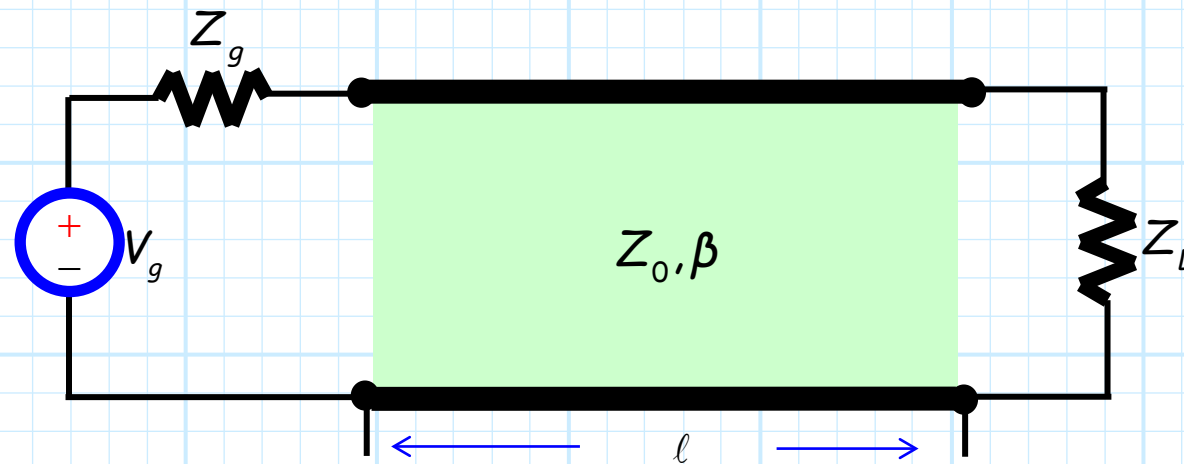


# Matching Networks and Transmission Lines



**Q:** But let's deal with the reality of a cold, *cruel*, non-ideal world.

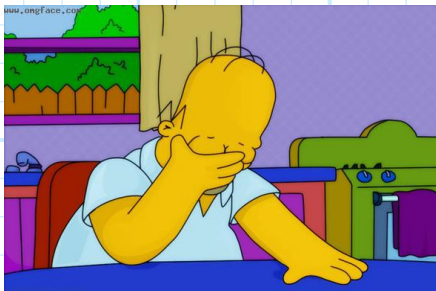
If we directly connect an **arbitrary** source to an **arbitrary** load via a length of transmission line, don't we just have to **accept** the hard truth that the power absorbed by the load will be **less** than that available from the source?

## You're just not that lucky!

**A:** We determined earlier that the efficacy of power transfer **depends** on:

1. the **source** impedance  $Z_g$ .
2. **load** impedance  $Z_L$ .
3. the transmission line **characteristic impedance**  $Z_0$ .
4. the transmission line **length**  $\ell$ .

Recall that **maximum** power transfer occurred **only** when these four parameters resulted in the **input impedance** of the transmission line being equal to the **complex conjugate** of the **source impedance** (i.e.,  $Z_{in}^* = Z_g$ ).



→ It is indeed **unlikely** that the very **specific** conditions of a **conjugate match** will occur **if** we simply connect a length of transmission line between an **arbitrary** source and load.

## What about a matching network?

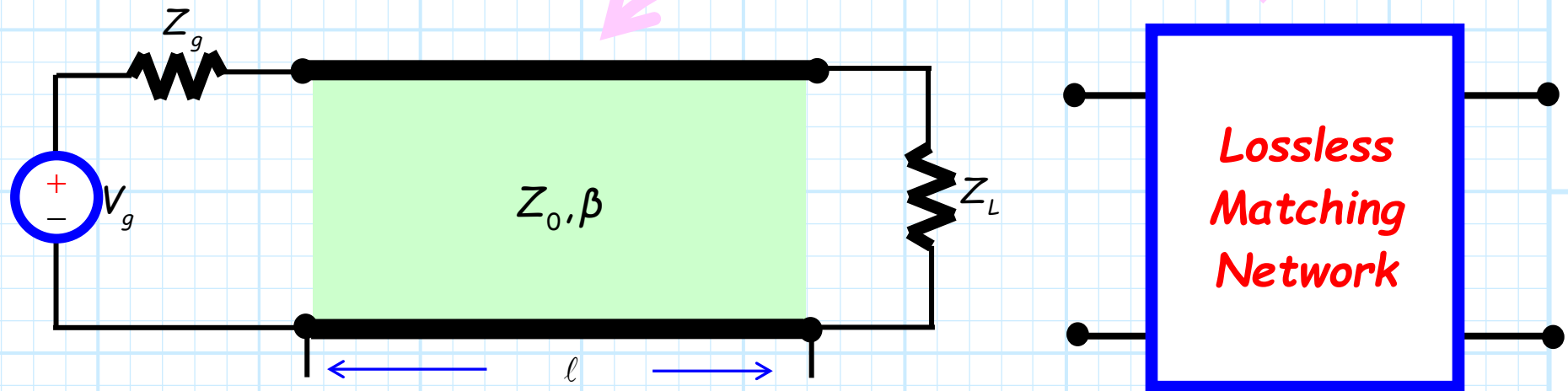
**Q:** Is there any way to use a **matching network** to fix this problem?

Can the power delivered to the load be increased to **equal** the available power of the source, even if there is a transmission line connecting them?

**A:** There sure is!

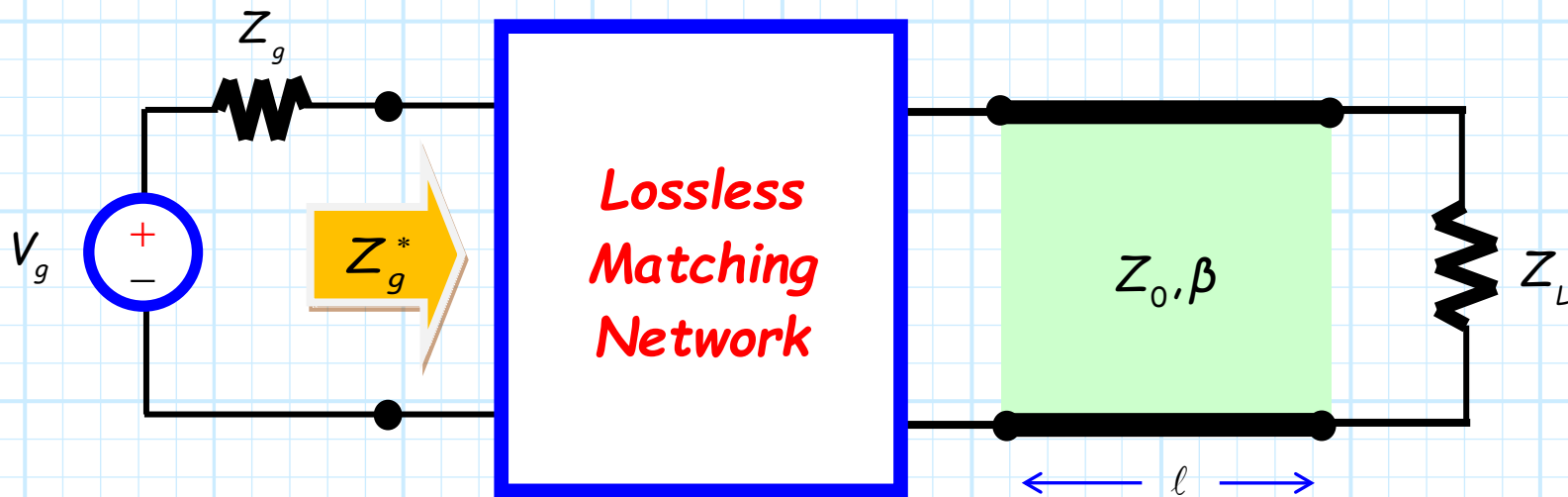
???

We **can** likewise construct a matching network for the case where the source and load are connected by a **transmission line**.



# Matching network to the rescue!

For example, we can construct a network to transform the **input impedance** of the transmission line into the complex conjugate of the **source impedance**:

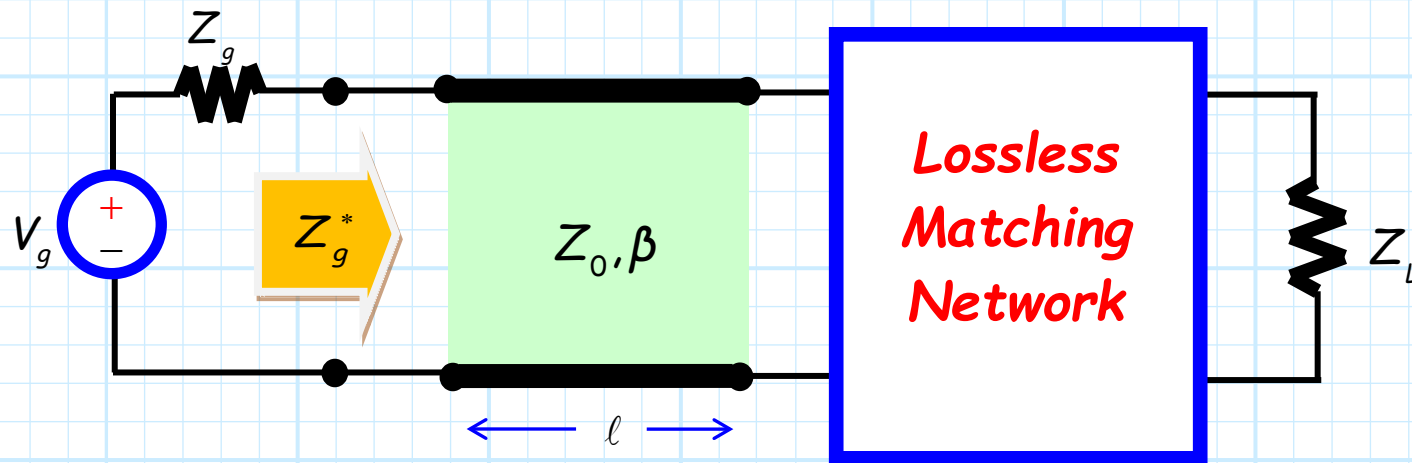


## But, where to put it?

**Q:** But, do we absolutely *have* to place the matching network between the source and the transmission line?

**A:** Nope!

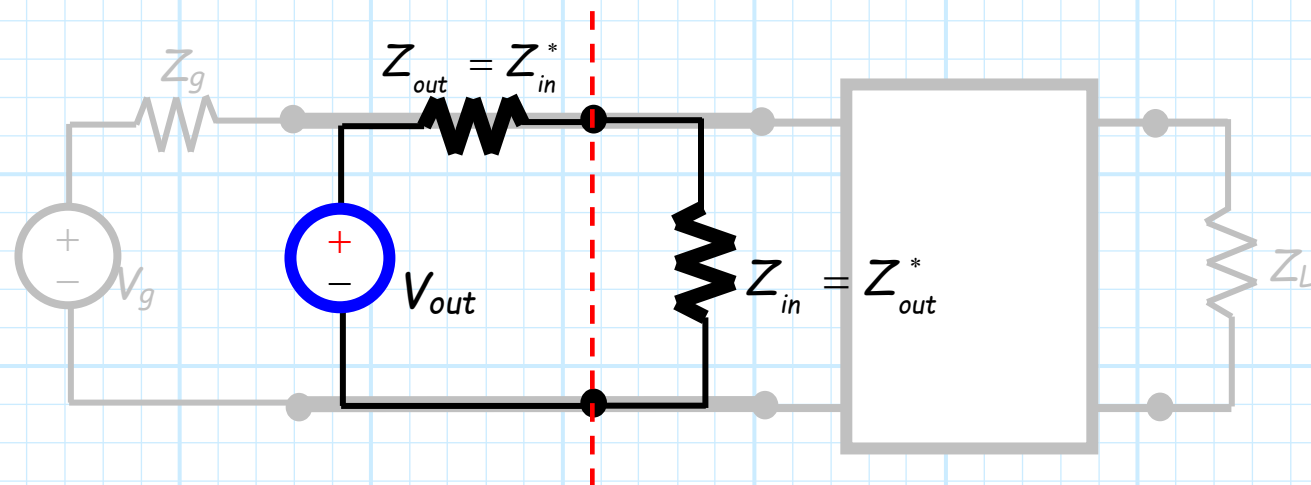
We could **also** place a (different) matching network between the transmission line and the load.



## A conjugate match at one location means a conjugate match at all locations!

In either case, we find at **any** and **all** points along this matched circuit that:

- a) the output impedance of the equivalent **source** (i.e., looking left), will be
- b) equal to the **complex conjugate** of the **input impedance** (i.e., looking right)!



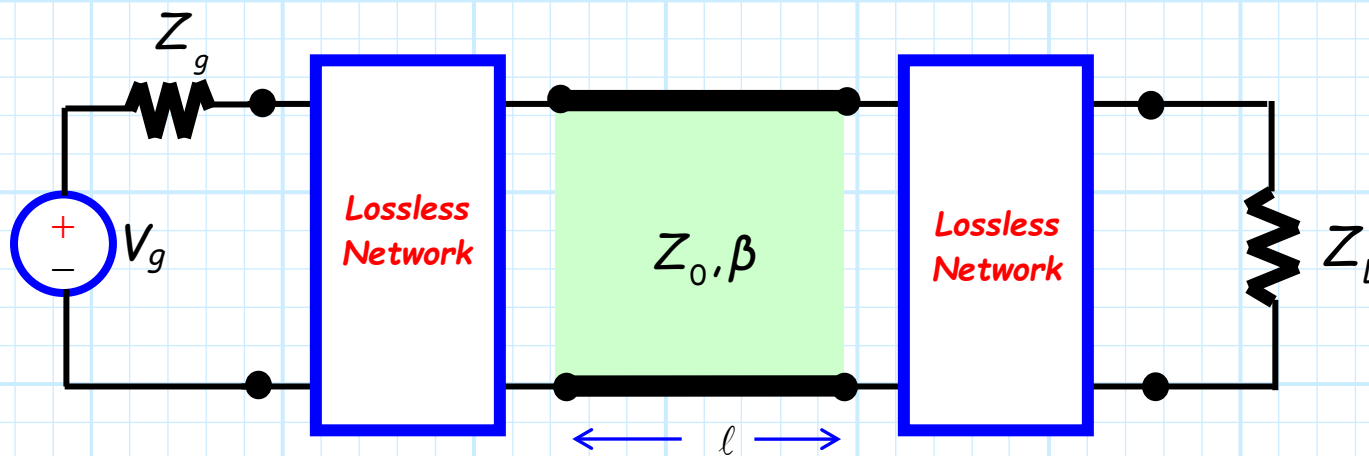
## Two networks are the solution!

**Q:** So *which* method should we chose?

Do engineers typically place the matching network between the source and the transmission line, *or* place it between the transmission line and the load?

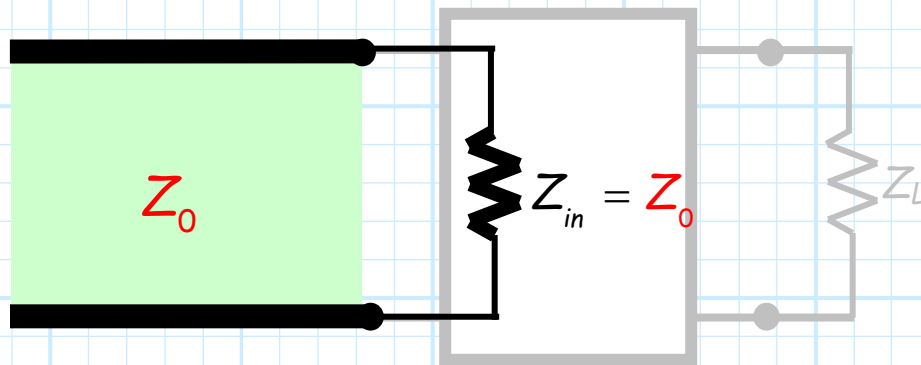
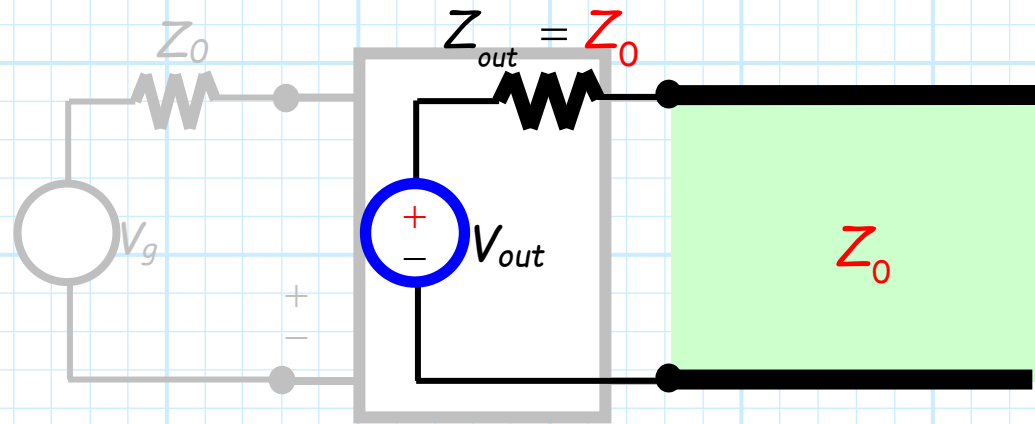
**A:** Actually, the typical solution is to **do both!**

We find that often there is a **lossless network** between the source and the transmission line, **and** between the line and the load.



## We put it at both ends!

The **first** lossless network transforms the **source**, such that the resulting **output** impedance is numerically equal to the **transmission line characteristic impedance**  $Z_0$ .



The **second** lossless network transforms the **load**, such that the resulting **input** impedance is numerically equal to the **transmission line characteristic impedance**  $Z_0$ :



## Why do we need two networks?

**Q:** *Yikes! Why would we want to build **two** lossless networks, instead of just **one**?*

**A:** By using two **separate** lossless networks, we can **decouple** the design problem.

Recall again that the design of a **single** matching network solution would depend on four separate parameters:

1. the source impedance  $Z_g$ .
2. load impedance  $Z_L$ .
3. the transmission line characteristic impedance  $Z_0$ .
4. the transmission line **length**  $\ell$ .

## The line length does not matter!!!!

Alternatively, the design of the lossless network transforming the source impedance to a value  $Z_0$  depends on only:

1. the source impedance  $Z_g$ .
2. the transmission line characteristic impedance  $Z_0$ .

Whereas, the design of the lossless network transforming the load impedance to a value  $Z_0$  depends on only:

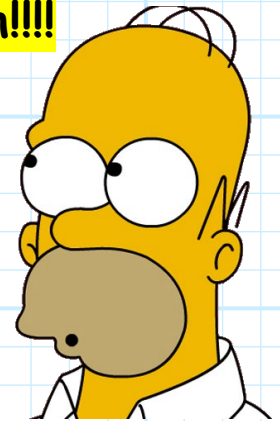
1. the load impedance  $Z_L$ .
2. the transmission line characteristic impedance  $Z_0$ .

→ Note that **neither** design depends on the transmission line length  $\ell$  !!!!

## Devices are typically matched to $50\Omega$

Thus, by transforming the source to characteristic impedance  $Z_0$  and likewise transforming the load to the line impedance, a conjugate match is assured.

And this is true regardless of the transmission line length!!!!



In fact, the typically **problem** for microwave engineers is to:

- a) transform a **load** (e.g., device **input** impedance) to a **standard** transmission line impedance (typically  $Z_0 = 50\Omega$ ); or to
- b) independently transform a **source** (e.g., device **output** impedance) to a **standard** line impedance.

# The ideal case: line lengths no longer matter!



A conjugate match is thus obtained by connecting the two with a transmission line **of any length!**

