure, slope of tangent at any temperature = heat capacity, C_p

For gases, at a given temperature the slope is steeper than that of internal energy versus temperature

$$C_{p,m} > C_{v,m}$$

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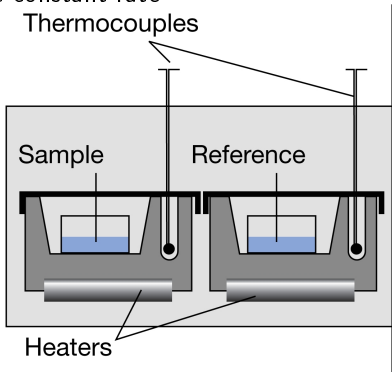
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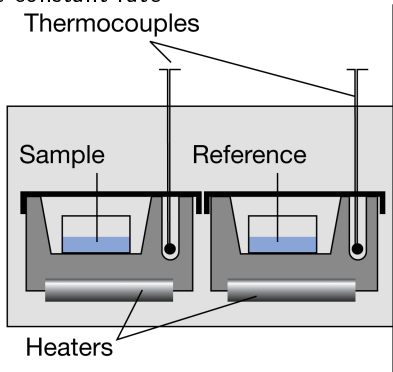
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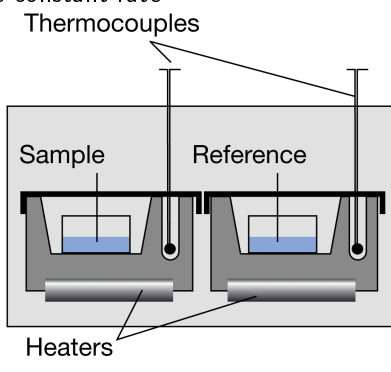


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 α = temperature scan rate (in Ks^{-1})

A computer controls electrical power to maintain same temperature in sample and reference compartments

sample temperature changes significantly relative to that of reference material if transfer of energy as heat occurs in the sample during the scan

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To maintain same temperature in both compartments, excess energy is transferred as heat to or from sample during the process

an endothermic process lowers sample temperature relative to that of reference
and, as a result, the sample must be heated more strongly than reference in order
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heat transferred to sample, $q_p = C_p \Delta T$

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$\therefore C_{p, ex} = \frac{q_{p, ex}}{\Delta T} = \frac{q_{p, ex}}{\alpha t} = \frac{P_{ex}}{\alpha}$; P_{ex} = excess electrical power necessary to equalize the temperature of sample and reference compartments

DSC trace - a thermogram : plot
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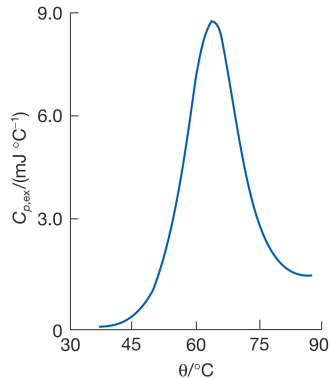
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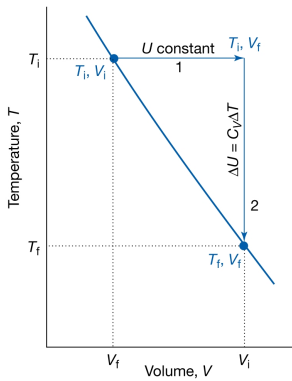
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thermogram for protein ubiquitin at pH = 2.45

native structure up to $\approx 45^\circ\text{C}$ and then endothermic conformational change

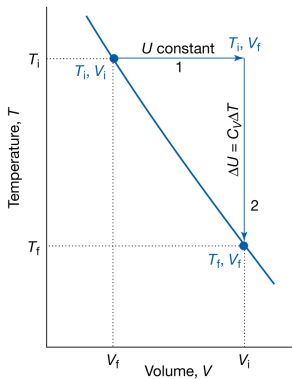


Adiabatic expansion : $T_i, V_i \longrightarrow T_f, V_f$



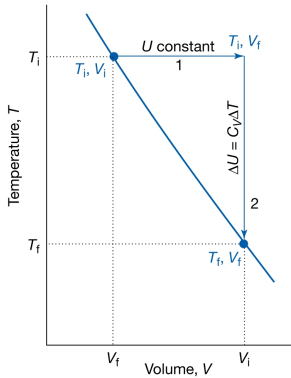
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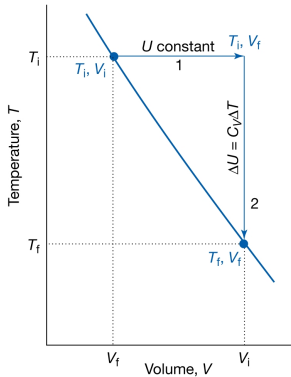


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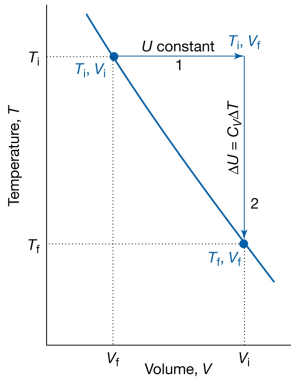


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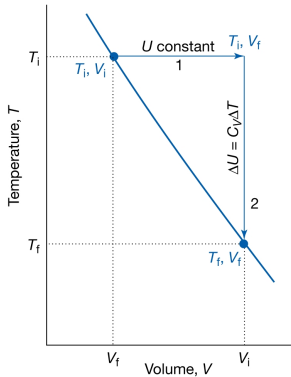
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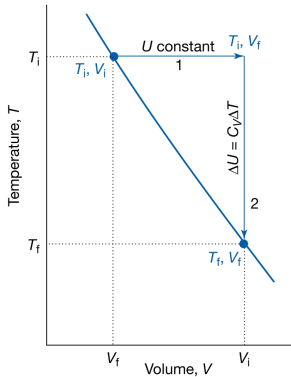
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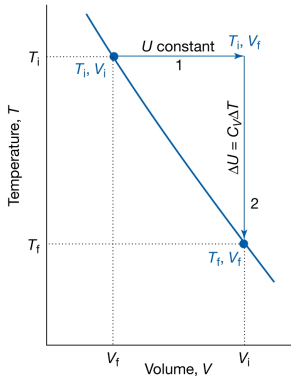


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U for perfect gas is independent of volume of
molecules, the overall ΔU arises solely from
second step, the change in temperature at
constant volume

$$\Delta U = C_v (T_f - T_i) = w_{ad}$$

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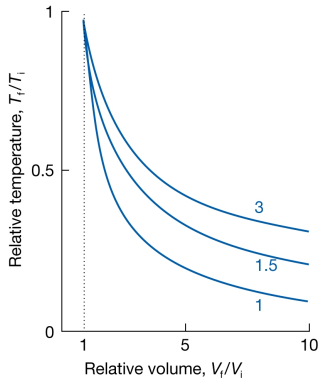
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$$\frac{T_2}{T_1} = \left(\frac{V_1}{V_2} \right)^{\frac{nR}{C_v}} = \left(\frac{V_1}{V_2} \right)^{\gamma-1} \text{ or, } TV^{\gamma-1} = \text{const.}$$

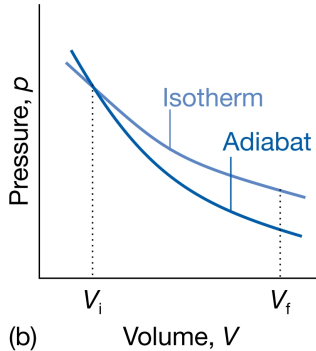
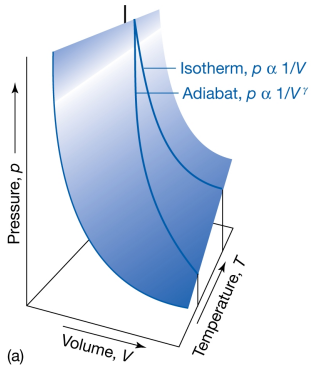
show: $pV^\gamma = \text{const}$



label : $\frac{C_v}{R}$

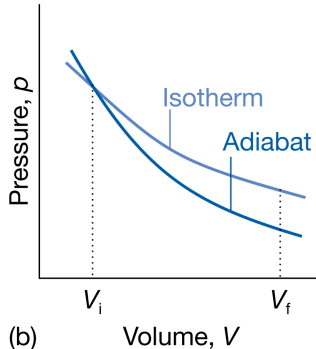
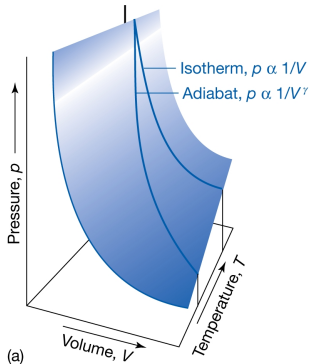
p-V-T plots : isotherms and adiabats

pressure declines more steeply for an adiabat than for an isotherm



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in isothermal expansion, energy flows into the system as heat and maintains the temperature; as a result, pressure does not fall as much as in adiabatic expansion

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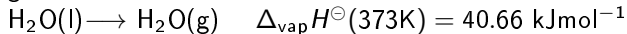
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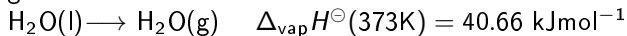
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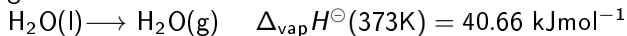
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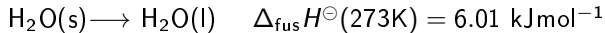
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standard enthalpies may be reported for any temperature

enthalpy is a state function

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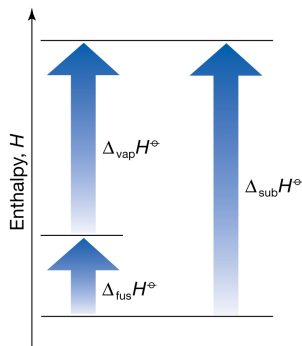
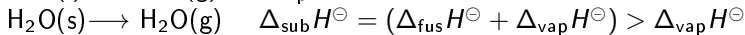
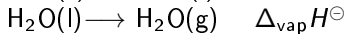
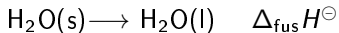
ΔH is independent of path between the two states

enthalpy is a state function

ΔH is independent of path between the two states

same ΔH^\ominus for change brought about between same initial and final states

e.g., conversion of a solid to a vapour either as occurring by sublimation

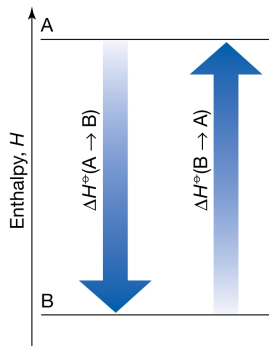


ΔH^\ominus for a forward process and its reverse
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e.g., conversion of a solid to a vapour either as occurring by sublimation

$$\Delta H^\ominus(\text{A} \rightarrow \text{B}) = -\Delta H^\ominus(\text{B} \rightarrow \text{A})$$



Transition	Process	Symbol
Transition	Phase $\alpha \rightarrow$ phase β	$\Delta_{\text{trs}}H$
Fusion	$s \rightarrow l$	$\Delta_{\text{fus}}H$
Vaporization	$l \rightarrow g$	$\Delta_{\text{vap}}H$
Sublimation	$s \rightarrow g$	$\Delta_{\text{sub}}H$
Mixing	Pure \rightarrow mixture	$\Delta_{\text{mix}}H$
Solution	Solute \rightarrow solution	$\Delta_{\text{sol}}H$
Hydration	$X^{\pm}(g) \rightarrow X^{\pm}(aq)$	$\Delta_{\text{hyd}}H$
Atomization	Species(s, l, g) \rightarrow atoms(g)	$\Delta_{\text{at}}H$
Ionization	$X(g) \rightarrow X^{+}(g) + e^{-}(g)$	$\Delta_{\text{ion}}H$
Electron gain	$X(g) + e^{-}(g) \rightarrow X^{-}(g)$	$\Delta_{\text{eg}}H$
Reaction	Reactants \rightarrow products	Δ_rH
Combustion	Compounds(s, l, g) + $O_2(g) \rightarrow CO_2(g), H_2O(l, g)$	Δ_cH
Formation	Elements \rightarrow compound	Δ_fH
Activation	Reactants \rightarrow activated complex	$\Delta^{\ddagger}H$

Standard reaction enthalpy :

change in enthalpy for

Pure, separate reactants in standard states \longrightarrow

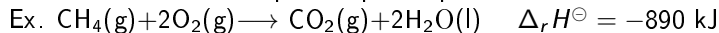
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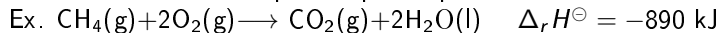


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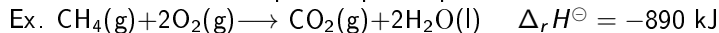
For the reaction $2\text{A} + \text{B} \longrightarrow 3\text{C} + \text{D}$

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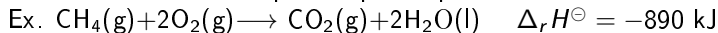


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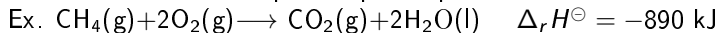
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$$\Delta_r H^\ominus = \{3H_m^\ominus(\text{C}) + H_m^\ominus(\text{D})\} - \{2H_m^\ominus(\text{A}) + H_m^\ominus(\text{B})\}$$

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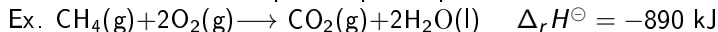
generally,
$$\Delta_r H^\ominus = \sum_{\text{products}} \nu H_m^\ominus - \sum_{\text{reactants}} \nu H_m^\ominus$$

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Pure, separate reactants in standard states \longrightarrow

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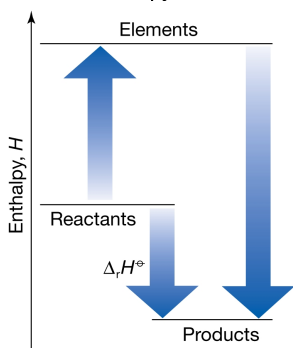
$$\Delta_r H^\ominus = \{3H_m^\ominus(\text{C}) + H_m^\ominus(\text{D})\} - \{2H_m^\ominus(\text{A}) + H_m^\ominus(\text{B})\}$$

generally, $\Delta_r H^\ominus = \sum_{\text{products}} \nu H_m^\ominus - \sum_{\text{reactants}} \nu H_m^\ominus$

standard enthalpy of combustion, $\Delta_c H^\ominus$ = standard reaction enthalpy for the complete oxidation of an organic compound to CO_2 gas and liquid water if the compound contains C, H, and O, and to N_2 gas if N is also present

reaction enthalpy in terms of enthalpies of formation

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$$\Delta_r H^\ominus = \sum_{\text{products}} \nu \Delta_f H^\ominus - \sum_{\text{reactants}} \nu \Delta_f H^\ominus$$

Can we construct $\Delta_f H^\ominus$ from a knowledge of chemical constitution of the species?

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no thermodynamically exact way of expressing enthalpies of formation in terms of contributions from individual atoms and bonds

$$dH = C_p dT \quad \implies \quad H(T_2) = H(T_1) + \int_{T_1}^{T_2} C_p dT \quad \text{assuming no phase transition in}$$

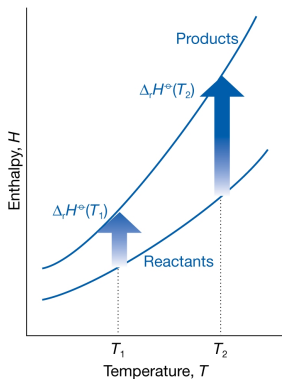
temperature range of interest

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Kirchhoff's law :

$$\Delta_r H^\ominus(T_2) = \Delta_r H^\ominus(T_1) + \int_{T_1}^{T_2} \Delta_r C_p^\ominus dT$$

where $\Delta_r C_p^\ominus = \sum_{\text{products}} \nu C_{p,m}^\ominus - \sum_{\text{reactants}} \nu C_{p,m}^\ominus$



solved prob.: $\Delta_f H^\ominus(\text{H}_2\text{O}(\text{g}); 298 \text{ K}) = -241.82 \text{ kJ mol}^{-1}$

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Estimate $\Delta_f H^\ominus$ at 100°C

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Estimate $\Delta_f H^\ominus$ at 100°C

given $C_{p,m}(\text{H}_2\text{O,g}) = 33.58 \text{ J K}^{-1} \text{ mol}^{-1}$; $C_{p,m}(\text{H}_2,\text{g}) = 28.84 \text{ J K}^{-1} \text{ mol}^{-1}$;
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$$\Delta_r C_p^\ominus = C_{p,m}(\text{H}_2\text{O}, \text{g}) - \{C_{p,m}(\text{H}_2, \text{g}) + \frac{1}{2} C_{p,m}(\text{O}_2, \text{g})\} = -9.94 \text{ J K}^{-1} \text{ mol}^{-1}$$

solved prob.: $\Delta_f H^\ominus(\text{H}_2\text{O}(\text{g}); 298 \text{ K}) = -241.82 \text{ kJ mol}^{-1}$

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$$\begin{aligned}\therefore \Delta_r H^\ominus(T_2) &= \Delta_r H^\ominus(T_1) + (T_2 - T_1) \Delta_r C_p^\ominus \\ &= -241.82 - 75 \times 9.94 \times 10^{-3} = -242.6 \text{ kJ mol}^{-1}\end{aligned}$$