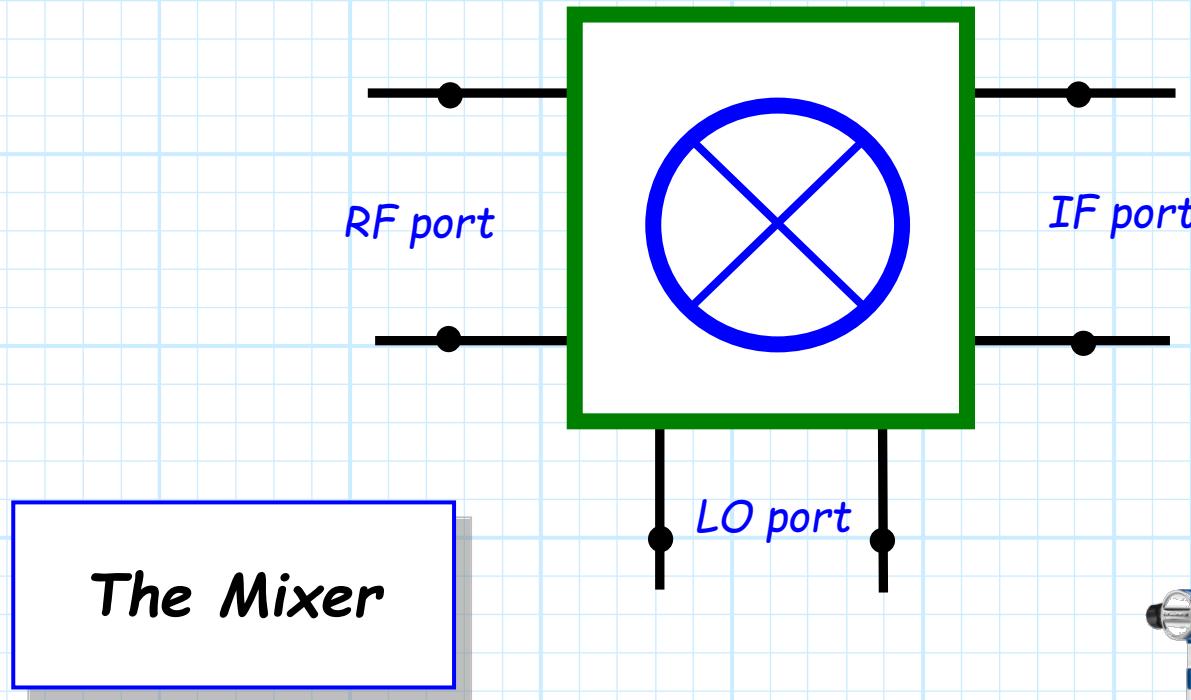


Mixers

A mixer is a three-port, non-linear microwave device.



Usually mixers are **passive devices**, but **active** mixers also exist, and are becoming **more and more prevalent**.



It's a multiplier

The three ports of a mixer are **distinct** and **unique**, and are typically referred to as:

- 1) The **RF** (Radio Frequency) port
- 2) The **IF** (Intermediate Frequency) port
- 3) The **LO** (Local Oscillator) port

Q: So just what does a mixer do??

A: A **clue** is in its **symbol**: \otimes

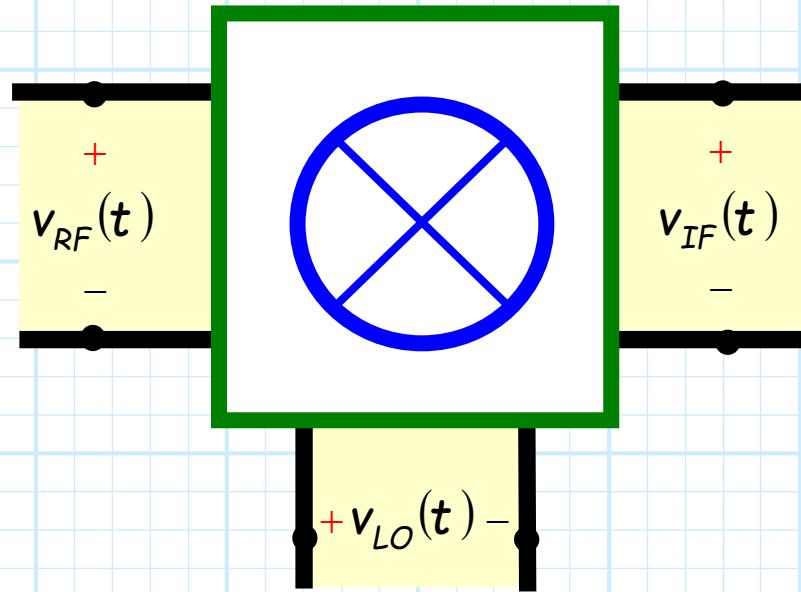
→ A mixer is a **multiplier** (\times) !!

An IDEAL Mixer

Say there is a real-valued signal $v_{RF}(t)$ at the RF mixer port, and a signal $v_{LO}(t)$ at the LO mixer port.

An ideal mixer would then produce at the IF port, a signal $v_{IF}(t)$, where:

$$v_{IF}(t) = v_{RF}(t) v_{LO}(t) \quad (\text{an ideal mixer})$$



REAL-valued multiplication

Note the multiplied voltages in this case (i.e., $v_{RF}(t)$ and $v_{LO}(t)$) are:

- a) real-valued, and
- b) some arbitrary function of time!

In other words, a mixer does **NOT** multiply two **complex** voltages (e.g., $V_{RF} = j$ and $V_{LO} = e^{j\pi/4}$)!

Instead, it multiplies two **arbitrary real-valued function of time**.

For example, if:

$$v_{RF}(t) = 2t - 3t^2 \quad \text{and} \quad v_{LO}(t) = 4t^2$$

then:

$$v_{IF}(t) = v_{RF}(t) v_{LO}(t) = 8t^3 - 12t^4$$

How and why?

Q: The *only* things I don't understand are:

- a) how this is possible, and
- b) why would this be useful?

A: Let's answer the **second** part (i.e., why would this be **useful**) first.

To see why multiplication might be **useful**, consider a case where both the RF and LO port signals are **time-harmonic**:

$$v_{RF}(t) = \cos[w_{RF}t] \quad \text{and} \quad v_{LO}(t) = \cos[w_{LO}t]$$

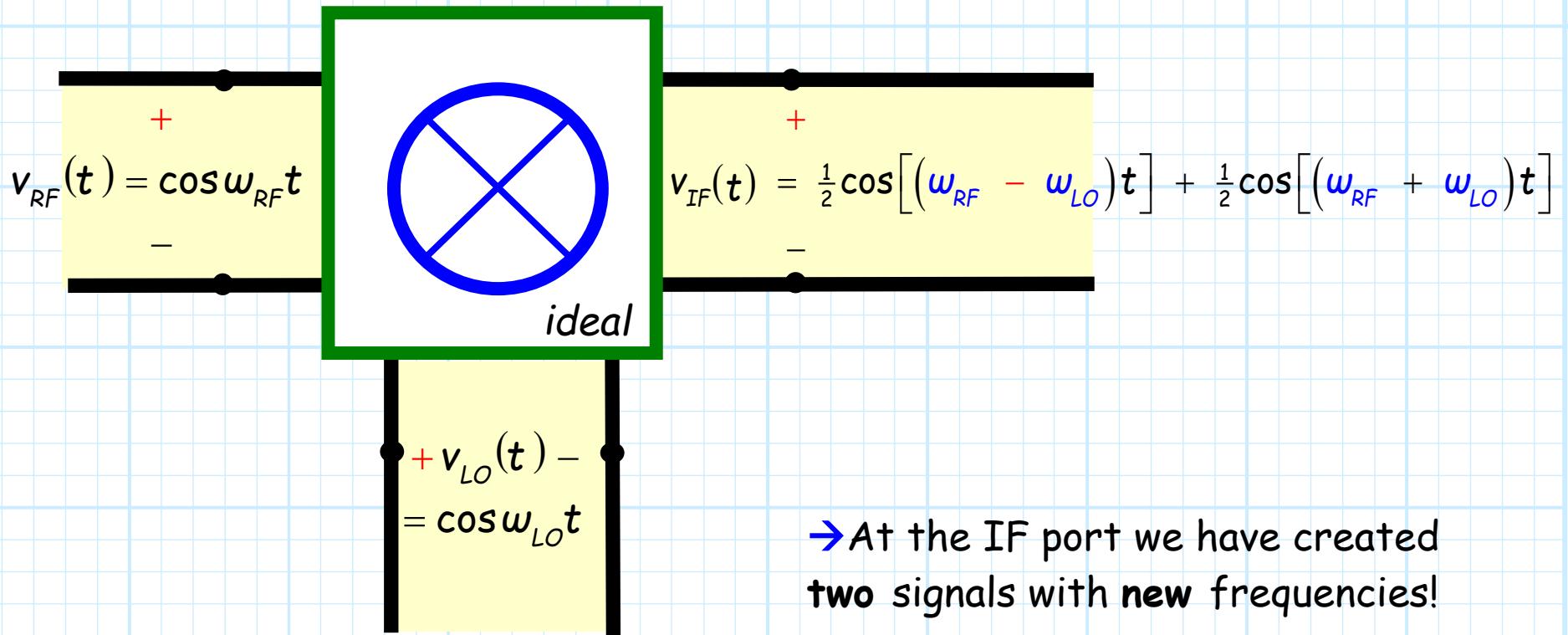
Note again that these are **NOT** complex values—they are instead **real-valued** functions of time!

The output of an IDEAL mixer

Multiplying these signals, we get (remember your trig identities!):

$$\begin{aligned} v_{IF}(t) &= v_{RF}(t) v_{LO}(t) \\ &= \cos[\omega_{RF} t] \cos[\omega_{LO} t] \\ &= \frac{1}{2} \cos[(\omega_{RF} - \omega_{LO})t] + \frac{1}{2} \cos[(\omega_{RF} + \omega_{LO})t] \end{aligned}$$

New signals are created!



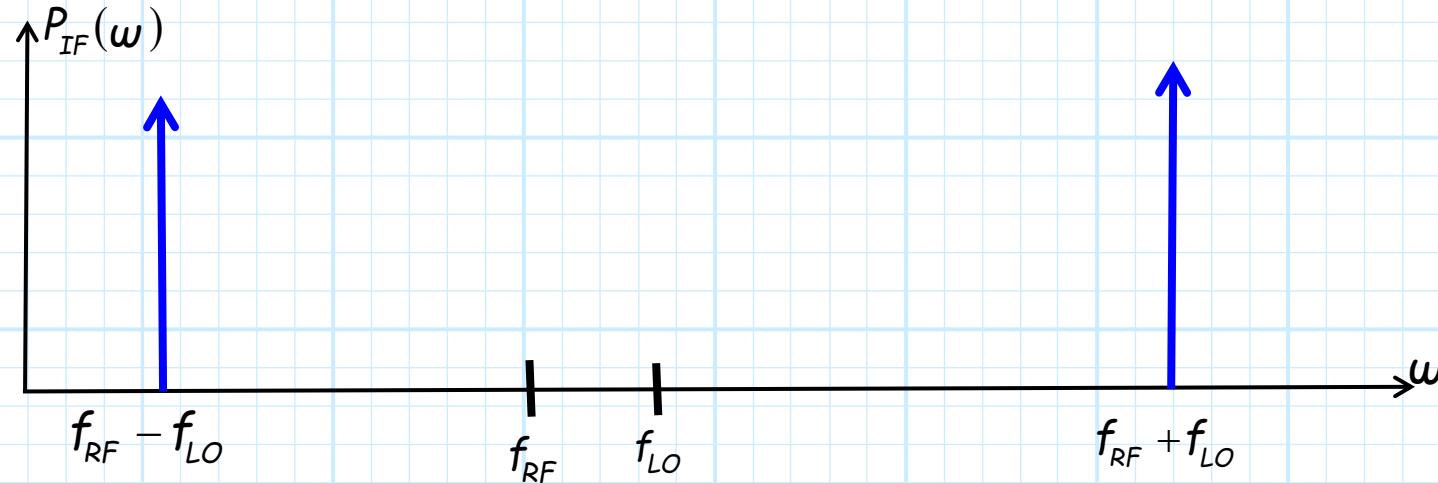
The IDEAL Mixer Output

One new signal has a frequency ω_Δ , that is the **difference** of the LO and RF signal frequencies:

$$\frac{1}{2} \cos[(\omega_{RF} - \omega_{LO})t] \doteq \frac{1}{2} \cos[\omega_\Delta t]$$

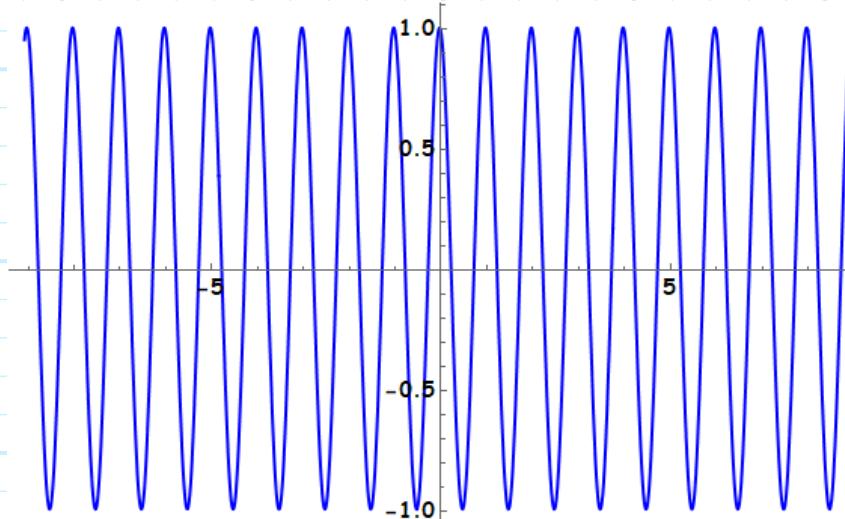
While the **other** new signal has a frequency ω_Σ , that is the **sum** of the LO and RF signal frequencies:

$$\frac{1}{2} \cos[(\omega_{RF} + \omega_{LO})t] \doteq \frac{1}{2} \cos[\omega_\Sigma t]$$



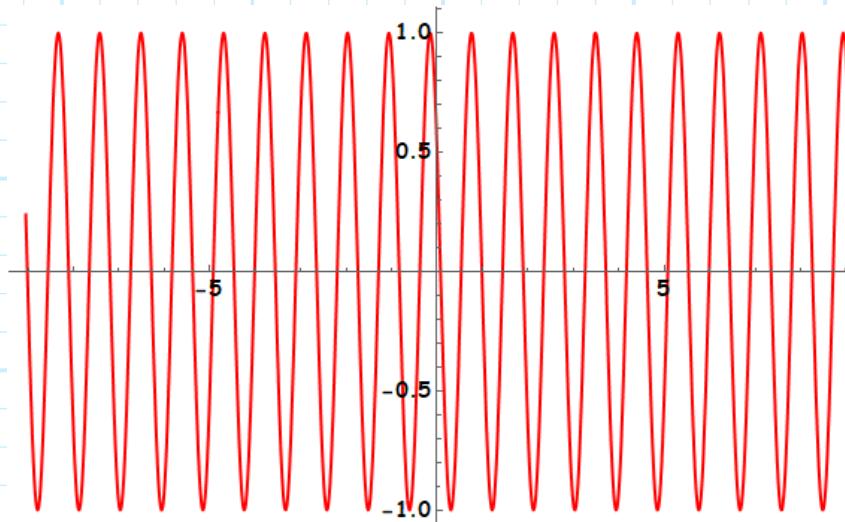
An example...

For example, consider this sinusoid with frequency $\omega_{LO} = 2.0\pi$:



$$v_{LO}(t) = \cos(2.0\pi t)$$

Along with this sinusoid, with higher frequency $\omega_{RF} = 2.2\pi$:

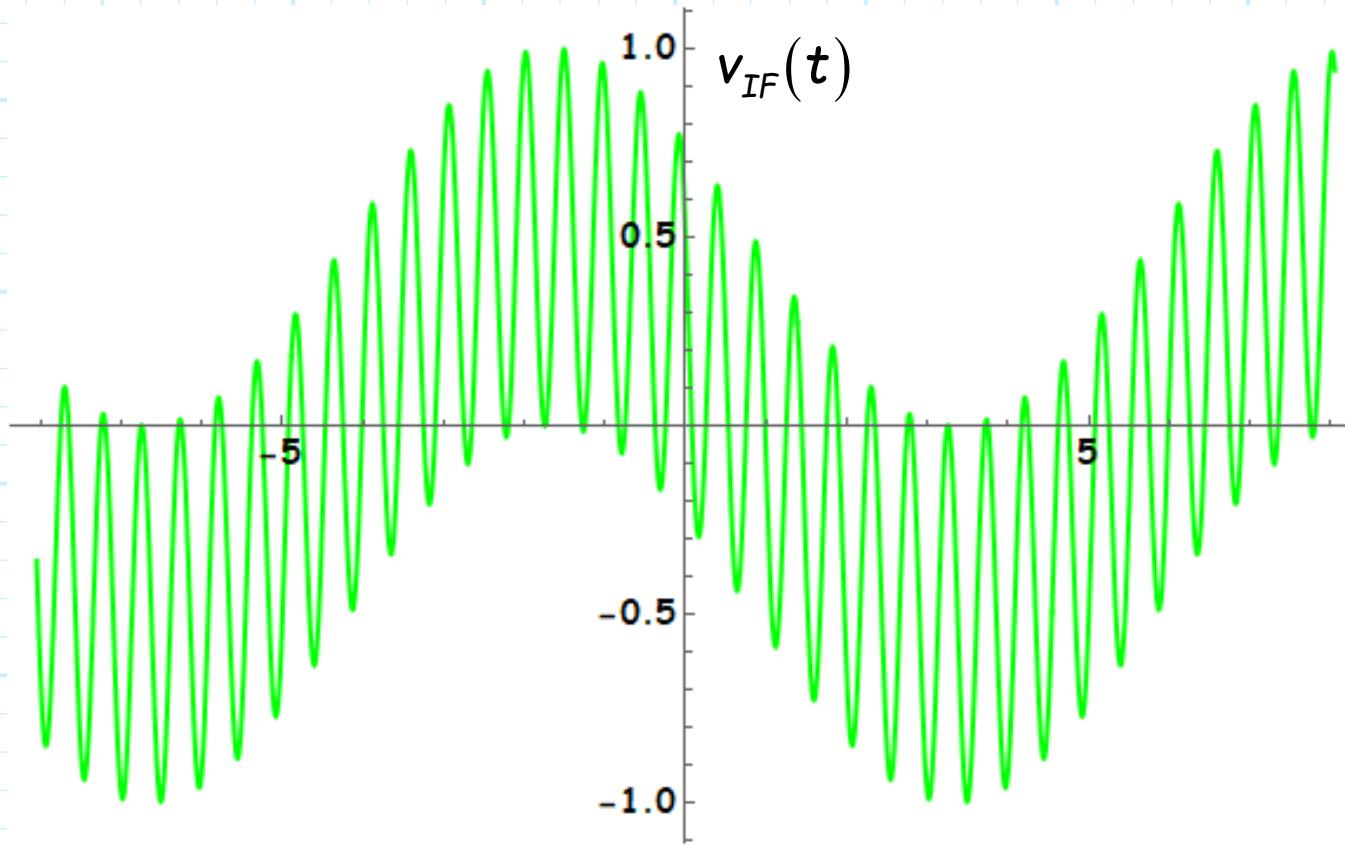


$$v_{RF}(t) = \cos(2.2\pi t + \pi/3)$$

The example output signal

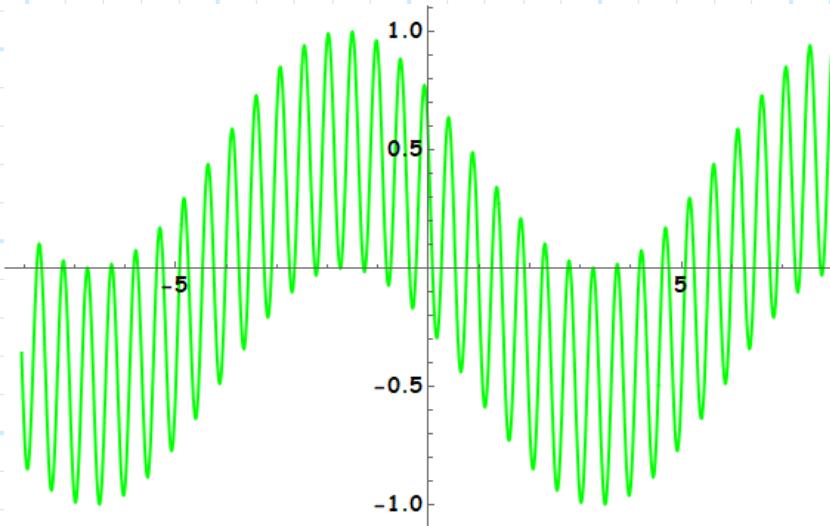
Multiplying these two signals together, we get:

$$\begin{aligned}v_{IF}(t) &= v_{RF}(t)v_{LO}(t) \\&= \cos(2.2\pi t + \pi/3) \cos(2.0\pi t) \\&= \frac{1}{2}\cos(0.2\pi t + \pi/3) + \frac{1}{2}\cos(4.2\pi t + \pi/3)\end{aligned}$$



Not the mess you think it is

Q: What a mess! I don't see two sinusoids in there at all!



A: Say we pass the above signal through a **bandpass filter**—one which rejects the higher frequency signal.

+

$$v_{IF}(t) = \frac{1}{2} \cos(0.2\pi t + \pi/3) + \frac{1}{2} \cos(4.2\pi t + \pi/3)$$

-

$T(\omega = 0.2\pi) = 1.0$

$T(\omega = 4.2\pi) \approx 0.0$

+

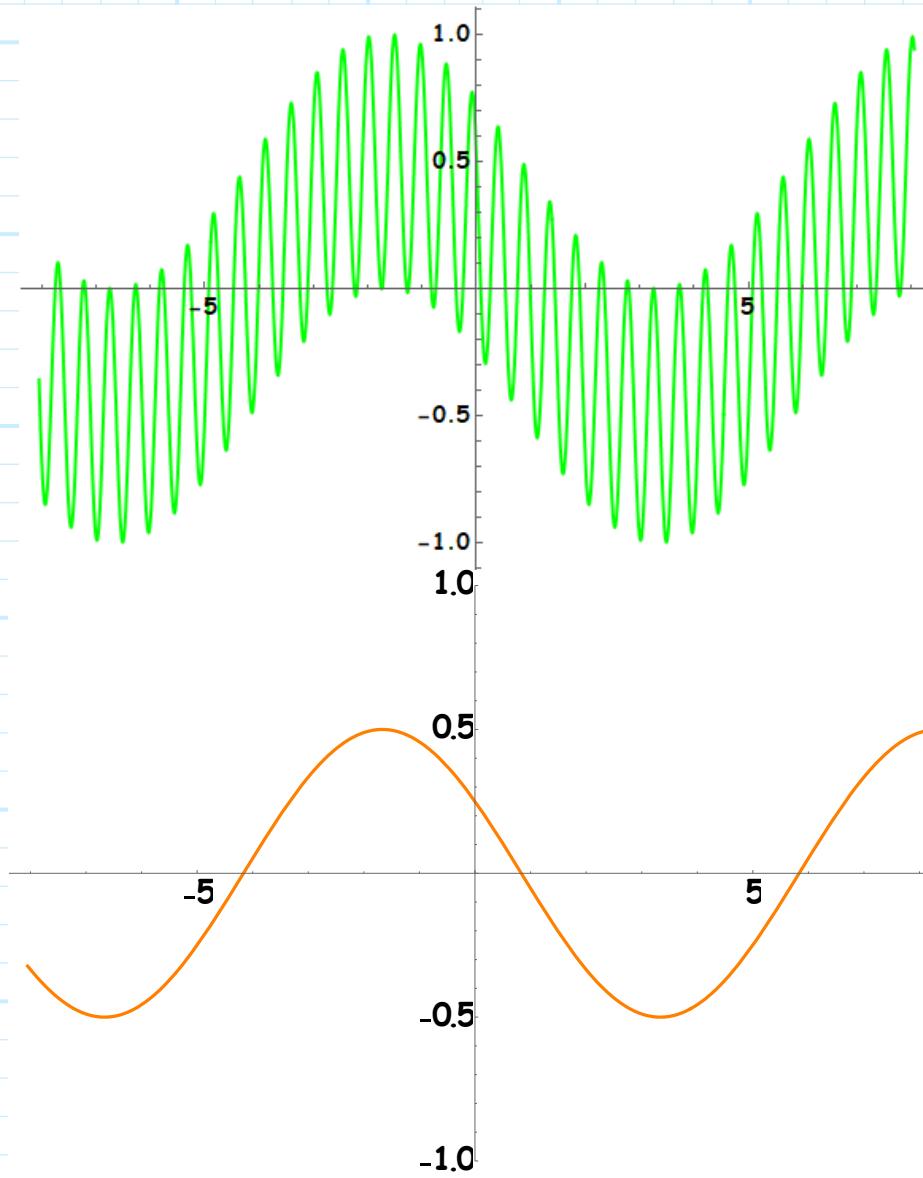
$$v_{IF}^{filtered}(t) \approx \frac{1}{2} \cos(0.2\pi t + \pi/3)$$

-

A low-frequency component

The output of the filter is thus simply the low-frequency component of $v_{IF}(t)$.

$$v_{IF}(t) = \frac{1}{2}\cos(0.2\pi t + \pi/3) + \frac{1}{2}\cos(4.2\pi t + \pi/3)$$



$$v_{IF}^{\text{filtered}}(t) \approx \frac{1}{2}\cos(0.2\pi t + \pi/3)$$

Or, the high-frequency component

Alternatively, we could pass the signal $v_{IF}(t)$ through a bandpass filter that rejects the low-frequency signal.

$$v_{IF}(t) = \frac{1}{2}\cos(0.2\pi t + \pi/3) + \frac{1}{2}\cos(4.2\pi t + \pi/3)$$

$$T(\omega = 0.2\pi) \approx 0.0$$

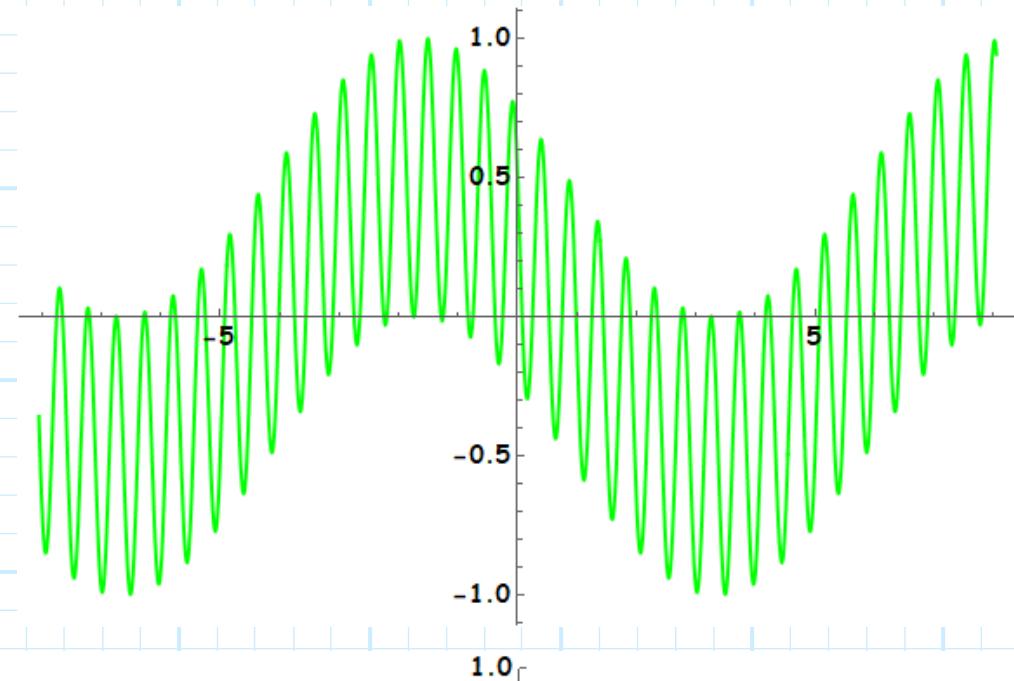
$$T(\omega = 4.2\pi) = 1.0$$

$$v_{IF}^{filtered}(t) \approx \frac{1}{2}\cos(4.2\pi t + \pi/3)$$

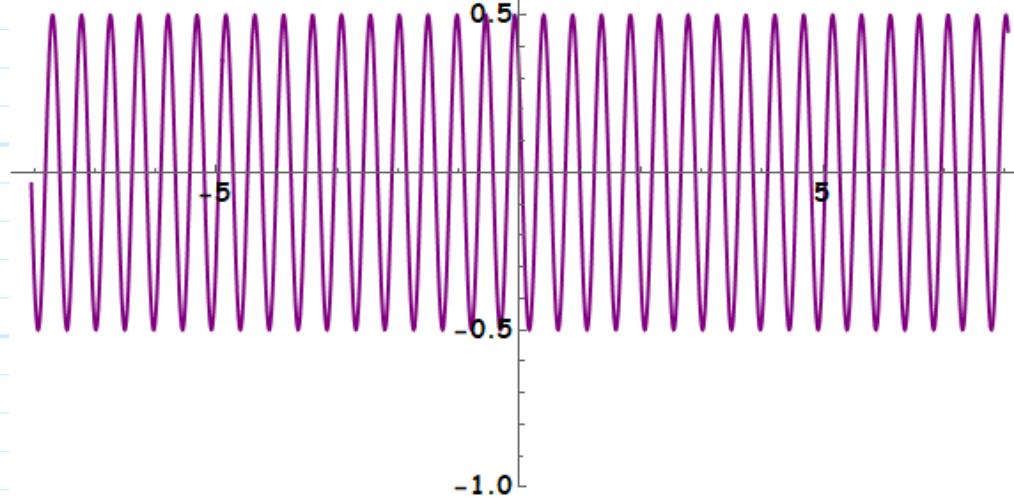
The output of the filter is thus simply the high-frequency component of $v_{IF}(t)$.

For example...

$$v_{IF}(t) = \frac{1}{2}\cos(0.2\pi t + \pi/3) + \frac{1}{2}\cos(4.2\pi t + \pi/3)$$



$$v_{IF}^{filtered}(t) \approx \frac{1}{2}\cos(4.2\pi t + \pi/3)$$



These don't behave like eigen functions!

Q: Wait!

You made a big, dramatic deal about sinusoids being "eigen functions".

You said that a sinusoid with a frequency ω at one place in a circuit would mean that everywhere in the circuit one would see the same sinusoid with the exact same frequency ω .

But.

You now provide an example where the input frequencies are $\omega = 2.0\pi$ and $\omega = 2.2\pi$ —yet the output frequencies are a remarkably different $\omega = 0.2\pi$ and $\omega = 4.2\pi$!

You must be really confused about this "eigen function" thing?

A mixer is NOT a linear device!

A: No confusion.

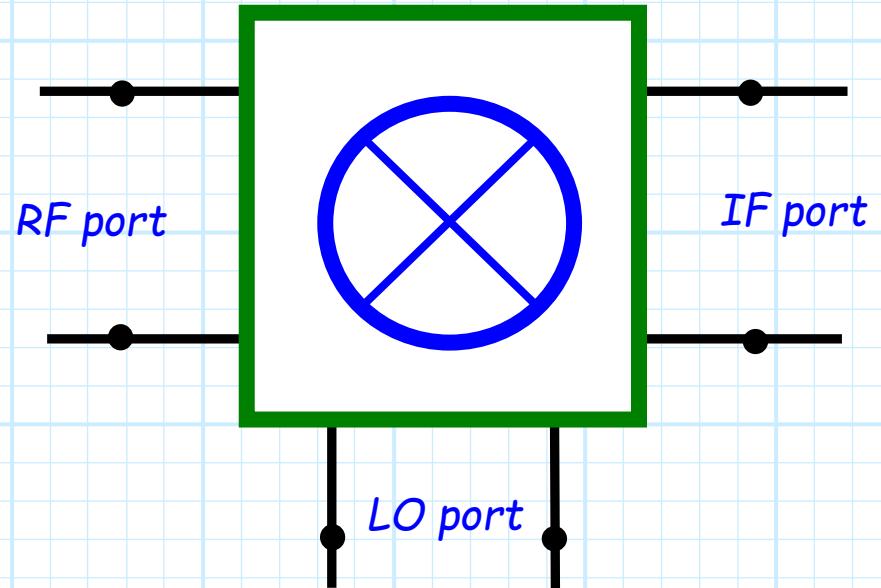
Sinusoids are the eigen functions of **ALL** linear, time-invariant circuits—but **ONLY** of linear, time-invariant circuits.

The mathematical operation:

$$v_{IF}(t) = v_{RF}(t) v_{LO}(t)$$

is decidedly **NON-linear**.

This means that an **ideal mixer** is likewise a **non-linear circuit**—the **frequencies of a sinusoid can thus be altered!**



A switch is a multiplier

Q: OK, so I'll return to my first question:

a) how is this possible?

A: Initially, it indeed appears the math associated with "signal multiplication":

$$v_{IF}(t) = v_{RF}(t) v_{LO}(t)$$

is inconsistent with any electrical engineering circuit element (e.g., resistor, capacitors, inductors, transistors, diodes), nor with any microwave components that we have previously studied.

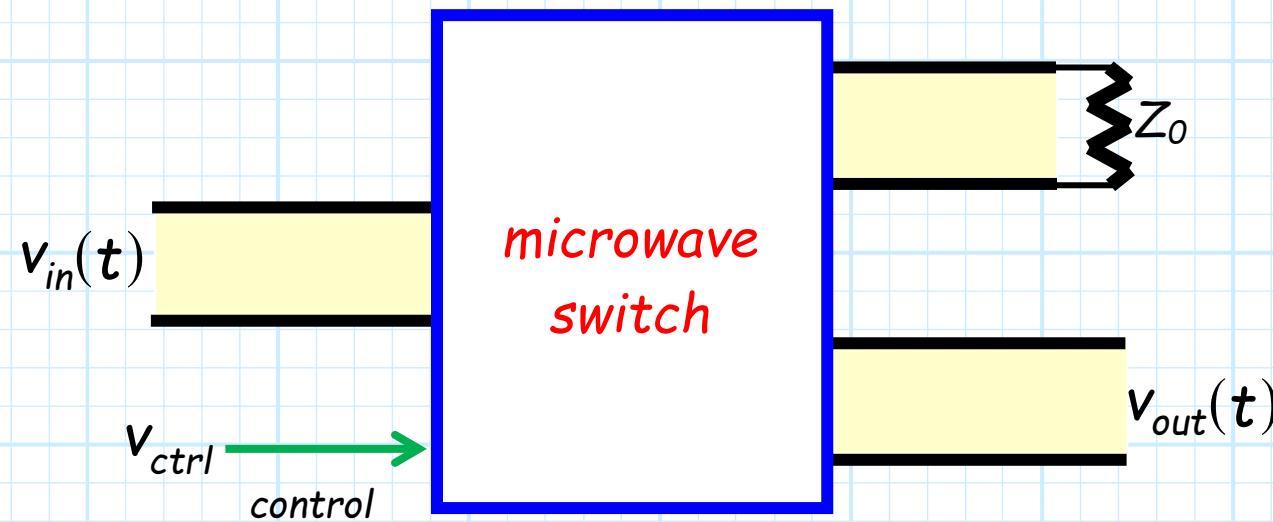
But, this initial appearance is not correct!

We in fact can achieve signal multiplication with the microwave device we just examined—the microwave switch!

Q: ?????

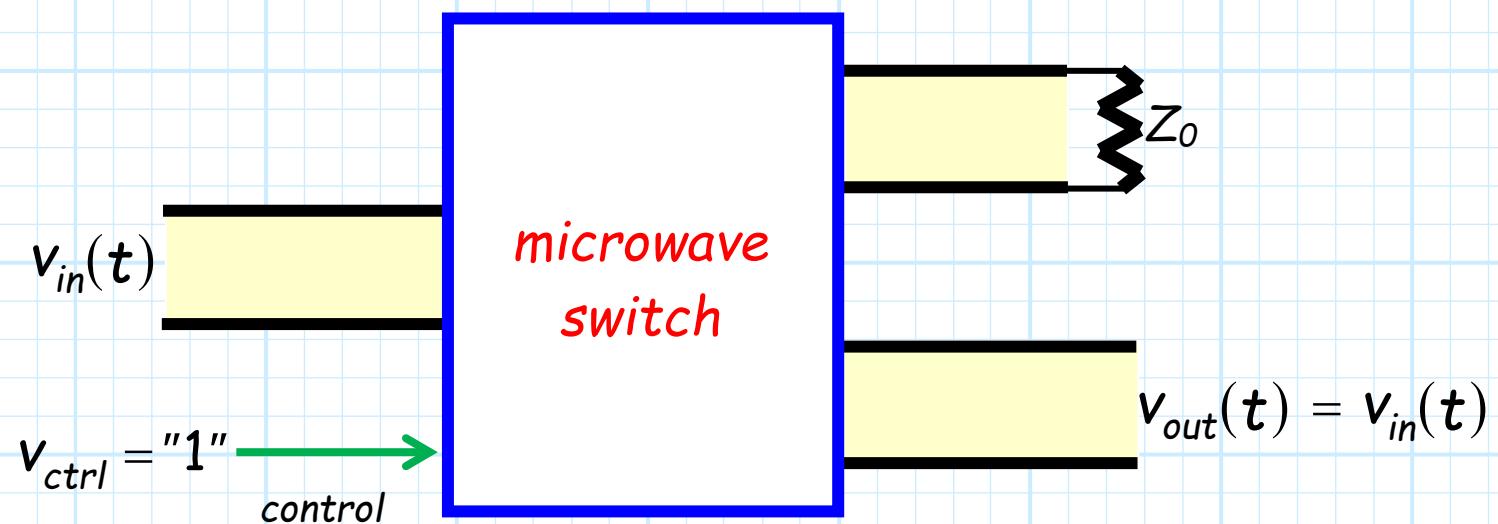
Again, a microwave switch

A: Consider this **switch** with an **input voltage** $v_{in}(t)$ and an **output voltage** $v_{out}(t)$:



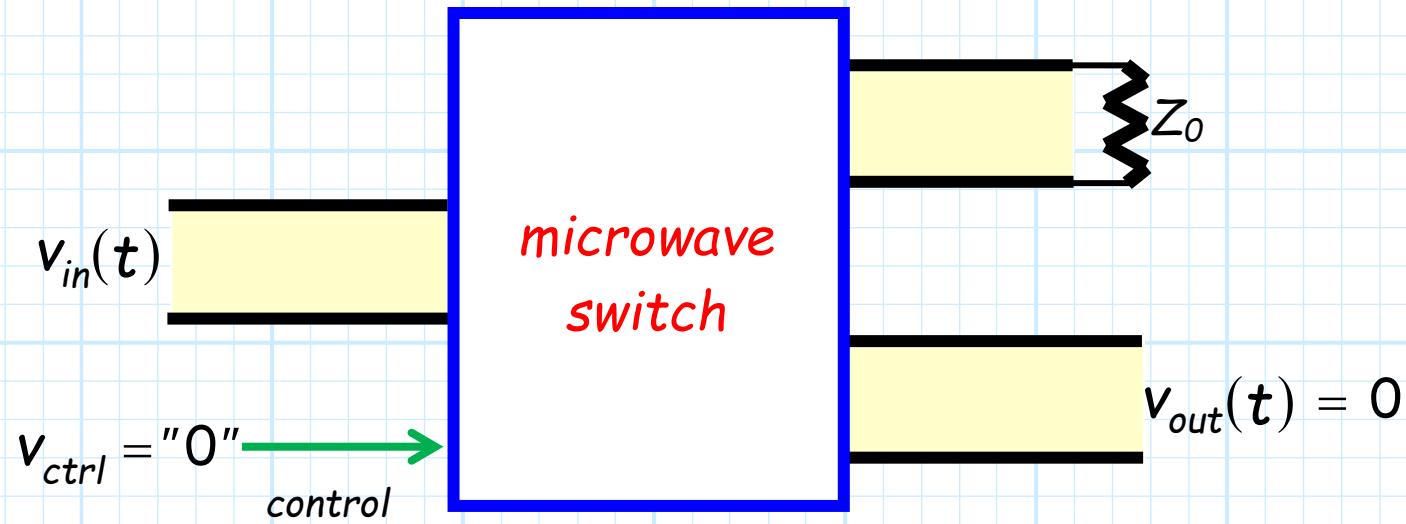
This state: the output is equal to the input

For one switch state, the output voltage (at least ideally) is **equal** to the input voltage:



This state: the output is equal to zero

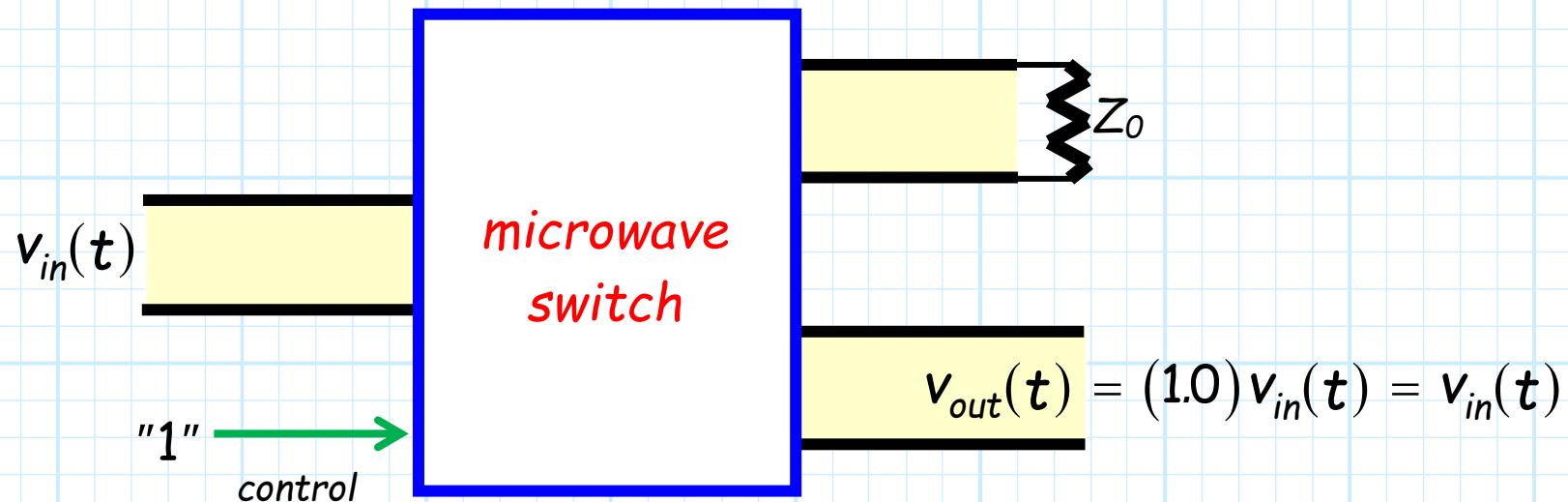
While for the other state, the output voltage is zero:



It's like it multiplies by one...

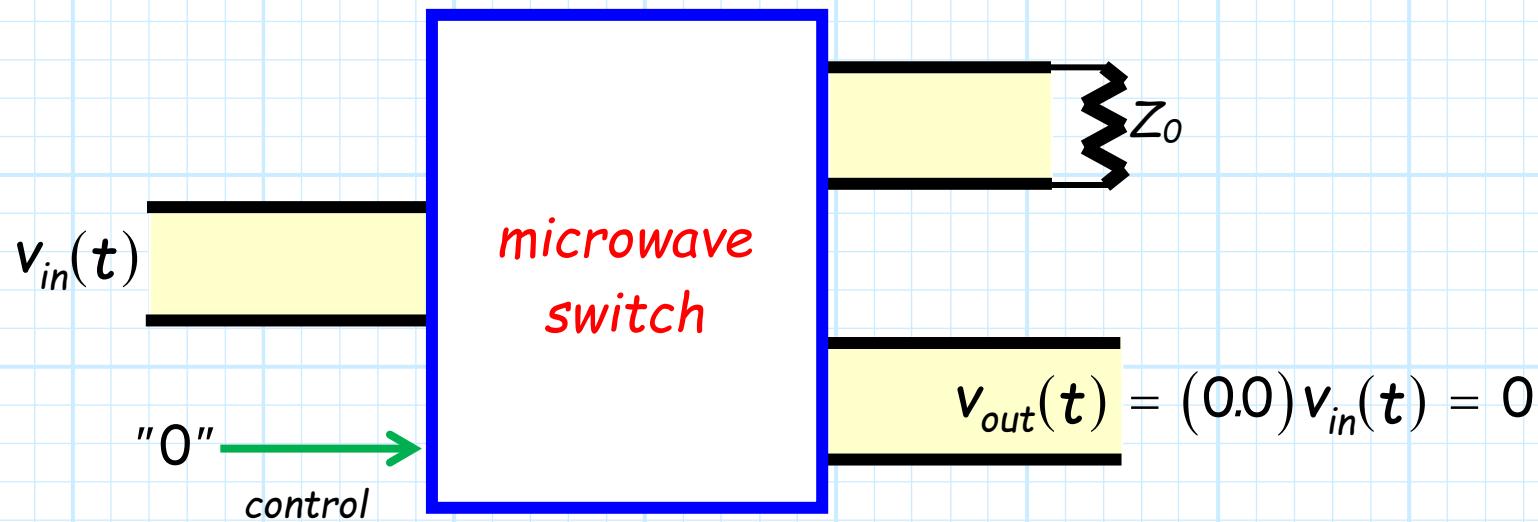
Although we know these results are determined from the internal circuitry of the switch (e.g., diodes or transistors), we could interpret these results in another way.

We could argue that for one state, the switch multiplies $v_{in}(t)$ with the value 1.0:



...or it multiples by zero

While for the other state, the switch multiplies $v_{in}(t)$ with the value 0.0:



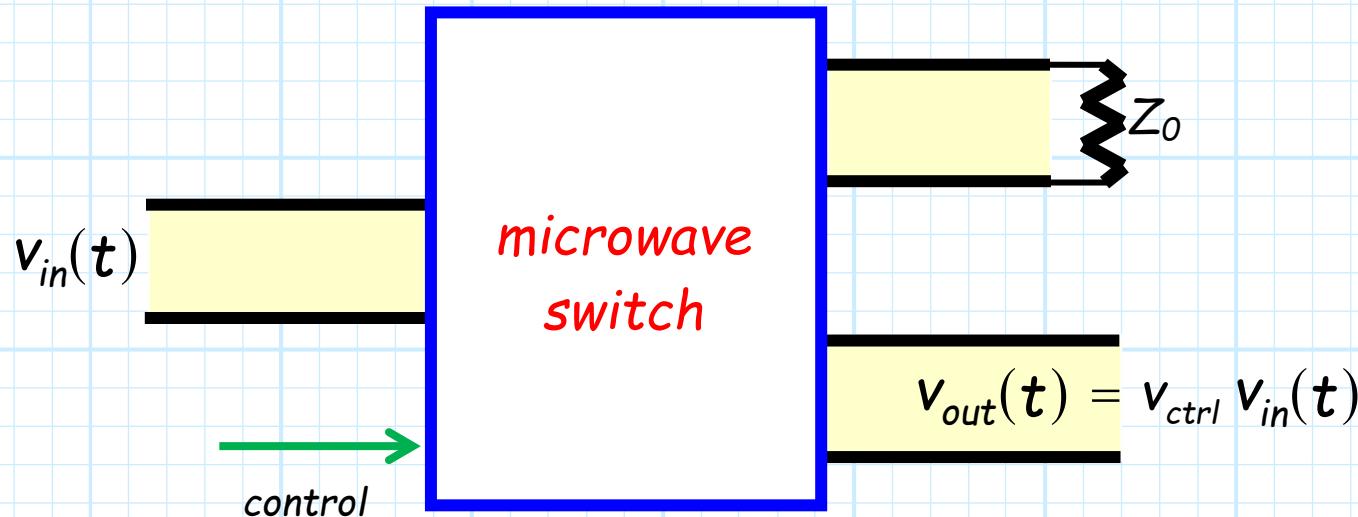
It's multiplied by a control voltage

Say now we define a control voltage v_{ctrl} , which can have either one of two states:

$$v_{ctrl} = 0.0 \quad \text{or} \quad v_{ctrl} = 1.0$$

we can write the switch output as:

$$v_{out}(t) = v_{ctrl} v_{in}(t)$$



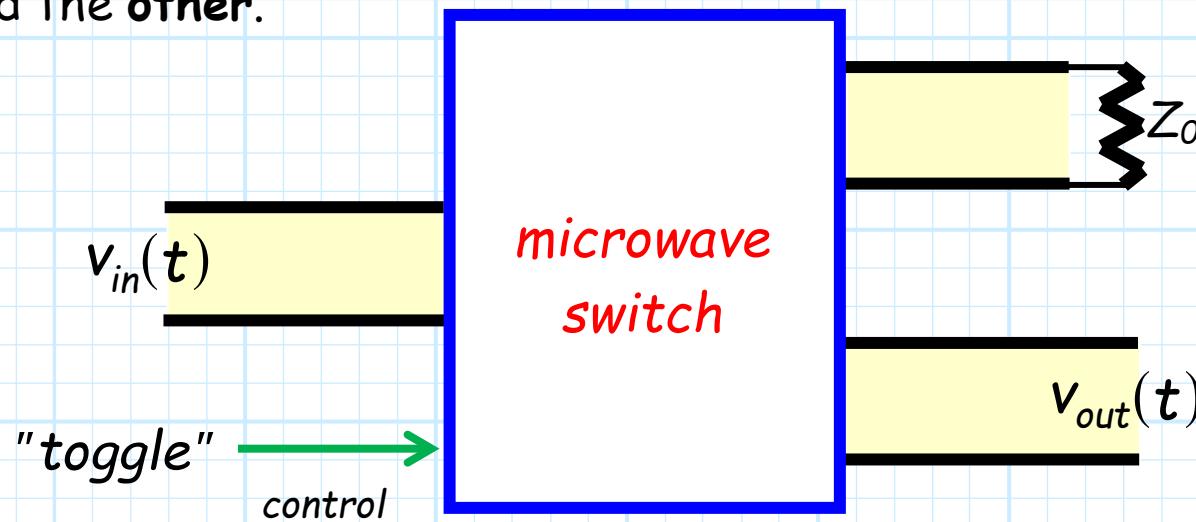
The switch appears to multiply voltages v_{ctrl} and $v_{in}(t)$!

Toggle the control

Q: This "multiplier" seems quite useless; nothing at all like:

$$\begin{aligned} v_{IF}(t) &= \cos(2.2\pi t + \pi/3) \cos(2.0\pi t) \\ &= \frac{1}{2}\cos(0.2\pi t + \pi/3) + \frac{1}{2}\cos(4.2\pi t + \pi/3) \end{aligned}$$

A: But, say we continuously "toggle" the switch control, between one state and the other.



The output will thus also **toggle** between a value of $v_{in}(t)=0$ and $v_{in}(t)=v_{out}(t)$.

We “chop” the input

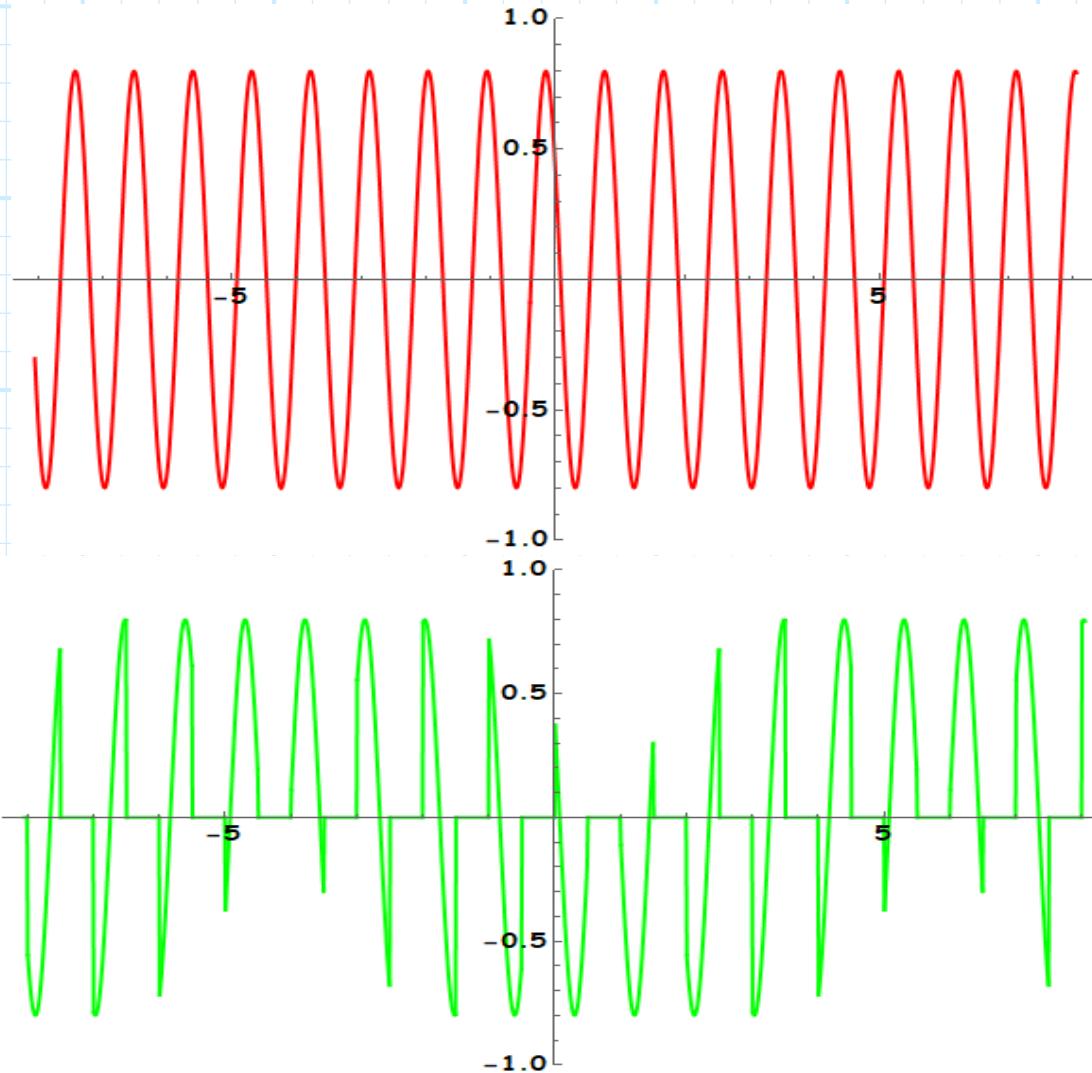
Say also that we toggle at a **constant rate**, and with a **50% duty cycle**.
The output will thus be a “chopped” version of the input:

$$v_{in}(t) =$$

$$0.8 \cos(2.2\pi t + \pi/3)$$

$$v_{out}(t)$$

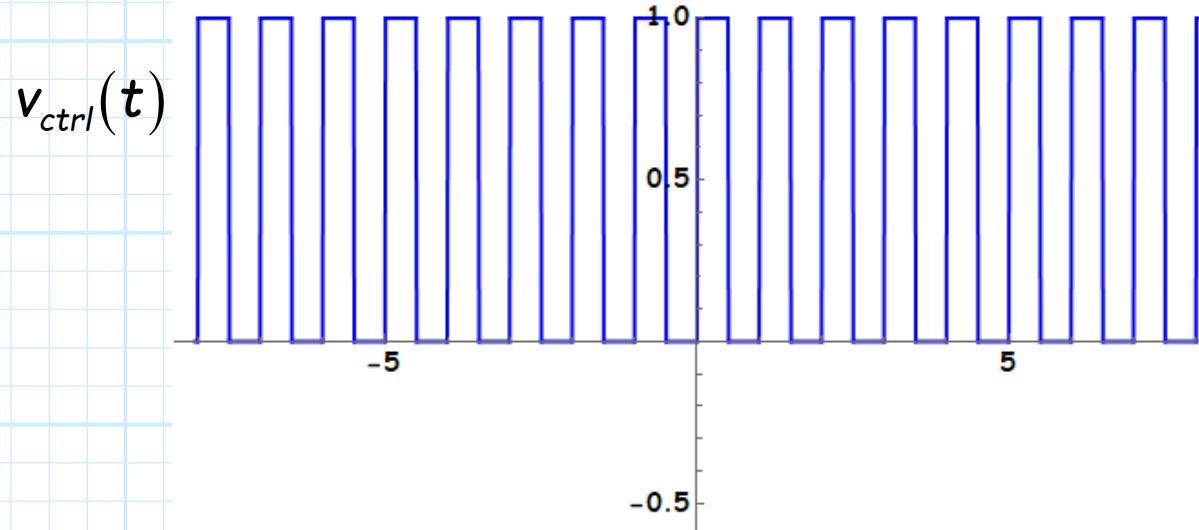
Q: ??????



"Chopping" is multiplying by a square wave

A: This "chopped" result can likewise be interpreted as multiplication!

The switch multiplies the **input voltage** $v_{in}(t)$ with a **control voltage** v_{ctrl} —a control voltage that **toggles** between a value of $v_{ctrl} = 0.0$ and $v_{ctrl} = 1.0$!



The control voltage is a "square wave"!

One signal must be a square wave

Thus, a microwave switch can be used as a device that multiplies some arbitrary input signal $v_{in}(t)$ with some arbitrary square wave $v_{ctrl}(t)$!

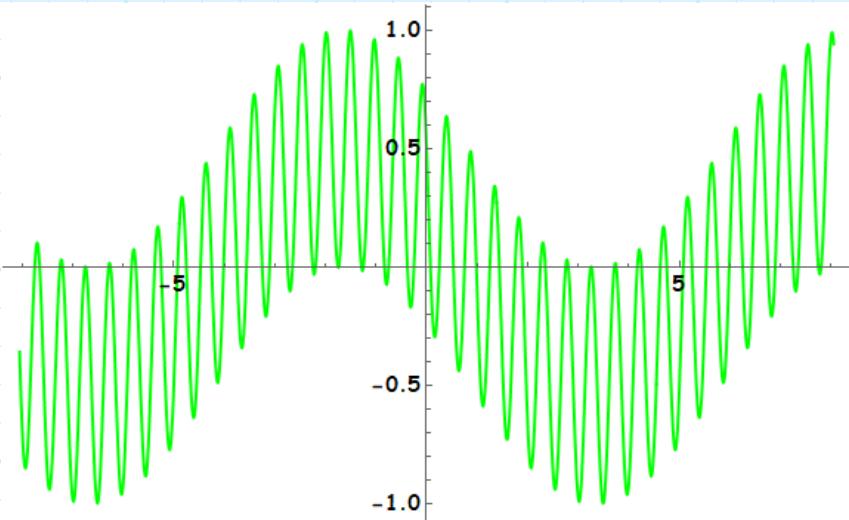
Q: I don't understand.

You said a mixer can be used to multiply two sinusoids, giving the quite useful output:

$$v_{IF}(t) = v_{RF}(t)v_{LO}(t)$$

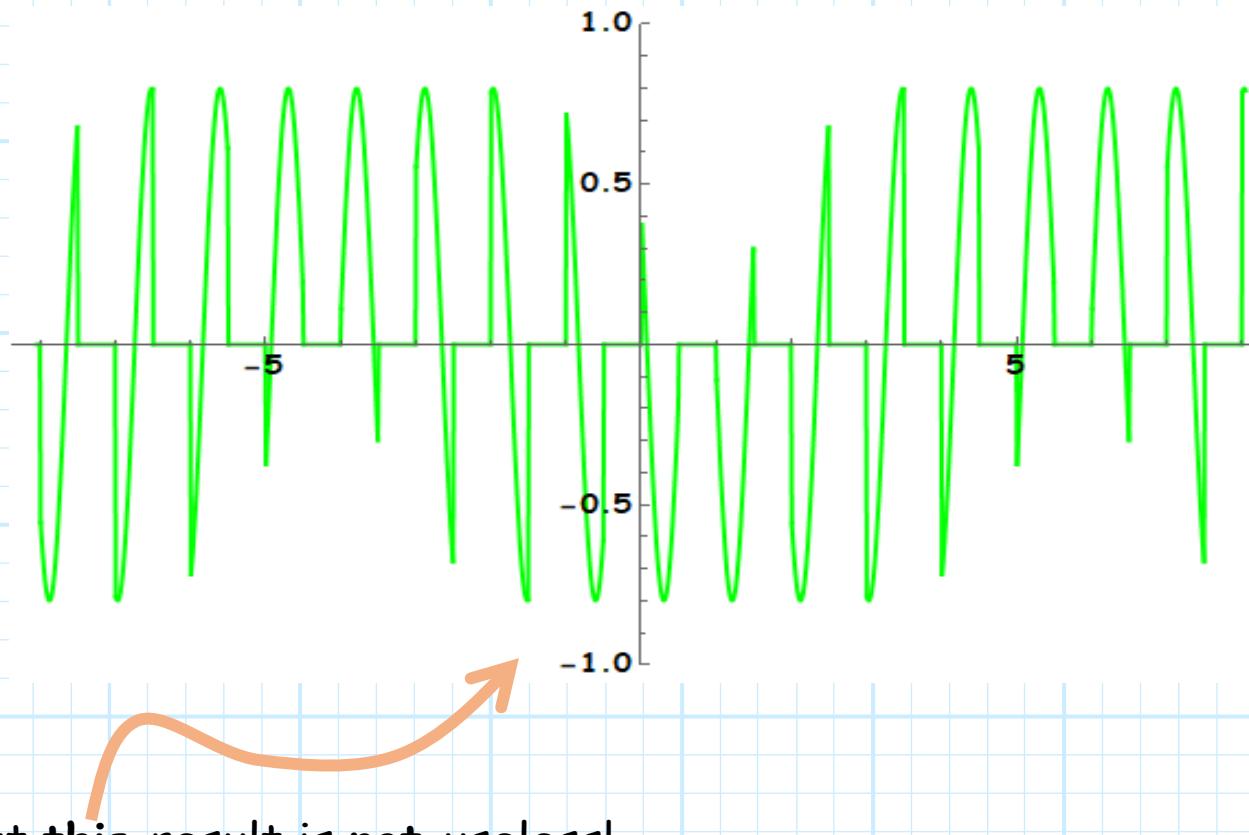
$$= \cos(2.2\pi t + \pi/3) \cos(2.0\pi t)$$

$$= \frac{1}{2}\cos(0.2\pi t + \pi/3) + \frac{1}{2}\cos(4.2\pi t + \pi/3)$$



Apparently, both ugly and useless

But, this switch “multiplier” can only multiply a sinusoid and a square wave, giving a result both ugly and apparently useless:



A: But this result is not useless!

As usual, the Fourier transform reveals all

The usefulness of this switch multiplier output is revealed by examining it in the frequency domain—i.e., by evaluating its Fourier Transform:

$$V_{out}(w) = \int_{-\infty}^{\infty} v_{out}(t) e^{+jwt} dt = \int_{-\infty}^{\infty} v_{in}(t) v_{ctrl}(t) e^{+jwt} dt$$

Q: I'm slightly embarrassed to admit that I'm not really sure how to evaluate this integral.

A: YOU of course recall that:

the Fourier Transform of the product of two functions is simply the convolution of the Fourier Transform of each separate function!

Trust me, it makes things WAY easier

In other "words", for our **multiplier**:

$$V_{out}(w) = V_{in}(w) * V_{ctrl}(w)$$

where:

$$V_{in}(w) = \int_{-\infty}^{\infty} v_{in}(t) e^{+j\omega t} dt \quad \text{and} \quad V_{ctrl}(w) = \int_{-\infty}^{\infty} v_{ctrl}(t) e^{+j\omega t} dt$$

This makes things much easier.

Q: Umm...it appears to me to instead to make things much more difficult.

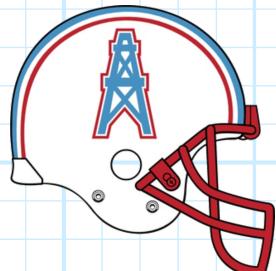
A: Not for this problem! (You can skip ahead to page 50 if you want).

Consider arbitrary sinusoid at the input

Consider an arbitrary sinusoidal input function of the form:

$$v_{in}(t) = A_{in} \cos(\omega_{in}t + \varphi_{in})$$

From Euler's identity, this input can be expressed as:



$$\begin{aligned} v_{in}(t) &= A_{in} \cos(\omega_{in}t + \varphi_{in}) \\ &= \frac{1}{2} A_{in} (e^{+j(\omega_{in}t + \varphi_{in})} + e^{-j(\omega_{in}t + \varphi_{in})}) \\ &= \frac{1}{2} A_{in} e^{+j\varphi_{in}} e^{+j\omega_{in}t} + \frac{1}{2} A_{in} e^{-j\varphi_{in}} e^{-j\omega_{in}t} \end{aligned}$$

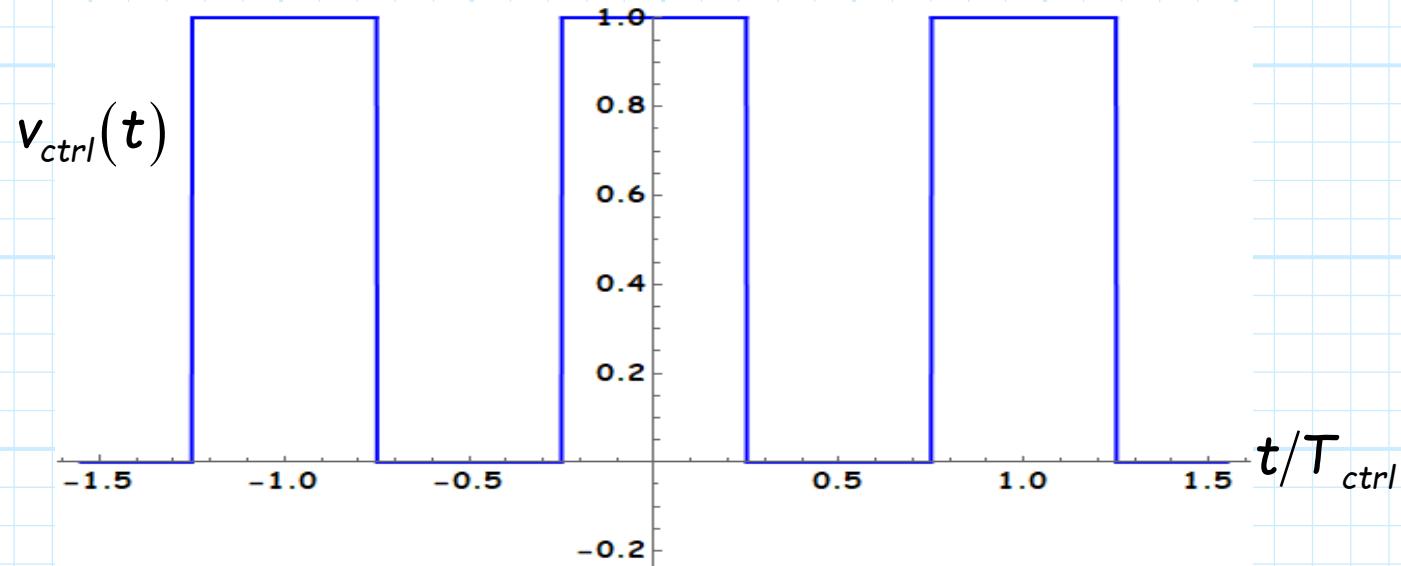
Impulse functions—make sure you understand them!

The Fourier Transform of this arbitrary sinusoid is thus:

$$\begin{aligned}
 V_{in}(\omega) &= \int_{-\infty}^{\infty} v_{in}(t) e^{+j\omega t} dt \\
 &= \int_{-\infty}^{\infty} \left(\frac{1}{2} A_{in} e^{+j\varphi_{in}} e^{+j\omega_{in}t} + \frac{1}{2} A_{in} e^{-j\varphi_{in}} e^{-j\omega_{in}t} \right) e^{+j\omega t} dt \\
 &= \frac{1}{2} A_{in} e^{+j\varphi_{in}} \int_{-\infty}^{\infty} e^{+j(\omega + \omega_{in})t} dt + \frac{1}{2} A_{in} e^{-j\varphi_{in}} \int_{-\infty}^{\infty} e^{+j(\omega - \omega_{in})t} dt \\
 &= \frac{1}{2} A_{in} e^{-j\varphi_{in}} 2\pi \delta(\omega + \omega_{in}) + \frac{1}{2} A_{in} e^{+j\varphi_{in}} 2\pi \delta(\omega - \omega_{in}) \\
 &= \pi A_{in} e^{-j\varphi_{in}} \delta(\omega + \omega_{in}) + \pi A_{in} e^{+j\varphi_{in}} \delta(\omega - \omega_{in})
 \end{aligned}$$

A periodic square wave

Now the **square-wave** control voltage, which is **periodic** with time T_{ctrl} :



Mathematically, this is described as:

$$v_{LO}(t) = \begin{cases} 0 & (n - \frac{1}{2})T_{ctrl} < t < (n - \frac{1}{4})T_{ctrl} \\ 1 & (n - \frac{1}{4})T_{ctrl} < t < (n + \frac{1}{4})T_{ctrl} \\ 0 & (n + \frac{1}{4})T_{ctrl} < t < (n + \frac{1}{2})T_{ctrl} \end{cases}$$

where n is any arbitrary integer.

Its Fourier transform

The Fourier transform of this square-wave is therefore:

$$\begin{aligned}
 V_{ctrl}(w) &= \int_{-\infty}^{\infty} v_{ctrl}(t) e^{+j\omega t} dt \\
 &= \sum_n \left(\int_{(n-\frac{1}{2})T_{ctrl}}^{(n-\frac{1}{4})T_{ctrl}} 0 e^{+j\omega t} dt + \int_{(n-\frac{1}{4})T_{ctrl}}^{(n+\frac{1}{4})T_{ctrl}} 1 e^{+j\omega t} dt + \int_{(n+\frac{1}{4})T_{ctrl}}^{(n+\frac{1}{2})T_{ctrl}} 0 e^{+j\omega t} dt \right) \\
 &= \sum_n \int_{(n-\frac{1}{4})T_{ctrl}}^{(n+\frac{1}{4})T_{ctrl}} e^{+j\omega t} dt
 \end{aligned}$$

Evaluating that integral

Evaluating the **integral** of this last result:

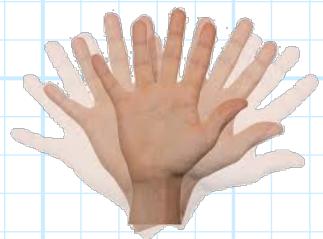
$$\begin{aligned}
 \int_{(n-\frac{1}{4})T_{ctrl}}^{(n+\frac{1}{4})T_{ctrl}} e^{+j\omega t} dt &= \frac{1}{j\omega} e^{+j\omega t} \Big|_{(n-\frac{1}{4})T_{ctrl}}^{(n+\frac{1}{4})T_{ctrl}} \\
 &= \frac{1}{j\omega} \left(e^{+j\omega(n+\frac{1}{4})T_{ctrl}} - e^{+j\omega(n-\frac{1}{4})T_{ctrl}} \right) \\
 &= \frac{e^{+jn\omega T_{ctrl}}}{j\omega} \left(e^{+j\omega T_{ctrl}/4} - e^{-j\omega T_{ctrl}/4} \right) \\
 &= \frac{e^{+jn\omega T_{ctrl}}}{j\omega} \left(j2 \sin[\omega T_{ctrl}/4] \right) \\
 &= \frac{T_{ctrl}}{2} \left(\frac{\sin[\omega T_{ctrl}/4]}{\omega T_{ctrl}/4} \right) e^{+jn\omega T_{ctrl}}
 \end{aligned}$$

I'm kinda embarrassed

And so the Fourier transform of the square wave is:

$$\begin{aligned}
 V_{ctrl}(\omega) &= \int_{-\infty}^{\infty} v_{ctrl}(t) e^{+j\omega t} dt \\
 &= \sum_n \int_{(n-\frac{1}{4})T_{ctrl}}^{(n+\frac{1}{4})T_{ctrl}} e^{+j\omega t} dt \\
 &= \sum_n \frac{T_{ctrl}}{2} \left(\frac{\sin[\omega T_{ctrl}/4]}{\omega T_{ctrl}/4} \right) e^{+jn\omega T_{ctrl}} \\
 &= \frac{T_{ctrl}}{2} \left(\frac{\sin[\omega T_{ctrl}/4]}{\omega T_{ctrl}/4} \right) \sum_n e^{+jn\omega T_{ctrl}}
 \end{aligned}$$

The summation can be shown (hand-waving time!) to be:



$$\sum_{n=-\infty}^{\infty} e^{+jn\omega T_{ctrl}} = \frac{1}{T_{ctrl}} \sum_{n=-\infty}^{\infty} \delta\left(\omega - n\left(\frac{2\pi}{T_{ctrl}}\right)\right)$$

The result

Defining:

$$f_{ctrl} \doteq \frac{1}{T_{ctrl}}$$

and

$$\omega_{ctrl} \doteq 2\pi f_{ctrl} = \frac{2\pi}{T_{ctrl}}$$

this summation is then:

$$\sum_n e^{+jn\omega T_{ctrl}} = \frac{1}{T_{ctrl}} \sum_n \delta(\omega - n\left(\frac{2\pi}{T_{ctrl}}\right)) = \frac{1}{T_{ctrl}} \sum_n \delta(\omega - n\omega_{ctrl})$$

And so finally:

$$\begin{aligned} V_{ctrl}(\omega) &= \int_{-\infty}^{\infty} v_{ctrl}(t) e^{+j\omega t} dt \\ &= \frac{T_{ctrl}}{2} \left(\frac{\sin[\omega T_{ctrl}/4]}{\omega T_{ctrl}/4} \right) \sum_n e^{+jn\omega T_{ctrl}} \\ &= \frac{1}{2} \left(\frac{\sin[\omega T_{ctrl}/4]}{\omega T_{ctrl}/4} \right) \sum_n \delta(\omega - n\omega_{ctrl}) \end{aligned}$$

In summary

So, we have determined the Fourier transform of the input sinusoid:

$$V_{in}(w) = \pi A_{in} e^{-j\varphi_{in}} \delta(w + \omega_{in}) + \pi A_{in} e^{+j\varphi_{in}} \delta(w - \omega_{in})$$

And also for the control square wave:

$$V_{ctrl}(w) = \frac{1}{2} \left(\frac{\sin[wT_{ctrl}/4]}{wT_{ctrl}/4} \right) \sum_n \delta(w - n\omega_{ctrl})$$

Not as difficult as it looks

The Fourier transform of the **output** signal $v_{out}(t) = v_{in}(t)v_{ctrl}(t)$ is therefore the **convolution** of these two spectra:

$$\begin{aligned} V_{out}(w) &= \int_{-\infty}^{\infty} v_{out}(t) e^{+j\omega t} dt \\ &= V_{in}(w) * V_{ctrl}(w) \\ &= \int_{-\infty}^{\infty} V_{in}(w-w') V_{ctrl}(w') dw' \end{aligned}$$

Q: I thought you said this would be **easy**?

A: It is easy!

The Dirac delta function!

$$\begin{aligned}
 V_{out}(\omega) &= \int_{-\infty}^{\infty} V_{in}(\omega - \omega') V_{ctrl}(\omega') d\omega' \\
 &= \int_{-\infty}^{\infty} \pi V_{in} e^{-j\varphi} \delta(\omega - \omega' - \omega_{in}) \sum_n \frac{1}{2} \left(\frac{\sin[\omega' T_{ctrl}/4]}{\omega' T_{ctrl}/4} \right) \delta(\omega' - n\omega_{ctrl}) d\omega' \\
 &\quad + \int_{-\infty}^{\infty} \pi V_{in} e^{+j\varphi} \delta(\omega - \omega' + \omega_{in}) \sum_n \frac{1}{2} \left(\frac{\sin[\omega' T_{ctrl}/4]}{\omega' T_{ctrl}/4} \right) \delta(\omega' - n\omega_{ctrl}) d\omega' \\
 &= V_{in} e^{-j\varphi} \frac{\pi}{2} \sum_n \int_{-\infty}^{\infty} \delta(\omega - \omega' - \omega_{in}) \left(\frac{\sin[\omega' T_{ctrl}/4]}{\omega' T_{ctrl}/4} \right) \delta(\omega' - n\omega_{ctrl}) d\omega' \\
 &\quad + V_{in} e^{+j\varphi} \frac{\pi}{2} \sum_n \int_{-\infty}^{\infty} \delta(\omega - \omega' + \omega_{in}) \left(\frac{\sin[\omega' T_{ctrl}/4]}{\omega' T_{ctrl}/4} \right) \delta(\omega' - n\omega_{ctrl}) d\omega'
 \end{aligned}$$

Q: I'm still not seeing easy anywhere.

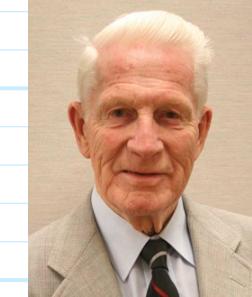
A: Look closely at the integrals—they involve **Dirac delta function** $\delta(x)$!

As a professor once said to me

And, integrating with the Dirac delta function is "joy itself"!

Recall that:

$$\int_{-\infty}^{\infty} f(x) \delta(x) dx = f(x=0)$$



In other words, we evaluate the integral simply by evaluating the function $f(x)$ at $x=0$ (the result $f(x=0)$ is thus a number).

A corollary to this result is the "sampling integral":

$$\int_{-\infty}^{\infty} f(x) \delta(x-c) dx = f(x=c)$$

The integral returns the value of function $f(x)$, evaluated at some arbitrary value $x=c$ (e.g., $x=2.7$).

Cake simple

Happily, our integrals involve the Dirac delta function:

$$\delta(w' - nw_{ctrl})$$

Thus, we simply evaluate the remainder of the integrand at $w' = nw_{ctrl}$:

$$\begin{aligned} & \int_{-\infty}^{\infty} \delta(w - w' - w_{in}) \left(\frac{\sin[w' T_{ctrl}/4]}{w' T_{ctrl}/4} \right) \delta(w' - nw_{ctrl}) dw' \\ &= \delta(w - nw_{ctrl} - w_{in}) \left(\frac{\sin[nw_{ctrl} T_{ctrl}/4]}{nw_{ctrl} T_{ctrl}/4} \right) \end{aligned}$$



Wait! It gets even better!

And so:

$$\begin{aligned} V_{\text{out}}(\omega) &= V_{\text{in}} e^{-j\varphi} \frac{\pi}{2} \sum_n \delta(\omega - n\omega_{\text{ctrl}} - \omega_{\text{in}}) \left(\frac{\sin[n\omega_{\text{ctrl}} T_{\text{ctrl}}/4]}{n\omega_{\text{ctrl}} T_{\text{ctrl}}/4} \right) \\ &+ V_{\text{in}} e^{+j\varphi} \frac{\pi}{2} \sum_n \delta(\omega - n\omega_{\text{ctrl}} + \omega_{\text{in}}) \left(\frac{\sin[n\omega_{\text{ctrl}} T_{\text{ctrl}}/4]}{n\omega_{\text{ctrl}} T_{\text{ctrl}}/4} \right) \end{aligned}$$

Now, recalling that:

$$\omega_{\text{ctrl}} \doteq 2\pi f_{\text{ctrl}} = \frac{2\pi}{T_{\text{ctrl}}}$$

So that:

$$n\omega_{\text{ctrl}} T_{\text{ctrl}} = n2\pi$$

Simple

We can express:

$$\frac{\sin[nw_{ctrl} T_{ctrl}/4]}{nw_{ctrl} T_{ctrl}/4} = \frac{\sin[n2\pi/4]}{n2\pi/4nw_{ctrl}} = \frac{\sin[n(\pi/2)]}{n(\pi/2)}$$

So that finally:

$$V_{out}(w) = V_{in} e^{-j\varphi} \frac{\pi}{2} \sum_n \delta(w - nw_{ctrl} - w_{in}) \frac{\sin[n(\pi/2)]}{n(\pi/2)} + V_{in} e^{+j\varphi} \frac{\pi}{2} \sum_n \delta(w - nw_{ctrl} + w_{in}) \frac{\sin[n(\pi/2)]}{n(\pi/2)}$$

Even values result in zero

Evaluating over different integers n :

n	$\frac{\sin[n(\pi/2)]}{n(\pi/2)}$
-4	0
-3	$2/(3\pi)$
-2	0
-1	$2/\pi$
0	1.0
+1	$2/\pi$
+2	0
+3	$2/(3\pi)$
+4	0

Even simpler

It is apparent that all (non-zero) **even** values of integer n result in a **zero** value, and that odd values of n result in $(2/|n|\pi)$.

Therefore:

$$\begin{aligned}
 V_{out}(\omega) &= V_{in} e^{-j\varphi} \frac{\pi}{2} \left(\delta(\omega - \omega_{in}) + \sum_{n \in \text{odd}} \frac{2}{\pi|n|} \delta(\omega - nw_{ctrl} - \omega_{in}) \right) \\
 &\quad + V_{in} e^{+j\varphi} \frac{\pi}{2} \left(\delta(\omega + \omega_{in}) + \sum_{n \in \text{odd}} \frac{2}{\pi|n|} \delta(\omega - nw_{ctrl} + \omega_{in}) \right)
 \end{aligned}$$

Rearrange the delta functions

Q: I'm not sure I understand what those Dirac delta functions mean.

A: Remember, the value of $\delta(x)$ is zero at all $x \neq 0$.

Thus, the Dirac delta functions in the above Fourier transform indicate zero energy for all frequencies—**except** those **specific few** which make the argument of the delta function zero!

Q: Just what "specific few" frequencies are those?

A: Let's rewrite the Dirac delta function to see them clearly.

$$\delta(\omega - nw_{ctrl} - \omega_{in}) = \delta(\omega - (nw_{ctrl} + \omega_{in}))$$

$$\delta(\omega - nw_{ctrl} + \omega_{in}) = \delta(\omega - (nw_{ctrl} - \omega_{in}))$$

Zero almost everywhere

$$\begin{aligned}
 V_{\text{out}}(\omega) &= V_{\text{in}} e^{-j\varphi} \frac{\pi}{2} \left(\delta(\omega - \omega_{\text{in}}) + \sum_{n \in \text{odd}} \frac{2}{\pi|n|} \delta(\omega - (n\omega_{\text{ctrl}} + \omega_{\text{in}})) \right) \\
 &\quad + V_{\text{in}} e^{+j\varphi} \frac{\pi}{2} \left(\delta(\omega + \omega_{\text{in}}) + \sum_{n \in \text{odd}} \frac{2}{\pi|n|} \delta(\omega - (n\omega_{\text{ctrl}} - \omega_{\text{in}})) \right)
 \end{aligned}$$

The Fourier transform of $v_{\text{out}}(t)$ is therefore non-zero only at frequencies:

$$\omega = n\omega_{\text{ctrl}} + \omega_{\text{in}}$$

and also:

$$\omega = n\omega_{\text{ctrl}} - \omega_{\text{in}}$$

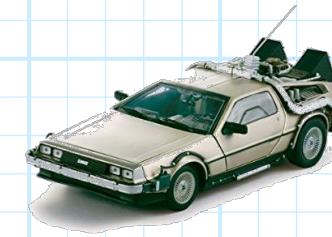
Or equivalently, they are non-zero at these "specific few" frequencies:

$$\omega = n\omega_{\text{ctrl}} \pm \omega_{\text{in}}$$

Back to the time domain!

To see this more explicitly, let's take the **Inverse Fourier transform** of this result, returning again to a **real-valued time domain function**:

$$\begin{aligned}
 v_{out}(t) &= \frac{1}{2\pi} \int_{-\infty}^{\infty} V_{out}(\omega) e^{-j\omega t} d\omega \\
 &= \frac{1}{2\pi} \int_{-\infty}^{\infty} V_{in} e^{-j\varphi} \frac{\pi}{2} \left(\delta(\omega - \omega_{in}) + \sum_{n \in \text{odd}} \frac{2}{\pi |n|} \delta(\omega - (n\omega_{ctrl} + \omega_{in})) \right) e^{-j\omega t} d\omega \\
 &\quad + \frac{1}{2\pi} \int_{-\infty}^{\infty} V_{in} e^{+j\varphi} \frac{\pi}{2} \left(\delta(\omega + \omega_{in}) + \sum_{n \in \text{odd}} \frac{2}{\pi |n|} \delta(\omega - (n\omega_{ctrl} - \omega_{in})) \right) e^{-j\omega t} d\omega \\
 &= \frac{V_{in}}{4} e^{+j\varphi} \left(e^{-j\omega_{in}t} + \sum_{n \in \text{odd}} \frac{2}{\pi |n|} e^{-j(n\omega_{ctrl} + \omega_{in})t} \right) \\
 &\quad + \frac{V_{in}}{4} e^{-j\varphi} \left(e^{+j\omega_{in}t} + \sum_{n \in \text{odd}} \frac{2}{\pi |n|} e^{+j(n\omega_{ctrl} + \omega_{in})t} \right) \\
 &= \frac{V_{in}}{4} \left(e^{-j[\omega_{in}t - \varphi]} + \sum_{n \in \text{odd}} \frac{2}{\pi |n|} e^{-j[(n\omega_{ctrl} + \omega_{in})t - \varphi]} \right) \\
 &\quad + \frac{V_{in}}{4} \left(e^{+j[\omega_{in}t - \varphi]} + \sum_{n \in \text{odd}} \frac{2}{\pi |n|} e^{+j[(n\omega_{ctrl} + \omega_{in})t - \varphi]} \right)
 \end{aligned}$$



Sinusoids!

Now applying Euler's equation to this output signal:

$$\begin{aligned}
 v_{out}(t) &= \frac{V_{in}}{4} \left(e^{-j[\omega_{in}t - \varphi]} + \sum_{n \in odd} \frac{2}{\pi |n|} e^{-j[(n\omega_{ctrl} + \omega_{in})t - \varphi]} \right) \\
 &\quad + \frac{V_{in}}{4} \left(e^{+j[\omega_{in}t - \varphi]} + \sum_{n \in odd} \frac{2}{\pi |n|} e^{+j[(n\omega_{ctrl} + \omega_{in})t - \varphi]} \right) \\
 &= \frac{V_{in}}{4} \left(e^{-j[\omega_{in}t - \varphi]} + e^{+j[\omega_{in}t - \varphi]} \right) \\
 &\quad + \frac{V_{in}}{4} \left(\sum_{n \in odd} \frac{2}{\pi |n|} e^{-j[(n\omega_{ctrl} + \omega_{in})t - \varphi]} + \sum_{n \in odd} \frac{2}{\pi |n|} e^{+j[(n\omega_{ctrl} + \omega_{in})t - \varphi]} \right) \\
 &= \frac{V_{in}}{2} \cos[\omega_{in}t - \varphi] + V_{in} \sum_{n \in odd} \frac{1}{\pi |n|} \cos[(n\omega_{ctrl} + \omega_{in})t - \varphi]
 \end{aligned}$$



We've seen these before!

Among the most "energetic" of these sinusoidal output terms are for $n \in \{-1, 0, 1\}$, such that the output can be approximated as:

$$v_{out}(t) \approx \frac{V_{in}}{2} \cos[\omega_{in}t - \varphi] + \frac{V_{in}}{\pi} \cos[(\omega_{in} - \omega_{ctrl})t - \varphi] + \frac{V_{in}}{\pi} \cos[(\omega_{in} + \omega_{ctrl})t - \varphi]$$

Compare these last two terms with the output of an ideal mixer:

$$v_{IF}(t) = \frac{1}{2} \cos[(\omega_{RF} - \omega_{LO})t] + \frac{1}{2} \cos[(\omega_{RF} + \omega_{LO})t] !$$

Input is RF, output is IF, control is LO

If we equate the **input** signal with the RF signal:

$$v_{in}(t) = v_{RF}(t)$$

and the **control** signal with the LO signal:

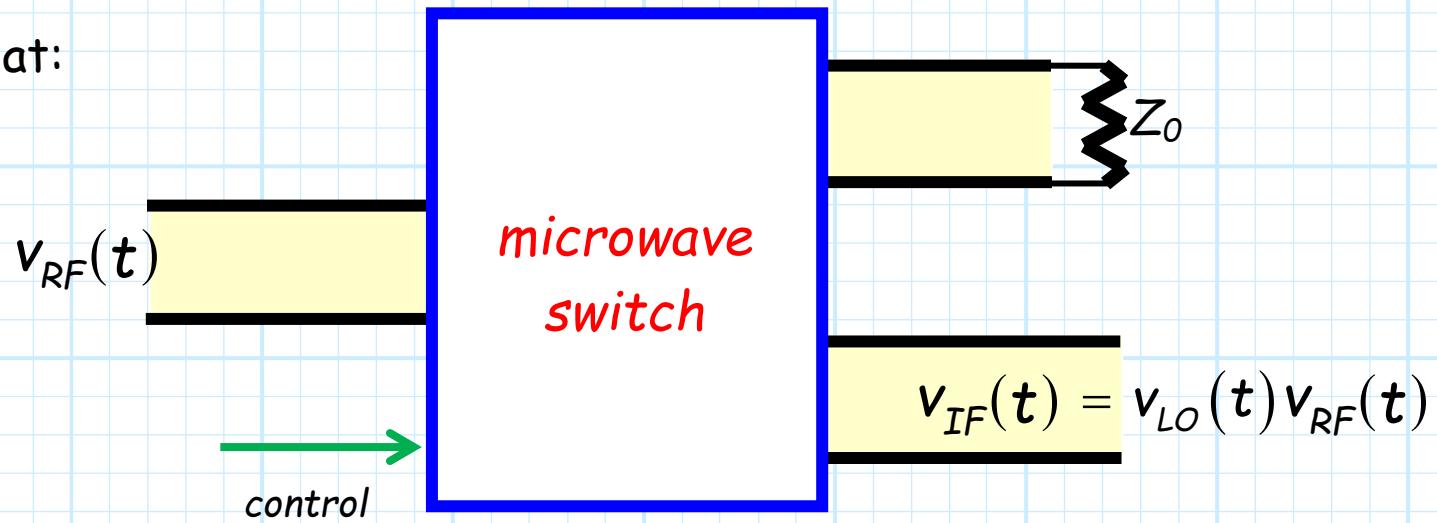
$$v_{ctrl}(t) = v_{LO}(t)$$

and the **output** signal with the IF signal:

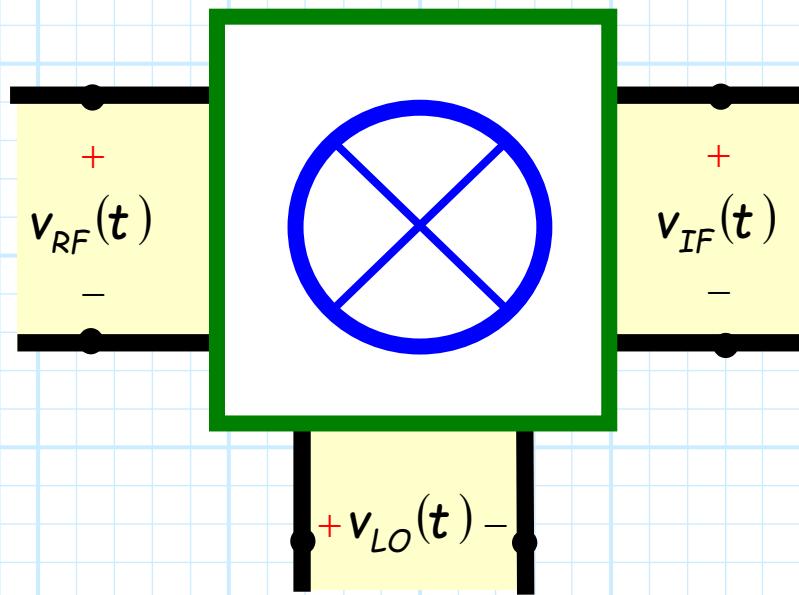
$$v_{out}(t) = v_{IF}(t)$$

A microwave mixer is a toggled switch

Such that:



We see the output of our "toggled" switch is similar to an ideal mixer:



The two signals we need

Each device produces a sinusoid that is the **sum** (ω_{Σ}) of the two frequencies:

$$\cos[(\omega_{RF} + \omega_{LO})t] = \cos[(\omega_{in} + \omega_{ctrl})t]$$

and a sinusoid that is the **difference** (ω_{Δ}) of the two frequencies:

$$\cos[(\omega_{RF} - \omega_{LO})t] = \cos[(\omega_{in} - \omega_{ctrl})t]$$

A "toggled" switch can be used to create similar signals as an **ideal mixer!**

NOT an ideal mixer term

Q: Yes, but this toggled switch mixer seems also to generate some other signals as well. Most notably a one at *input frequency* ω_{in} (ω_{RF}):

$$\frac{V_{in}}{2} \cos[\omega_{in}t - \varphi] = \frac{V_{RF}}{2} \cos[\omega_{RF}t - \varphi]$$

A: Yes it does.

Q: Is that a bad thing?

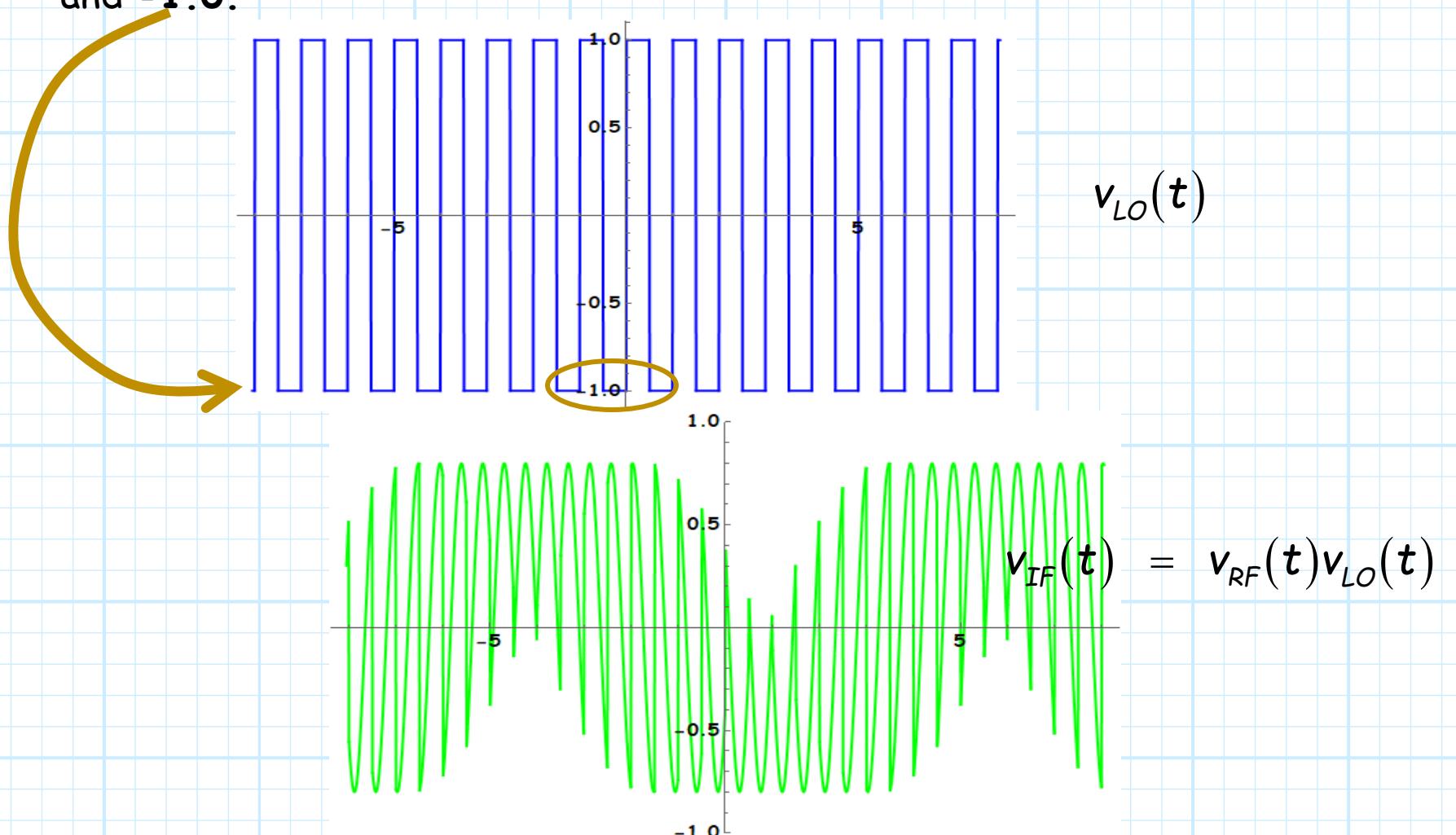
A: Yes it is.

Among other things, this "extra" signal reduces the power of the two desired signals (i.e., conservation of energy at work):

$$\frac{V_{RF}}{\pi} \cos[(\omega_{RF} - \omega_{LO})t - \varphi] \quad \text{and} \quad \frac{V_{in}}{\pi} \cos[(\omega_{RF} + \omega_{LO})t - \varphi]$$

A different square wave

To "fix" this problem, we can instead "multiply" the input with a different square wave—one instead that toggles between a value of 1.0 and -1.0.



I'll let you verify this

Reworking all the math, **you** will find that the IF (i.e., the output) is now:

$$v_{IF}(t) = V_{RF} \sum_{n \in \text{odd}} \frac{2}{\pi |n|} \cos[(n w_{LO} + w_{RF})t - \varphi]$$

So that the IF (i.e., the output) is **approximately**:

$$v_{IF}(t) \approx V_{RF} \frac{2}{\pi} \cos[(w_{RF} - w_{LO})t - \varphi] + V_{RF} \frac{2}{\pi} \cos[(w_{RF} + w_{LO})t - \varphi]$$

Note the w_{RF} sinusoid is **missing**, and the remaining two terms are **twice as large!**

Balanced and unbalanced

The first result (where the LO toggles between 1.0 and 0.0), is known as an **unbalanced mixer**:

$$\begin{aligned} v_{IF}^{unbal}(t) &\approx \frac{V_{RF}}{2} \cos[\omega_{RF}t - \varphi_{RF}] \\ &+ \frac{V_{RF}}{\pi} \cos[(\omega_{RF} - \omega_{LO})t - \varphi_{RF}] + \frac{V_{RF}}{\pi} \cos[(\omega_{in} + \omega_{ctrl})t - \varphi_{RF}] \end{aligned}$$

This last result (where the LO toggles between 1.0 and -1.0), is known as a **balanced mixer**:

$$v_{IF}^{bal}(t) \approx V_{RF} \frac{2}{\pi} \cos[(\omega_{RF} - \omega_{LO})t - \varphi_{RF}] + V_{RF} \frac{2}{\pi} \cos[(\omega_{in} + \omega_{ctrl})t - \varphi_{RF}]$$

The vast majority of microwave mixers are "balanced"!

A balanced mixer!

Q: But how can we make these balanced mixers? How can we multiply by -1.0?

A: Remember, multiplying a sinusoid by -1 is the same thing as phase shifting it by π radians (i.e., $-1 = e^{j\pi}$).

Thus, we can equivalently say that a balanced mixer toggles between a 0° phase shift and a 180° phase shift!

