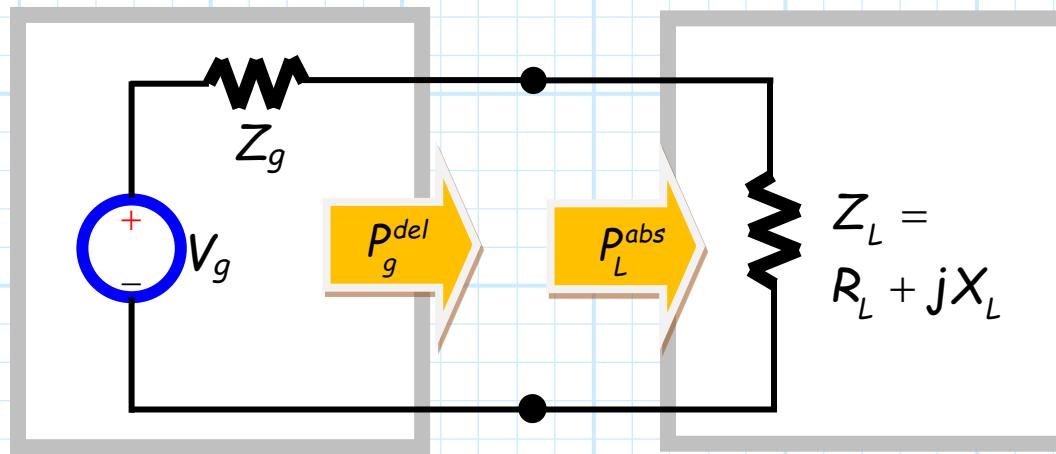


Matching Networks

Consider again the problem where a load is directly attached to a source:



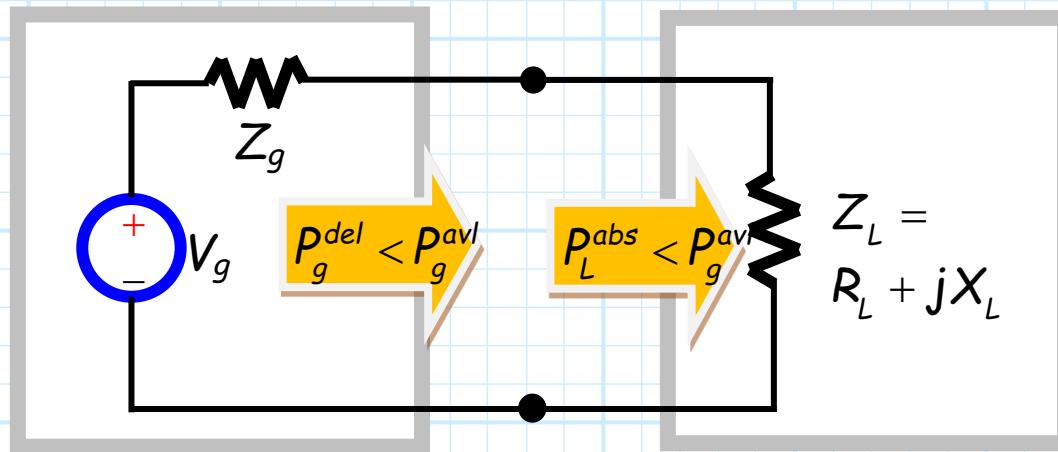
The load will **absorb energy**—at a rate equal to that **delivered** to it by the source.

$$P_L^{\text{abs}} = \frac{1}{2} \text{Re}\{V_L I_L^*\} = \frac{1}{2} |V_g|^2 \frac{R_L}{|Z_g + Z_L|^2} = P_g^{\text{del}}$$

Less than what's available

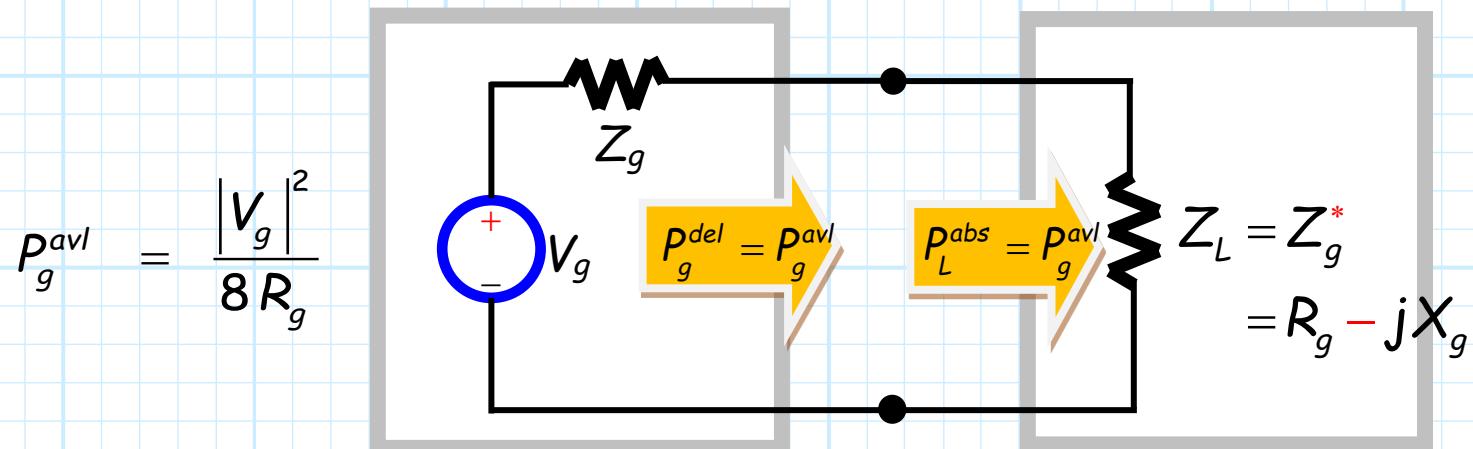
Generally speaking though, this absorbed/delivered power will be **less** than the power **available** from the source.

$$P_g^{\text{avl}} = \frac{|V_g|^2}{8R_g}$$



If we could only change Z_L ...

Only if we alter the load impedance Z_L —such that it is a “conjugate match” to the source—will all the available source power be released.



...but we can't change Z_L !

Q: But, you said that load impedance Z_L is usually just the equivalent circuit of some more useful device or network.

We don't then typically get to "alter" or select this impedance—it is what it is.

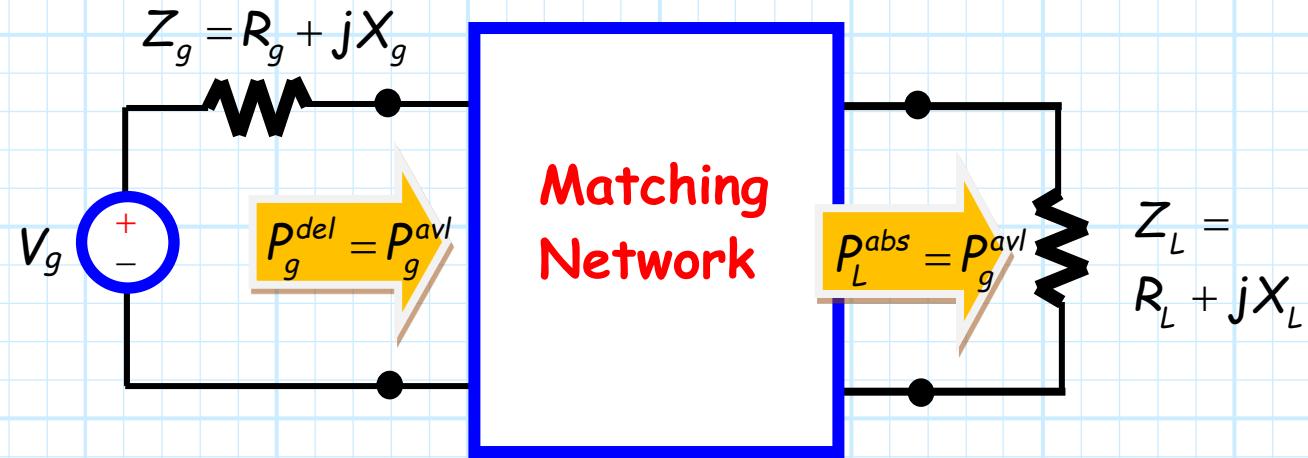
Must we then simply accept the fact that the absorbed power will be less than the power available from the source?

A: NO! We can in fact modify our circuit such that all available source power is delivered to the load—without in any way altering the impedance value of that load!



Eat cake; have it too!

To accomplish this, we must insert a two-port network—a matching network—between the source and the load:



If properly designed, we find that all available power from the source is indeed absorbed by the (unaltered) load Z_L :

$$P_g^{del} = P_g^{avl} = P_L^{abs} \quad !!!!!$$

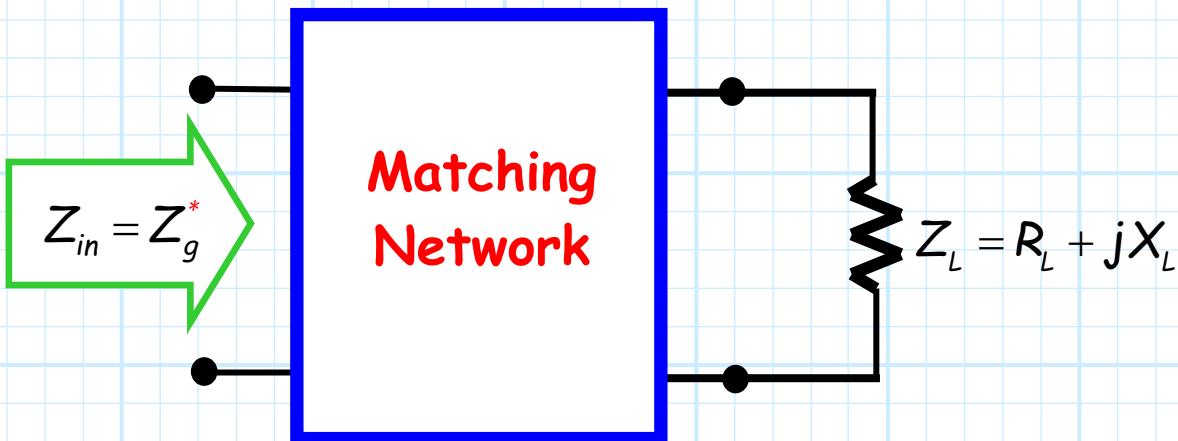
An impedance transformer

Q: But how can this be?

After all, load impedance Z_L is not conjugate matched to source impedance Z_g :

$$Z_L \neq Z_g^* !!$$

A: We can view the matching network as an **impedance transformer**—one whose sole purpose is to “transform” the load impedance Z_L into an input impedance Z_{in} that is conjugate matched to the source! I.E.:

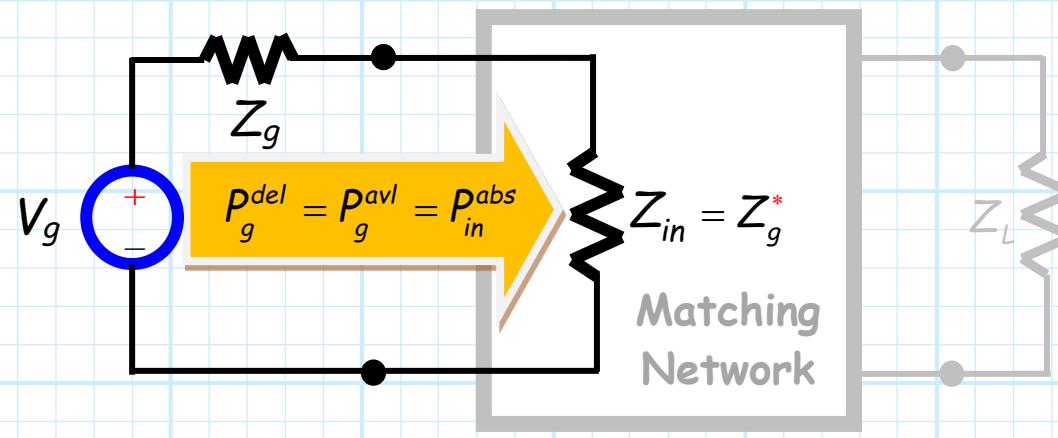


All available power is delivered to Z_{in}

Because the input impedance Z_{in} is conjugate matched to the source impedance:

$$Z_{in} = Z_g^*$$

all available source power is absorbed by the input impedance Z_{in} of the matching network:



Don't forget conservation of energy!

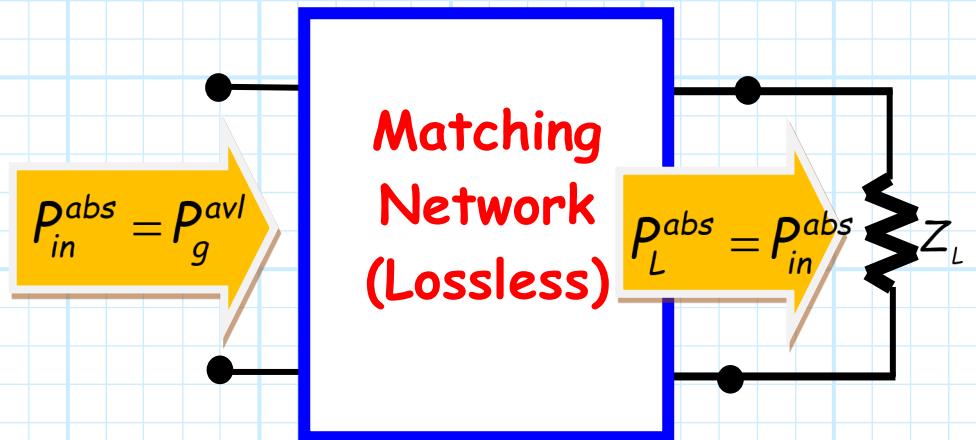
Q: Wait one second!

The matching network ensures that all available source power is absorbed by the input impedance (i.e., $P_{in}^{abs} = P_g^{avl}$), but that does not mean (necessarily) that all this power will be absorbed by the load Z_L

Couldn't the power absorbed by the load be much less than the available power (i.e., $P_L^{abs} < P_{in}^{abs} = P_g^{avl}$)???

A: True enough!

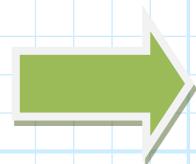
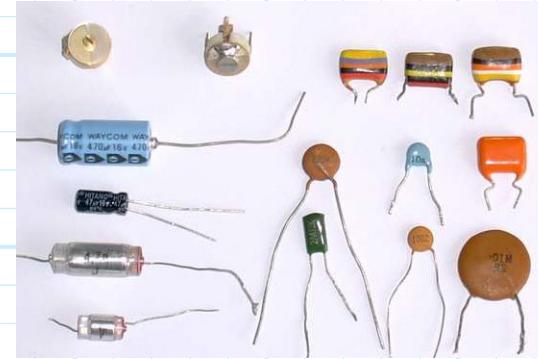
So to ensure that the available source power is entirely absorbed by the load, the matching network must also be lossless!



Inductors and capacitors



$$Z_{\text{lossless}} = \begin{bmatrix} jX_{11} & jX_{12} \\ jX_{12} & jX_{22} \end{bmatrix}$$



Therefore, we must construct our matching network entirely with **reactive elements!**

But, constructing a **proper lossless matching network** will lead to the happy condition where:

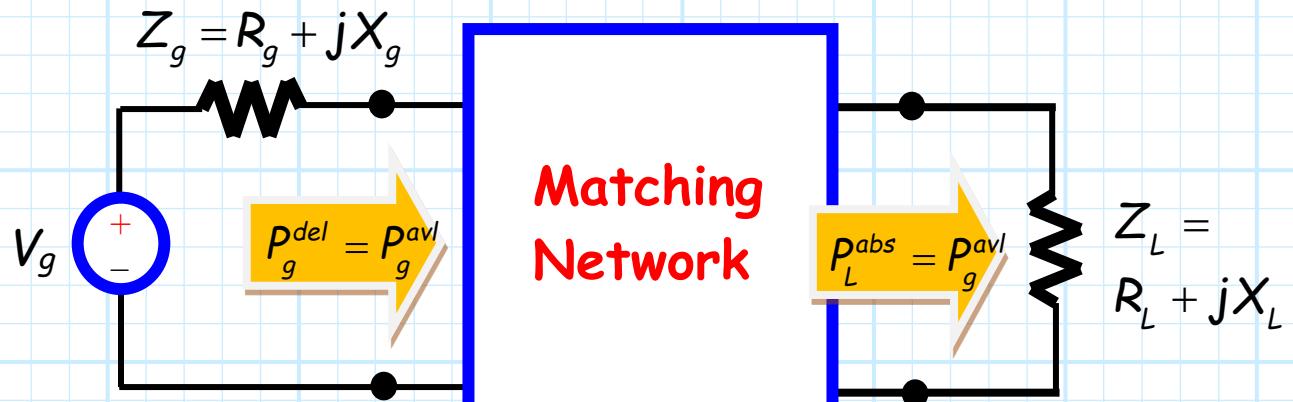
$$P_g^{\text{del}} = P_g^{\text{avl}} = P_L^{\text{abs}}$$

It depends on source and load— but does not alter them

- The design and construction of this lossless impedance transformer will depend on both source impedance Z_g and load impedance Z_L .

$$Z_{in} = Z_g^* = jX_{11} + \frac{(X_{12})^2}{jX_{22} + Z_L}$$

- However, the impedance transformer does **not physically alter** either of these two quantities—the source and load are left **physically unchanged!**

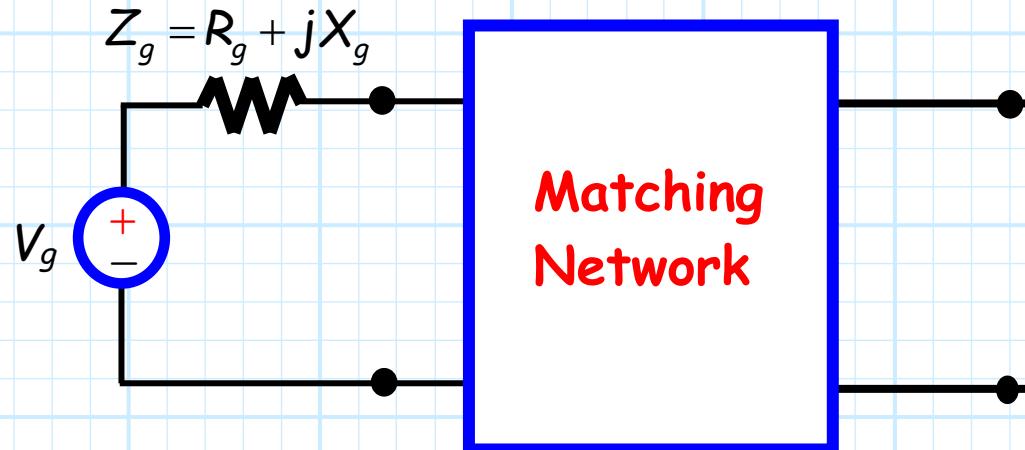


A different perspective



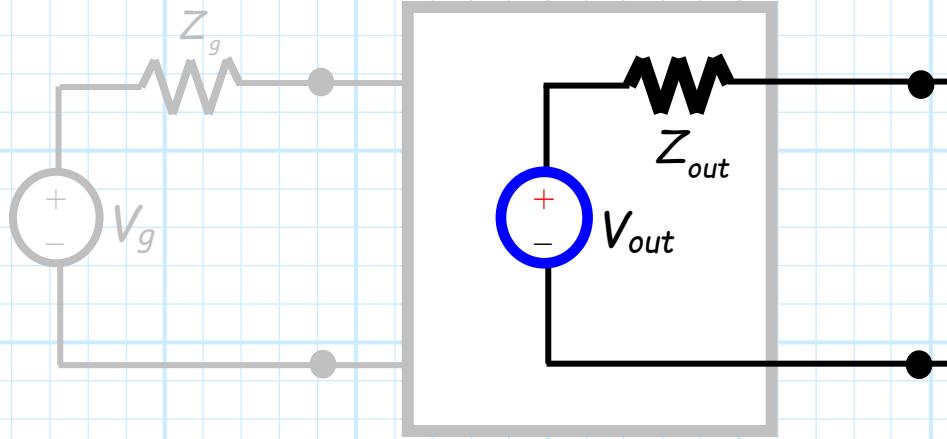
Now, let's consider the matching network from a **different perspective**.

Instead of thinking of it as an impedance transformer, think of it as a **source transformer**!



The matching network is instead a source transformer!

This transformed source (i.e., the original source with the matching network attached) can be expressed in terms of its Thevenin's equivalent circuit:



Recall that in general $V_{out} \neq V_g$ and $Z_{out} \neq Z_g$ —the matching network “transforms” both the values of both the impedance and the voltage source.

A lossless network does NOT alter available power!

Q: Doesn't that also mean that the available power of this "transformed" source will be different from the original?



A: Remember, because the matching network is lossless, the available power of this transformed source is identical to the available power of the original source.

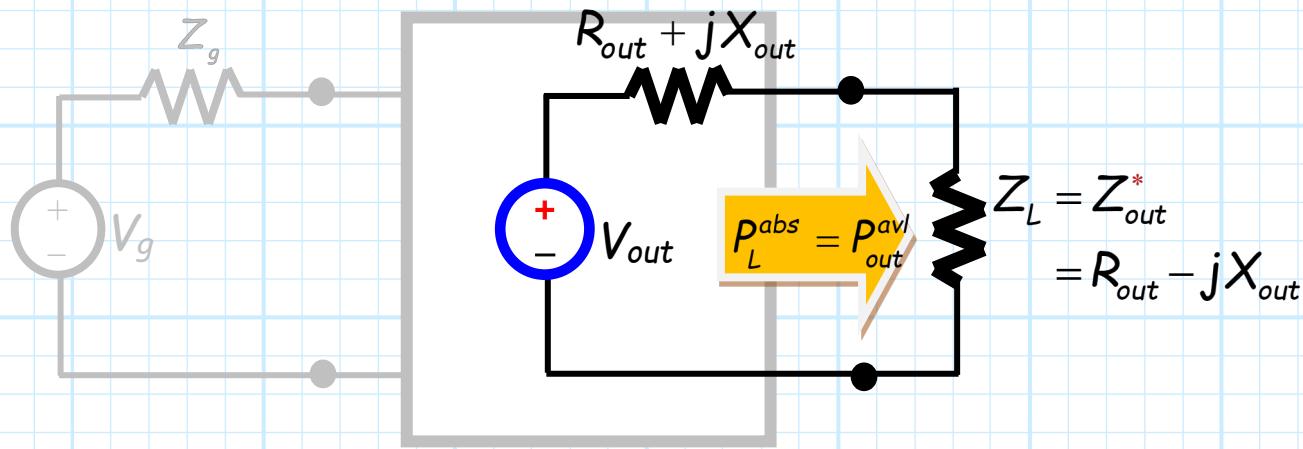
$$P_{out}^{avl} = P_g^{avl}$$

A lossless network (matching or otherwise) cannot alter the available power of the transformed source!

The load is matched to the transformed source

Q: So what is the purpose of the source transformer; just what are we attempting to accomplish with it?

A: We want all the available power of the transformed source to be absorbed by the load (i.e., want $P_L^{\text{abs}} = P_{\text{out}}^{\text{avl}}$).



This will occur only if the transformed source impedance is conjugate matched to the load (i.e., $Z_{\text{out}} = Z_L^*$).

All available power is delivered to the load!

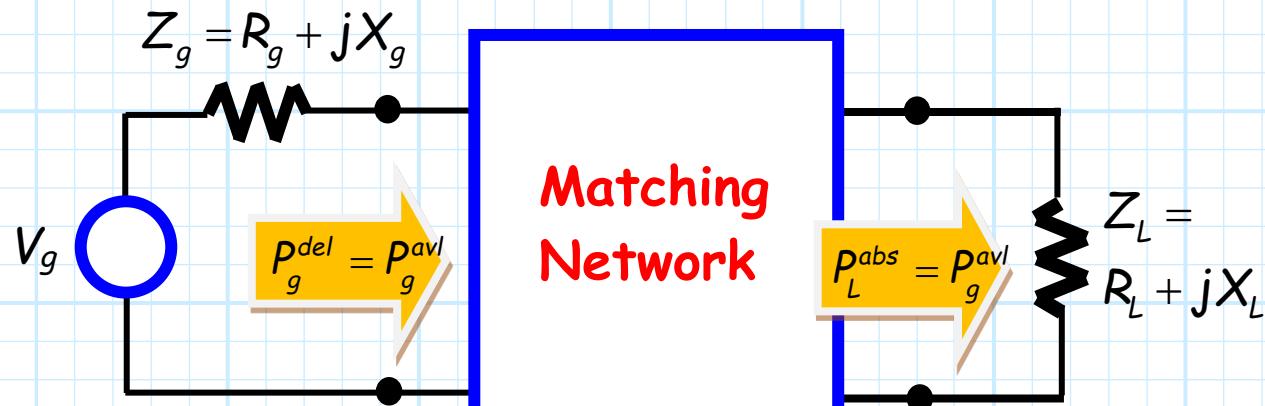
Because the matching network is **lossless**, the available power of the transformed source is **equal** to that of the original:

$$P_{\text{out}}^{\text{avl}} = P_g^{\text{avl}}$$

Therefore, the power **absorbed** by the load is also equal to the power available from the **original** source:

$$P_L^{\text{abs}} = P_{\text{out}}^{\text{avl}} = P_g^{\text{avl}}$$

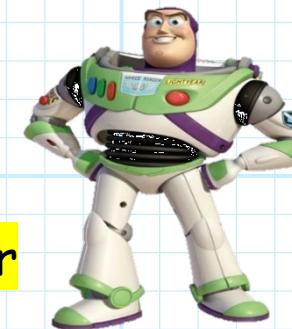
And that's just what we were after!



Making R_{out} really small is not the answer

Q: Wait, shouldn't we transform the source to one that increases the available power (preferably to infinity)?

A: Remember, a lossless source transformer cannot alter the available power (either up or down).



If we transform the source to have a **really small** value of R_{out} , we will find that the transformed value $|V_{out}|^2$ is proportionately just as small.

→ Thus, the available power is an invariant.

All we can do is to insert a lossless source transformer so that **all this** (unalterable) available power is **absorbed** by the load! I.E., by making:

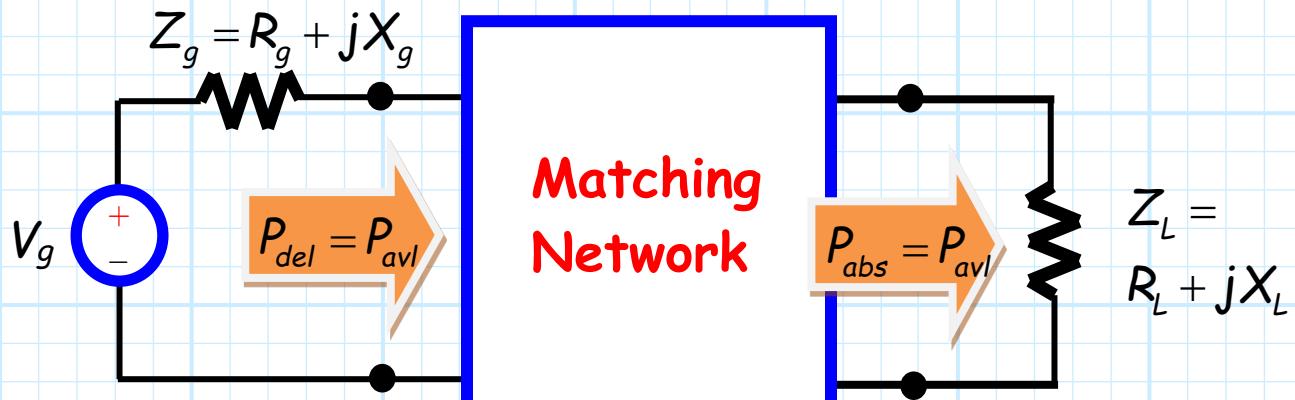
$$Z_{out} = jX_{22} + \frac{(X_{12})^2}{jX_{11} + Z_g} = Z_L^*$$

It depends on source and load— but does not alter them

1. The design and construction of this lossless source transformer will depend on both source impedance Z_g and load impedance Z_L .

$$Z_{out} = jX_{22} + \frac{(X_{12})^2}{jX_{11} + Z_g} = Z_L^*$$

2. However, the source transformer does not physically alter either of these two quantities, the source and load are left physically unchanged!



Transform the source, or transform the load?

Q: So which one is better: matching with a lossless impedance transformer, or matching with a lossless source transformer?

A: They are the same—and I mean that very literally!

Look at the design equation for a matching network that implements an impedance transformer:

$$Z_{in} = jX_{11} + \frac{(X_{12})^2}{jX_{22} + Z_L} = Z_g^*$$

meaning that we need to find a lossless two-port network with trans-impedance values X_{11}, X_{12}, X_{22} that satisfy this equation:

$$Z_g^* = jX_{11} + \frac{(X_{12})^2}{jX_{22} + Z_L}$$

A design for the source transformer

Now consider the design equation for a matching network that implements a **source transformer**:

$$Z_{out} = jX_{22} + \frac{(X_{12})^2}{jX_{11} + Z_g} = Z_L^*$$

meaning that we need to find a lossless two-port network with trans-impedance values X_{11}, X_{12}, X_{22} that satisfy this equation:

$$Z_L^* = jX_{22} + \frac{(X_{12})^2}{jX_{11} + Z_g}$$

The same solutions satisfy both!

But now, let's take the **complex conjugate** of the impedance transformer design equation:

$$Z_g = jX_{11} + \frac{(X_{12})^2}{jX_{22} + Z_L^*}$$

and now solve for Z_L^* :

$$Z_L^* = jX_{22} + \frac{(X_{12})^2}{jX_{11} + Z_g}$$

This is precisely the design equation for the **source** transformer!!!!

Q: ???

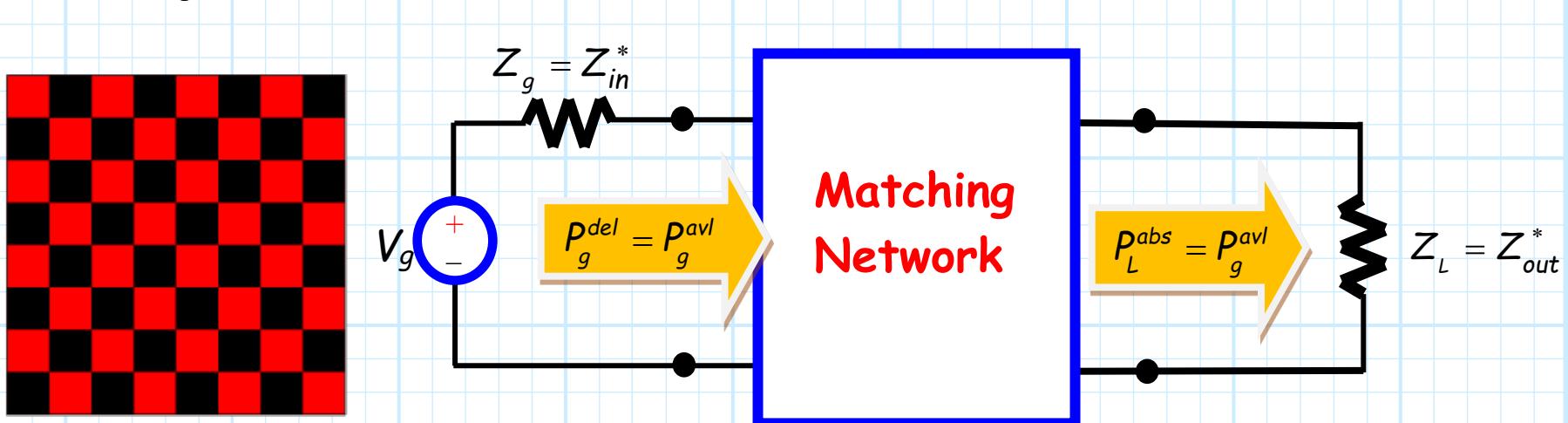
A: This means that if a lossless network has trans-impedance values X_{11}, X_{12}, X_{22} that satisfy **one** design equation, then they likewise satisfy the **other** design equation!!

A red board with black squares, or a black board with red squares?

Q: ???

A: An **impedance** transformer that matches **input** impedance Z_{in} to source impedance Z_g , is likewise a **source** transformer that matches Z_{out} to Z_L !!!

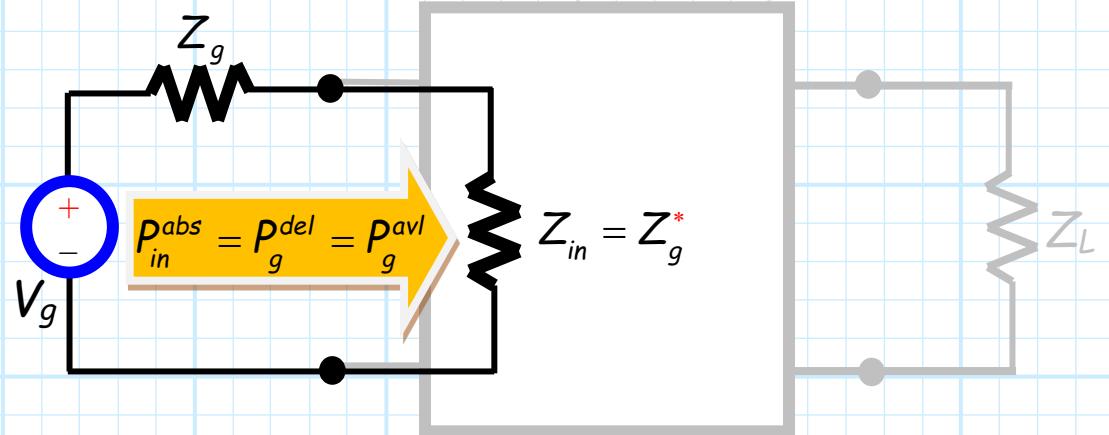
Similarly, a **source** transformer that matches **output** impedance Z_{out} to load impedance Z_L , is likewise an **impedance** transformer that matches Z_{in} to Z_g !



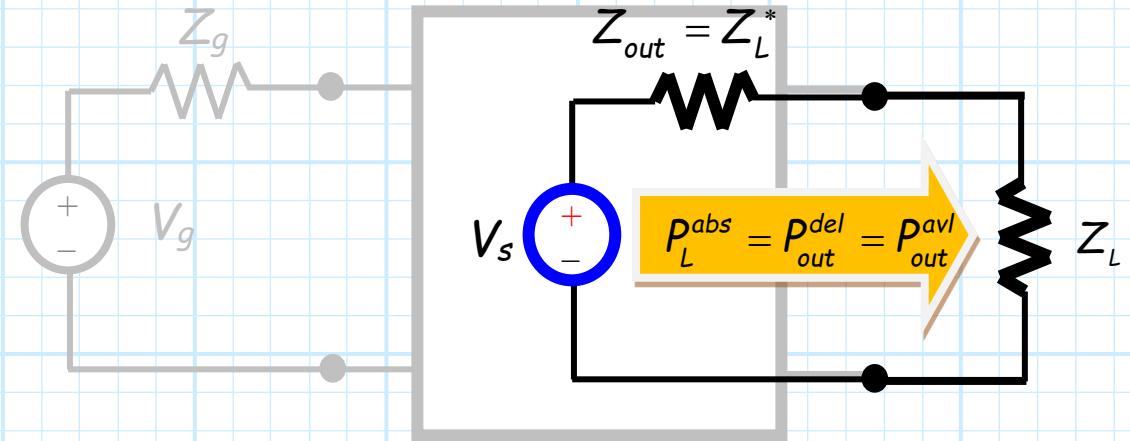
Two ways to consider the same thing

Thus, we can look at the matching network in two equivalent ways:

1. As a network attached to a load, one that "transforms" its impedance to Z_{in} —a value matched to the source impedance Z_g :



2. Or, as network attached to a source, one that "transforms" its impedance to Z_{out} —a value matched to the load impedance Z_L :



Make this make sense

Consider these **three** conditions:

1. $Z_{in} = Z_g^*$ (therefore $P_{in}^{abs} = P_g^{avl}$).

2. $Z_{out} = Z_L^*$ (therefore $P_L^{abs} = P_{out}^{avl}$).

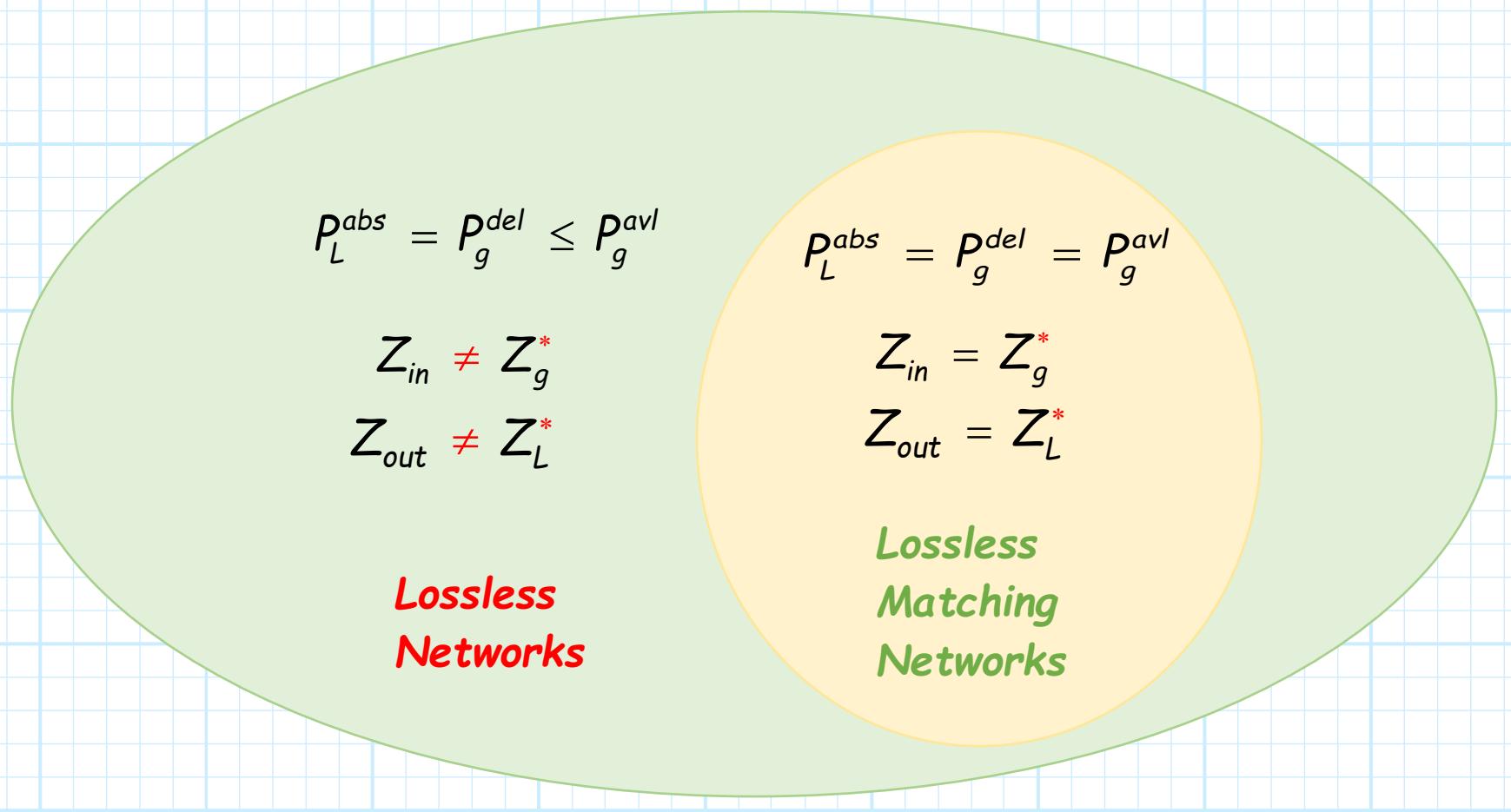
3. $P_L^{abs} = P_g^{avl}$ (since $P_g^{out} = P_{out}^{avl}$).

If **any one** of these 3 conditions is true, then the **other two** conditions must be **true also!**

Thus:

- * A conjugate match **anywhere** means there is a conjugate match **everywhere!**
- * If $P_L^{abs} = P_g^{avl}$, then a **conjugate match exists everywhere** (and **vice versa!**).

Matching is a subset of all lossless



Although matching networks are lossless, most lossless networks are not matching networks!