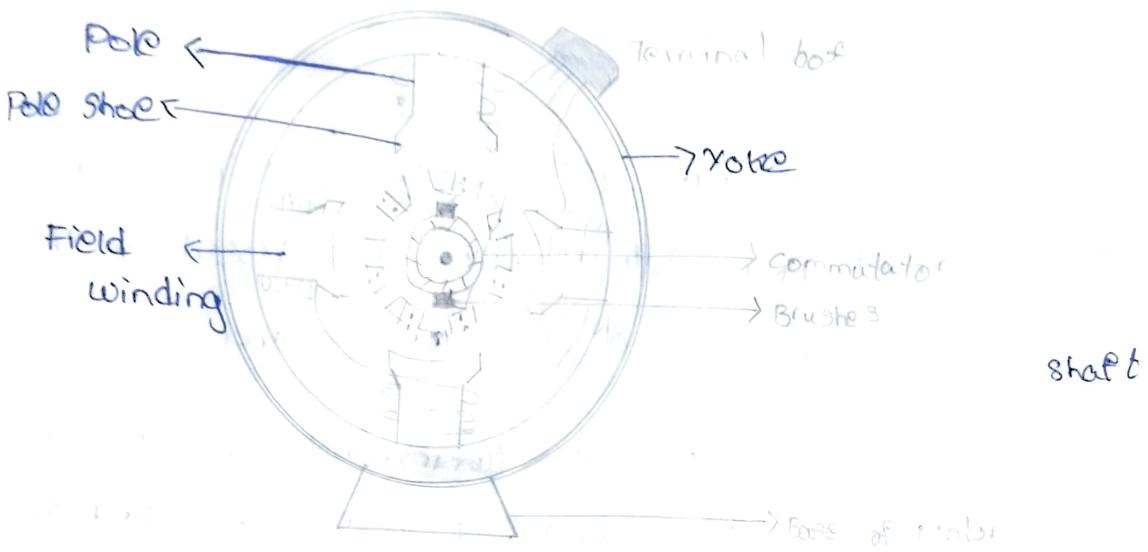


Date  
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## Module - L

### DC Machines



A DC Machine mainly consist of two parts stationary part , rotating part.

- The stationary part produces constant magnetic flux and Rotating part converts mechanical energy into electrical energy.
- The stationary part & rotating part are separated by small air gap.
- The stationary part consist of yoke, main poles along with the pole shoes, Base plate .
- Rotating part consist of Armature coil, commutator, shaft and brushes.

→ Yoke is the outer core of D.C machine and is cylindrical in shape . For small generators it is

makeup of cast iron & for large generators  
makeup of cast steel.

→ Base plate & terminal box are integrated.  
Yoke base plate enables the machine to be placed  
on the ground. The terminal box contains output  
terminals.

→ Main pole + The main poles are madeup of  
steel of high permeability. Poles are fixed to the  
yoke with the help of bolt or welding.

→ Pole shoes + pole shoes are laminated and fixed  
to pole core with screws. It helps to spread  
flux uniformly in the air gap and reduces  
reluctance of the path.

→ Pole coils are connected to pole shoes and  
produces main flux when dc current pass through  
it.

→ Armature + Armature consist of Armature core &  
Armature winding.

Armature core is makeup of silicon steel laminated  
and they are slots & cut uniformly and the slots  
are ferri ferri to place Armature conductor.

The Armature conductors are placed in the slots  
of Armature core forming Armature winding.

→ commutator + commutator converts alternative  
generator in Armature winding into D.C. out.

Shaft : shaft of DC generator is actuated by prime mover. For small generator roller bearings are used at the both end of the shaft and for larger generator roller bearing are used for driving and ball bearings are used at other ends.

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Equation for induced emf [dc generator] :

Let  $P$  = Number of poles of generator

$\phi$  = flux produced by each pole in webers.

$N$  = speed of armature (rpm).

$Z$  = total number of conductors in the slots of armature.

$A$  = Number of parallel paths.

According to Faraday's law of electromagnetic induction

Induced emf = Rate of cutting of magnetic flux.

$$e = \frac{d\phi}{dt} \rightarrow ①$$

Total flux ( $\Phi$ ) = flux produced by Number of each pole  $\times$  poles

$$\text{Total } (\Phi) = \phi \times P \rightarrow ②$$

$$\text{Time required for one revolution} = \frac{60}{N} \rightarrow ③$$

Substitute ② and ③ in ①

$$e = \frac{\Phi \times P}{N} = \frac{\Phi PN}{60} \rightarrow ④$$

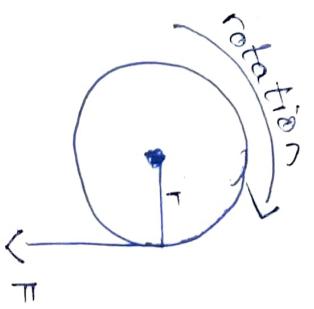
$Z$  conductors are distributed in a parallel path, effectively  $\frac{Z}{A}$  conductors need to be multiplied with emf induced in one conductor.

Total emf induced

$$E = \frac{\Phi PN}{60} \times \frac{Z}{A} \text{ volts.}$$

Torque equation of DC motor:

Torque is turning the point about its axis. It is equal to the product of the force and the radius at which it acts consider the armature of DC motor to have radius  $r$  and  $F$  is the force acting tangentially on it



$$\boxed{\text{Torque} = F \times r} \text{ Nm} \rightarrow ①$$

$$T_a = F \times r \text{ N-m}$$

Work done by the  $F^\circ$  in one revolution

$$W = \text{Force} \times \text{distance moved}$$

$$\omega = F \times 2\pi r \rightarrow ②$$

Total power developed by armature

$$P = \frac{\text{work done}}{\text{time}}$$

$$P = \frac{F \times 2\pi r}{60}$$

$$P = \boxed{F \times r \times 2\pi N}$$

\* The power in armature is equal to power at output

$$E_b \times I_a = \frac{T_a \times 2\pi N}{60}$$

$$\frac{\Phi P M z}{60 A} \times I_a = \frac{T_a \times 2\pi N}{60}$$

$$T_a = \frac{1}{2\pi} \frac{\Phi P I_a Z}{A}$$

$$\boxed{T_a = 0.159 \times P I_a \frac{Z}{A} N m}$$

$$\frac{1}{2} \left( \frac{\alpha^2}{\beta} \right) \frac{V}{\frac{\alpha \omega}{\beta}} = \frac{\pi}{\alpha \beta}$$

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of  
Type of  
dc machines based on excitation.

- ① Separately excited dc machine

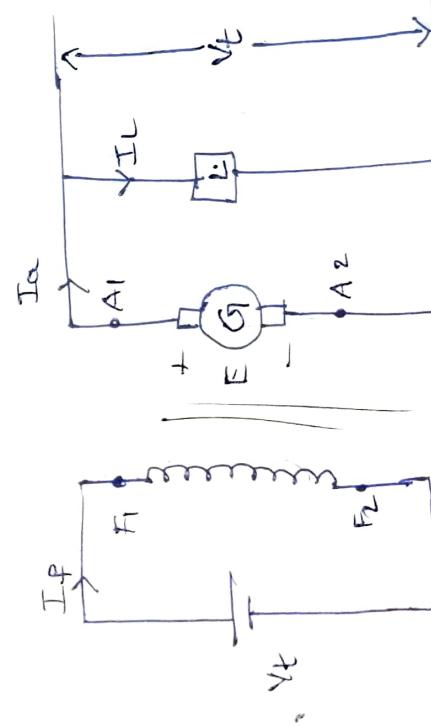
- ② Self excited dc machine

Self excited dc machine : Generated emf is due to residual magnetism of the machine.  
\* Separate dc supply is used to excite the field circuit in separately excited dc machine.

Types of DC generator based on excitation

- ① separately excited dc generator
  - shunt generator
  - series generator
  - compound generator
- ② self excited dc generator
  - short-shunt generator
  - long-shunt generator

Separately excited dc generator :-



$I_a = I_t$       ;  
Current and Voltage relationship.

$$E = I_a R_a + V_t$$

$$\begin{cases} E = I_a R_a + V_t \\ E = I_a R_a - V_t \end{cases}$$

where  $E$  = induced emf  $E = \frac{\phi Z P N}{60 \pi}$

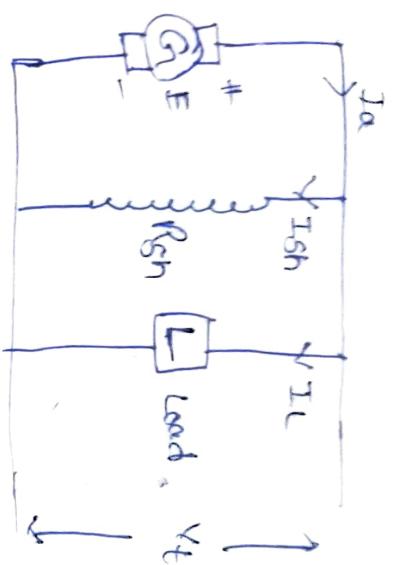
$I_a$  = armature current

$R_a$  = internal resistance of armature

$V_t$  = terminal voltage.

(2) Short generator:

self generated generator:



In short generator field winding is parallel with armature winding.

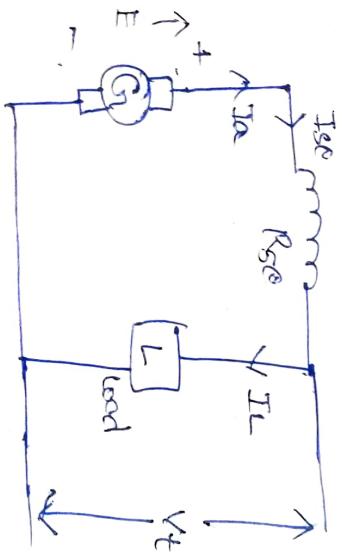
current and voltage relationship.

$$I_a = I_{sh} + I_L$$

$$\cancel{E - I_a R_a - V_t = 0}$$

$$\boxed{E = I_a R_a + V_t}$$

3) series generator:



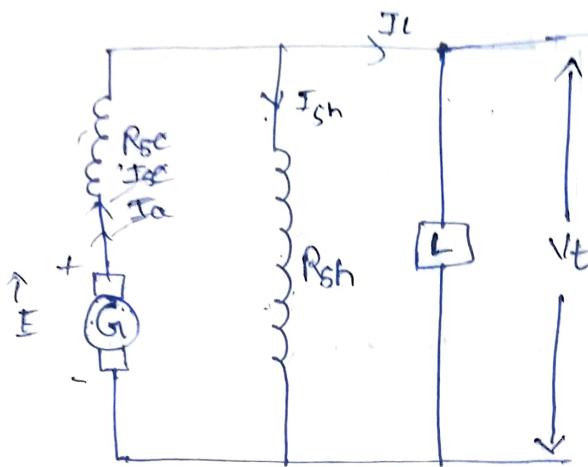
$$I_a = I_{se} = I_L$$

$$E - I_a R_a - I_{se} R_{se} - V_t = 0 \quad \textcircled{1}$$

$$\boxed{E = I_a R_a + I_{se} R_{se} + V_t}$$

## Compound generator +

### i) Long shunt generator:



long shunt compound generator here shunt field winding is connected in parallel with both series field winding and armature winding.

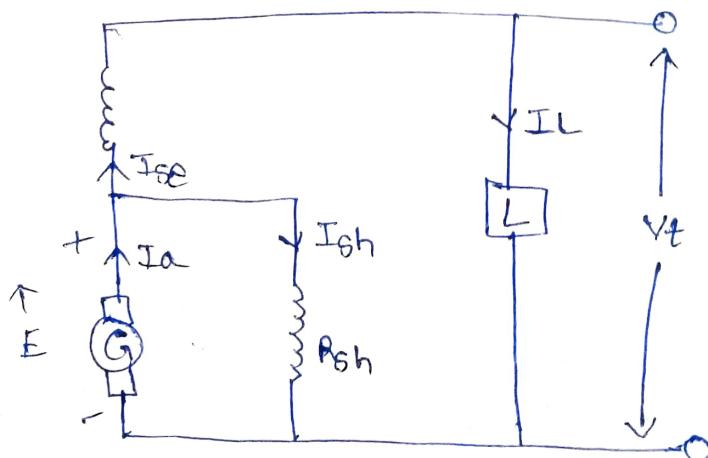
$$I_a = I_{se}$$

$$I_a = I_{sh} + I_L$$

$$E - I_a R_a - I_{se} R_{se} - V_t = 0$$

$$\therefore E = I_a R_a + I_{se} R_{se} + V_t$$

### ii) short shunt compound generator:



$$I_a = I_{so} + I_{sh}$$

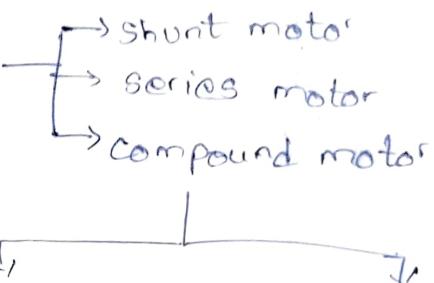
$$E = I_a R_a + I_{so} R_{so} + V_t$$

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## Types of dc motors based on excitation

### ① separately excited dc motor

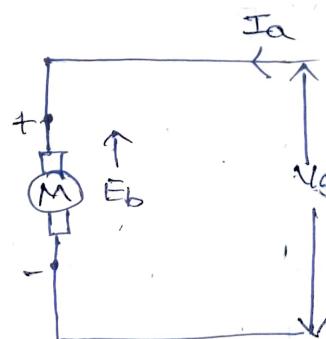
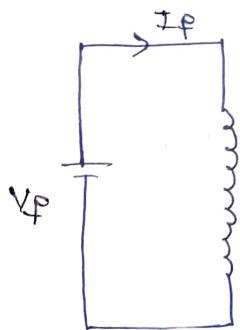
### ② self excited dc motor



long shunt

short shunt

### ③ separately excited dc motor

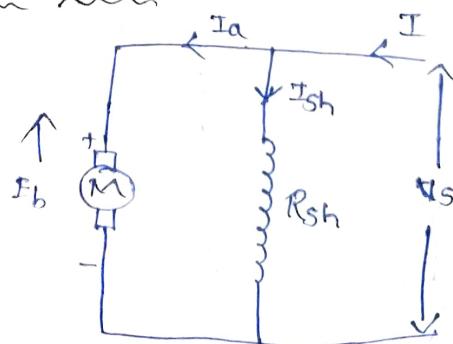


$$V_s - I_a R_a - E_b = 0$$

$$V_s = I_a R_a + E_b$$

### ④ Self excited dc motor

### ⑤ Shunt motor



$$V_s - I_a R_a - E_b = 0$$

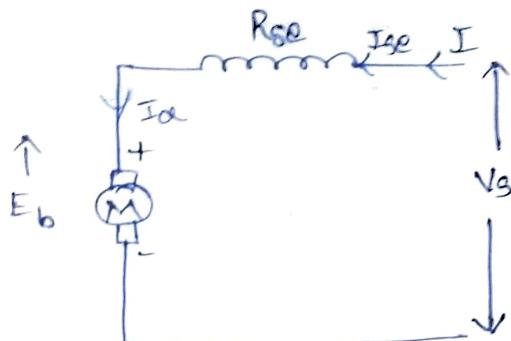
$$V_s = I_a R_a + E_b$$

$$I = I_a + I_{sh}$$

$$V_s - I_a R_a - E_b = 0$$

$$V_s = I_a R_a + E_b$$

### 2) series motor :



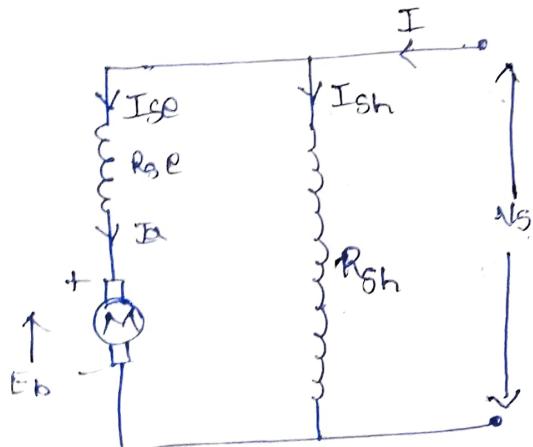
$$I_a = I = I_{se}$$

$$V_s - I_{se} R_{se} - I_a R_a - E_b = 0$$

$$V_s = I_a (R_{se} + R_a) + E_b$$

### ③ compound motor :

#### i) long-shunt motor :



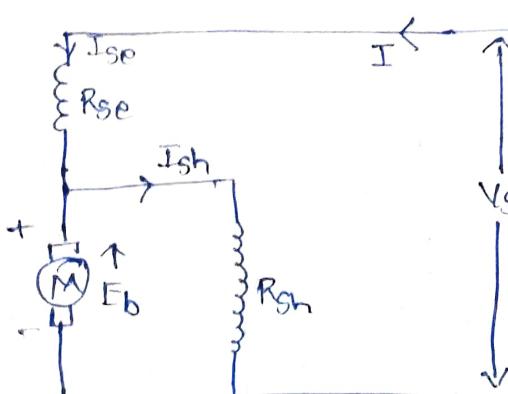
$$I = I_{se} + I_{sh}$$

$$I_{se} = I_a$$

$$V_s - I_{se} R_{se} - I_a R_a - E_b = 0$$

$$V_s = I_{se} R_{se} + I_a R_a + E_b$$

#### ii) short-shunt motor :



$$I = I_{se}$$

$$I_{se} = I_a + I_{sh}$$

$$V_s - I_{se} R_{se} - I_a R_a - E_b = 0$$

$$V_s = I_{se} R_{se} + I_a R_a + E_b$$

## Performance characteristics of DC machines

The speed of DC machine operated as a generator is operated by fixed prime mover. The generated performance deals primarily with relation among excitation, terminal voltage. The relation can be executed graphically by mean of curves is known as DC generator characteristics. The characteristic can be describe based on behaviour of generator under different load condition.

## DC generator characteristics

They are three important characteristics

- 1) open circuit characteristics (OCC)
- 2) load characteristics
  - Internal characteristics
  - External characteristics

## Separately excited DC machine

### 1) open circuit characteristics [OCC]

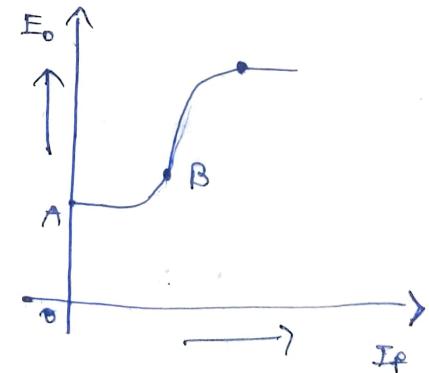
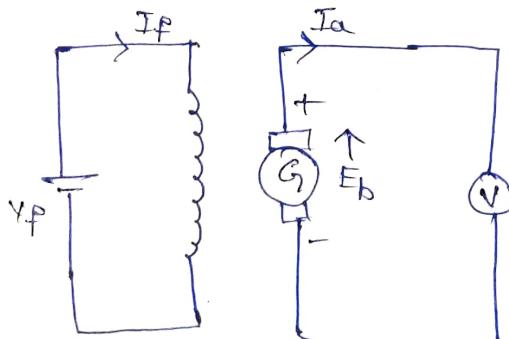


Fig: OCC characteristics of Separately excited DC generator

## Observation:

- ① When field current is zero some emf  $E_0$  is generated due to residual magnetism in the field poles.
- ② upto point B in the curve the relationship b/w  $I_f$  &  $E_f$  is linear because reluctance of iron is negligible.
- ③ After point B on the curve the reluctance of iron comes into the picture then curve deviates from linear relationship.
- ④ After point C, the magnetic saturation of pole begin &  $E_f$ .

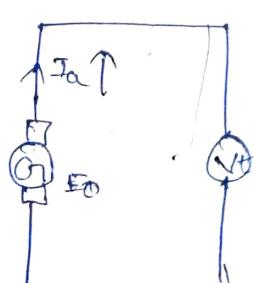
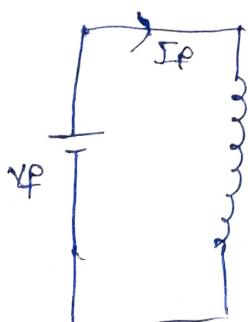
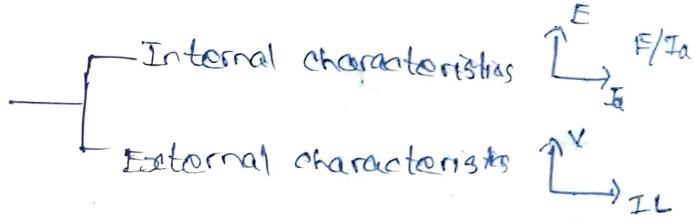
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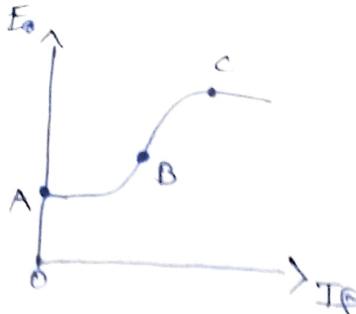
Performance characteristics of Separately excited DC generator

1) Open circuit characteristics [occ] No load

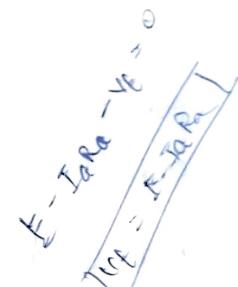
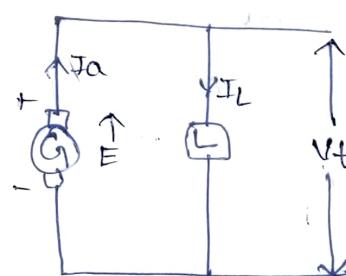
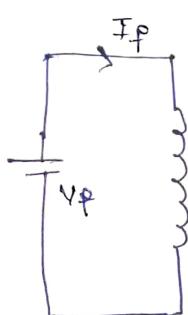
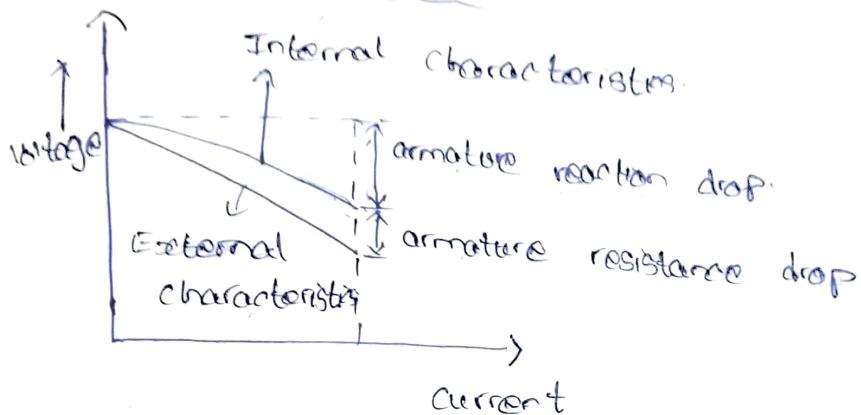


2) Load characteristic





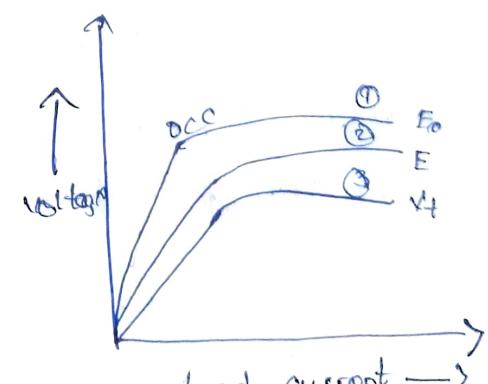
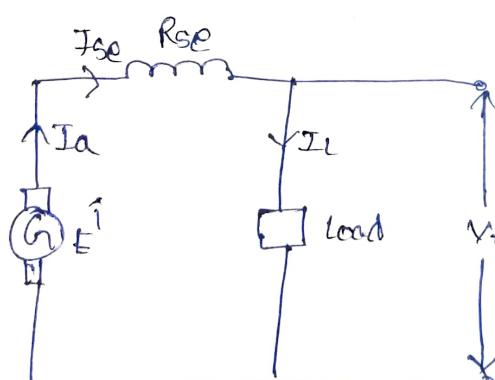
## Load characteristics



$$I_a = I_L$$

$$V_L = E - I_a R_a$$

## Performance characteristics of series generator +



$$I_a = I_{sgo} = I_L$$

$$E_o > E > V_L$$

curve ① — OCC chara  
 curve ② — Internal chara  
 curve ③ — External chara

## ① O.C.C.

Curve we draw the open circuit characteristics of series generator. It can be obtained easily by disconnecting field winding from the machine & exciting from separate DC source.

### ② internal characteristic :

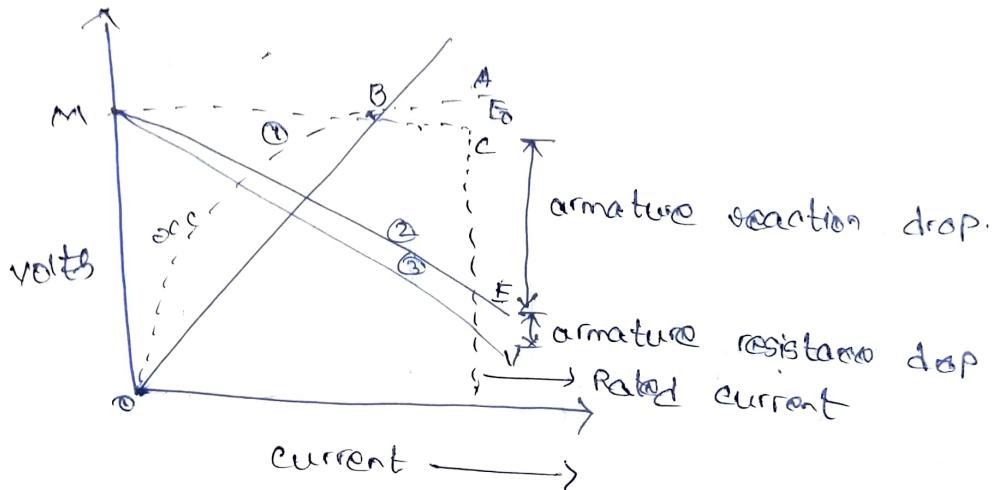
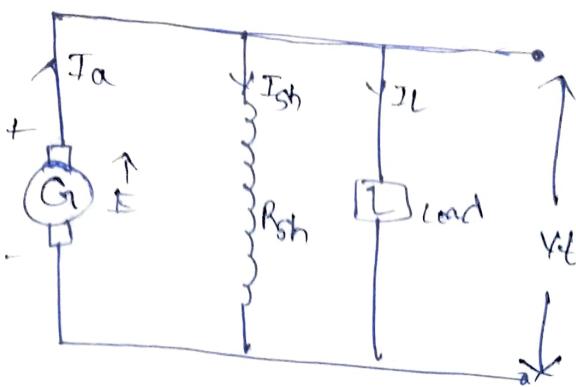
curve two shows internal characteristics of series generator. It gives relationship b/w generated emf E on load & armature current I. Due to armature reaction, the flux in the machine will be less than at no load. Hence the open generator under no load generator  $E_0$  is greater than  $E_{no load}$ . Consequently the internal characteristics curve lies below the curve, the difference b/w them representing the effect of armature reaction.

### ③ External characteristics:

curve three shows external characteristics of series generator. It gives the relationship b/w terminal voltage  $V_t$  & load current  $I_L$ . Therefore the external characteristics curve will lie below internal characteristics curve.

$$\boxed{V_t = E - I_a (R_a + R_{ap})}$$

## Performance characteristics of small generators



- ① OCC characteristics.
- ② internal characteristics.
- ③ external characteristics
- ④ OCC characteristics.

The line OA represent shunt field resistance. When the generator is run at normal speed, it build up the voltage (Emf) at no load.

## 2) Internal characteristic

When the generator is loaded, flux per pole is reduced due to armature reaction. Therefore Emf in generator on load is less than Emf generated at no load.

## 3) External

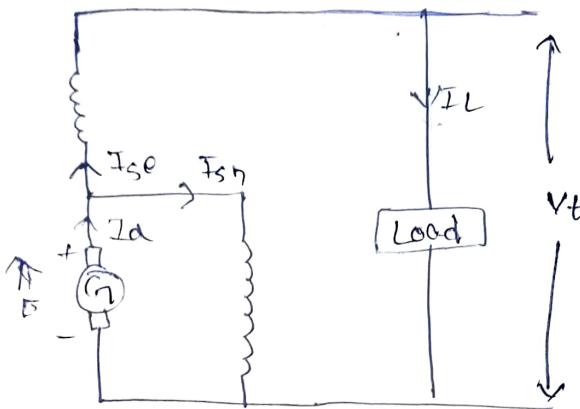
CURVE 3 show the external characteristics of Shunt generator

$$V_t = E - I_a R_a$$

Therefore external characteristic will lie below the internal characteristic because  $V_t < E$

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Performance characteristic of compound generator:



In compound generator, the shunt winding can be connected either across armature or across armature & series field. It may be noted that external characteristic of long shunt & shunt generator are almost identical.

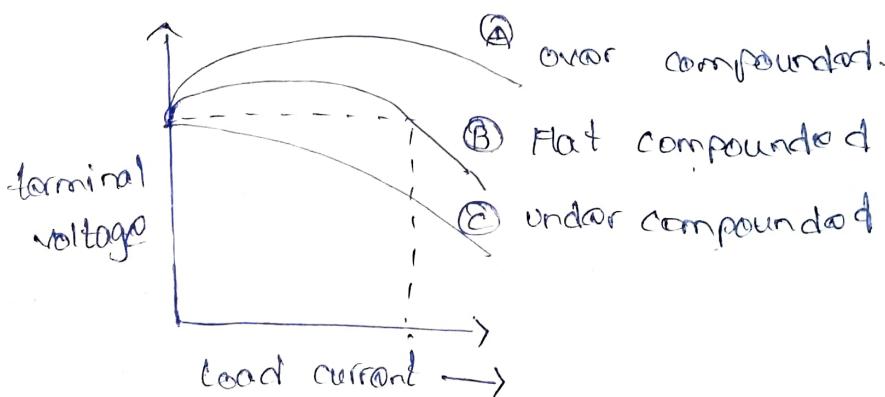


Figure shows external characteristic of compound generator. The series excitation aids the shunt excitation. The degree of compounding depends upon series

operation with increasing load current.

### 1) flat over compounded:

If series winding turns are adjusted such that with the increase in load current, the terminal voltage increases and it is called over compounded generator. As load current increases flux in the machine also increases & hence generator voltage also increases. The increasing generator voltage is greater than 'Fara drop' so that instead of decreasing, the terminal voltage increases as shown by curve (A) in the figure.

### 2) flat compounded

If series winding turns are adjusted such that with the increase in load current, the terminal voltage remains constant and it is called flat compounded generator. The series winding such a generator has lesser no. of turns than in over compounded machine & therefore flux is not increased for the given - load current. It is shown by curve (B) in the figure.

### 3) under compounded

If the series winding has lesser no. of turns than that of flat compounded machine, then terminal voltage falls with increasing load current as indicated by curve (C).

# ~~Date~~ Date Topic

## Performance characteristics of dc motor

The performance of dc motor can judge from its characteristics curves known as motor characteristics.

### i) Torque & armature current characteristic [T<sub>a</sub>/I<sub>a</sub>]

It is the curve between armature torque (torque produced by armature current  $I_a$ ) of dc motor. It is also known as electrical characteristics of dc motor.

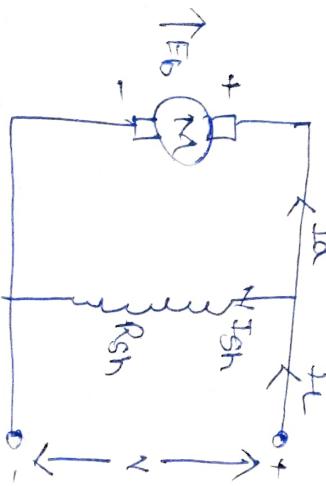
### ii) Speed & armature current characteristic [N/I<sub>a</sub>]

It is the curve between speed ( $N$ ) & armature current ( $I_a$ ). It is very important characteristic which serves as deciding factor for the selection of motor for

### iii) speed and torque characteristic [N/T<sub>a</sub>]

It is the curve between speed ( $N$ ) & armature torque ( $T_a$ ). It is also known as mechanical characteristics of dc motor.

## Characteristics of shunt motor

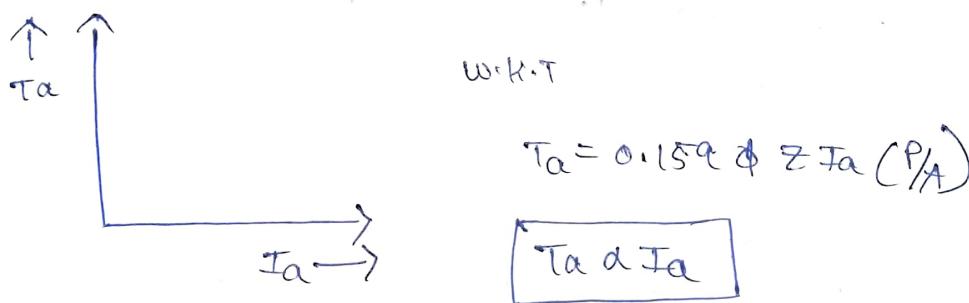


$$V = E_b + I_a R_a$$

$$V > E_b$$

Figure shows the connection of shunt motor. The field current  $I_{fsh}$  is constant since the field winding is directly connected to supply which is assumed directly constant. Hence the flux in the motor is approximately constant.

1) Torque & armature current of shunt motor:



since the motor is operating from the constant supply, flux  $\phi$  is almost constant. Hence  $T_a$  curve is straight line passing through origin.

2) speed & armature current characteristic [N/I\_a]:

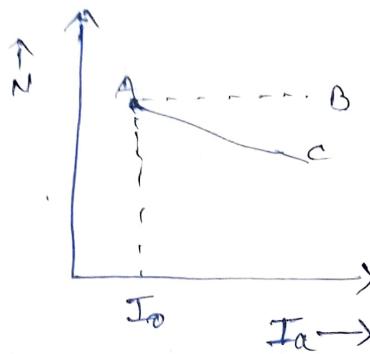
The speed of the motor is given by  $N \propto \frac{E_b}{\phi}$

The flux of & back emf in shunt motor

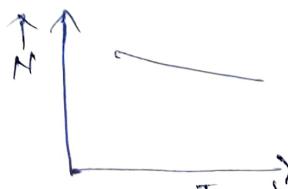
is almost constant under normal conditions.

Therefore speed of the shunt motor remains constant as armature current varies indicated by line AB in fig. when load is increased,  $E_b = V - I_a R_a$  & it decreases due to armature resistance & reaction drop. However  $E_b$  decreases

slipping slightly more than  $\phi$  so that speed of motor also decreases indicated by line  $n_2$  in fig.



iii) speed & armature torque =  $(n/T_a)$



It may be observed from the curve that speed decreases as low torque increases.

Characteristics of series motor :-

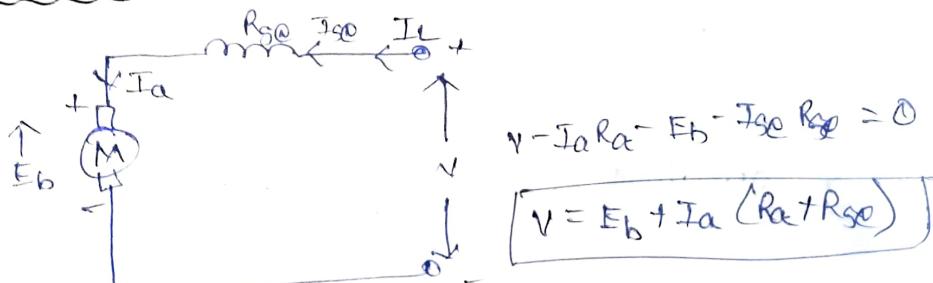


Figure shows the connection of series motor rot. that the current passing through field winding is same as that of in armature.

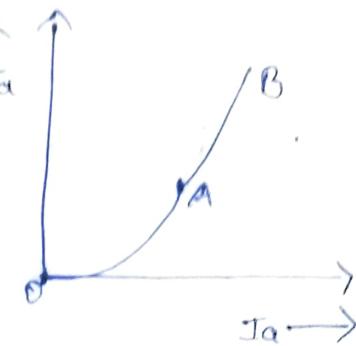
If mechanical load on the motor increase, armature current also increases, Hence flux in series motor increases with increasing in the armature current.

i) Torque and current ( $T_a/I_a$ ):

$$T_a \propto I_a \quad [T_a \propto I_a]$$

Upto magnetic saturation

$$[T_a \propto I_a^2]$$



After magnetic saturation

$$\alpha \text{ is constant} \quad [T_a \propto I_a]$$

upto magnetic saturation

Therefore  $T_a/I_a$  curve is parabola upto saturation

point OA in the fig. After magnetic saturation

Torque is directly proportional to armature current.

Hence  $T_a/I_a$  is straight line after saturation point

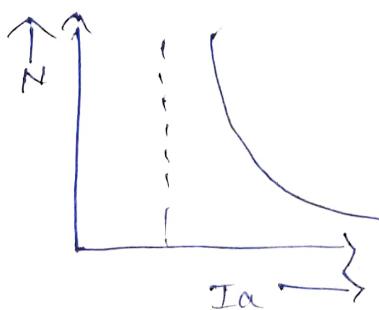
i.e. line AB in the figure.

ii) speed & current characteristic ( $N/I_a$ ):

$$[N \propto \frac{E_b}{\phi}]$$

when armature current increases, the back emf  $E_b$  decreases due to  $I_a(R_{so} + R_a)$  drop, while magnetic flux  $\phi$  increases. The drop  $I_a R_{so} + R_a$  is small & it can be neglected

$$[N \propto \frac{1}{\phi}]$$

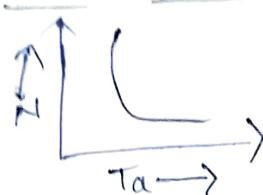


Upto magnetic saturation  $N/I_a$  curve follows

hyperbolic path as shown in the figure. After

Saturation of air gap remains constant & so does the speed also does the same.

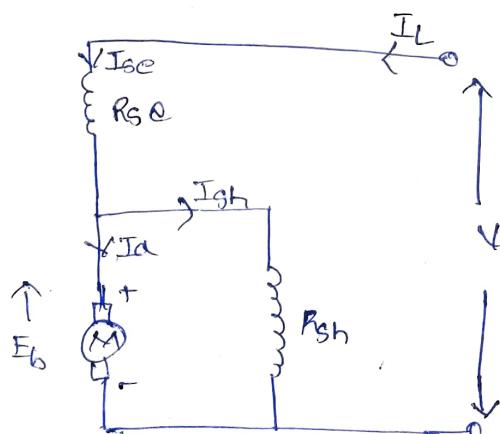
iii) speed & torque characteristic :  $(N/T_a)$  :



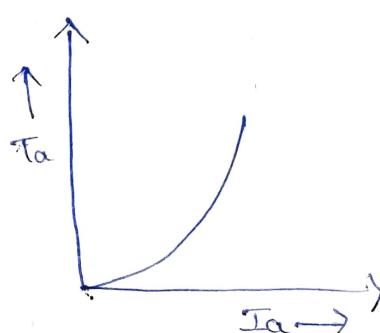
It is clear from the figure that the motor develops high Torque at low speed & vice versa. It is because an increase in torque requires increasing in armature current, which is also the field current. The result is flux is strength and speed drops.

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Performance characteristics of cumulative compound motor :

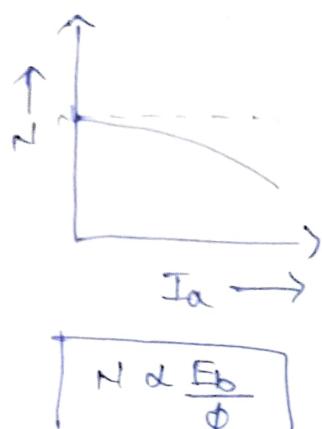


iv)  $T_a/I_a$  characteristic :

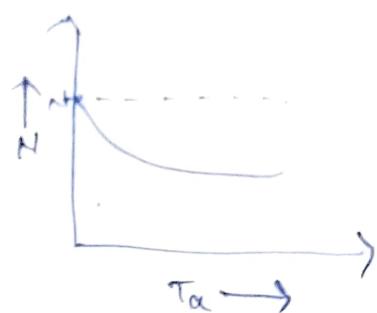


$T_a \propto I_a$

i)  $N/I_a$  characteristic :



ii)  $N/T_a$  characteristic



Losses in dc machines :-

- i) copper loss
- ii) iron or core losses
- iii) mechanical losses

i) Copper Loss :-

This loss is due to resistance present in the field winding & armature winding.

a) copper loss produced in armature due to armature resistance & armature current is given by  $I_a^2 R_a$ .

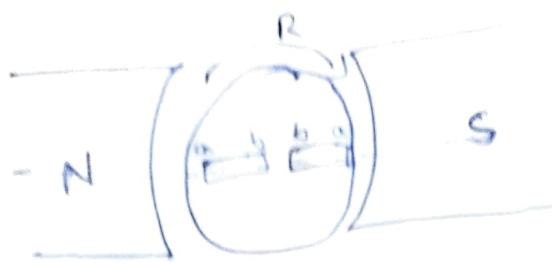
b) copper loss produced in shunt field winding is  $I_{sh}^2 R_{sh}$ .

c) copper loss produced in series winding is  $I_{sc}^2 R_{so}$ .

ii) Iron losses :-

- a) Hysteresis loss
- b) Eddy current loss

a) Hysteresis loss +



Hysteresis loss occur in the armature of a machine since any given part of armature is subjected to magnetic field reversal as it passes under successive poles. In order to generate continuous the molecular magnet in armature requires some amount of power to be spent it is called Hysteresis loss.

$$P_h = \eta B_{\text{max}}^{116} f V \text{ Watts}$$

where  $P_h$  - hysteresis loss

$B_{\text{max}}$  - maximum flux density in armature.

$f$  - Frequency of magnetic reversal.

$V$  - Volume of core in  $\text{m}^3$ .

$\eta$  - Steinmetz hysteresis coefficient.

By

In order to reduce hysteresis loss, armature core is made up of such material which have low value of hysteresis coefficient.

Eg's silicon steel.

## b) Eddy current loss :

when armature rotates in the magnetic field an emf is induced which circulates current in the armature. The power loss due to this current is called Eddy current loss.

$$P_e = K_a B_{max}^2 f^2 t^2 V \text{ watts}$$

where  $K_a$  - constant

$B_{max}$  - maximum flux density in armature

$f$  - frequency of magnetic reversal.

$t^2$  - thickness of lamination

$V$  - volume of core in  $m^3$ .

These losses can be reduced by building armature core by thin laminations insulated from each other.

## iii) Mechanical losses :

- a) frictional loss : Eg: bearing friction, brush friction
- b) windage loss : Eg: air friction of rotating armature

## Constant and variable losses :

Constant losses are the losses which remain constant at all nodes.

Eg: 1) Iron ~~loss~~

- 2) mechanical loss
- 3) shunt field loss