### TMR4243 - MARINE CONTROL SYSTEMS II

Homework assignment 4

## 1 Input-to-State Stability

### 1.1 Task: ISS-Lyapunov function

For the following systems, assume that  $||u|| \le u_{\text{max}}$ . Show that  $V(x) = \frac{1}{2}x^2$  is an ISS-Lyapunov function for the following systems:

 $\dot{x} = -x + u \tag{1}$ 

 $\dot{x} = -x^3 + x^2 u \tag{2}$ 

3.  $\dot{x} = -x^5 + x^3 u \tag{3}$ 

4.  $\dot{x} = -\left(1 + e^{|x|}\right)x + xu \tag{4}$ 

### 1.2 Task: ISS

In Homework Assignment 3 we were given the (simplified) mechanical dynamics of a diesel-generator

$$\dot{\delta} = \omega_B \left(\omega - \omega_0\right) \tag{5}$$

$$2H\dot{\omega} = t_m - D\omega - t_L + w(t) \tag{6}$$

where  $\omega$  is the frequency,  $\delta$  is the load angle,  $t_m$  is the control input torque,  $t_L$  is an electric load torque, w a bounded disturbance torque,  $(H, D, \omega_B) > 0$  are constants, and  $\omega_0$  is the frequency of the connected electric power bus. Controlling  $\delta$  to  $\delta_{ref}$  and  $\omega$  to  $\omega_0$ , we defined the error states  $x = \operatorname{col}(e_{\delta}, e_{\omega}) = \operatorname{col}(\delta - \delta_{ref}, \omega - \omega_0)$ , which gives

$$\dot{e}_{\delta} = \omega_B e_{\omega} \tag{7}$$

$$2H\dot{e}_{\omega} = t_m - De_{\omega} - D\omega_0 - t_L + w(t) \tag{8}$$

With the disturbance  $||w|| \le w_0$  as input, show that the control law

$$u = t_m = -k_p e_\delta - k_d e_\omega + D\omega_0 + t_L, \tag{9}$$

with  $k_p, k_d > 0$ , renders the resulting closed-loop system ISS with respect to x = 0.

#### 2 Feedback linearization

We will train on feedback linearization by considering the 3DOF horizontal vessel model

$$\dot{\eta} = R(\psi)\nu\tag{10}$$

$$M\dot{\nu} + C(\nu)\nu + D(\nu)\nu = \tau,\tag{11}$$

where  $\eta = col(x, y, \psi)$  is the position/heading;  $\nu = col(u, v, r)$  the velocities;  $C(\nu)$  the Coriolis/centripetal matrix;  $D(\nu) > 0$  a nonlinear damping matrix;  $M = M^{\top} > 0$ ;  $\tau$  the control force input; and  $R(\psi)$  the rotation matrix:

$$R(\psi) = \begin{bmatrix} \cos \psi & -\sin \psi & 0\\ \sin \psi & \cos \psi & 0\\ 0 & 0 & 1 \end{bmatrix}. \tag{12}$$

This has the properties that  $R(\psi)^{\top}R(\psi) = R(\psi)R(\psi)^{\top} = I$  and  $\dot{R} = R(\psi)S(r)$  where

$$S(r) = \begin{bmatrix} 0 & -r & 0 \\ r & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} = -S(r)^{\top}.$$
 (13)

#### 2.1 Task: Feedback linearization

If the output to be controlled is  $\eta \in \mathbb{R}^3$ , do the following:

- 1. Explain the term "vector relative degree", and calculate the vector relative degree for the 3DOF vessel model.
- 2. Differentiate  $\eta$  according to the vector relative degree. What is the dimension of the zero dynamics?
- 3. Perform a full state feedback linearization design by differentiating  $\eta$  according to the vector relative degree.

#### 2.2 Task: Feedback linarization by a nonlinear transformation

If the output to be controlled is  $\eta \in \mathbb{R}^3$ , define the transformation  $z_1 := \eta$ ,  $z_2 := R(\psi)\nu + C_1\eta$  where  $C_1 = C_1^{\top} > 0$ . This defines the state transformation  $z = \operatorname{col}(z_1, z_2) = T(x)$ , where  $x := \operatorname{col}(\eta, \nu)$ .

1. Show that this transforms the system into the controller form

$$\dot{z} = Az + B\Gamma(x)\left[u - \alpha(x)\right] \tag{14}$$

where (A, B) is controllable, and  $\Gamma(x)$  is nonsingular for all x.

2. Design a full-state feedback linearization control law, and prove UGES of z=0 using Lyapunov's Direct Method.

#### 2.3 Task: Zero dynamics

Assume for simplicity that  $C(\nu) = 0$  and  $D(\nu) = D > 0$  is a constant damping matrix.

For  $\tau = \operatorname{col}(\tau_u, \tau_v, \tau_r) \in \mathbb{R}^3$ , let

$$\tau_u = -k(u - u_0) = \gamma(u), \quad k > 0, u_0 > 0$$
(15)

$$\begin{bmatrix} \tau_v \\ \tau_r \end{bmatrix} = \begin{bmatrix} -Y_\delta \\ -N_\delta \end{bmatrix} \delta$$

$$\tau = B_1 \gamma(u) + B_2 \delta$$
(16)

$$\tau = B_1 \gamma(u) + B_2 \delta \tag{17}$$

$$B_1 = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}, \qquad B_2 = \begin{bmatrix} 0 \\ -Y_{\delta} \\ -N_{\delta} \end{bmatrix}$$
 (18)

where  $\delta \in \mathbb{R}$  is the new control input and  $(Y_{\delta}, N_{\delta})$  are control gains. Let now the output to be controlled be the heading  $\psi = h_{\psi}^{\top} \eta$ ,  $h_{\psi} := \text{col}(0, 0, 1)$ .

- 1. What is the relative degree of the system?
- 2. Differentiate the output according to the relative degree and identify the controlled dynamics and the internal dynamics (keeping vector notation).
- 3. Perform a partial feedback linearization design that controls the output to a constant reference heading  $\psi_{ref}$ .

# References