

# Marine Control Systems II

## Lecture 4: ISS and Feedback Linearization

Roger Skjetne

Department of Marine Technology  
Norwegian University of Science and Technology

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### Goals of lecture

- ▶ Understand the concept of Input-to-State-Stability (ISS)
  - ▶ ISS definition.
  - ▶ ISS-Lyapunov function.
- ▶ Understand concepts from linear systems theory and transfer some of these to nonlinear systems.
  - ▶ Poles, zeros, relative degree, and zero dynamics.
- ▶ Being able to perform feedback linearization:
  - ▶ Full state feedback linearization.
  - ▶ Partial state feedback linearization.

# Literature

- ▶ Khalil, H. K. (2015). Nonlinear Control:
  - ▶ Chapters: 4.2-4.4 and 9.1-9.4
- ▶ Lecture presentation.

## Nonlinear systems with inputs

Consider the system

$$\dot{x} = f(t, x, u)$$

where  $x(t) \in \mathbb{R}^n$ ,  $u(t) \in \mathbb{R}^m$ ,  $\forall t \geq 0$ , and the map  $f : \mathbb{R}_{\geq 0} \times \mathbb{R}^n \times \mathbb{R}^m \rightarrow \mathbb{R}^n$  is smooth.

$u$  is a measurable, locally essentially bounded function  $u : \mathbb{R}_{\geq 0} \rightarrow \mathbb{R}^m$ .

Space of such functions is  $\mathcal{L}_{\infty}^m$  with norm

$$\|u_{[t_0, \infty)}\| := \text{ess sup} \{u(t) : t \geq t_0 \geq 0\}.$$

Use  $\|u\| = \|u_{[t_0, \infty)}\|$  and let  $\|u_{[t_0, t]}\|$  be the signal norm over the truncated interval  $[t_0, t]$ .

For each initial condition  $t_0 \in [0, \infty)$ ,  $x_0 = x(t_0) \in \mathbb{R}^n$  and each  $u \in \mathcal{L}_{\infty}^m$ , let  $x(t, t_0, x_0, u)$  denote the solution at time  $t$ .

## Example 1

Consider

$$\dot{x} = f(x, u) = -x^3 + u$$

With  $u = 0$  we get that  $V(x) = \frac{1}{2}x^2$  is a Lyapunov function, and the origin  $x = 0$  is UGAS for  $\dot{x} = f(x, 0)$ .

Consider now  $u \neq 0$ . Differentiating  $V(x)$  gives

$$\begin{aligned}\dot{V} &= -x^4 + xu \\ &= -(1 - \lambda)x^4 - \lambda x^4 + xu, & \lambda \in (0, 1) \\ &\leq -(1 - \lambda)x^4 - \lambda |x|^4 + |x| \|u\| \\ &\leq -(1 - \lambda)x^4, & \forall |x| \geq \sqrt[3]{\frac{\|u\|}{\lambda}}\end{aligned}$$

For example,  $\|u\| \leq 4$  and setting  $\lambda = 0.5$ , then

$$\dot{V} \leq -\frac{1}{2}x^4, \quad \forall |x| \geq \sqrt[3]{8} = 2$$

## Input-to-State Stability (ISS)

### Definition

The system  $\dot{x} = f(t, x, u)$  is ISS with respect to the origin  $x = 0$  if there exist  $\beta \in \mathcal{KL}$  and  $\gamma \in \mathcal{K}$  such that for each  $u \in \mathcal{L}_{\infty}^m$ ,  $\forall x_0$ , and  $\forall t \geq t_0 \geq 0$ , the solution  $x(t, t_0, x_0, u)$  is defined and satisfies

$$|x(t, t_0, x_0, u)| \leq \beta(|x_0|, t - t_0) + \gamma(\|u_{[t_0, t]}\|).$$

# ISS-Lyapunov function

## Definition

A smooth ISS-Lyapunov function for  $\dot{x} = f(t, x, u)$  with respect to the origin is a smooth function  $V : \mathbb{R}_{\geq 0} \times \mathbb{R}^n \rightarrow \mathbb{R}_{\geq 0}$  that satisfies:

1. there exist two class- $\mathcal{K}_{\infty}$  functions  $\alpha_1$  and  $\alpha_2$  such that for any  $x \in \mathbb{R}^n$  and  $t \geq 0$ ,

$$\alpha_1(|x|) \leq V(t, x) \leq \alpha_2(|x|),$$

2. there exist a class- $\mathcal{K}$  function  $\alpha_3$  and a  $\mathcal{K}_{\infty}$ -function  $\chi$  such that for all  $t \geq 0$ ,  $x \in \mathbb{R}^n$ , and  $u \in \mathbb{R}^m$ ,

$$|x| \geq \chi(|u|) \Rightarrow V^t(t, x) + V^x(t, x)f(t, x, u) \leq -\alpha_3(|x|).$$

## Example 2

Consider

$$\dot{x} = f(x, u) = -x^3 + xu$$

Then  $V(x) = \frac{1}{2}x^2$  is an ISS-Lyapunov function.

*Proof:*

$$\begin{aligned} \dot{V} &= -x^4 + x^2u \\ &= -(1 - \lambda)x^4 - \lambda x^4 + x^2u, & \lambda \in (0, 1) \\ &\leq -(1 - \lambda)x^4 - \lambda |x|^4 + |x|^2 |u| \\ &\leq -(1 - \lambda)x^4, \quad \forall |x| \geq \sqrt{\frac{1}{\lambda}} |u| \end{aligned}$$

# ISS-Lyapunov function

An equivalent representation of this is:

**2.** *There exist two class- $\mathcal{K}_\infty$  functions  $\alpha_3$  and  $\alpha_4$  such that for all  $t \geq 0$ ,  $x \in \mathbb{R}^n$ , and  $u \in \mathbb{R}^m$ ,*

$$V^t(t, x) + V^x(t, x)f(t, x, u) \leq -\alpha_3(|x|) + \alpha_4(|u|).$$

## ...Example 2

Consider again

$$\dot{x} = f(x, u) = -x^3 + xu$$

for which with  $V(x) = \frac{1}{2}x^2$  we got

$$\dot{V} = -x^4 + x^2u$$

Using Young's inequality  $ab \leq \kappa a^2 + \frac{1}{4\kappa}b^2$ ,  $\kappa > 0$ , with  $a = x^2$  and  $b = u$ , gives

$$\begin{aligned}\dot{V} &\leq -x^4 + \kappa x^4 + \frac{1}{4\kappa}u^2 \\ &= -(1 - \kappa)|x|^4 + \frac{1}{4\lambda}|u|^2 =: -\alpha_3(|x|) + \alpha_4(|u|).\end{aligned}$$

Choosing  $\kappa \in (0, 1)$  ensures that ISS is proven.

# ISS-Lyapunov function

Note:

$$V^t(t, x) + V^x(t, x)f(t, x, u) \leq -\alpha_3(|x|) + \alpha_4(|u|)$$

$\Downarrow$

$$V^t(t, x) + V^x(t, x)f(t, x, u) \leq -\varepsilon\alpha_3(|x|)$$

$$\forall |x| \geq \alpha_3^{-1} \left( \frac{1}{1-\varepsilon} \alpha_4(|u|) \right) =: \chi(|u|)$$

where  $\varepsilon \in (0, 1)$ .

The converse is also true for stability of an equilibrium point.

## ISS sufficiency theorem

### Theorem

*Assume that  $x = 0$  is 0-invariant for  $\dot{x} = f(t, x, u)$ , i.e.  $x = 0$  is invariant for  $\dot{x} = f(t, x, 0)$  which means  $x_0 = 0 \implies x(t) = 0, \forall t \geq t_0$ .*

*If the system admits a smooth ISS-Lyapunov function with respect to the origin, then it is ISS.*

# ISS sufficiency theorem

## Corollary

*Suppose the system is ISS with respect to the origin. Then the origin of  $\dot{x} = f(t, x, 0)$  is UGAS.*

## Corollary

*Suppose the system is ISS with respect to the origin. Then*

$$\lim_{t \rightarrow \infty} |u(t)| = 0 \Rightarrow \lim_{t \rightarrow \infty} |x(t)| = 0.$$

# GES implies ISS theorem

We consider the system

$$\dot{x} = f(x, u) \tag{1}$$

where  $f$  is locally Lipschitz in  $x$  and  $u$ .

## Lemma

*(Khalil, 2015, Lemma 4.5)*

*Suppose  $f(x, u)$  is **continuously differentiable** and **globally Lipschitz** in  $(x, u)$ .*

*If  $x = 0$  is **GES** for  $\dot{x} = f(x, 0)$ , then (1) is ISS with respect to  $x = 0$ .*

# Linear transfer function

Consider the strictly proper transfer function

$$\frac{Y(s)}{U(s)} = G(s) = \frac{b(s)}{a(s)} = \frac{b_m s^m + b_{m-1} s^{m-1} + \dots + b_1 s + b_0}{a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0}, \quad n > m$$

The relative degree of this system is

$$r = n - m > 0.$$

We say that:

- ▶ The *zeros* are the roots of the numerator polynomial.
- ▶ The *poles* are the roots of the denominator polynomial.
- ▶ The system is *stable* if all its poles have nonpositive real part.
- ▶ A stable system is *minimum phase* if all zeros have negative real part.
- ▶ A stable system is *nonminimum phase* if some zero has positive real part.

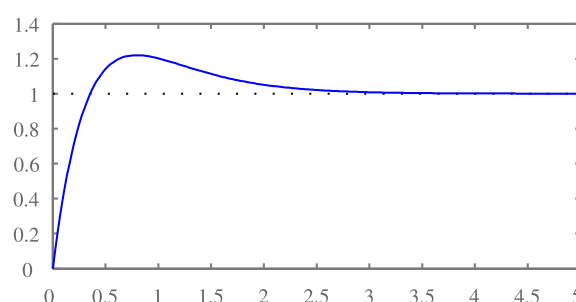
## Example 3

Consider

$$\frac{Y(s)}{U(s)} = G(s) = \frac{24}{5} \frac{(s+1)(s+5)}{(s+2)(s+3)(s+4)} = \frac{24}{5} \left( \frac{s^2 + 6s + 5}{s^3 + 9s^2 + 26s + 24} \right)$$

- ▶ Relative degree:  $r = 3 - 2 = 1$ .
- ▶ Zeros:  $z_1 = -1, z_2 = -5$
- ▶ Poles:  $p_1 = -2, p_2 = -3, p_3 = -4$
- ▶ System is stable and minimum phase.

Step response:





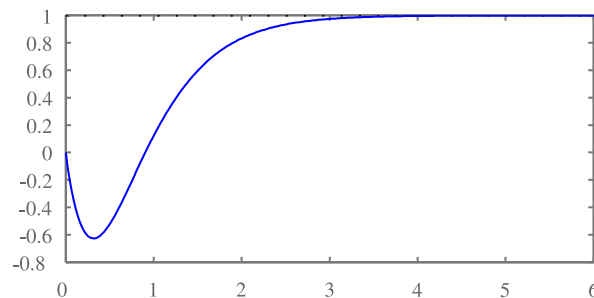
## Example 4

Consider

$$\frac{Y(s)}{U(s)} = G(s) = \frac{-24}{5} \frac{(s-1)(s+5)}{(s+2)(s+3)(s+4)} = \frac{-24}{5} \left( \frac{s^2 + 4s - 5}{s^3 + 9s^2 + 26s + 24} \right)$$

- Zeros:  $z_1 = +1, z_2 = -5$
- Poles:  $p_1 = -2, p_2 = -3, p_3 = -4$
- System is stable but **nonminimum** phase.

Step response:



## Zero dynamics

Consider the strictly proper transfer function

$$\frac{Y(s)}{U(s)} = G(s) = k \frac{(s - z_1)(s - z_2) \cdots (s - z_m)}{(s - p_1)(s - p_2) \cdots (s - p_n)}, \quad n > m$$

Suppose  $z_2 = p_2$ . Then we have a pole-zero cancellation. This gives rise to *zero dynamics* (or *internal dynamics*):

### Definition

**Zero dynamics** are (internal) states that are not observable from the output of the system.

## ...Zero dynamics

For the zero dynamics we have:

- ▶ The zero dynamics can be found by setting the output  $y(t)$  and its derivatives identically equal to zero. The remaining dynamics is then the zero dynamics.
- ▶ The zero dynamics can be stable or unstable. Even if the zero dynamics does not affect the output, unstable zero dynamics (that may grow unbounded) will typically have a detrimental effect on the system.
- ▶ If not stable, then one should aim for controllability of the zero dynamics to render it stable through control action.

### Example 5: Stable zero dynamics

Consider

$$\frac{Y(s)}{U(s)} = G(s) = \frac{2(s+1)}{(s+1)(s+2)} = \frac{2}{(s+2)}$$

which has a pole-zero cancellation of a stable pole. A state space realization of the complete system is:

$$\begin{aligned}\dot{x}_1 &= -3x_1 - \sqrt{2}x_2 + u, & \dot{x}_2 &= \sqrt{2}x_1 \\ y &= 2x_1 + \sqrt{2}x_2\end{aligned}$$

Differentiating  $y$  gives

$$\begin{aligned}\dot{y} &= 2\dot{x}_1 + \sqrt{2}\dot{x}_2 = 2(-3x_1 - \sqrt{2}x_2 + u) + \sqrt{2}\sqrt{2}x_1 \\ &= -6x_1 - 2\sqrt{2}x_2 + 2x_1 + 2u = -4x_1 - 2\sqrt{2}x_2 + 2u \\ &= -2(y - u)\end{aligned}$$

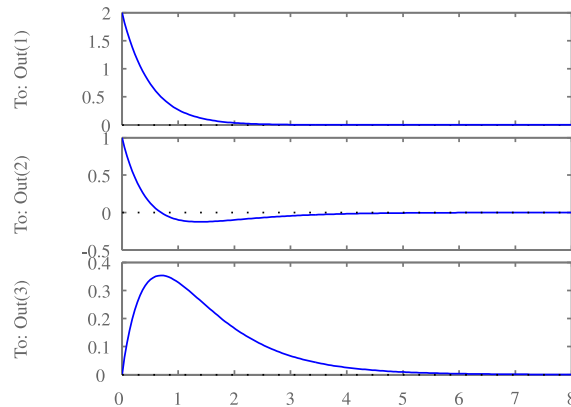
Setting  $y = \dot{y} = 0$  gives

$$2x_1 + \sqrt{2}x_2 = 0 \quad \Rightarrow \quad x_1 = -\frac{1}{2}\sqrt{2}x_2, \quad x_2 = -\sqrt{2}x_1$$

$$\dot{x}_1 = -\frac{1}{2}\sqrt{2}\dot{x}_2 = -\frac{1}{2}\sqrt{2}\sqrt{2}x_1 = -x_1$$

$$\dot{x}_2 = -\sqrt{2}\dot{x}_1 = -\sqrt{2} \left[ -3 \left( -\frac{1}{2}\sqrt{2}x_2 \right) - \sqrt{2}x_2 + u \right] = -x_2 - \sqrt{2}u$$

Impulse responses  $(y, x_1, x_2)$ :



## Example 6: Unstable zero dynamics

Consider

$$\frac{Y(s)}{U(s)} = G(s) = \frac{2(s-1)}{(s-1)(s+2)} = \frac{2}{(s+2)}$$

which has a pole-zero cancellation of an unstable pole. A state space realization is:

$$\begin{aligned} \dot{x}_1 &= -x_1 + \sqrt{2}x_2 + u, & \dot{x}_2 &= \sqrt{2}x_1 \\ y &= 2x_1 - \sqrt{2}x_2 \end{aligned}$$

Differentiating  $y$  gives

$$\begin{aligned} \dot{y} &= 2\dot{x}_1 - \sqrt{2}\dot{x}_2 = 2(-x_1 + \sqrt{2}x_2 + u) - \sqrt{2}\sqrt{2}x_1 \\ &= -2x_1 + 2\sqrt{2}x_2 - 2x_1 + 2u = -4x_1 + 2\sqrt{2}x_2 + 2u \\ &= -2(y - u) \end{aligned}$$

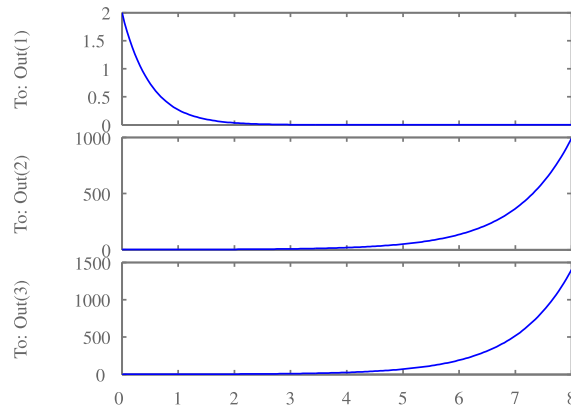
Setting  $y = \dot{y} = 0$  gives

$$2x_1 - \sqrt{2}x_2 = 0 \quad \Rightarrow \quad x_1 = \frac{1}{2}\sqrt{2}x_2, \quad x_2 = \sqrt{2}x_1$$

$$\dot{x}_1 = \frac{1}{2}\sqrt{2}\dot{x}_2 = \frac{1}{2}\sqrt{2}\sqrt{2}x_1 = x_1$$

$$\dot{x}_2 = \sqrt{2}\dot{x}_1 = \sqrt{2} \left[ -\left(\frac{1}{2}\sqrt{2}x_2\right) + \sqrt{2}x_2 + u \right] = x_2 + \sqrt{2}u$$

Impulse responses  $(y, x_1, x_2)$ :



## Example 7

Consider the nonlinear pendulum system

$$\dot{\theta} = \omega$$

$$\dot{\omega} = -\frac{g}{l} \sin \theta - \frac{k}{ml^2} \omega + \frac{\cos \theta}{ml} u$$

on the domain  $D = \{(\theta, \omega) \in \mathbb{R}^2 : \theta \in (-\frac{\pi}{2}, \frac{\pi}{2})\}$ . The control

$$u = \frac{ml}{\cos \theta} \left[ \frac{g}{l} \sin \theta + \frac{k}{ml^2} \omega + v \right], \quad (\theta, \omega) \in D$$

renders the system into the linear double integrator

$$\dot{\theta} = \omega$$

$$\dot{\omega} = v.$$

Setting  $v = -k_1\theta - k_2\omega$  will then make the system exponentially stable.

## Full state feedback linearization

We follow the lecture by Khalil (2002, Lecture 26) and consider a nonlinear system on affine form

$$\dot{x} = f(x) + G(x)u, \quad f(0) = 0, \quad x \in \mathbb{R}^n, \quad u \in \mathbb{R}^m$$

Suppose there is a coordinate transformation  $z = T(x)$ , defined  $\forall x \in \mathcal{D} \subset \mathbb{R}^n$ , that transforms the state into *controller form*

$$\dot{z} = Az + B\gamma(x) [u - \alpha(x)]$$

where  $[A, B]$  is a controllable pair, and  $\gamma(x)$  is nonsingular  $\forall x \in \mathcal{D}$ . Then we can apply the feedback linearizing control

$$u = \alpha(x) + \gamma(x)^{-1}v$$

where  $v$  is a new control input, resulting in the new system

$$\dot{z} = Az + Bv$$

## Full state feedback linearization

Now we can apply a linear state feedback control

$$v = -Kz$$

where  $K$  is designed to make  $A - BK$  Hurwitz.

Result: the origin  $z = 0$  of the closed-loop system

$$\dot{z} = (A - BK)z$$

is UGES.

In the  $x$ -dynamics we have designed the control and closed-loop

$$\begin{aligned} u &= \alpha(x) - \gamma(x)^{-1}KT(x) \\ \dot{x} &= f(x) + G(x) [\alpha(x) - \gamma(x)^{-1}KT(x)] \end{aligned}$$

But what about stability of  $x = 0$ ?

# Full state feedback linearization

Since  $x \mapsto T(x)$  is a *local diffeomorphism* on  $\mathcal{D}$ ,  $x = 0$  is LAS. However, note that it is not in general exponentially stable. Exponential convergence in the  $z$ -state is transformed to asymptotic convergence in the  $x$ -state.

In general  $x = 0$  is not globally stable. However, if  $T(x)$  is a *global diffeomorphism*, then  $x = 0$  is GAS.

## Robustness

Uncertainties in the models for  $\alpha$ ,  $\gamma$ , and  $T$  is typically the criticism for feedback linearization; it relies on exact cancellation of nonlinear dynamics.

Let  $\alpha_0(x)$ ,  $\gamma_0(x)$ , and  $T_0(x)$  be your nominal models for  $\alpha$ ,  $\gamma$ , and  $T$ , so that the realized control and closed-loop become

$$\begin{aligned} u &= \alpha_0(x) - \gamma_0(x)^{-1} K T_0(x) \\ \dot{z} &= (A - BK) z + B \delta(z) \\ \delta &= \gamma [\alpha_0 - \alpha + \gamma^{-1} K z - \gamma_0^{-1} K T_0] \end{aligned} \tag{2}$$

Let

$$\begin{aligned} V(z) &= z^\top P z, \quad P(A - BK) + (A - BK)^\top P = -qI \\ \dot{V} &= -q z^\top z + 2 z^\top P B \delta(z) \leq -q |z|^2 + 2 \|PB\| |z| |\delta(z)| \end{aligned}$$

# Robustness

## Lemma

*If  $\exists k$  satisfying  $0 \leq k < \frac{\lambda q}{2\|PB\|}$ , for  $\lambda \in (0, 1)$ , such that  $|\delta(z)| \leq k|z|$ ,  $\forall z \in \mathbb{R}^n$ , then  $z = 0$  of (2) is GES.*

**Proof:** We get

$$\begin{aligned}\dot{V} &= -qz^\top z + 2z^\top PB\delta(z) \\ &\leq -q|z|^2 + 2\|PB\| |z| |\delta(z)| \\ &\leq -(1-\lambda)q|z|^2 - \lambda q|z|^2 + 2k\|PB\| |z|^2 \\ &= -(1-\lambda)q|z|^2 - (\lambda q - 2k\|PB\|) |z|^2 \\ &\leq -(1-\lambda)q|z|^2, \quad \forall k < \frac{\lambda q}{2\|PB\|}, \quad \text{Q.E.D.}\end{aligned}$$

# Robustness

## Lemma

*If  $\exists k$  satisfying  $0 \leq k < \frac{\lambda q}{2\|PB\|}$  and  $\varepsilon > 0$  such that  $|\delta(z)| \leq k|z| + \varepsilon$ ,  $\forall z \in \mathbb{R}^n$ , then  $z = 0$  of (2) is globally ultimately bounded.*

**Proof:** We get

$$\begin{aligned}\dot{V} &\leq -(1-\lambda)q|z|^2 - \lambda q|z|^2 + 2\|PB\| |z| (k|z| + \varepsilon) \\ &\leq -(1-\lambda)q|z|^2 - (\lambda q + 2k\|PB\|) |z|^2 + 2\varepsilon\|PB\| |z| \\ &\leq -(1-\lambda)q|z|^2 + 2\varepsilon\|PB\| |z|, \quad \forall k < \frac{\lambda q}{2\|PB\|} \\ &\leq -\frac{1-\lambda}{2}q|z|^2 - \frac{1-\lambda}{2}q|z|^2 + 2\varepsilon\|PB\| |z| \\ &\leq -\frac{1-\lambda}{2}q|z|^2, \quad \forall |z| \geq \frac{4\varepsilon\|PB\|}{q(1-\lambda)}, \quad \text{Q.E.D.}\end{aligned}$$

## Example 8: Is feedback linearization a good idea?

See Khalil (2002, Lecture 26). Let

$$\begin{aligned}\dot{x} &= ax - bx^3 + u, & a, b > 0 \\ u &= -(k + a)x + bx^3, & k > 0 \\ \dot{x} &= -kx\end{aligned}$$

But we notice that  $-bx^3$  is a stabilizing nonlinear damping term. Why cancel this?

Instead

$$\begin{aligned}u &= -(k + a)x, & k > 0 \\ \dot{x} &= -kx - bx^3\end{aligned}$$

Which design is better?

## Partial feedback linearization

We follow the lecture by Khalil (2002, Lecture 27) and consider a nonlinear system on affine form

$$\dot{x} = f(x) + G(x)u, \quad f(0) = 0, \quad x \in \mathbb{R}^n, \quad u \in \mathbb{R}^m$$

Suppose there is a coordinate transformation

$$z = \begin{bmatrix} \eta \\ \xi \end{bmatrix} = T(x) = \begin{bmatrix} T_1(x) \\ T_2(x) \end{bmatrix}$$

defined  $\forall x \in \mathcal{D} \subset \mathbb{R}^n$ , that transforms the system into

$$\begin{aligned}\dot{\eta} &= f_0(\eta, \xi) \\ \dot{\xi} &= A\xi + B\gamma(x) [u - \alpha(x)]\end{aligned}$$

where  $[A, B]$  is a controllable pair, and  $\gamma(x)$  is nonsingular  $\forall x \in \mathcal{D}$ .



## Partial feedback linearization

Applying the partial feedback linearizing control

$$\begin{aligned}u &= \alpha(x) + \gamma(x)^{-1}v \\v &= -K\xi\end{aligned}$$

where  $A - BK$  is Hurwitz. Then

### Lemma

*The origin  $(\eta, \xi) = 0$  of*

$$\begin{aligned}\dot{\eta} &= f_0(\eta, \xi) \\ \dot{\xi} &= (A - BK)\xi\end{aligned}$$

*is LAS if  $\eta = 0$  of the zero-dynamics  $\dot{\eta} = f_0(\eta, 0)$  is LAS.*

**Proof:** We have  $V_1(\eta)$ , with bounds  $V_1^\eta f_0(\eta, 0) \leq -\alpha_1(\eta)$  and  $|V_1^\eta| \leq \rho(|\eta|)$ . We use

$$V(z) = V_1(\eta) + c\sqrt{\xi^\top P \xi}$$

Differentiating...

## Partial feedback linearization

...

$$\begin{aligned}\dot{V} &= V_1^\eta \dot{\eta} + c \frac{1}{2\sqrt{\xi^\top P \xi}} 2\xi^\top P \dot{\xi} \\ &= V_1^\eta f_0(\eta, \xi) \pm V_1^\eta f_0(\eta, 0) + \frac{c}{2\sqrt{\xi^\top P \xi}} \xi^\top \left[ P(A - BK) + (A - BK)^\top P \right] \xi \\ &\leq -\alpha_1(\eta) + |V_1^\eta| |f_0(\eta, \xi) - f_0(\eta, 0)| - \frac{c}{2\sqrt{\xi^\top P \xi}} \xi^\top \xi \\ &\leq -\alpha_1(\eta) + L\rho(|\eta|) |\xi| - \frac{c|\xi|^2}{2\sqrt{\lambda_{\max}(P)}\sqrt{|\xi|^2}}, \quad L \text{ a Lipschitz const.} \\ &\leq -\alpha_1(\eta) - \left[ \frac{c}{2\sqrt{\lambda_{\max}(P)}} - L\rho(|\eta|) \right] |\xi| \\ &< 0, \quad c > 2\sqrt{\lambda_{\max}(P)} Lr\end{aligned}$$

where  $r$  is a bound on  $\rho(|\eta|)$  on a neighborhood of the origin.

## Partial feedback linearization

If  $\eta = 0$  of the zero-dynamics  $\dot{\eta} = f_0(\eta, 0)$  is GAS,

will then the origin  $(\eta, \xi) = 0$  of

$$\begin{aligned}\dot{\eta} &= f_0(\eta, \xi) \\ \dot{\xi} &= (A - BK) \xi\end{aligned}$$

be GAS?

## Partial feedback linearization

**In general, NO!**

**Example 9:** Consider

$$\dot{\eta} = f_0(\eta, \xi) = -\eta + \eta^2 \xi, \quad \dot{\xi} = v.$$

The origin of the zero dynamics is GES,

$$\dot{\eta} = f_0(\eta, 0) = -\eta,$$

but the origin of

$$\dot{\eta} = -\eta + \eta^2 \xi, \quad \dot{\xi} = -k\xi, \quad k > 0$$

is not GAS. It has an ROC

$$\{(\eta, \xi) : \eta\xi < 1 + k\}.$$

# Partial feedback linearization

Sufficiency can be assured by ...

## Lemma

*The origin  $(\eta, \xi) = 0$  of*

$$\begin{aligned}\dot{\eta} &= f_0(\eta, \xi) \\ \dot{\xi} &= (A - BK)\xi\end{aligned}$$

*is GAS if the system  $\dot{\eta} = f_0(\eta, \xi)$  is ISS.*

**Proof:** Use Lemma 4.6 in Khalil (2015):

If  $\dot{x}_1 = f_1(x_1, x_2)$  is ISS, and the origin of  $\dot{x}_2 = f_2(x_2)$  is GAS, then the origin of the cascaded system is GAS.

See also (Loría and Panteley, 2005) for more relevant results on stability of cascades and interconnections.

## Effect of uncertainties

See Khalil (2002, Lecture 27) Let  $\alpha_0(x)$ ,  $\gamma_0(x)$ , and  $T_{20}(x)$  be your nominal models for  $\alpha$ ,  $\gamma$ , and  $T_2$ , so that the realized control and closed-loop become

$$\begin{aligned}u &= \alpha_0(x) - \gamma_0(x)^{-1}KT_{20}(x) \\ \dot{\eta} &= f_0(\eta, \xi), \quad \dot{\xi} = (A - BK)\xi + B\delta(z) \\ \delta &= \gamma [\alpha_0 - \alpha + \gamma^{-1}K\xi - \gamma_0^{-1}KT_{20}]\end{aligned}\tag{3}$$

## Lemma

- ▶ If  $|\delta(z)| \leq \varepsilon$ ,  $\forall z$ , and  $\dot{\eta} = f_0(\eta, \xi)$  is ISS, then the state  $z = (\eta, \xi)$  is globally ultimately bounded by a class- $\mathcal{K}$  function of  $\varepsilon$ .
- ▶ If  $|\delta(z)| \leq k|z|$  in some neighborhood of  $z = 0$ , with  $k$  sufficiently small, and  $\dot{\eta} = f_0(\eta, 0)$  is LES, then  $z = 0$  is LES for (3).

## Example 10: Linearized pendulum-cart

The linearized inverted pendulum-cart system can be written (see Lecture 3)

$$\begin{aligned}\dot{p} &= v \\ \dot{v} &= \frac{gm}{M}\theta + \frac{1}{M}u \\ \dot{\theta} &= \omega \\ \dot{\omega} &= \frac{g}{L} \left( \frac{m}{M} + 1 \right) \theta + \frac{1}{ML}u\end{aligned}$$

Let the control objective be to regulate  $(\theta, \omega) \rightarrow 0$ , and apply the control

$$\begin{aligned}u &= ML \left[ -\frac{g}{L} \left( \frac{m}{M} + 1 \right) \theta + u_0 \right] \\ u_0 &= -k_1\theta - k_2\omega.\end{aligned}$$

Letting  $\eta = (p, v)$  and  $\xi = (\theta, \omega)$  renders the closed-loop system

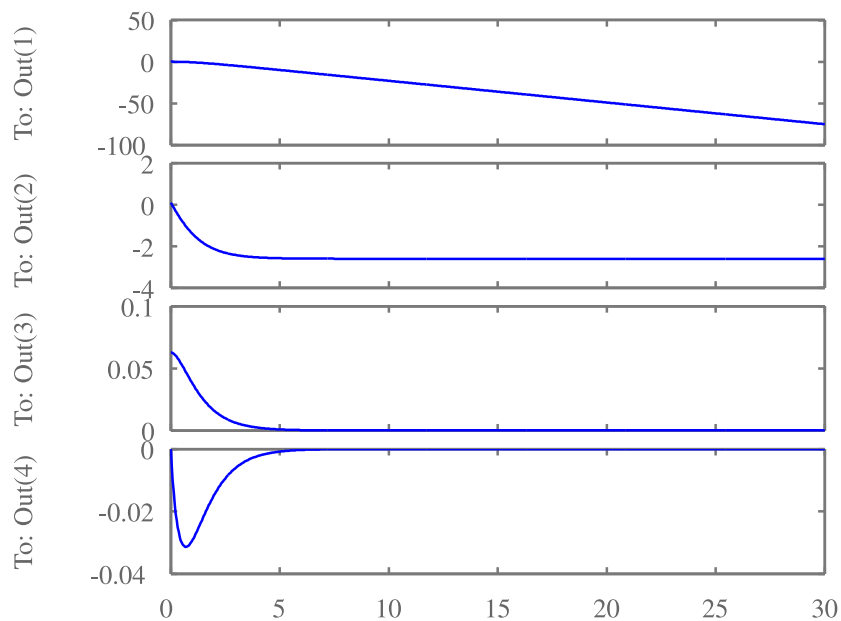
$$\begin{aligned}\dot{\eta} &= \begin{bmatrix} \dot{p} \\ \dot{v} \end{bmatrix} = \begin{bmatrix} v \\ -g(1 + Lk_1)\theta - Lk_2\omega \end{bmatrix} = f_0(\eta, \xi) \\ \dot{\xi} &= \begin{bmatrix} \dot{\theta} \\ \dot{\omega} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -k_1 & -k_2 \end{bmatrix} \begin{bmatrix} \theta \\ \omega \end{bmatrix} = A\xi\end{aligned}$$

In this case, the zero dynamics, given by  $\xi \equiv 0$ , is

$$\dot{\eta} = f_0(\eta, 0) \Rightarrow \begin{bmatrix} \dot{p} \\ \dot{v} \end{bmatrix} = \begin{bmatrix} v \\ 0 \end{bmatrix},$$

which is not stable (position will drift).

Simulating the response of the system to the initial conditions  $p_0 = 0$ ,  $v_0 = 0.1$ ,  $\theta_0 = \frac{\pi}{50}$ , and  $\omega_0 = 0$  gives the responses for  $(p, v, \theta, \omega)$ :



## Preparations for next lecture

### Backstepping:

- ▶ Note on Mathematical notations, section on inequalities: Especially Young's inequality.
- ▶ Khalil, H. K. (2015). Nonlinear Control.
  - ▶ Chapters: 9.7 and 9.5.
- ▶ Skjetne, R. (2005). The Maneuvering Problem.
  - ▶ Ch. 4.1 (for presentation of systematic ISS backstepping design).
- ▶ Lecture presentation.

# Bibliography

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Khalil, H. K. (2015). *Nonlinear Control*. Pearson Education Ltd., global edition.

Loría, A. and Panteley, E. (2005). Cascaded systems: Stability and stabilization. Lecture notes, NTNU, Dept. Eng. Cybernetics. April 21, 2005.