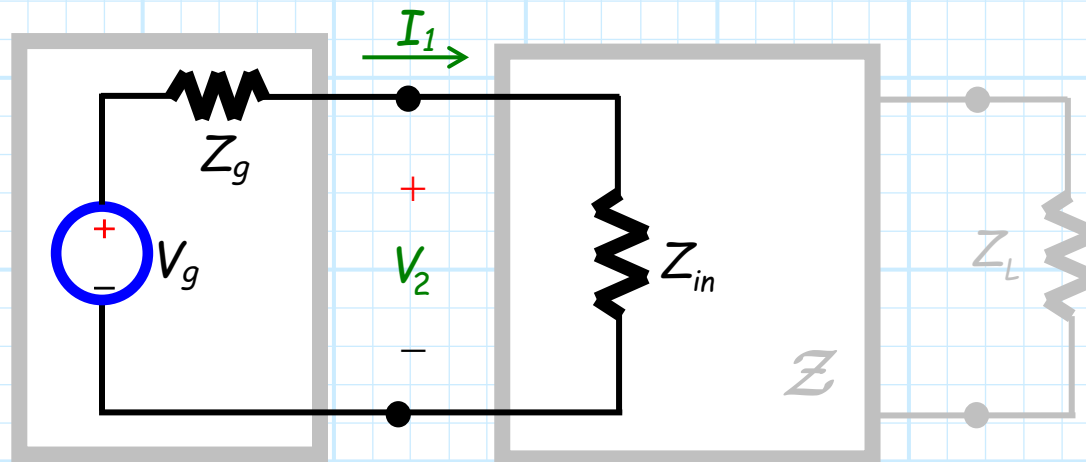


# Source Transformers

**Q:** So we *combined* the two-port network with the load, in order to make an equivalent *input impedance*.

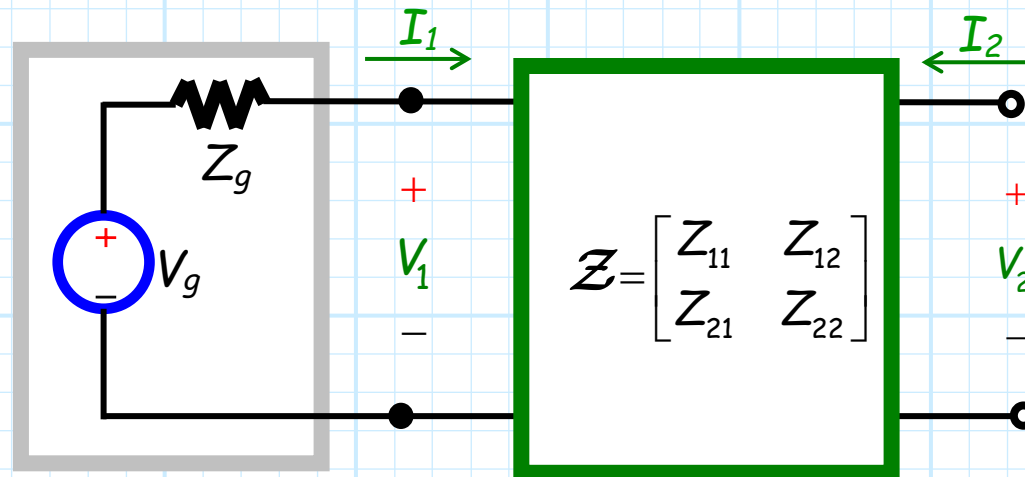


Couldn't we have *alternatively* combined the *source* and the two-port network?

**A:** What a *great* idea! Let's try it and *see what happens*.

## A new one-port network

For this case, you simply need to determine an **equivalent source** for the following one-port network:



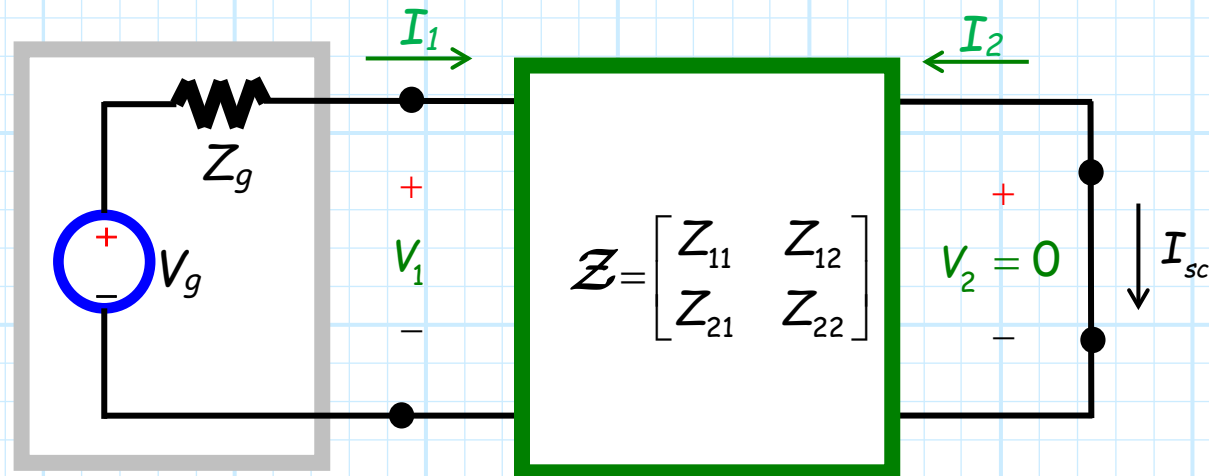
**Q:** Yikes! How do I accomplish that?

**A:** You already know how! Just determine:

**a)** the short-circuit output current  $I_{sc}$

**b)** the open-circuit output voltage  $V_{oc}$

## Four equations and four unknowns



From the **trans-impedance** parameters of the two-port device, we know  $\rightarrow$

$$V_1 = Z_{11}I_1 + Z_{12}I_2$$

$$V_2 = Z_{21}I_1 + Z_{22}I_2$$

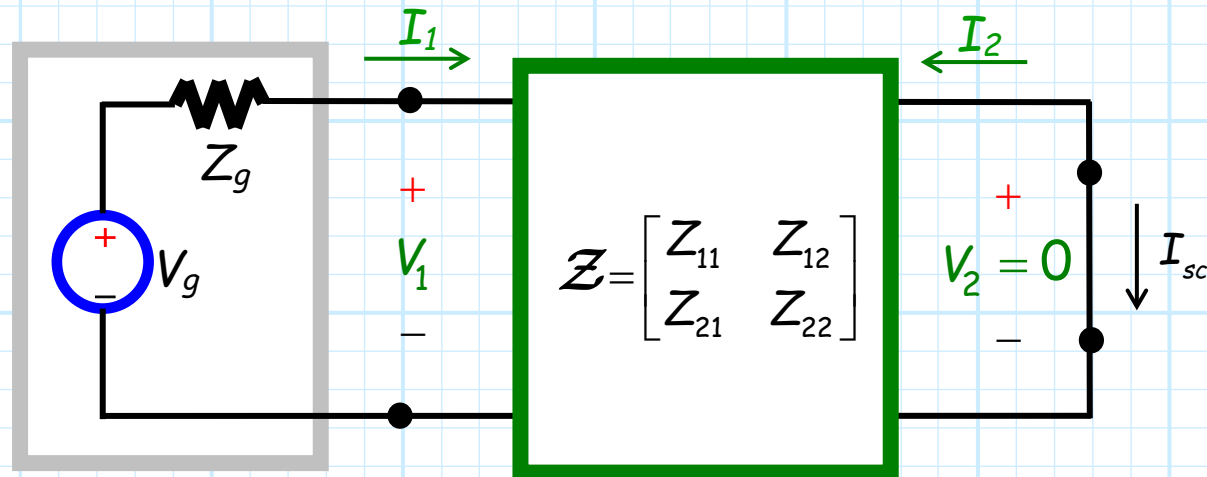
And for the **source**  $\rightarrow$

$$I_1 = \frac{V_g - V_1}{Z_g}$$

And of course for the **short-circuit**  $\rightarrow$

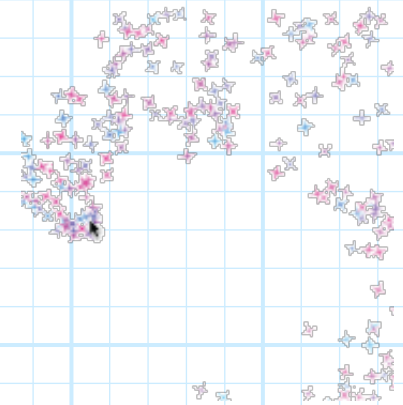
$$V_2 = 0$$

# The short-circuit output current

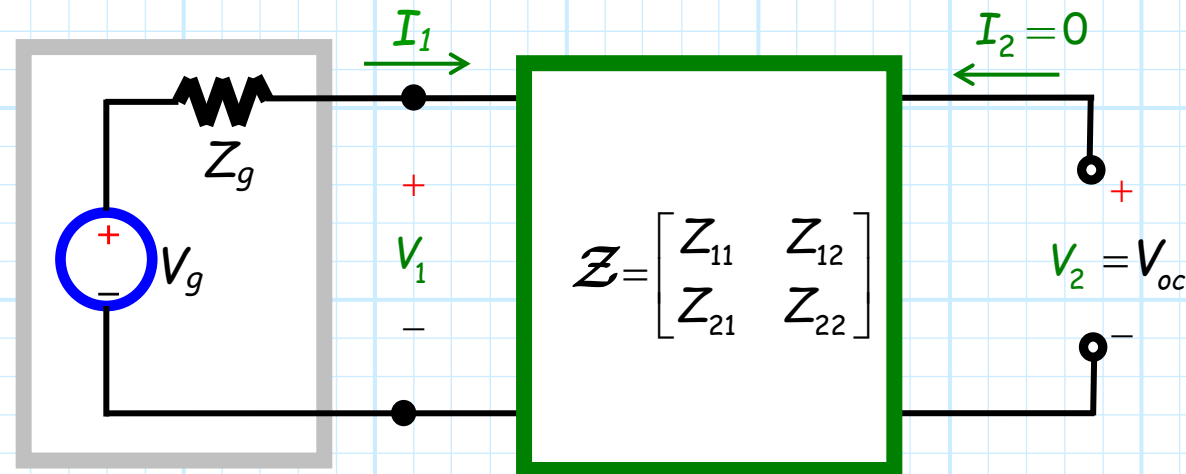


With some algebraic **elbow grease** we can determine the **short-circuit** current:

$$I_{sc} = -I_2 = V_g \left[ \frac{Z_{22}}{Z_{21}} (Z_{11} + Z_g) - Z_{12} \right]^{-1}$$



## Now for an open-circuit at the output



From the **trans-impedance** parameters of the two-port device, we know  $\rightarrow$

$$V_1 = Z_{11}I_1 + Z_{12}I_2$$

$$V_2 = Z_{21}I_1 + Z_{22}I_2$$

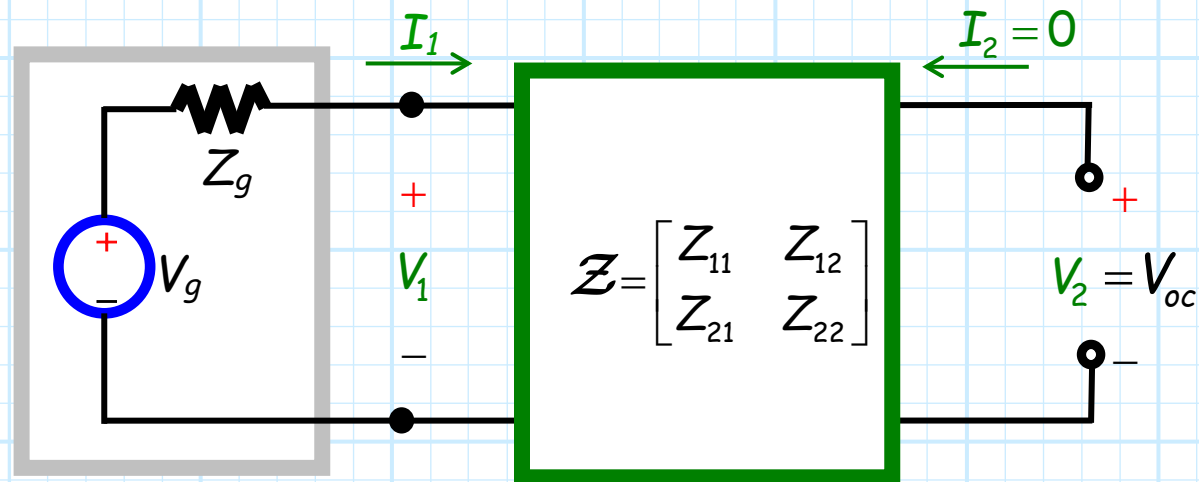
And for the **source**  $\rightarrow$

$$I_1 = \frac{V_s - V_1}{Z_1}$$

And of course for the **open-circuit**  $\rightarrow$

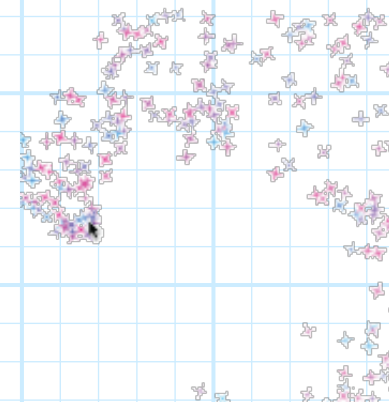
$$I_2 = 0$$

# The open-circuit output voltage



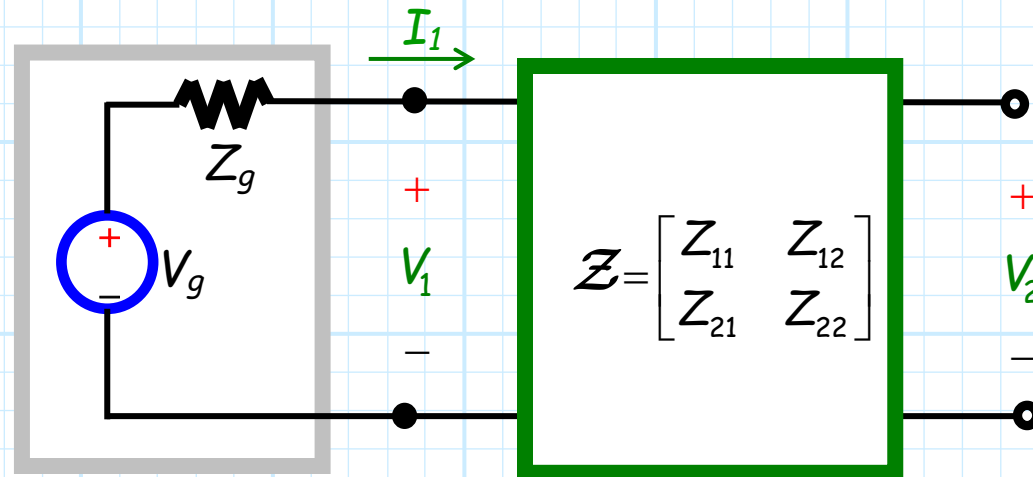
With even **more** algebraic elbow grease, we can determine the **open-circuit** voltage:

$$V_{oc} = V_2 = V_g \left( \frac{Z_{21}}{Z_{11} + Z_g} \right)$$



## Thevenin's equivalent

Thus, the Thevenin's equivalent of **this** circuit →



has a **voltage source** of value  $V_{out}$  :

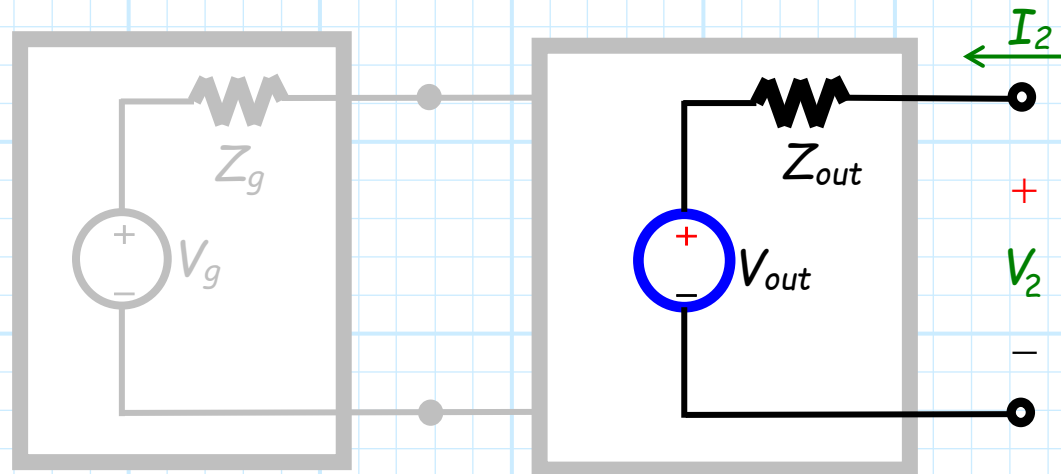
$$V_{out} = V_{oc} = V_g \left( \frac{Z_{21}}{Z_{11} + Z_g} \right)$$

and an output **impedance**  $Z_{out}$  :

$$Z_{out} = \frac{V_{oc}}{I_{sc}} = \left( \frac{Z_{21}}{Z_{11} + Z_s} \right) \left( \frac{Z_{22}}{Z_{21}} (Z_{11} + Z_s) - Z_{12} \right) = Z_{22} - \frac{Z_{21} Z_{12}}{Z_{11} + Z_g}$$

## A source transformer!!!!

In this case, the two-port device can be viewed as a **source transformer**.



$$V_{out} = V_g \left( \frac{Z_{21}}{Z_{11} + Z_g} \right)$$

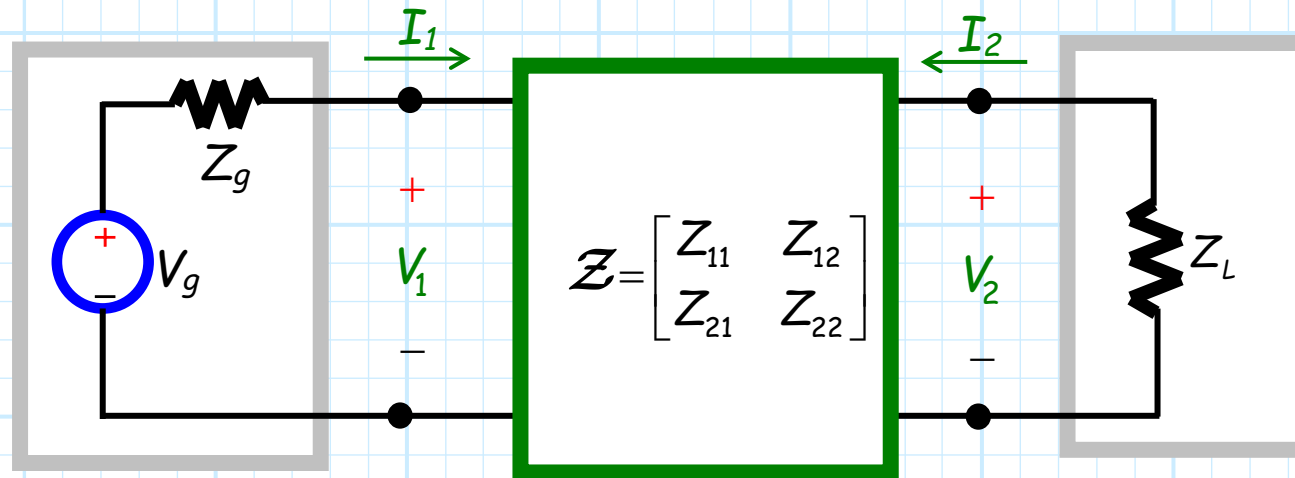
$$Z_{out} = Z_{22} - \frac{Z_{21} Z_{12}}{Z_{11} + Z_g}$$

→ Note that **BOTH** the voltage source **AND** the impedance are transformed!

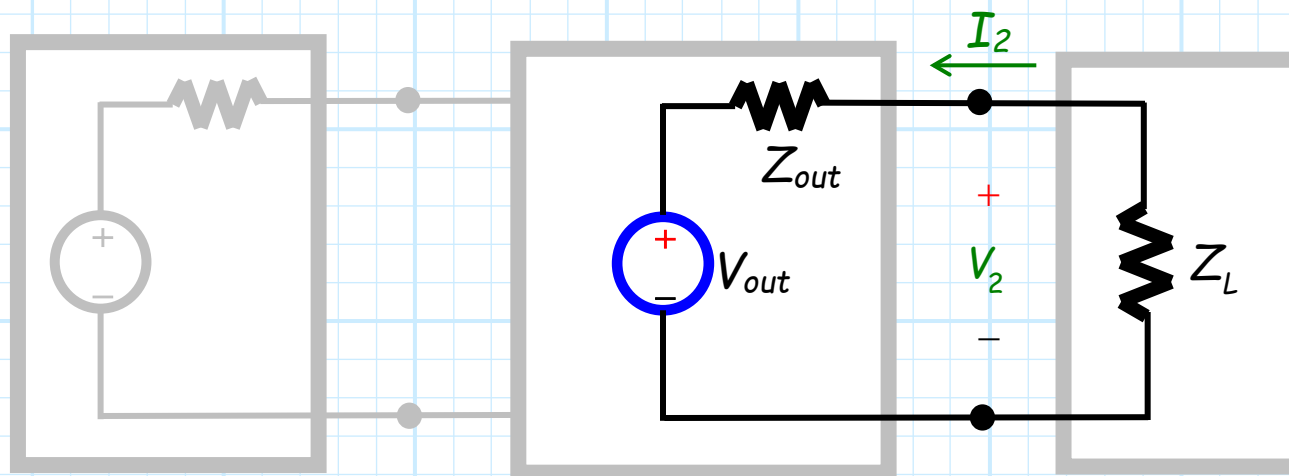


# An alternate equivalent circuit

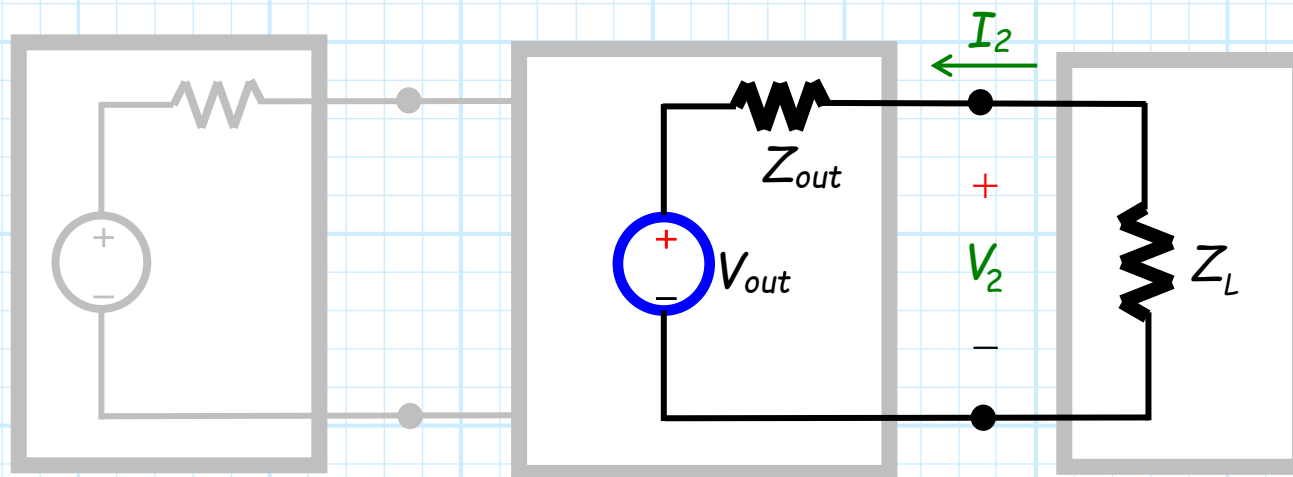
An equivalent circuit to **this**:



is therefore **this**:



# Evaluate the output port values



Evaluating this **equivalent** circuit, we can **quickly** determine:

$$I_2 = \frac{V_{out}}{Z_{out} + Z_L} \qquad V_2 = V_{out} \left( \frac{Z_L}{Z_{out} + Z_L} \right)$$

## Whew! We passed the sanity check!


As a **sanity check**, we can **insert** these results:

$$V_{out} = V_g \left( \frac{Z_{21}}{Z_{11} + Z_g} \right) \quad Z_{out} = Z_{22} - \frac{Z_{21} Z_{12}}{Z_{11} + Z_g}$$

into these:

$$I_2 = \frac{V_{out}}{Z_{out} + Z_L} \quad V_2 = V_{out} \left( \frac{Z_L}{Z_{out} + Z_L} \right)$$

and find that results to be the **same** as before!

$$I_2 = -V_g \frac{Z_{21}}{(Z_{11} + Z_g)(Z_{22} + Z_L) - Z_{12}Z_{21}}$$


$$V_2 = V_g \frac{Z_L Z_{21}}{(Z_{11} + Z_g)(Z_{22} + Z_L) - Z_{12}Z_{21}}$$
