

State-Space Analysis

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Linear Systems

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The desired transfer function:

$$g(s) = \frac{-2.5(s^2 + 8s + 15)}{(s - 0.4)(s - 0.5)(s^2 - 10s + 29)}$$

$$= \frac{-2.5s^2 - 20s - 37.5}{s^4 - 10.9s^3 + 38.2s^2 - 28.1s + 5.8}$$

$$g(s) = \frac{b(s)}{a(s)} = \frac{b_{n-1}s^{n-1} + b_{n-2}s^{n-2} + \dots + b_0}{s^n + a_{n-1}s^{n-1} + \dots + a_0}$$

$$\Rightarrow \begin{cases} a_3 = -10.9 \\ a_2 = 38.2 \\ a_1 = -28.1 \\ a_0 = 5.8 \end{cases}$$

$$\Rightarrow \begin{cases} b_3 = 0 \\ b_2 = -2.5 \\ b_1 = -20 \\ b_0 = -37.5 \end{cases}$$

Obtaining the state-space using MATLAB:

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$y(t) = Cx(t) + Du(t)$$

Codes:

```
>> a=conv([-2.5],[1 8 15]);
b=conv([1 -0.9 0.2],[1 -10 29]);
g1=tf(a,b);
[A,B,C,D]=tf2ss(a,b);
g1 =
```

-2.5 s^2 - 20 s - 37.5

s^4 - 10.9 s^3 + 38.2 s^2 - 28.1 s + 5.8

A =

```
10.9000 -38.2000 28.1000 -5.8000
1.0000 0 0 0
0 1.0000 0 0
0 0 1.0000 0
```

B =

1
0
0
0

C =

0 -2.5000 -20.0000 -37.5000

D =

0

Section A: State Feedback Linear Control Systems: Regulator Design

1. Minimal State-Space Realization and Analysis of Controllability, Stability, and Open-Loop Response (if stable)

Controllability:

The minimal realization of the state-space transformation is achieved when it is both controllable and observable.

Approach 1: Utilize the `ctrb` command to obtain the controllability matrix. If the matrix is full rank, controllability is achieved.

Codes:

```
Co=ctrb(A,B)
rankCo=rank(Co)
```

Co =

```
1.0000 10.9000 80.6100 490.3690
0 1.0000 10.9000 80.6100
0 0 1.0000 10.9000
0 0 0 1.0000
```

rankCo =

4

➔ It is observed that since the rank of the matrix is complete, this realization is controllable.

Approach 2: Another method is to obtain the canonical controller realization of the transformation function, which is always controllable. Then, the controllability matrix can be examined, and if its rank is complete, it indicates controllability.

Canonical Controller Realization:

The matrix form of it is as follows ->

$$\dot{x}(t) = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \cdots & 0 \\ \vdots & & & & \\ 0 & 0 & 0 & \cdots & 1 \\ -a_0 & -a_1 & -a_2 & \cdots & -a_{n-1} \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} u(t)$$

$$y(t) = [b_0 \quad b_1 \quad b_2 \quad \cdots \quad b_{n-1}] x(t)$$

$$\Phi_{cc} = [b_c \quad A_c b_c \quad \dots \quad A_c^{n-1} b_c]$$

As a result, we have:

```
>> A=[0 1 0 0;0 0 1 0;0 0 0 1;-5.8 28.1 -38.2 10.9];
B=[0;0;0;1];
C=[-37.5 -20 -2.5 0];
D=[0;0;0;0];
>> A
```

A =

```
    0    1.0000    0    0
    0    0    1.0000    0
    0    0    0    1.0000
-5.8000 28.1000 -38.2000 10.9000
```

```
>> B
```

B =

```
    0
    0
    0
    1
```

```
>> C
```

C =

```
-37.5000 -20.0000 -2.5000    0
```

```
>> D
```

D =

```
    0
    0
    0
    0
```

```
phicc=[B,A*B,(A^2)*B,(A^3)*B];
```

```
rankphicc=rank(phicc)
```

```
rankphicc =
```

```
4
```

→ It is evident that since the rank of the matrix is complete, this realization is controllable.

Stability:

The system is stable if all the eigenvalues of matrix A are negative, i.e.:

```
>> eig_A=eig(A)
```

```
eig_A =
```

```
5.0000 + 2.0000i
```

```
5.0000 - 2.0000i
```

```
0.5000 + 0.0000i
```

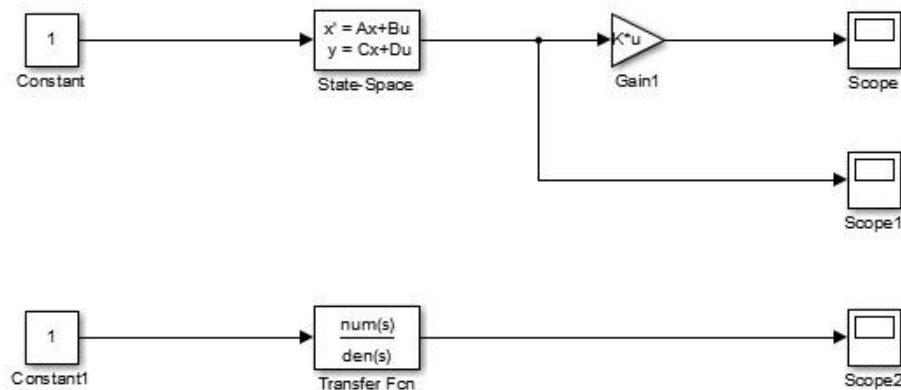
```
0.4000 + 0.0000i
```

→ Because the eigenvalues are positive, the system is unstable.

In the case of stability, the open-loop response is as follows:

The system is unstable.

In the simulation section, we have:

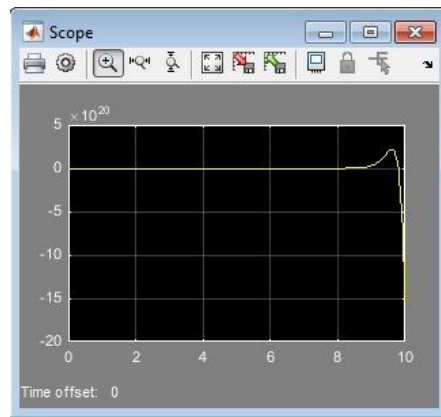


Settings:

State Space	
State-space model: $\frac{dx}{dt} = Ax + Bu$ $y = Cx + Du$	
Parameters	
A:	[10.9 -38.2 28.1 -5.8; 1 0 0 0; 0 1 0 0; 0 0 1 0]
B:	[1; 0; 0; 0]
C:	[0 -2.5 -20 -37.5]
D:	0

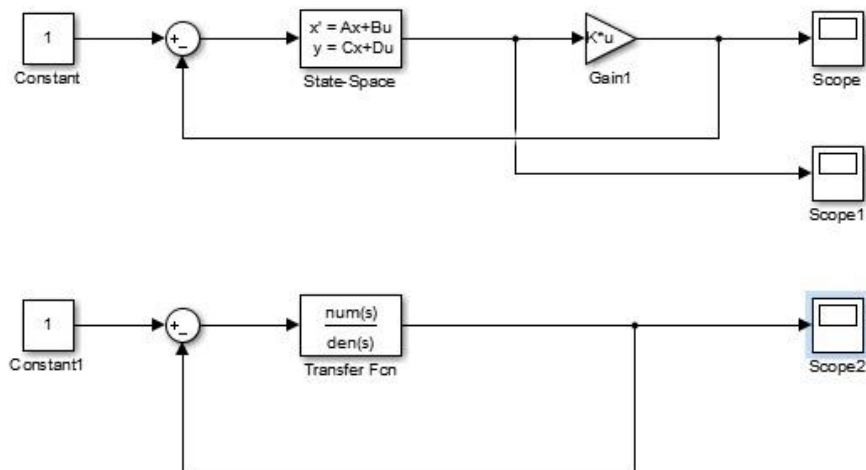
Function Block Parameters: Transfer Fcn	
Transfer Fcn	
The numerator coefficient can be a vector or n denominator coefficient must be a vector. The number of rows in the numerator coefficient. Y coefficients in descending order of powers of s	
Parameters	
Numerator coefficients:	[-2.5 -20 -37.5]
Denominator coefficients:	[1 -10.9 38.2 -28.1 5.8]

Input:

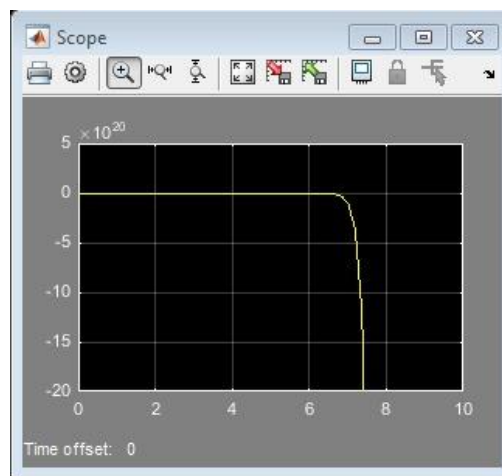


→ We observe that the system is unstable.

2. The closed-loop behaviour of the system (unity feedback)



Input:



→ We observe that the system is unstable again.

3&4. State Feedback Gain for Two Categories of Fast and Slow Poles Using 3 Methods and Analyzing the Closed-Loop Response, etc.

Slow Poles:

Bass-Gura Method:

$$a = [a_{n-1} \ a_{n-2} \ \dots \ a_0] = [-10.9 \ 38.2 \ -28.1 \ 5.8]$$

$$\psi = \begin{bmatrix} 1 & a_3 & a_2 & a_1 \\ 0 & 1 & a_3 & a_2 \\ 0 & 0 & 1 & a_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 - 10.9 & 38.2 - 28.1 \\ 0 & 1 - 10.9 & 38.2 \\ 0 & 0 & 1 - 10.9 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

If we consider the closed-loop poles to be from -1 to -4:

$$\alpha(s) = (s + 1)(s + 2)(s + 3)(s + 4) = s^4 + 10s^3 + 35s^2 + 50s + 24$$

$$\Rightarrow \alpha = [10 \ 35 \ 50 \ 24]$$

Then, with the following commands, we can obtain (k) using the [Bass-Gura method](#):

```
>> a=conv([-2.5],[1 8 15]);  
b=conv([1 -0.9 0.2],[1 -10 29]);  
g1=tf(a,b);  
[A,B,C,D] =tf2ss(a,b);  
a=[-10.9 38.2 -28.1 5.8];  
sai=[1 -10.9 38.2 -28.1;0 1 -10.9 38.2;0 0 1 -10.9;0 0 0 1];  
phic=[B,A*B,(A^2)*B,(A^3)*B];  
alpha=[10 35 50 24];  
k1=(alpha-a)*(inv(sai))*(inv(phic))
```

k1 =

20.9000 -3.2000 78.1000 18.2000

[Ackermann's Method](#):

We can obtain (k) using the acker command:

```
k2=acker(A,B,[-1 -2 -3 -4])  
k2 =
```

18.2000 78.1000 -3.2000 20.9000

[Canonical Controller Realization Method](#):

We can obtain (k) using the canonical controller realization method:

$$k = \alpha - a \Rightarrow$$

```
k_3=alpha-a;
k3=zeros(1,4);
for i=1:4
    k3(1,i)=k_3(1,5-i);
end
k3;
eig1=eig(A-B*k1);
>> eig1

eig1 =

    -4.0000
    -3.0000
    -2.0000
    -1.0000
k3 =

20.9000  3.2000- 78.1000  18.2000
k_3 =

18.2000  78.1000  3.2000- 20.9000
```

For fast poles:

If we consider the closed-loop poles to be from -20 to -23:

$$\begin{aligned}\alpha(s) &= (s + 20)(s + 21)(s + 22)(s + 23) \\ &= s^4 + 86s^3 + 2771s^2 + 39646s + 212520\end{aligned}$$

We have:

Bass-Gura method:

```
a=conv([-2.5],[1 8 15]);
b=conv([1 -0.9 0.2],[1 -10 29]);
g1=tf(a,b);
[A,B,C,D]=tf2ss(a,b);
a=[-10.9 38.2 -28.1 5.8];
sai=[1 -10.9 38.2 -28.1;0 1 -10.9 38.2;0 0 1 -10.9;0 0 0 1];
phic=[B,A*B,(A^2)*B,(A^3)*B];
alpha=[86 2771 39646 212520];
k1=(alpha-a)*(inv(sai))*(inv(phic))
k1 =

1.0e+05 *

    0.0010    0.0273    0.3967    2.1251
```


Ackermann's Method:

```
K2=acker(A,B,[-20 -21 -22 -23])  
k2 =
```

```
1.0e+05 *
```

```
2.1251  0.3967  0.0273  0.0010
```

Canonical Controller Realization Method:

```
k3=zeros(1,4);  
for i=1:4  
    k3(1,i)=k_3(1,5-i);  
end  
k3;  
eig1=eig(A-B*k1);  
>> k_3
```

```
k_3 =
```

```
1.0e+05 *
```

```
0.0010  0.0273  0.3967  2.1251
```

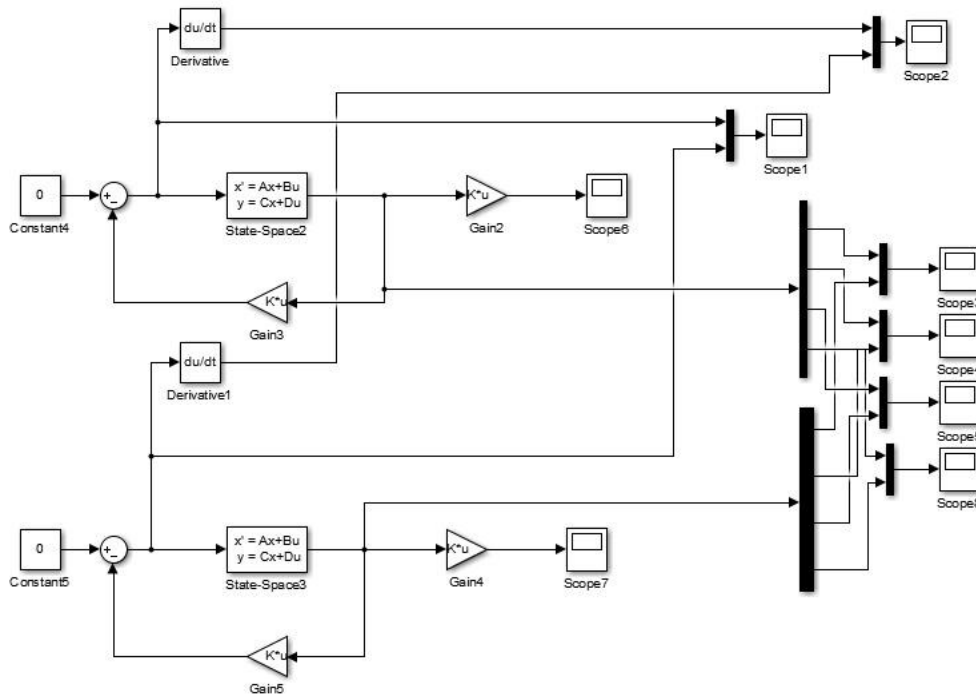
```
>> eig1
```

```
eig1 =
```

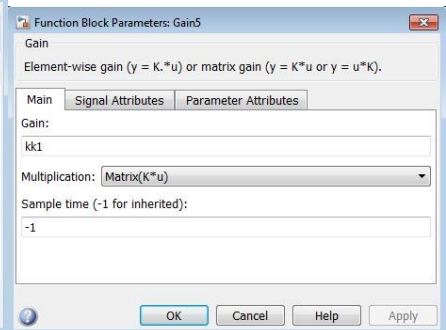
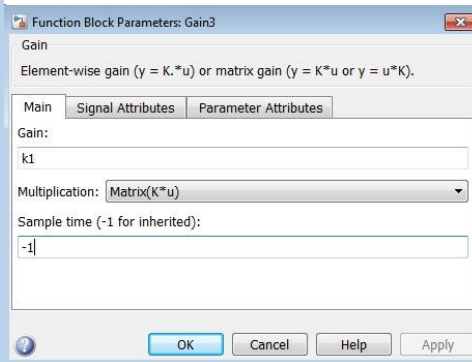
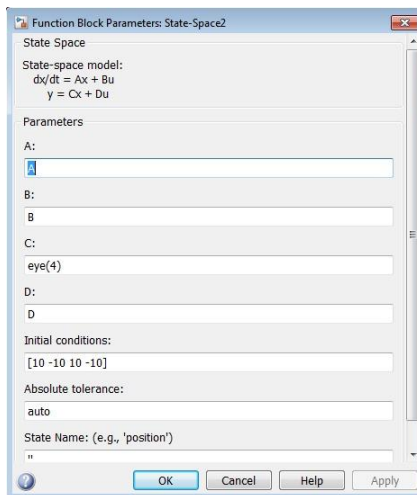
```
-23.0000  
-22.0000  
-21.0000  
- 20.0000
```

➔ It is observed that they have become stable.

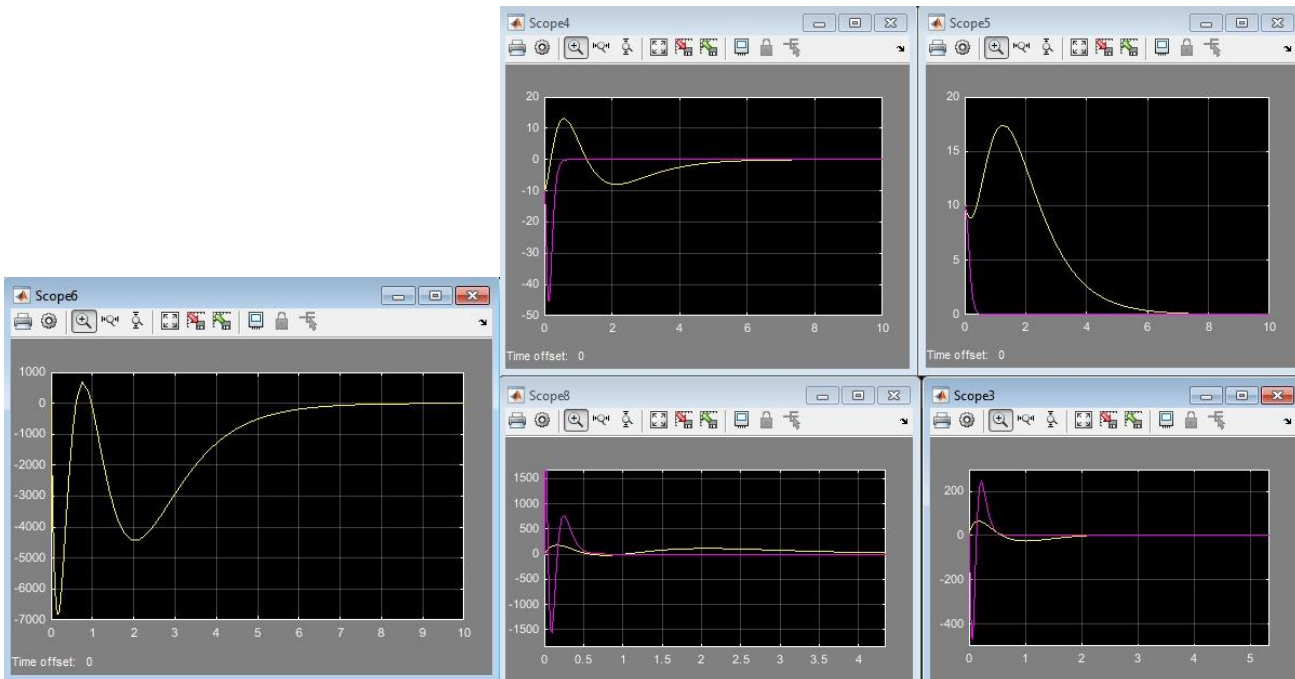
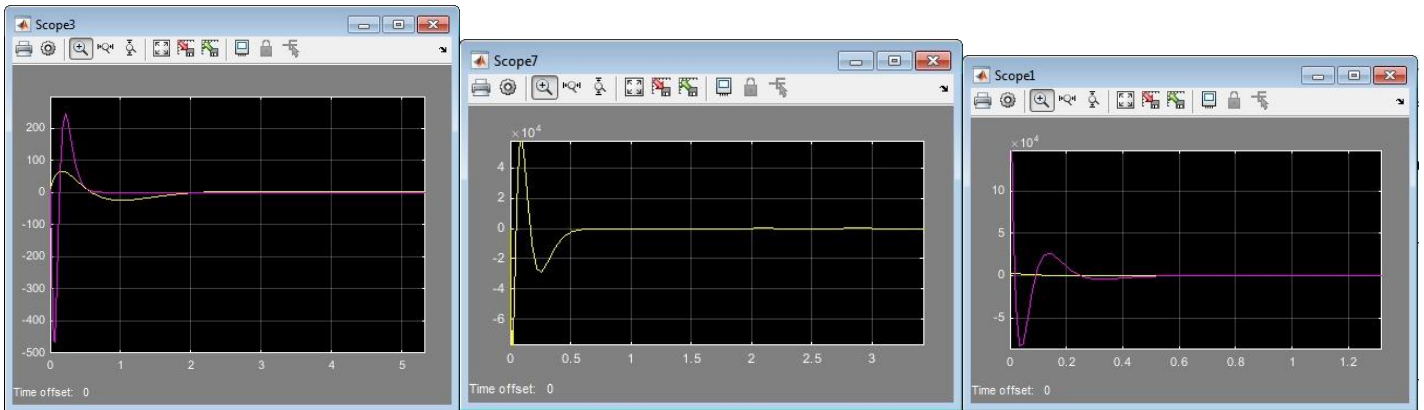
In the simulation section, we have:



Settings:



Outputs:



Scope 6: Output for Slow Pole

Scope 7: Output for Fast Pole

Scopes 3, 4, 5, 8: Comparison of States 1 to 4

Scope 1: Comparison of Command Signal

Scope 2: Comparison of Command Signal Derivative

➔ Result: It is observed that stabilization has been achieved, and the convergence of fast pole graphs is faster than that of slow poles.

5. Transforming the system into a system with two inputs and calculating the state feedback matrix, etc.

```
>> A=[0 1 0 0;0 0 1 0;0 0 0 1;-5.8 28.1 -38.2 10.9];
BB=[0 1;0 0;0 0;1 0];
DD=[0 0;0 0;0 0;0 0];
PHIC=[BB,A*BB,(A^2)*BB,(A^3)*BB];
F=[-1 0 0 0;0 -2 0 0;0 0 -3 0;0 0 0 -4];
Kbar1=[1 1 0 0;0 0 1 1];
Kbar2=[1 1 1 0;0 0 1 1];
phio1=[Kbar1;Kbar1*F;Kbar1*(F^2);Kbar1*(F^3)];
phio2=[Kbar2;Kbar2*F;Kbar2*(F^2);Kbar2*(F^3)];
rankphio1=rank(phio1);
rankphio2=rank(phio2);
T1=lyap(A,-F,-BB*Kbar1);
T2=lyap(A,-F,-BB*Kbar2);
K1=Kbar1*inv(T1);
K2=Kbar2*inv(T2);
eig1=eig(A-BB*K1);
eig2=eig(A-BB*K2);
>> rankphio1
```

rankphio1 =

4

rankphio2 =

4

```
>> K1
```

K1 =

```
-5.8899  38.1171 -21.0171  18.9760
 1.9240  53.5661  76.9821  25.3400
```

```
>> K2
```

K2 =

```
-6.1131  43.1238 -13.1163  21.6467
-0.7467 113.4745 171.5185  57.2973
```

```
>> eig1
```

eig1 =

```
-4.0000
-3.0000
-2.0000
-1.0000
```

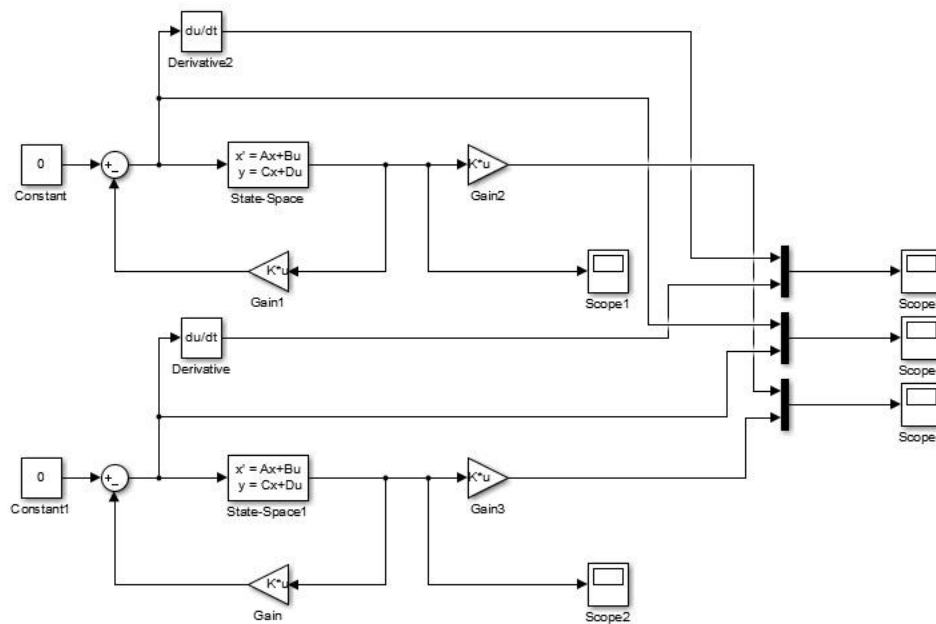
```
>> eig2
```

eig2 =

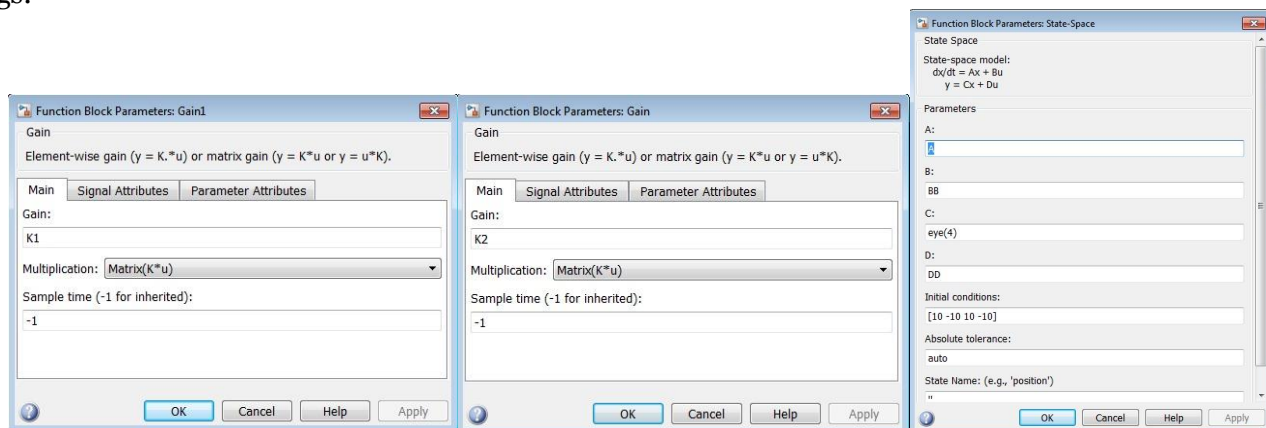
-4.0000
-3.0000
-2.0000
-1.0000

→ The rank of matrices Φ_{i1} and Φ_{i2} is complete so we can use matrices $kbar$ and F .

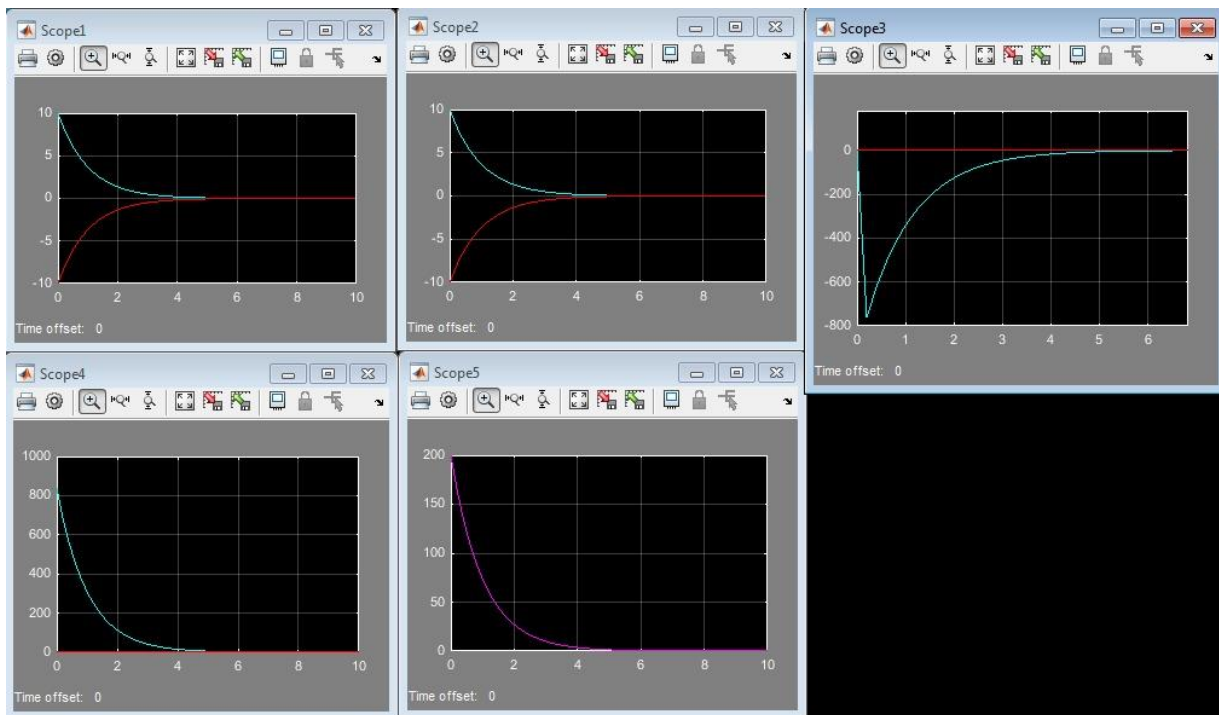
In the simulation section, we have:



Settings:



Outputs:



Scope 1 and 2: States 1 and 2

Scope 5: Output Comparison

Scope 4: Control Signal Comparison

Scope 3: Comparison of Control Signal Derivatives

→ It is observed that stabilization has been achieved, and for each state feedback matrix 2, we have control signals.

Section B: Linear Feedback Control Systems: Tracking Design

1, 2, 3) Designing Static Precompensators for Tracking with Integral Control for the System and Analyzing the Tracking Performance and Robustness in the Presence of Model Parameter Changes and Closed-Loop System Performance by Introducing Constant Disturbances:

```
> A=[10.9 -38.2 28.1 -5.8;1 0 0 0;0 1 0 0;0 0 1 0];
B=[1;0;0;0];
C=[0 -2.5 -20 -37.5];
D=[0;0;0;0];
Aa=[10.95 -38.22 28.1 -5.82;1.01 -0.01 0.02 0;-0.02 1.02 0.01 0;0.03 -0.01 1.01 0];
Bb=[-0.01;0.001;-0.001;1];
Cc=[0.02 -2.51 -20.001 -37.49];
%static compensator
K1=[18.2 78.1 -3.2 20.9];
invGclz=inv(-C*inv(A-B*K1)*B);
%INTEGRAL CONTROL SINGLE INPUT
Abar=[A zeros(4,1);-C 0];
Bbar=[B;0];
Cbar=[C 0];
phic=[A B;0 -C];
rankphic=rank(phic);
eig(Abar);
K2=acker(Abar,Bbar,[-1 -2 -3 -4 -5]);
Acl=Abar-Bbar*K2;
eig1=eig(Acl)
```

Result:

eig1 =

```
-5.0000
-4.0000
-3.0000
-2.0000
-1.0000
```

>> invGclz

invGclz =

```
-0.7120
```

>> rankphic

rankphic =

```
5
```

>> eig1

eig1 =

-5.0000
-4.0000
-3.0000
-2.0000
-1.0000

>> >> K2

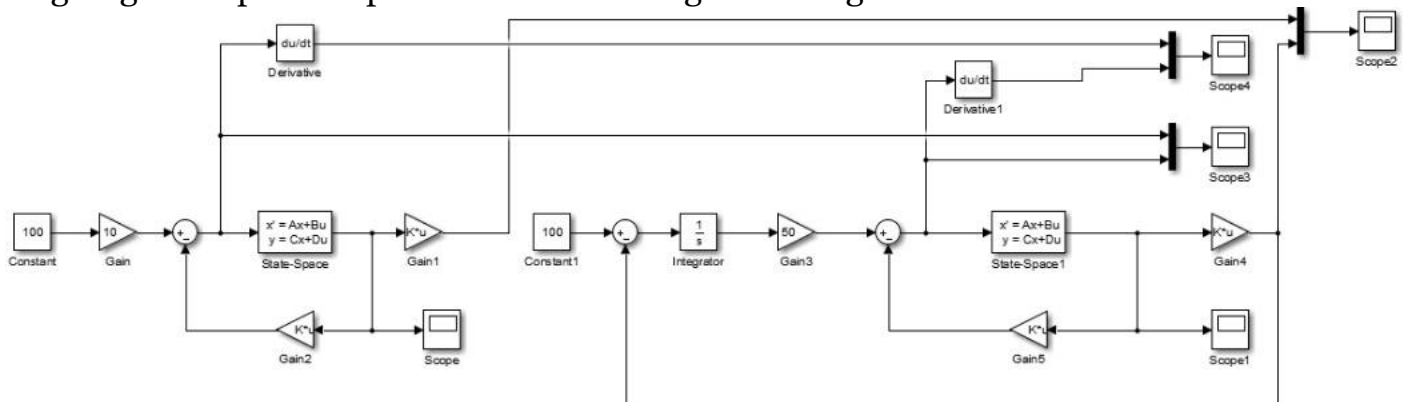
K2 =

25.9000 46.8000 245.1000 204.2000 3.2000

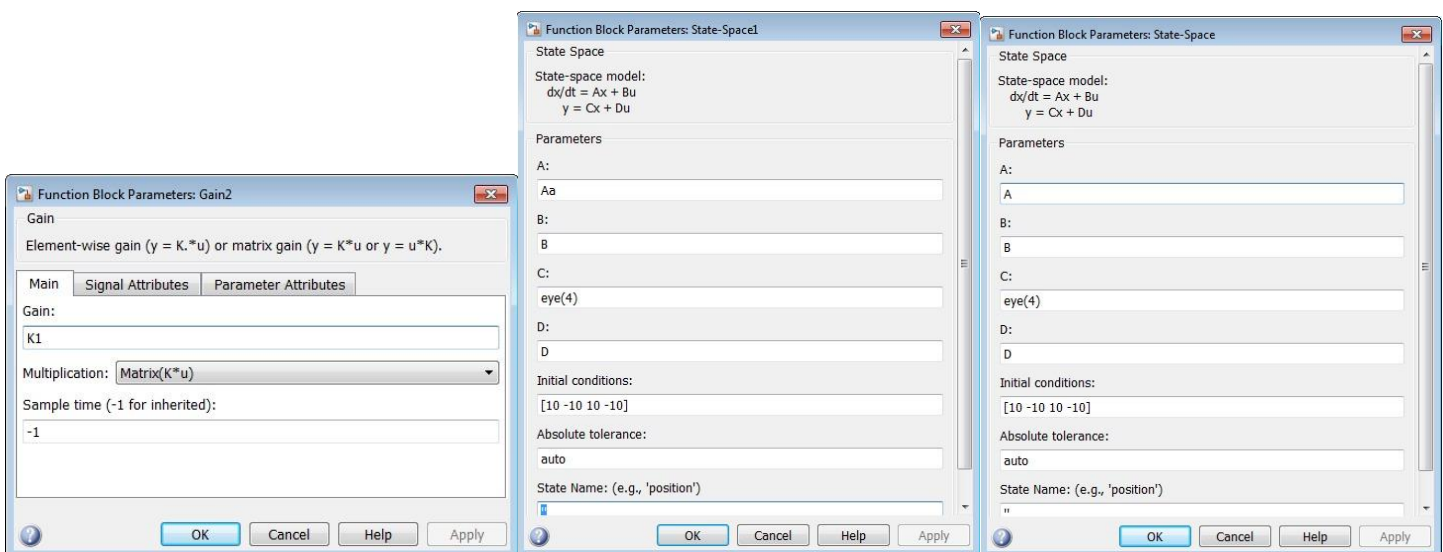
→ The rank of the completed matrix is full, so we can use integral control for gain calculation, and since we have 5 states, we also have 5 eigenvalues.

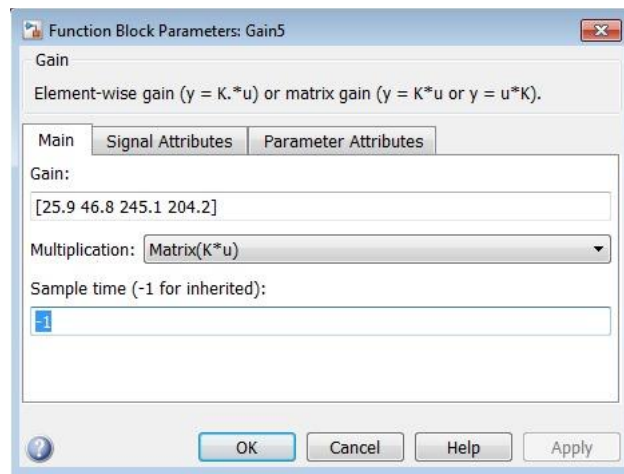
Simulation:

Designing static pre-compensators for tracking with integral control:

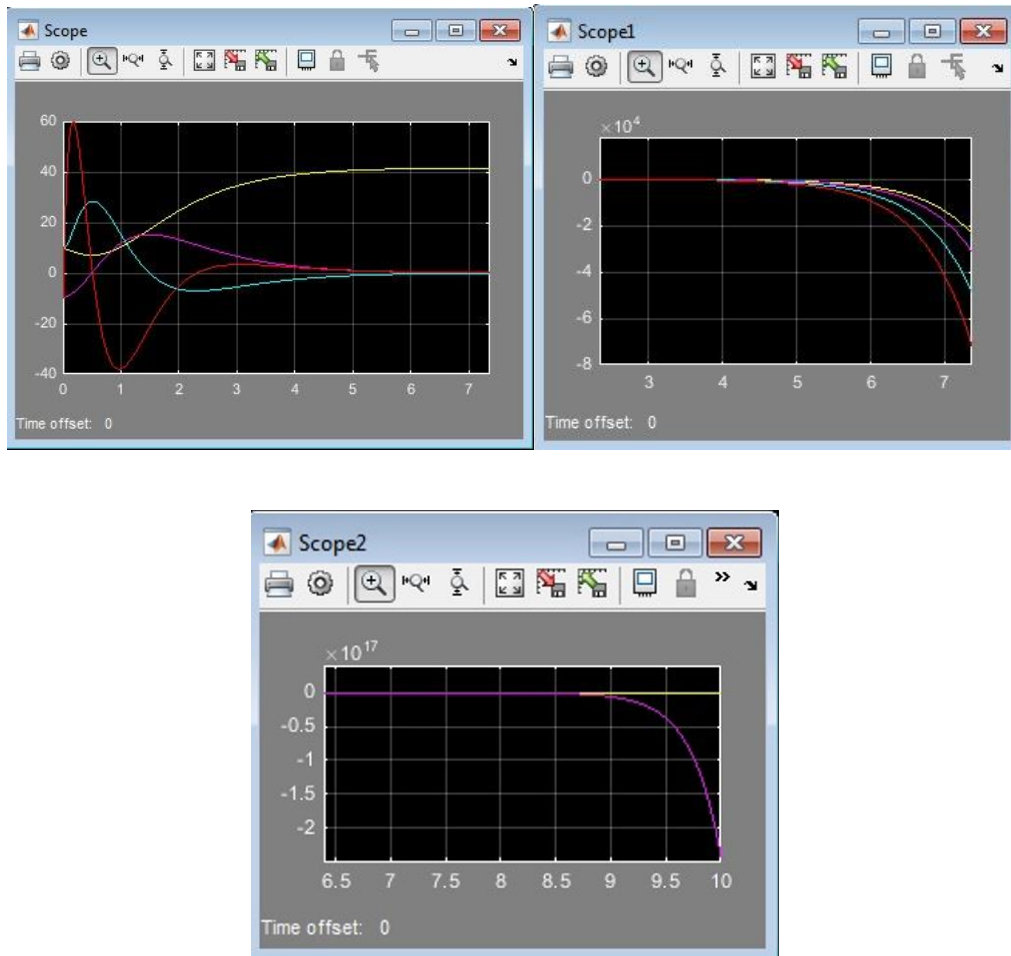


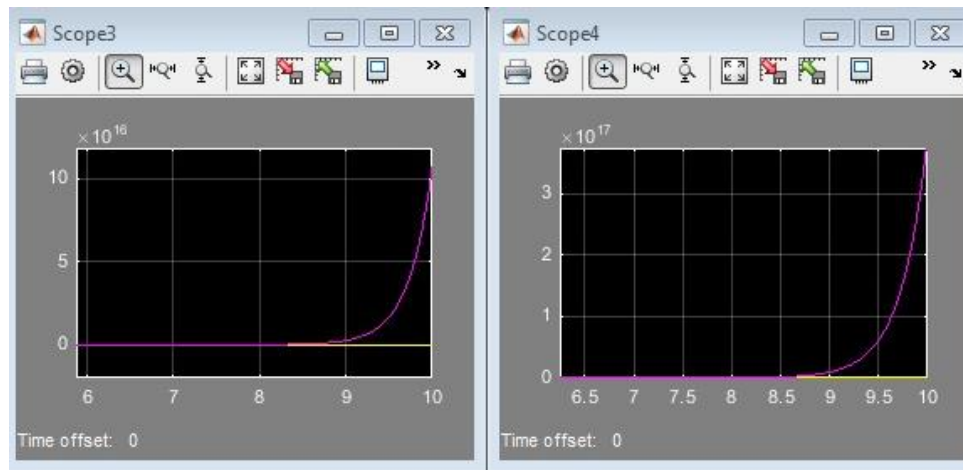
Setting:



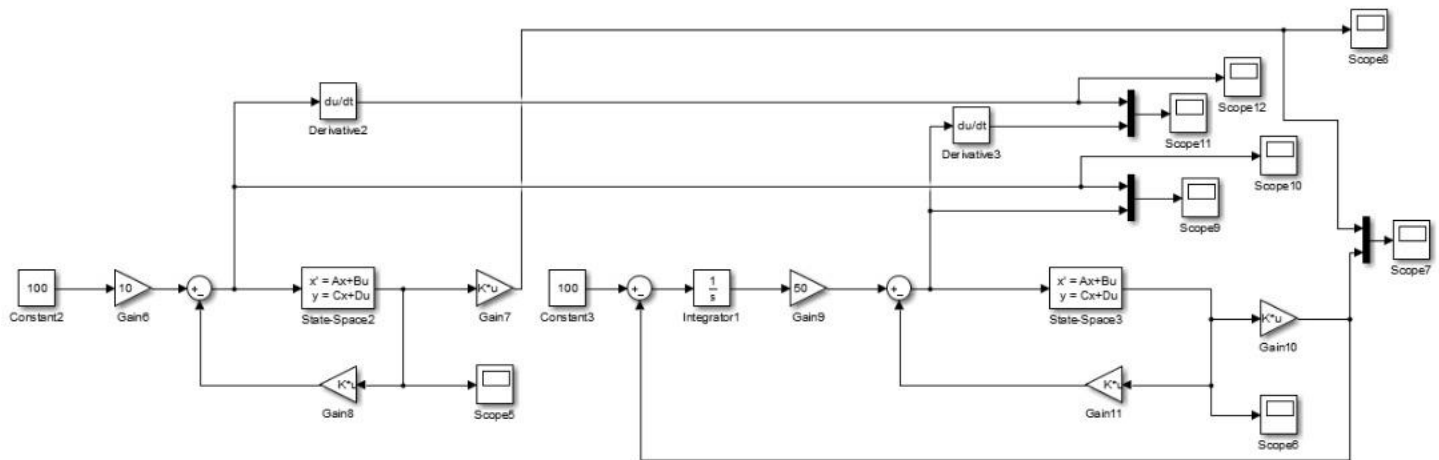


Output:

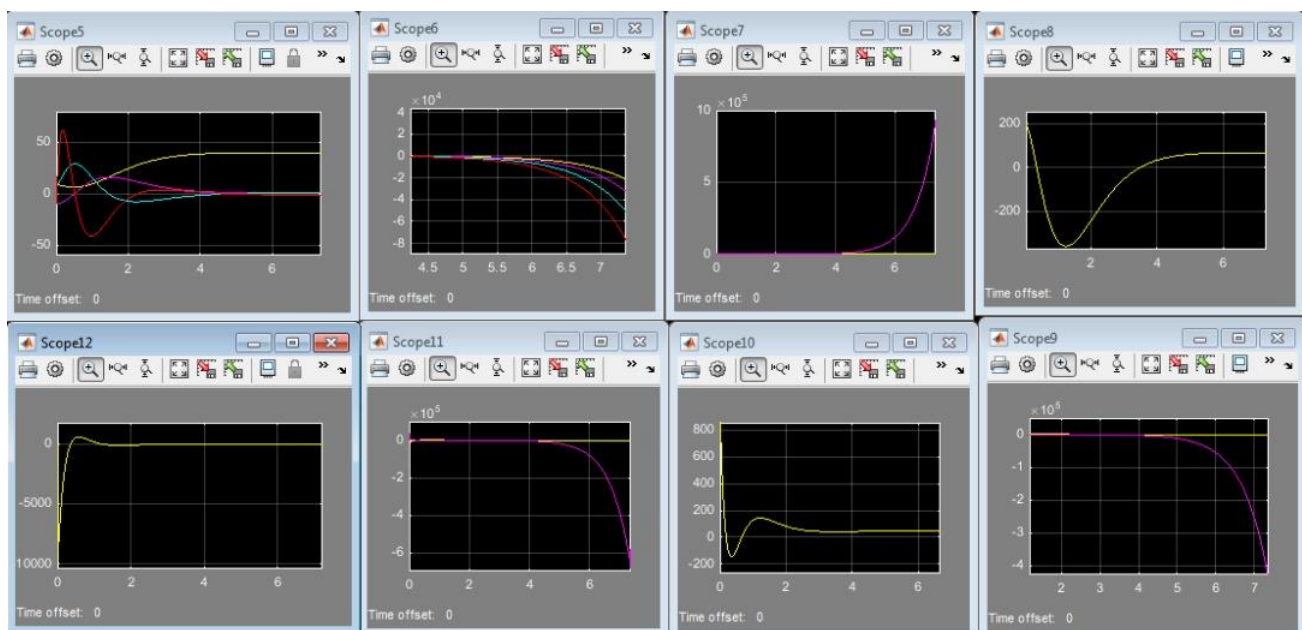




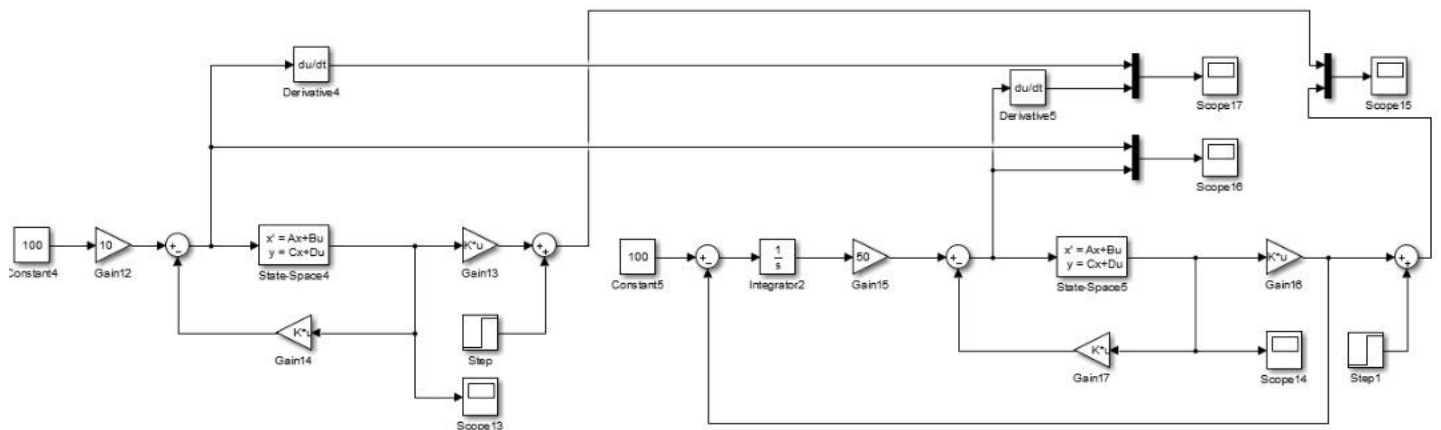
Robustness against parameter changes:



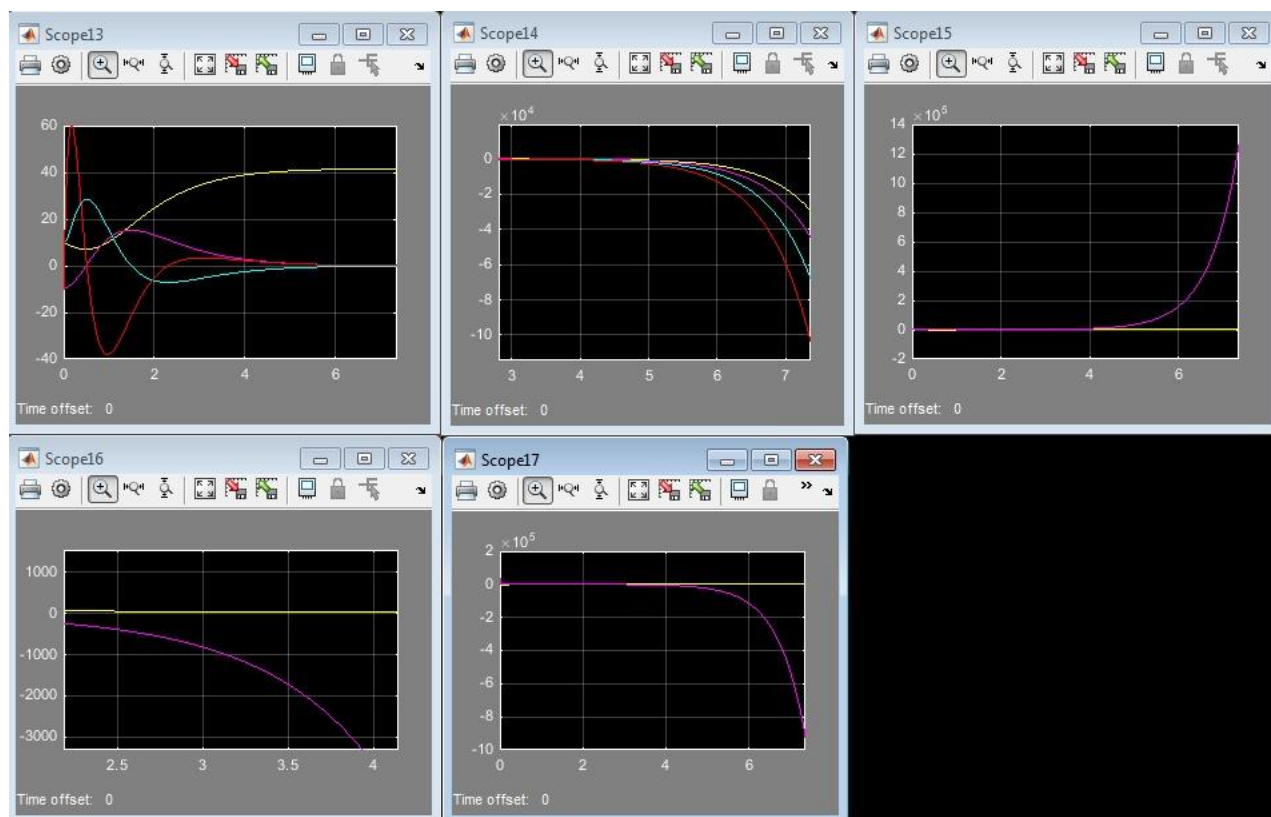
Output:



Closed-loop system performance with the introduction of constant disturbances:



Output:



→ Conclusion:

The state plots, output, command signal, and command signal variations obtained from the static precompensator method are better than the integral control method.

4. Designing a tracker for a two-input system:

```
A=[10.9 -38.2 28.1 -5.8;1 0 0 0;0 1 0 0;0 0 1 0];
BB=[1 0;0 0;0 0;0 1];
DD=[0 0;0 0;0 0;0 0];
ABAR=[A zeros(4,1);-C 0];
BBAR=[BB;0 0];
CBAR=[C 0];
PHIC=[BB A;0 0 -C];
RANKPHIC=rank(PHIC);
F=[-1 0 0 0 0;0 -2 0 0 0;0 0 -3 0 0;0 0 0 -4 0;0 0 0 0 -5];
kbar=[1 1 1 0 0;0 0 0 1 1];
PHIO=[kbar;kbar*F;kbar*(F^2);kbar*(F^3);kbar*(F^4)];
rankPHIO=rank(PHIO);
T=lyap(ABAR,-F,-BBAR*kbar);
K=kbar*inv(T);
eig2=eig(ABAR-BBAR*K);
>> rankPHIC
Undefined function or variable 'rankPHIC'.
```

```
>> RANKPHIC
```

```
RANKPHIC =
```

```
5
```

```
>> rankPHIO
```

```
rankPHIO =
```

```
5
```

```
>> T
```

```
T =
```

```
0.0119  0.0252  0.0334  0.0551  0.0469
-0.0119 -0.0126 -0.0111 -0.0138 -0.0094
0.0119  0.0063  0.0037  0.0034  0.0019
-0.0119 -0.0031 -0.0012  0.2491  0.1996
0.2381  0.0118 -0.0000 -2.3443 -1.5000
```

```
>> K
```

```
K =
```

```
16.3641 -29.8897 31.1490 -4.9149 0.0841
-3.1360 -15.1811 -14.1407 9.5359 0.5816
```

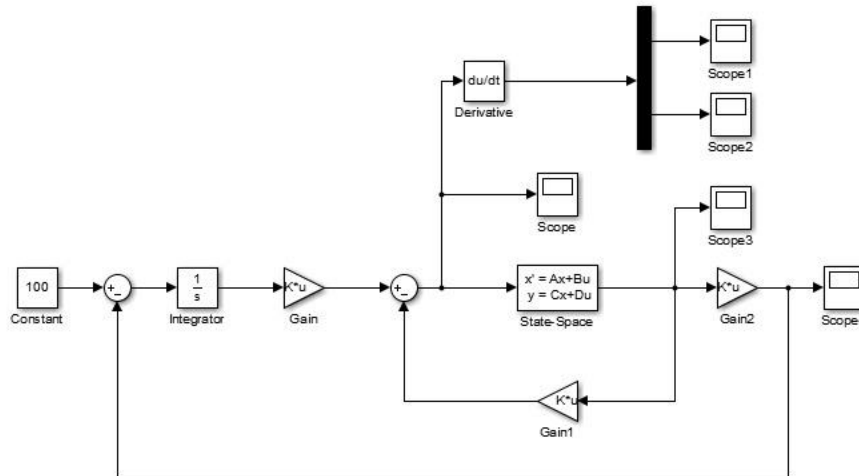
```
>> eig2
```

```
eig2 =
```

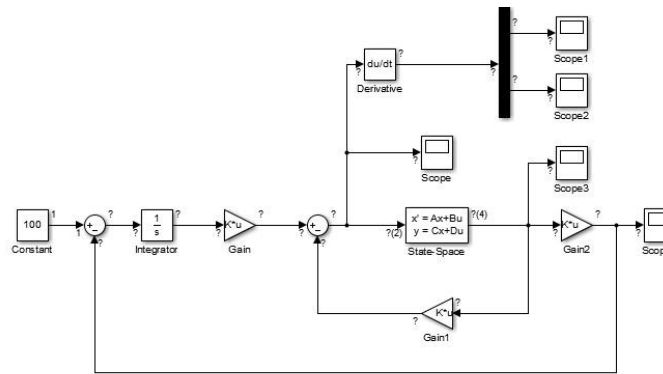
```
-1.0000
-2.0000
```

-5.0000
-3.0000
-4.0000

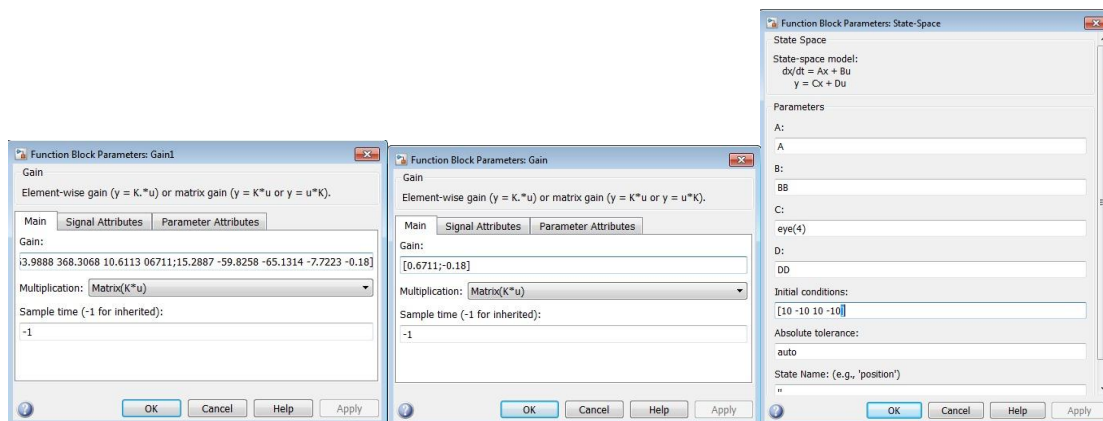
Simulink:



Error:



Settings:



➔ We are unable to find the tracker.

5. Adding (s=0) as a transfer function:

```
s=tf('s');  
gg=(-2.5*(s^2+8*s+15)*(s))/((s-0.4)*(s-0.5)*(s^2-10*s+29));  
A=[10.9 -38.2 28.1 -5.8;1 0 0 0;0 1 0 0;0 0 1 0];  
B=[0;0;0;0];  
CC=[-37.5 -2.5 -20 0];  
Abarr=[A zeros(4,1);-CC 0];  
Bbarr=[B;0];  
Cbarr=[CC 0];  
phicc=[B A;0 -CC];  
rankphicc=rank(phicc)  
eig(Abarr);  
K3=acker(Abarr,Bbarr,[-1 -2 -3 -4 -5]);  
ACL=Abarr-Bbarr*K3;  
eig3=eig(ACL)
```

rankphicc =

5

eig3 =

-5.0000
-4.0000
-3.0000
-2.0000
-1.0000

>> K3 =

-56.7431 165.7379 -169.1362 25.9000 -1.0345

→ We observe that the rank of the completed matrix is full, so we can use the integral control method for gain calculation.

Section C: Observer

1. Observability:

```
>> A=[10.9 -38.2 28.1 -5.8;1 0 0 0;0 1 0 0;0 0 1 0];  
B=[0;0;0;1];  
C=[0 -2.5 -20 -37.5];  
D=[0;0;0;0];  
phio=obsv(A,C);  
Rankphio=rank(phio);  
>> Rankphio
```

Rankphio =

4

→ The rank of the completed matrix is full, so this realization is observable.

2 and 3) Selecting 2 sets of poles and obtaining the gains and variable state response, etc.

```
>> A=[10.9 -38.2 28.1 -5.8;1 0 0 0;0 1 0 0;0 0 1 0];  
C=[0 -2.5 -20 -37.5];  
DD=[0 0;0 0;0 0;0 0];  
L1=acker(A',C',[-1 -2 -3 4])';  
L2=acker(A',C',[-50 -51 -52 -53])';
```

Result:

```
>> L1
```

L1 =

-42.3697

-5.1989

-0.3922

-0.0016

```
>> L2
```

L2 =

1.0e+03 *

-5.7076

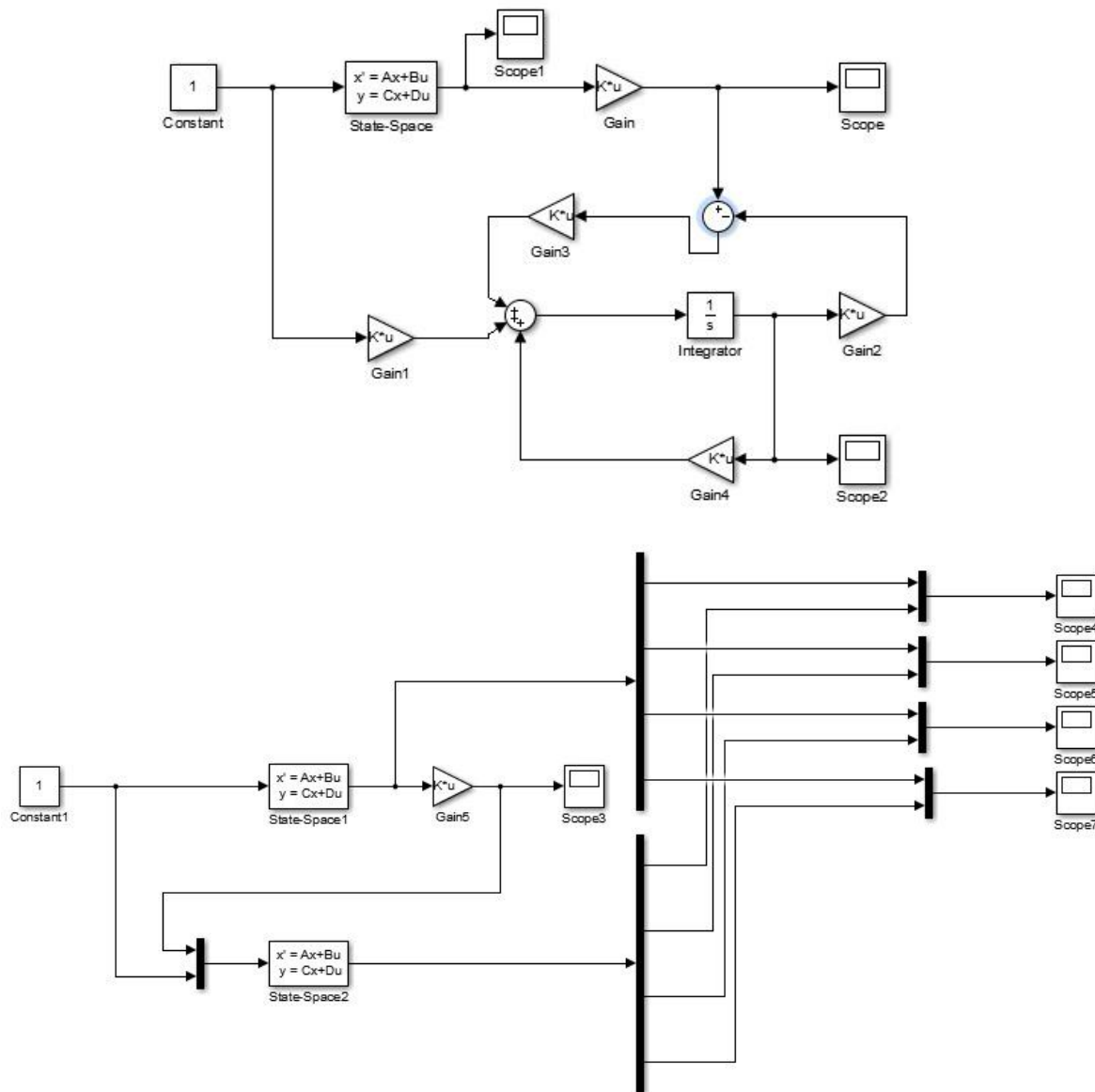
4.6518

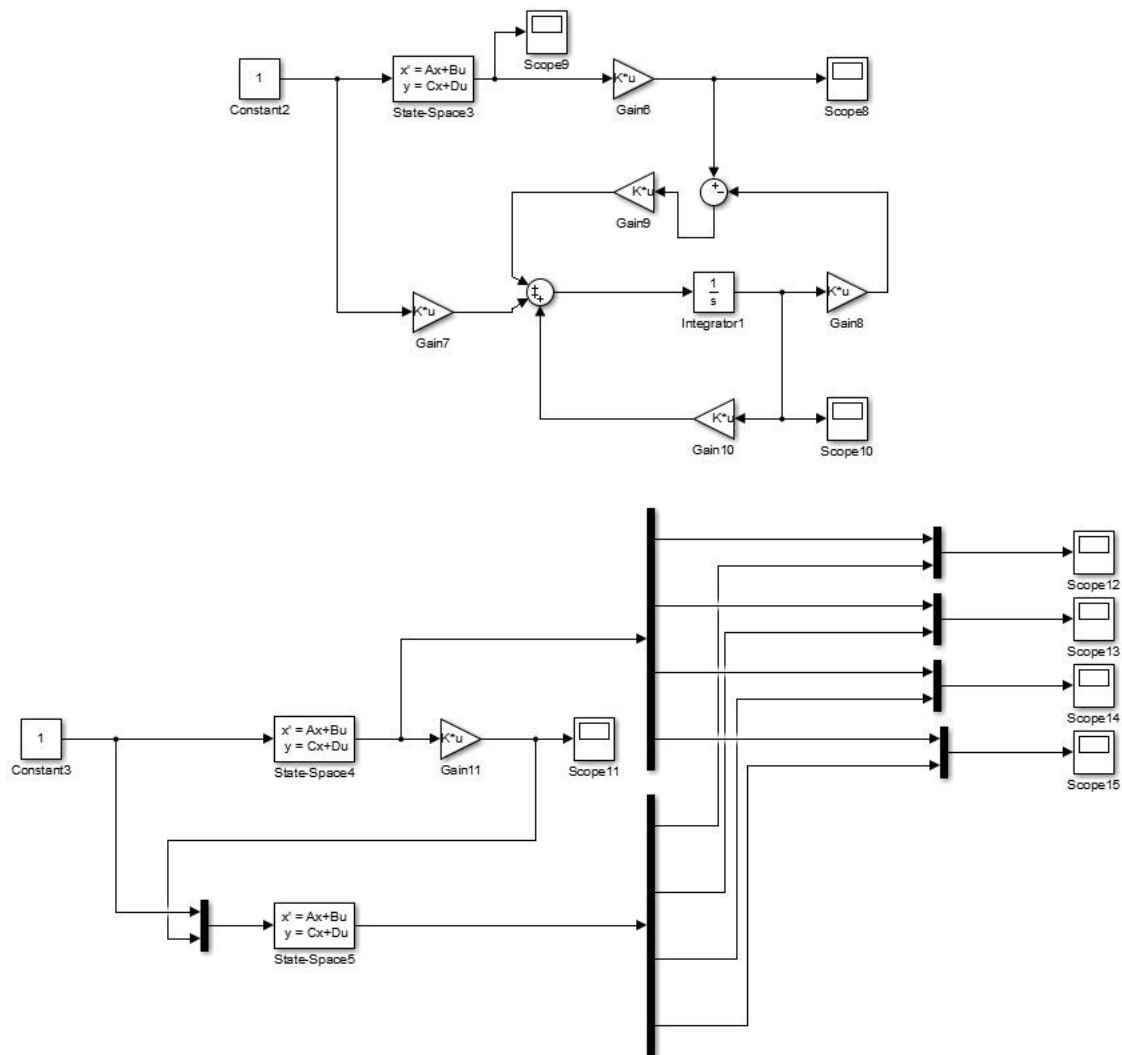
-2.5868

1.0637

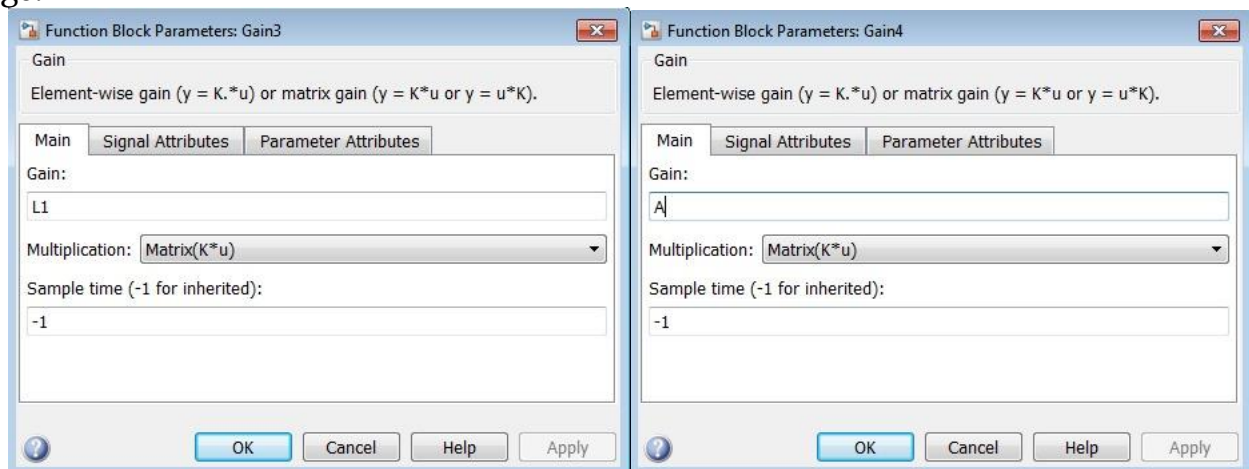
→ So, we were able to obtain the observer gains for slow and fast poles.

Simulink:
For slow & fast poles:
L1





Settings:



Function Block Parameters: Gain1

Gain
Element-wise gain ($y = K \cdot u$) or matrix gain ($y = K \cdot u$ or $y = u \cdot K$).

Main | Signal Attributes | Parameter Attributes

Gain:
B

Multiplication: Matrix($K \cdot u$)

Sample time (-1 for inherited):
-1

OK Cancel Help Apply

Function Block Parameters: State-Space7

State Space
State-space model:
 $\frac{dx}{dt} = Ax + Bu$
 $y = Cx + Du$

Parameters

A:
[Aa-L1*Cc]

B:
[Bb L1]

C:
eye(4)

D:
DD

Initial conditions:
0

Absolute tolerance:
auto

State Name: (e.g., 'position')
"

OK Cancel Help Apply

Function Block Parameters: State-Space6

State Space
State-space model:
 $\frac{dx}{dt} = Ax + Bu$
 $y = Cx + Du$

Parameters

A:
Aa

B:
Bb

C:
eye(4)

D:
D

Initial conditions:
[10 -10 10 -10]

Absolute tolerance:
auto

State Name: (e.g., 'position')
"

OK Cancel Help Apply

Function Block Parameters: State-Space2

State Space
State-space model:
 $\frac{dx}{dt} = Ax + Bu$
 $y = Cx + Du$

Parameters

A:
[A-L1*C]

B:
[B L1]

C:
eye(4)

D:
DD

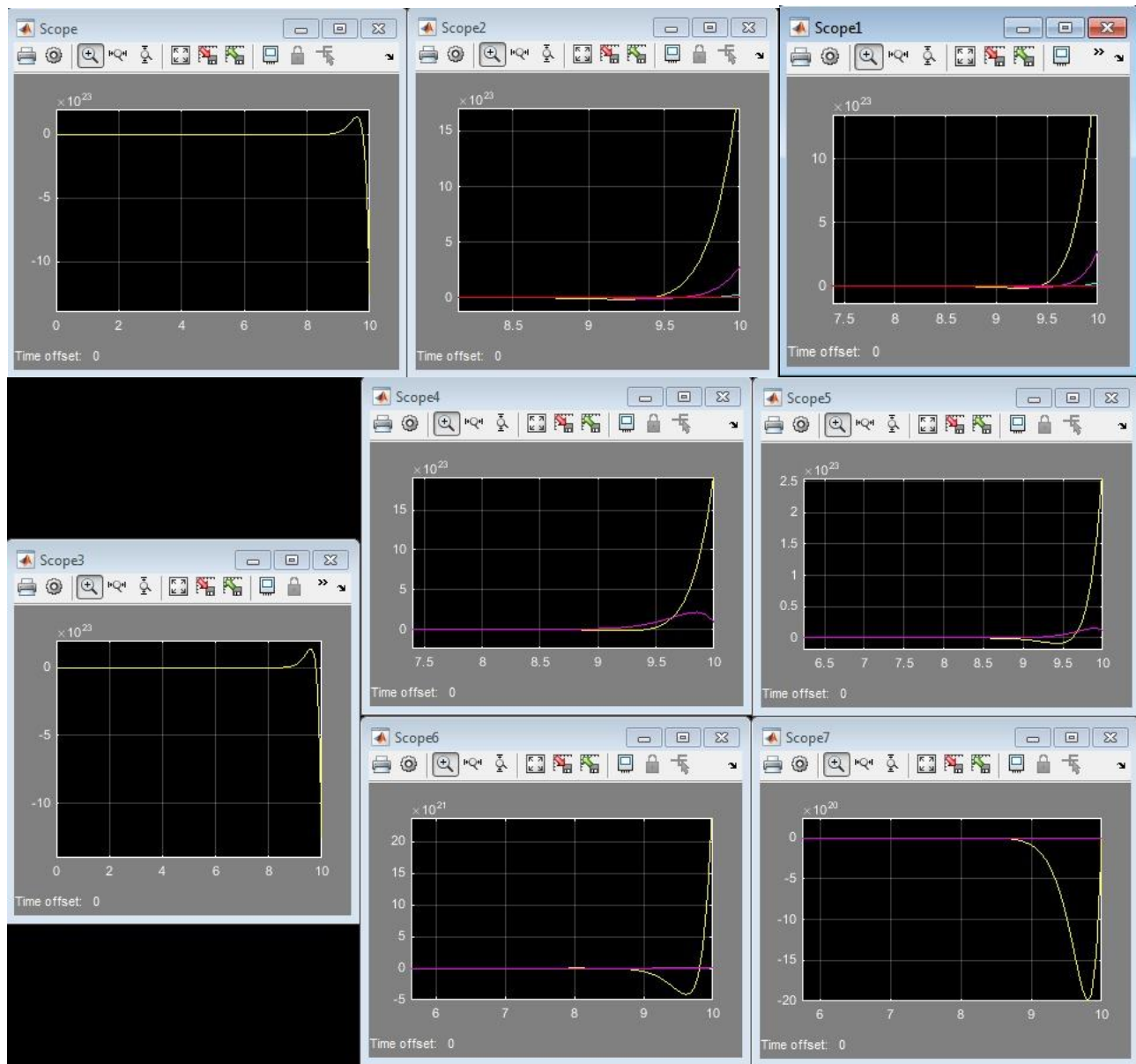
Initial conditions:
0

Absolute tolerance:
auto

State Name: (e.g., 'position')
"

OK Cancel Help Apply

Output L1:



Scopes:

3: Output

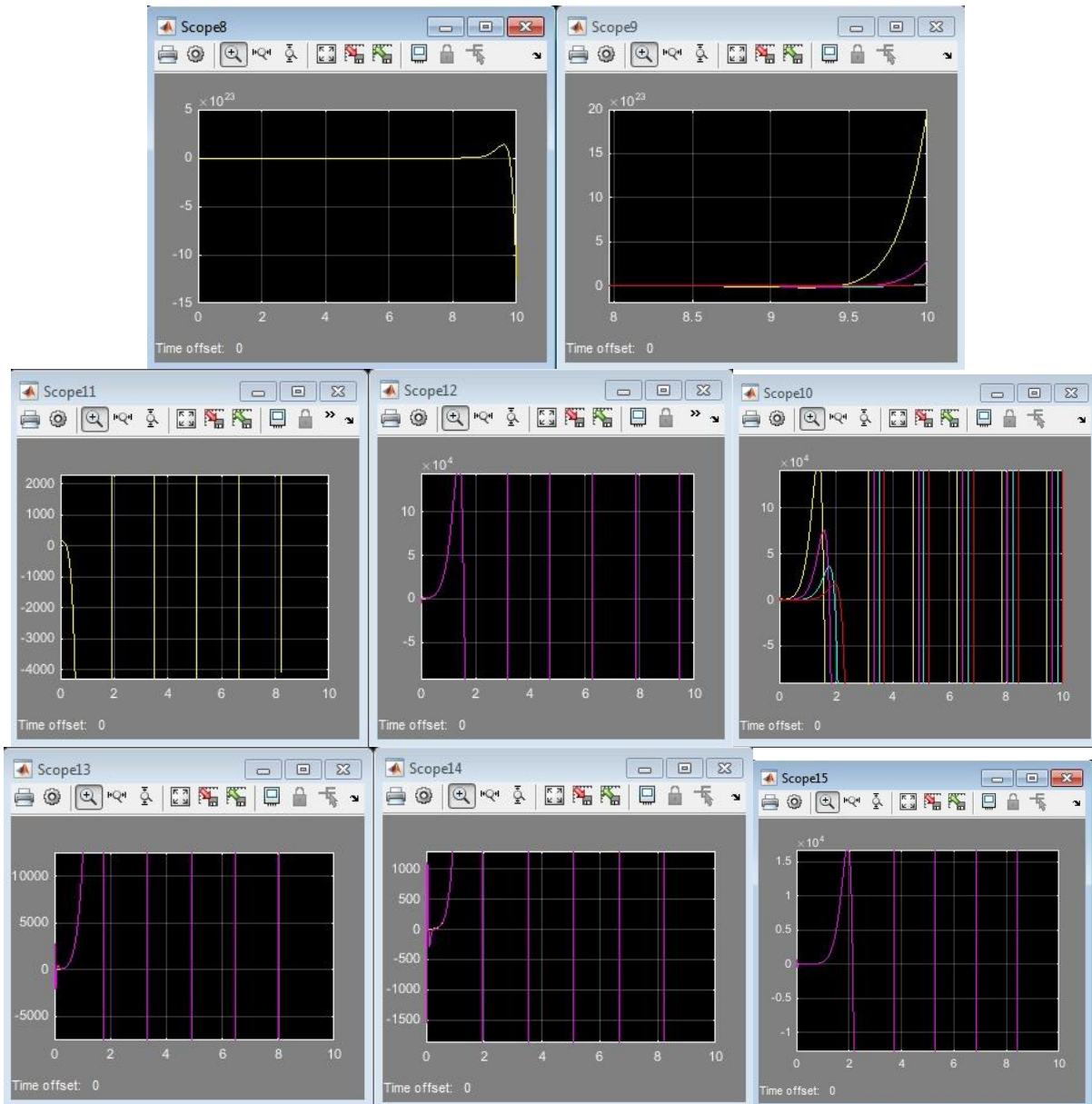
4: Comparison of the first state of the system and full-order observer for slow poles

5: Comparison of the second state of the system and full-order observer for slow poles

6: Comparison of the third state of the system and full-order observer for slow poles

7: Comparison of the fourth state of the system and full-order observer for slow poles

Output L2:



Scopes:

11: Output

12: Comparison of the first state of the system and full-order observer for fast poles

13: Comparison of the second state of the system and full-order observer for fast poles

14: Comparison of the third state of the system and full-order observer for fast poles

→ Result:

The convergence of states for the full-order observer for fast poles is faster compared to slow poles.

6. Robustness against parameter changes and using the same observer for estimating the changed system state.

Coding section:

```
D=[0;0;0;0];  
DD=[0 0;0 0;0 0;0 0];  
Aa=[10.95 -38.22 28.1 -5.82;1.01 -0.01 0.02 0;-0.02 1.02 0.01 0;0.03 -0.01 1.01 0];  
Bb=[1;0.001;-0.001;-0.01];  
Cc=[0.02 -2.51 -20.001 -37.49];  
L1=acker(A',C',[-1 -2 -3 -4])';
```

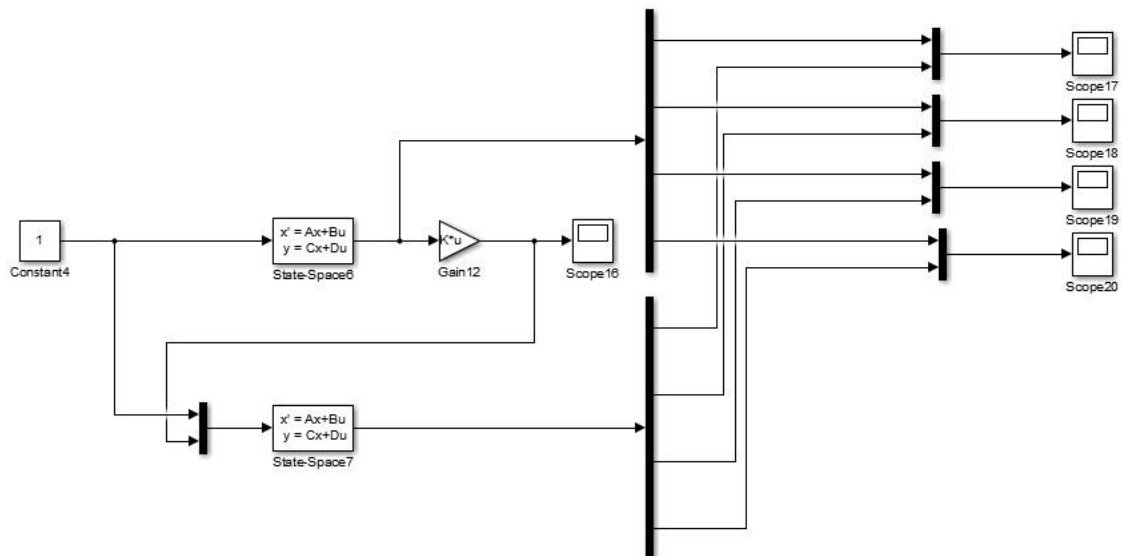
Result:

```
>> L1
```

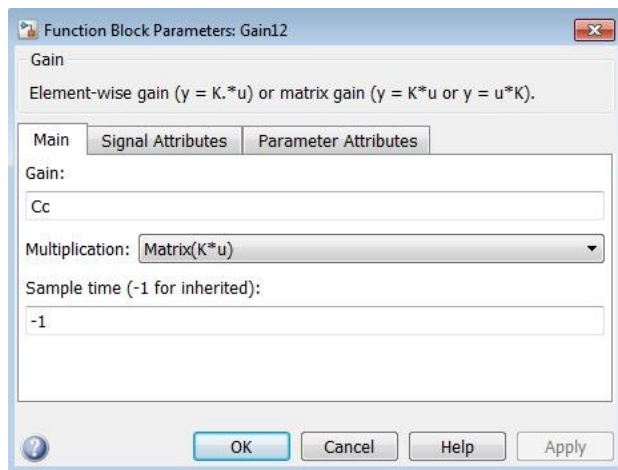
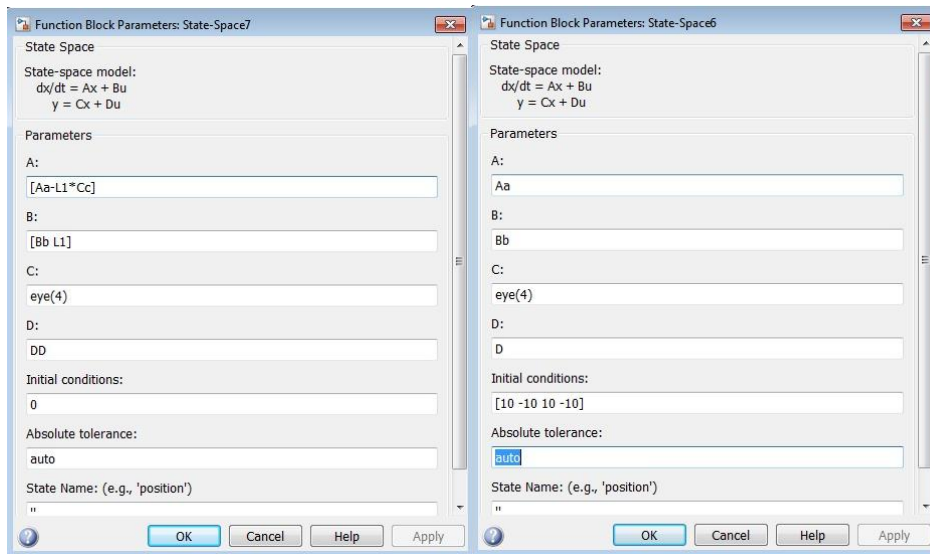
L1 =

```
-42.3697  
-5.1989  
-0.3922  
-0.0016
```

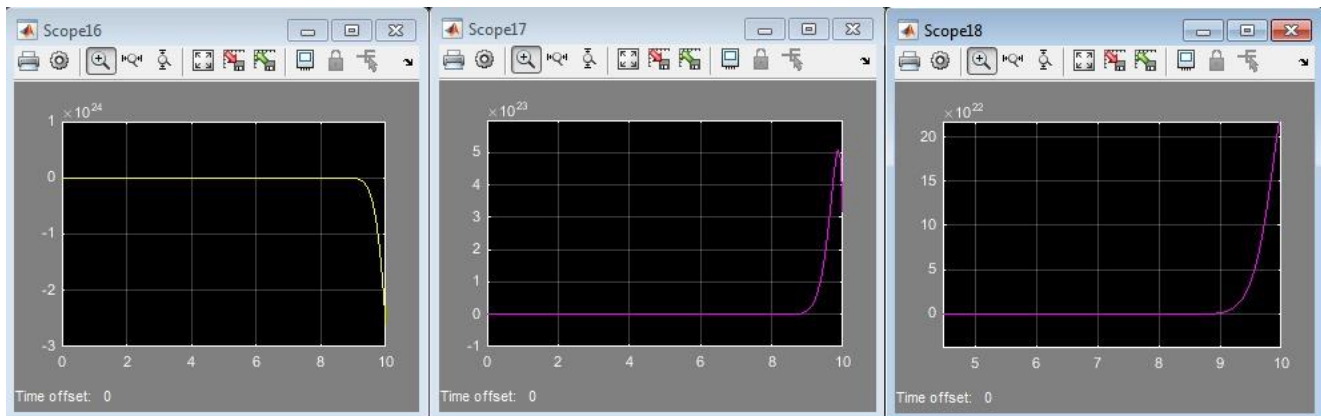
Simulink:

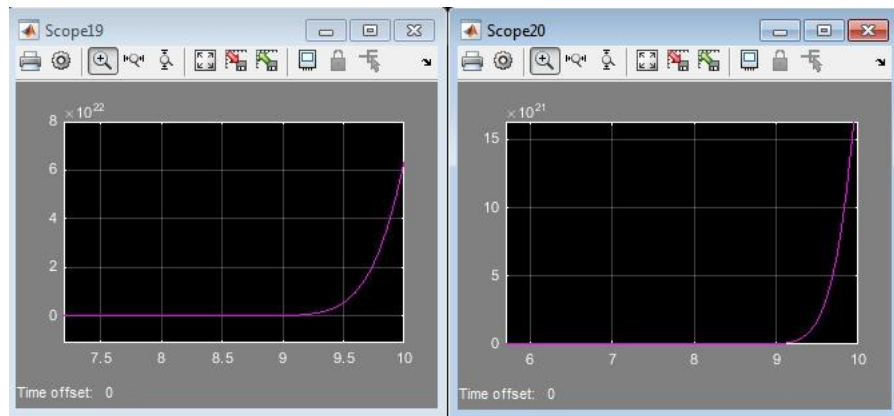


Setting:



Outputs:





16: Output

17: Comparison of the first state of the system and observer

18: Comparison of the second state of the system and observer

19: Comparison of the third state of the system and observer

20: Comparison of the fourth state of the system and observer

→ Result:

It is observed that the convergence of observer states to the system states has been achieved.

Section D: Feedback Control System with Observer

1) Feedback control system with full-order observer

```
>> A=[10.9 -38.2 28.1 -5.8;1 0 0 0;0 1 0 0;0 0 1 0];  
B=[1;0;0;0];  
C=[0 -2.5 -20 -37.5];  
D=[0;0;0;0];  
DD=[0 0;0 0;0 0;0 0];  
L=acker(A',C',[-50 -51 -52 -53])';  
k=[18.2 78.1 -3.2 20.9]
```

result:

L =

1.0e+03 *

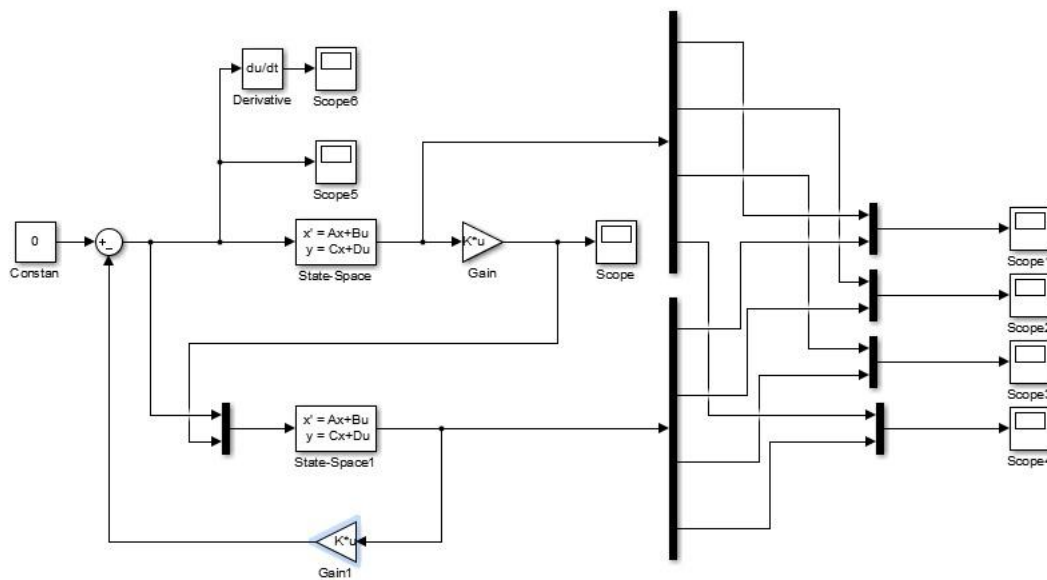
-5.7076

4.6518

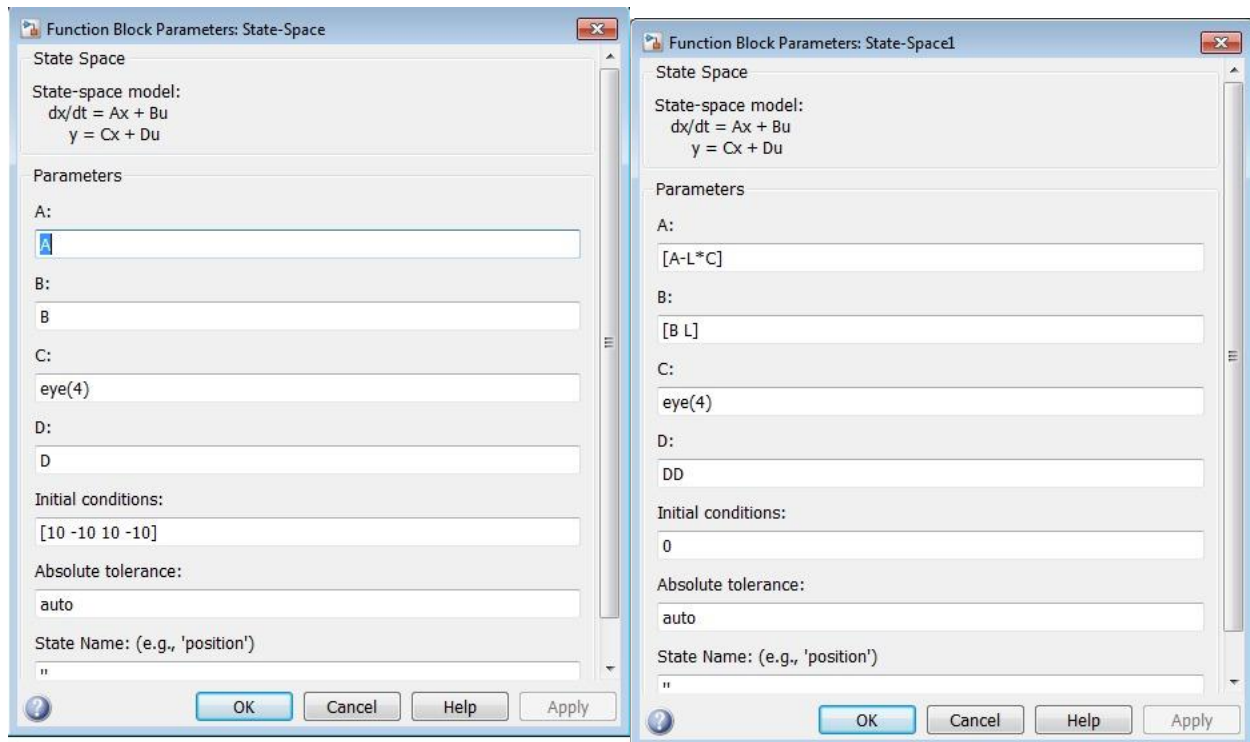
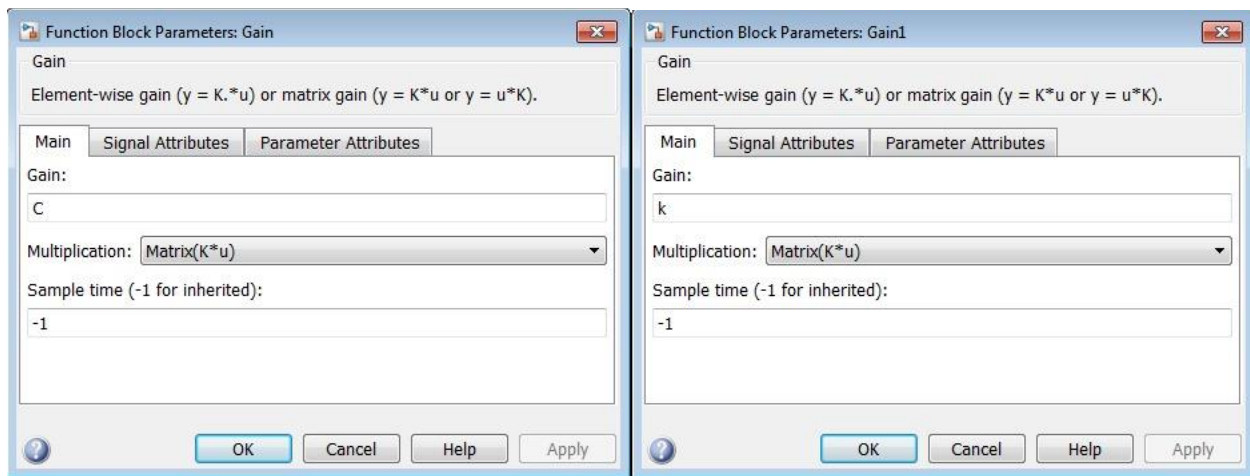
-2.5868

1.0637

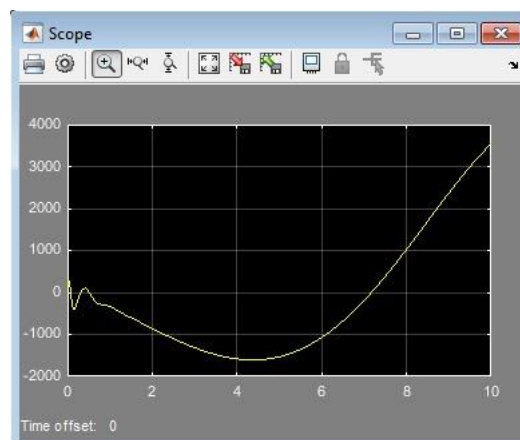
Simulink:



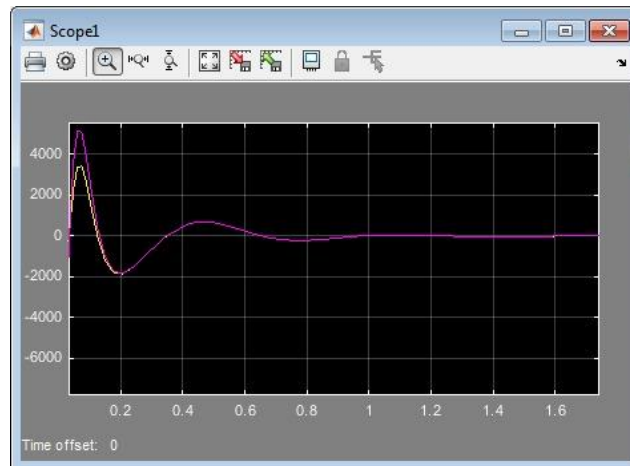
Settings:



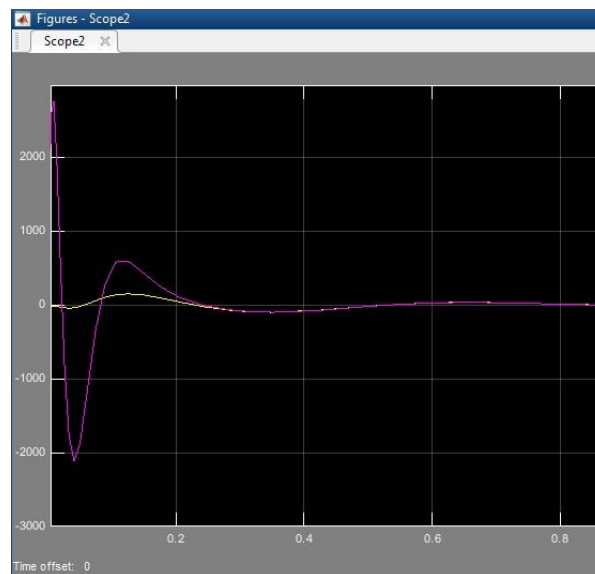
Outputs:



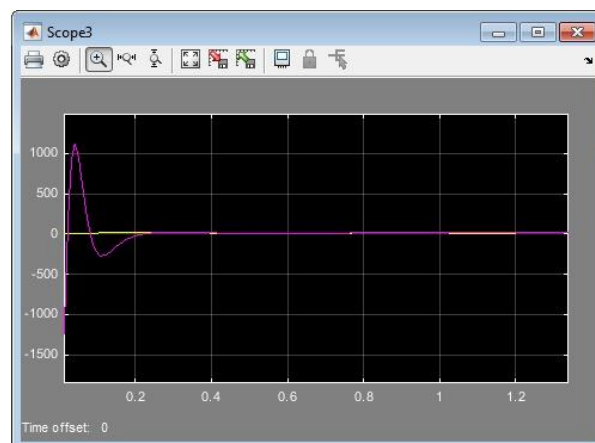
Comparison of the first state of the system and observer:



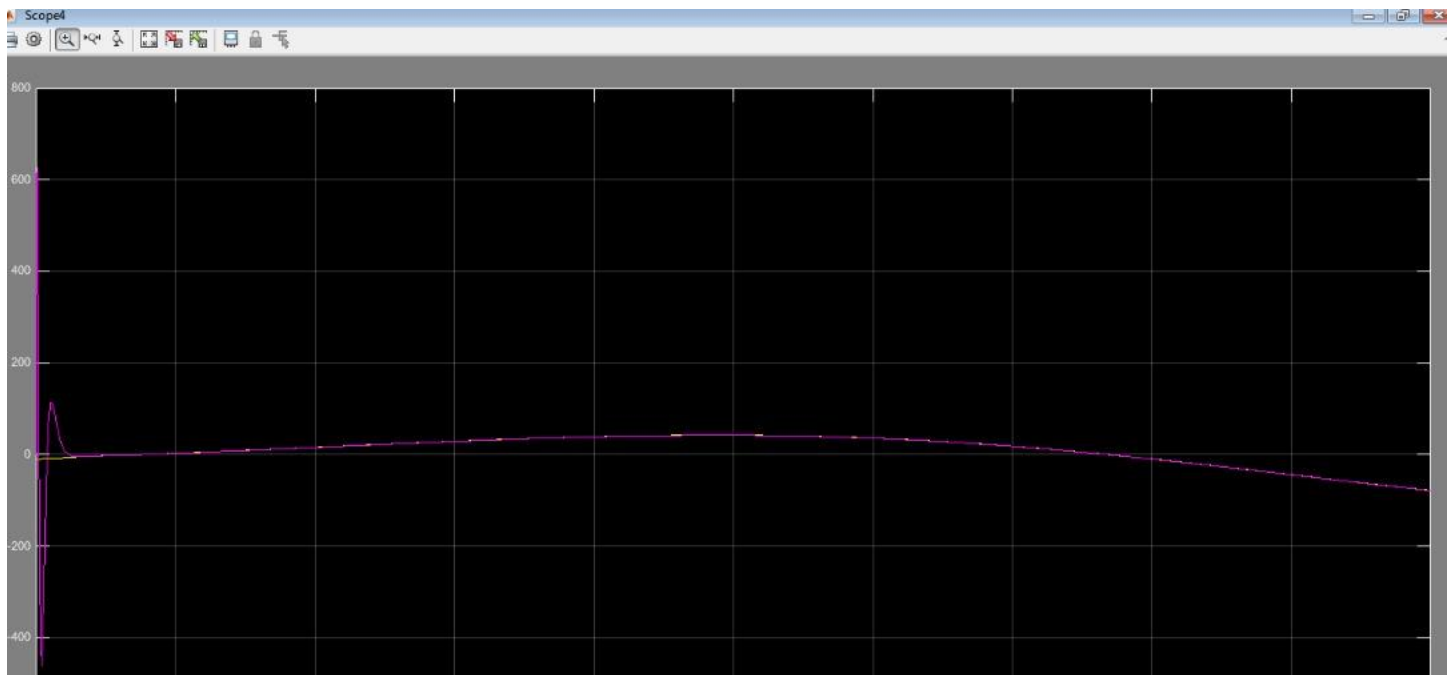
Second state:



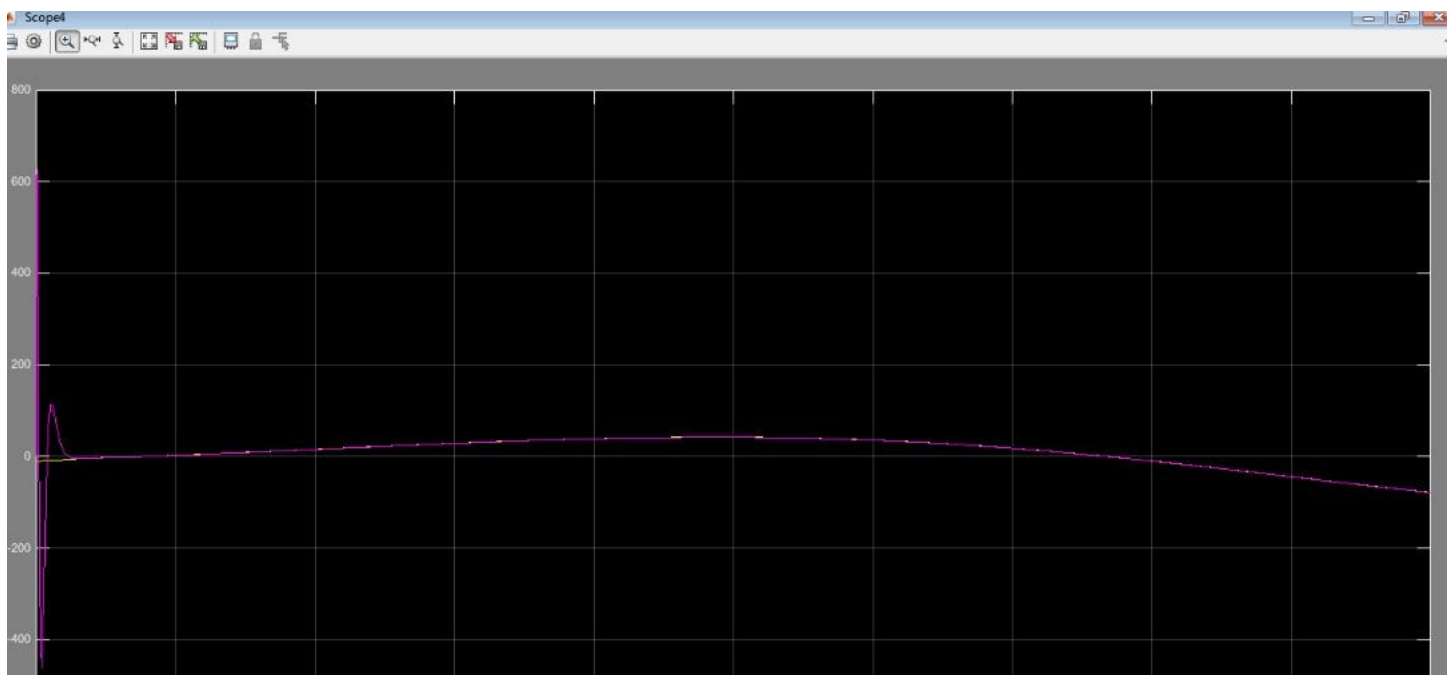
Third state:



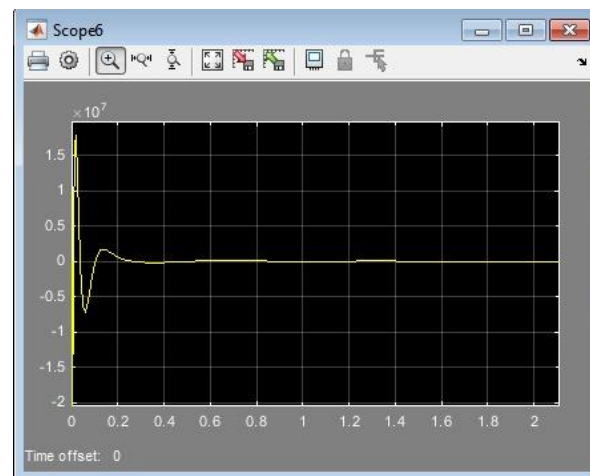
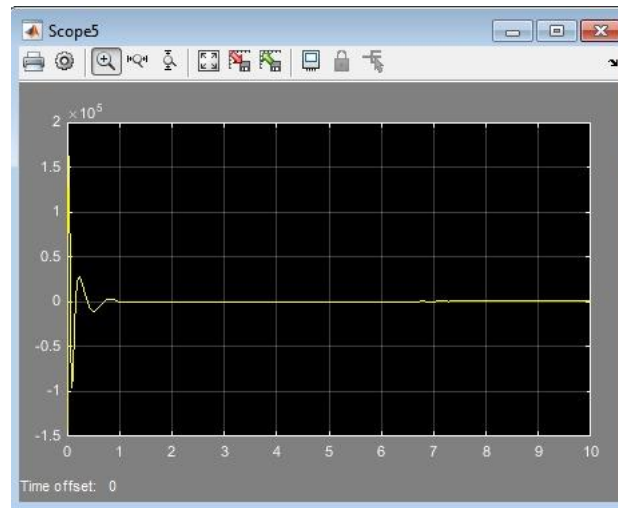
Forth state:



Control Signal:



Control signal derivative:

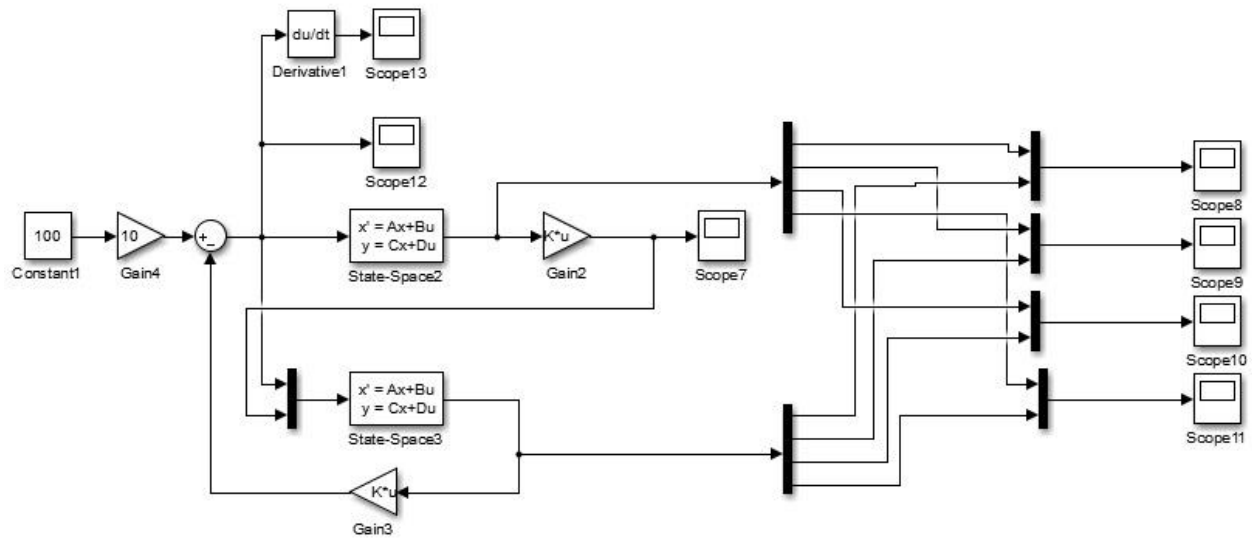


→ Result:

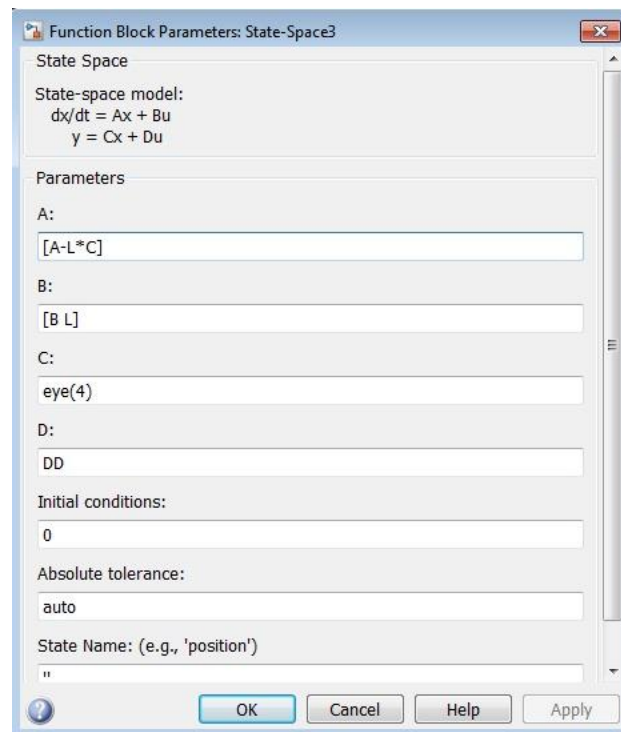
It is observed that stabilization has been achieved.

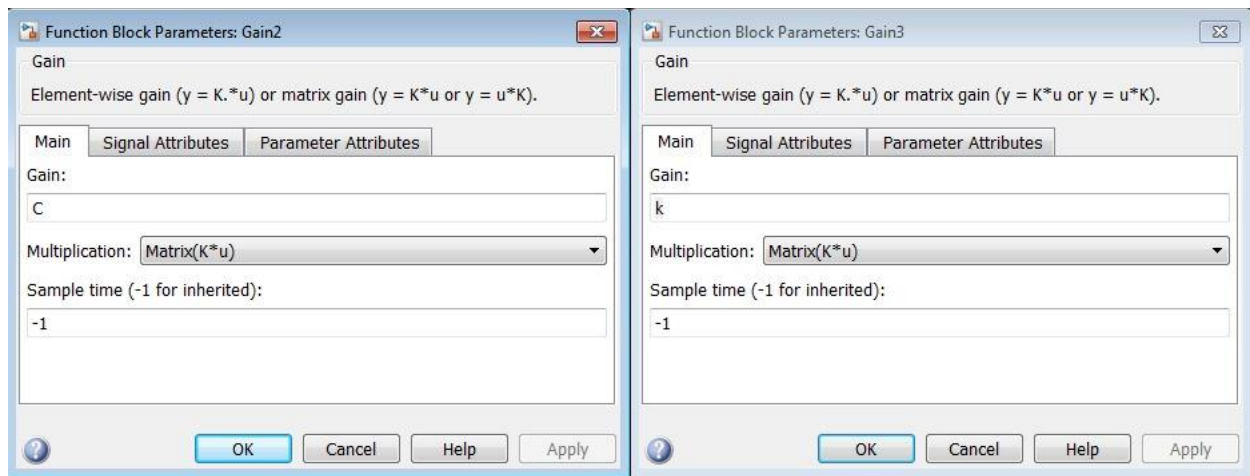
3. Static Precompensator Tracking - State Feedback - Full-Order Observer:

Simulink:

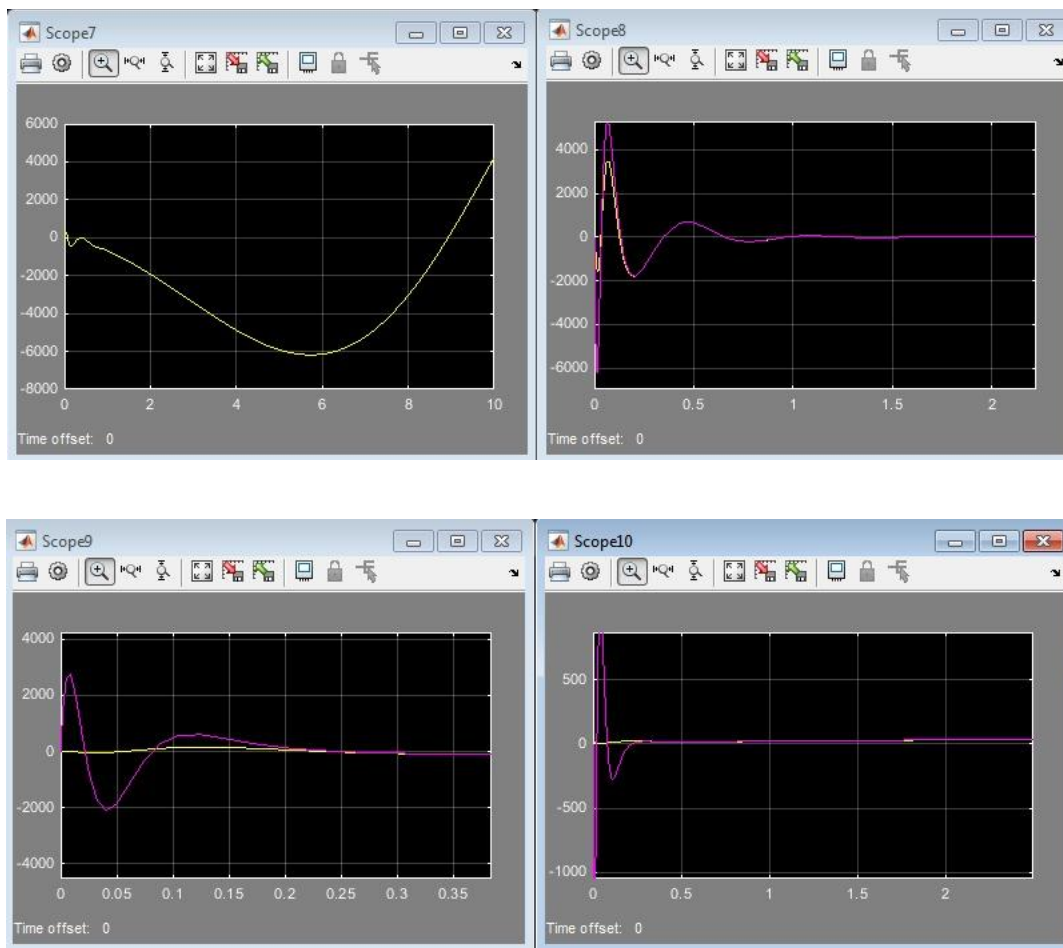


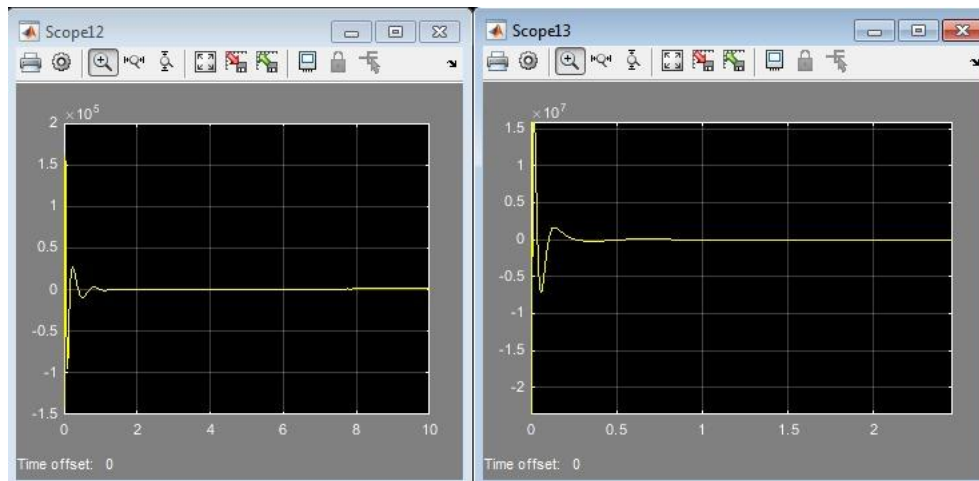
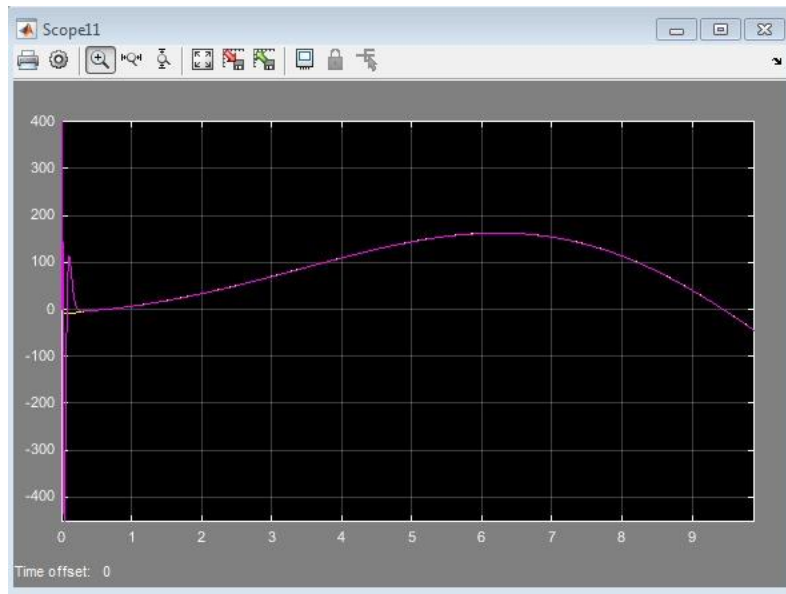
Settings:





Outputs:





Scopes:

7: Output

8: Comparison of the first state of the system and observer

9: Comparison of the second state of the system and observer

10: Comparison of the third state of the system and observer

11: Comparison of the fourth state of the system and observer

12: Control Signal

13: Control Signal Derivative

→ Result:

It is observed that tracking has been achieved.