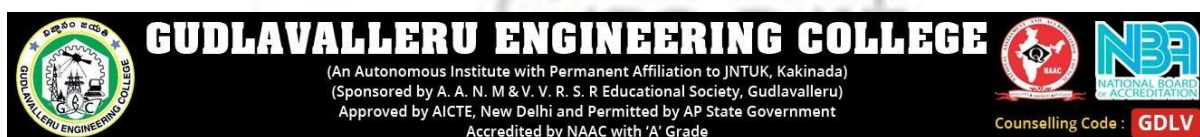


Internship Program ReportBy

MANDALA RAMESH BABU-18481A0260



In association with



Contents

Introduction	3
Program organiser.....	3
Courtesy	3
Program details	3
Internship program	3
3 rd May2021: Introduction to EPC Industry	4
4 th May2021: Engineering documentation for EPC projects.....	5
5 th May2021: Engineering documentation for commands and formulae.....	6
7 th May2021: Engineering documentation for Electrical system design.....	7
10 th May2021: Engineering documentation for Typical diagrams	8
11 th May2021: Classification of Transformers and Generators.....	9
12 th May2021: Classification of Switchgare construction and power factor improvement.....	10
17 th May2021: Detailing about UPS system and Busducts.....	11
18 th May2021: Detailing about Motor Starters and Sizing of motors.	12
19 th May2021: Discribing about Earthing system and Lighting Protection.....	13
20 th May2021: Lighting or illumination systems and calculations.	14
21 th May2021: Lighting or illumination systems using DIALUX software.....	15
24 th May2021: Cabling and their calculations and types	16
25 th May2021: Cabling calculations and Cable gland selection.....	17
28 th May2021: Load calculations and Transformer sizing calculations	18
29th May2021: DG set calculations.	19
2nd june2021: Caluculations of Earthing and Lighting protection.....	20
5 th june 2021: Cable sizing and cable tray sizing calculations.....	21
Conclusion	22
Feedback:	22

Introduction

Internship program arranged by GUDLAVALLERU ENGINEERING COLLEGE in association with Smart Internz, Hyderabad for the benefit of 3rd year EEE batch 2018-2022 on Electrical Detailed design Engineering for Oil& Gas, Power and Utility industrial sectors.

Program organiser

Smart Bridge, Hyderabad.

Pioneer in organising Internships, knowledge workshops, debates, hackathons, Technical



sessions and Industrial Automation projects.

Courtesy

Dr. Sri B. Dasu – HOD – EEE, GEC

Mr. G. Srinivasa Rao – Internship coordinator

Mr. Ramesh V - Mentor

Mr. Vinay Kumar - System Support

Mr. Harikanth – Software/Technical Support

Program details

Smart Internz program schedule: 4 weeks starting from 3rd May 2021

Daily schedule time shall be 4PM to 6.30PM

Mode of Classes: On line through ZOOM

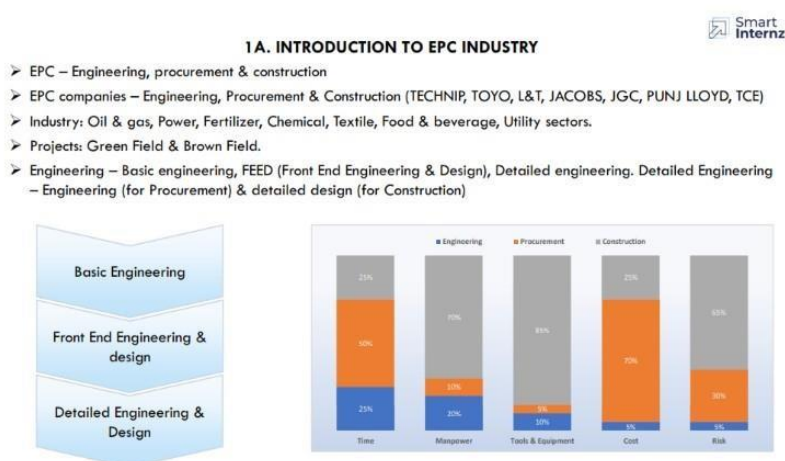
Presenter: Mr Ramesh V

Internship program

We have been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

3rd May2021: Introduction to EPC Industry

1	EPC Industry & Electrical Detailed Engineering	EPC Industry	Introduction
		Engineering	Types of Engineering
		Procurement	Engineering role in procurement
		Construction	Engineering role during construction



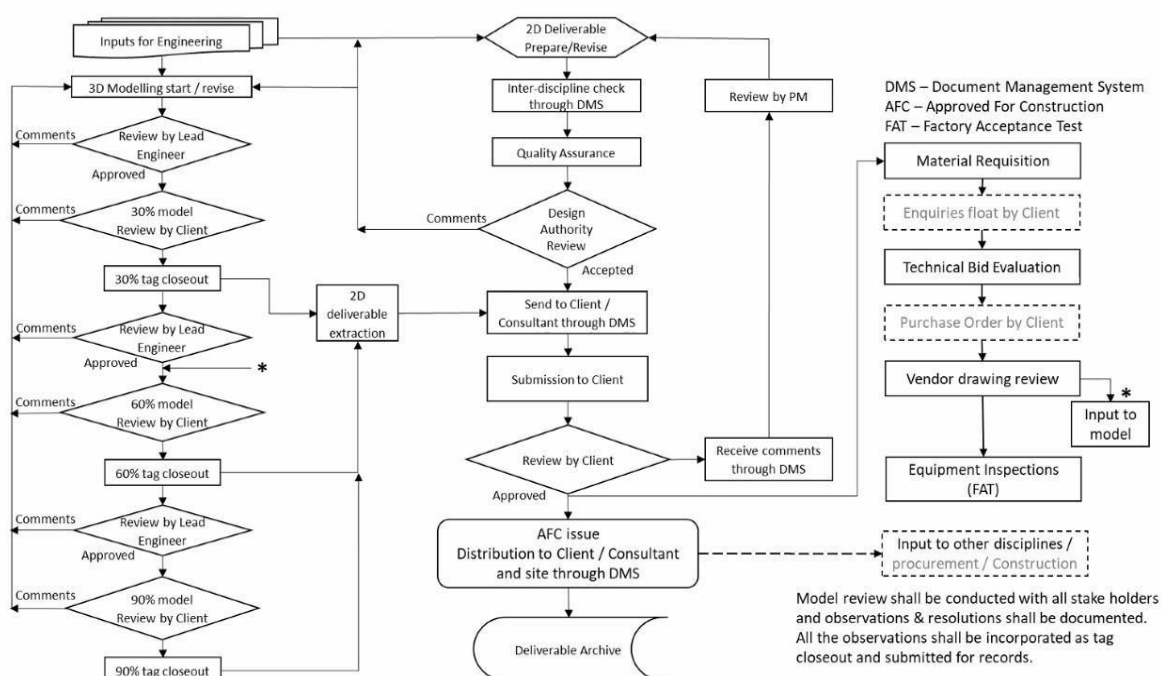
Topic details:

Engineering phases, Engineering deliverables (drawings & documents) list, Design Engineer role at various phases of project.

4th May2021: Engineering documentation for EPC projects

2	Electrical Design Documentation	Engineering Deliverables list	Sequence of deliverables
		Detailed Engineering work flow	Detailed engineering process
		Document transmission	Document submission and info exchange
		Deliverables types	Different types of deliverables

3. ELECTRICAL DESIGN & DETAILED ENGINEERING - PROCESS



Topic details:

Engineering deliverables list, detailed engineering flow, engineering support flow, engineering support to procurements.

5 th May2021: Engineering documentation for commands and formulae

3	Document & Drawing tools	MS Word	Report / Calculations formats
		MS Excel	Basic excel commands
		Autocad	Basic line diagrams and layout commends

3C. AUTOCAD BASIC COMMANDS



AUTOCAD BASIC KEYS							
STANDARD		DRAW		MODIFY		FORMAT	
NEW	Ctrl+N	LINE	L	ERASE	E	PROPERTIES	MO
OPEN	Ctrl+O	RAY	RAY	COPY	CO	SELECT COLOR	COL
SAVE	Ctrl+S	PLINE	PL	MIRROR	MI	LAYER	LA
PLOT	Ctrl+P	3DPOLY	3P	OFFSET	O	LINETYPE	LT
PLOT PREVIEW	PRE	POLIGONE	POL	ARRAY	AR	LINEWEIGHTS	LW
CUT	Ctrl+X	RECTANGLE	REC	MOVE	M	LT SCALE	LTS
COPY	Ctrl+C	ARC	A	ROTATE	RO	LIST	LI
PASTE	Ctrl+V	CIRCLE	C	SCALE	SC	DIMEN. STYLE	D
MATCH PROPE.	MA	SPLINE	SPL	STRECH	S	RENAME	REN
CLOSE	Ctrl+F4	ELLIPSE	EL	TRIM	TR	OPTION	OP
EXIT	Ctrl+Q	BLOCK	B	EXTENED	EX		
		POINT	PO	BRAKE	BR		
		HATCH	H	CHAMFER	CHA		
		GRADIENT	GD	FILLET	F		
		REGION	REG	EXPLODE	X		
		BOUNDARY	BO				
		DONUT	DO				

EXTRA				DRAFTING		PAPER SIZE
UNIT	UN	UCS	UCS	ORTHO	F8, Ctrl+L	A4=210*297
LIMITS	LIMITS	SINGLE TEXT	DT	OSNAP	F3, Ctrl+F	A3=297*420
(0,0; 1000,1000)		MULTILINE TEXT	MT	POLAR	F10, Ctrl+U	A2=420*594
ZOOM	Z	EDIT TEXT	ED	GRID	F7, Ctrl+G	A1=594*841
ALL	A	OBJECT SNAP	OB	OTRACK	F11	A0=841*1189
PAN	P	DIMENTION	DIM	SNAP	F9	
CLEAN SCREEN	Ctrl+O	HORIZONTAL	HOR			
COMMAMD WIN	Ctrl+9	VERTICAL	VER			



Topic details:

Here we need to learn the basis of the autocadbasic keys like standard, modify,draw,format,papersize etc..

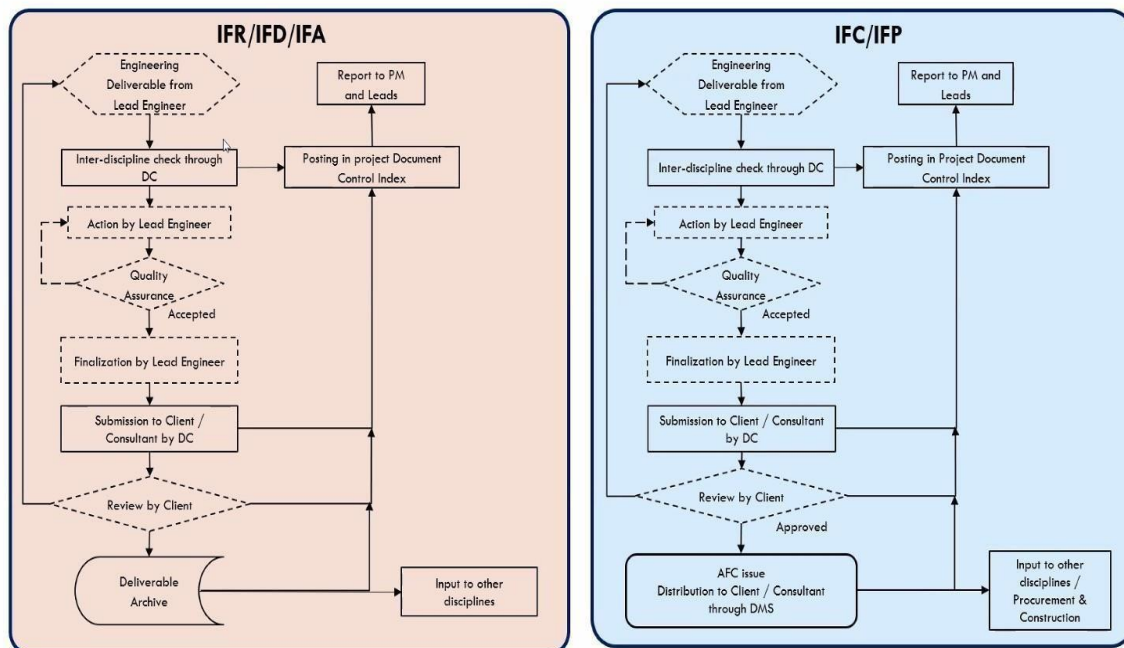
7 th May2021: Engineering documentation for Electrical system design

4	Electrical system design for a small small project	Overall plant description
		Sequence of approach
		Approach to detailed design

Topic details:



1C. DETAILED ENGINEERING



Here we observed that how to do a project and Sequence of approach, Approach to detail design and Overall plant distribution system.

5	Electrical system design for typical diagrams		
		Load lists shedule	Power flow diagram
		Single line diagram	Typical schematic diagram

Page 8 of 23

11th May2021: Classification of Transformers and Generators

6	Classification of Transformers and Generators	Different types of Transformers	Different types of Generators
---	---	---------------------------------	-------------------------------

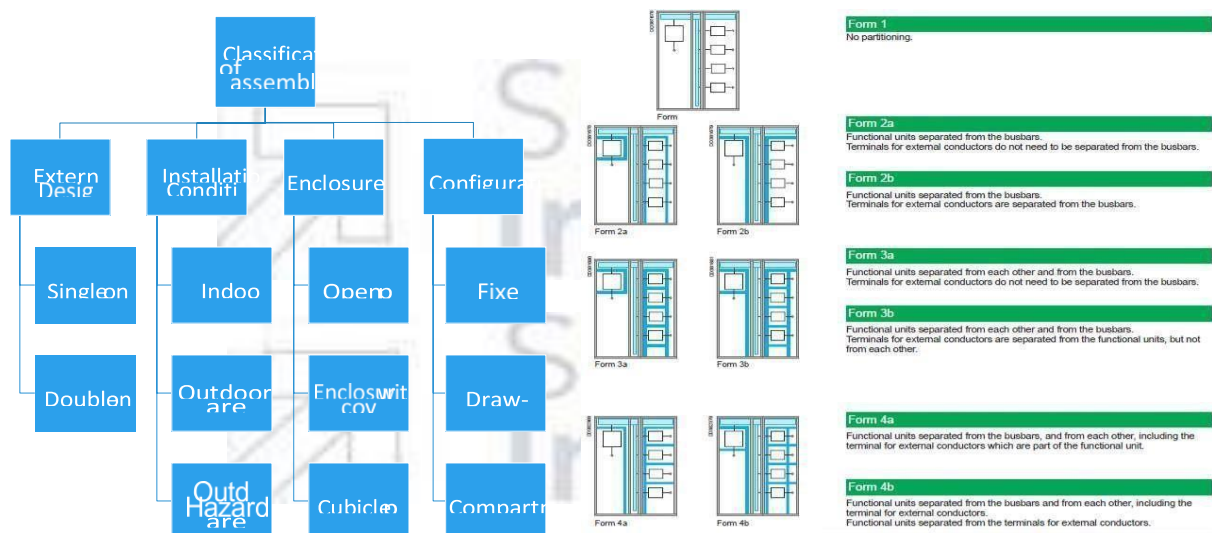


Topic details:

Classification of Transformers and Generators

12th May2021: Classification of Switchgare construction and power factor improvement

7	Classification of Switchgare construction and power factor improvement	Different types of Switchgare assemblies	Power factor improvement
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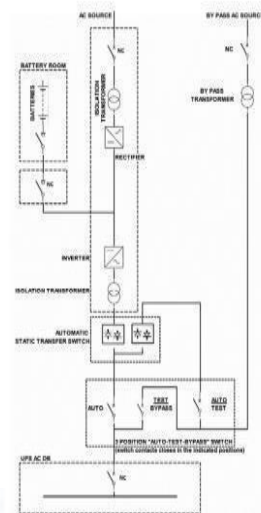
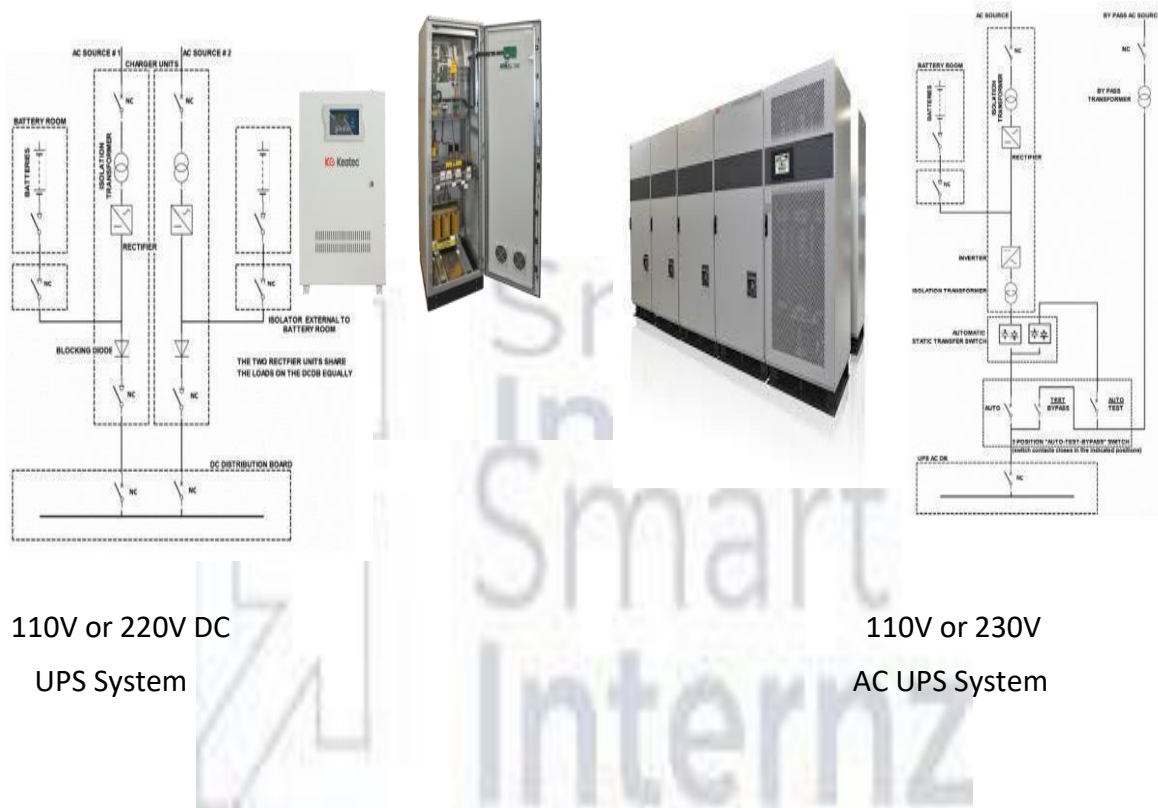


Topic details:

Classification of Switchgare contruction and Power Factor Improvement

17th May2021: Detailing about UPS system and Busducts.

8	Detailing about UPS system and Busducts	Uninterruptible power supply system	Busducts of the system
---	---	-------------------------------------	------------------------

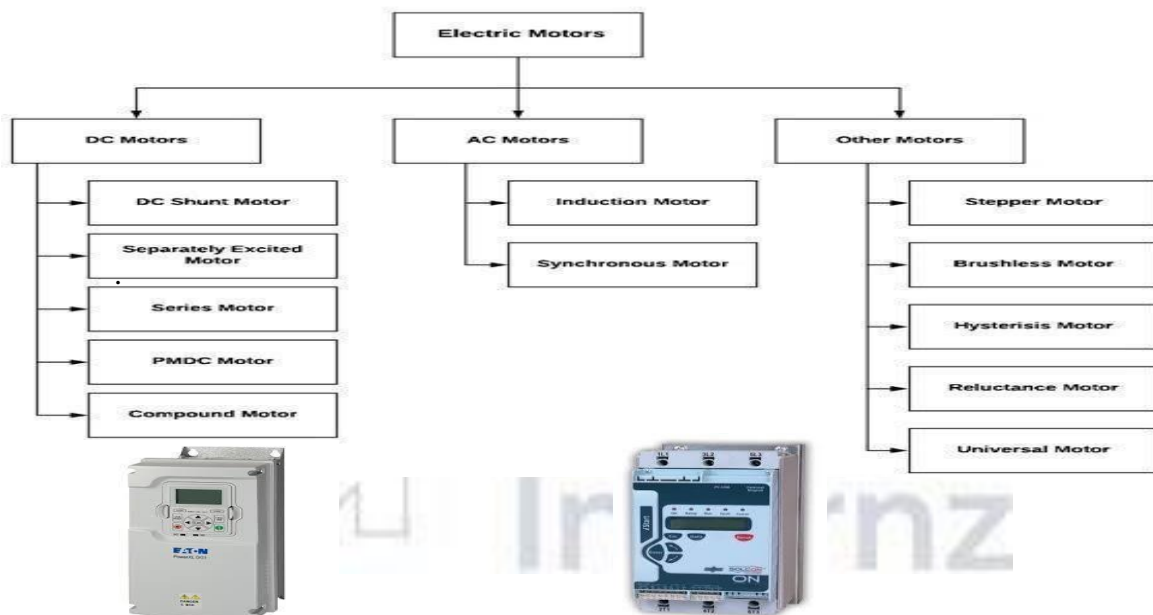


Topic details: Power distribution of UPS system and Busducts.

UPS systems are designed to provide continuous power to a load, even with an interruption or loss of utility supply power. UPS generally involves a balance of cost Vs need.

18th May2021: Detailing about Motor Starters and Sizing of motors.

9	Detailing about Motor Starters and Sizing of motors	Motor starters and drives	Sizing and selection of motors
---	---	---------------------------	--------------------------------



Topic details: Detailing about Motor Starter and Sizing of motors and their selection.

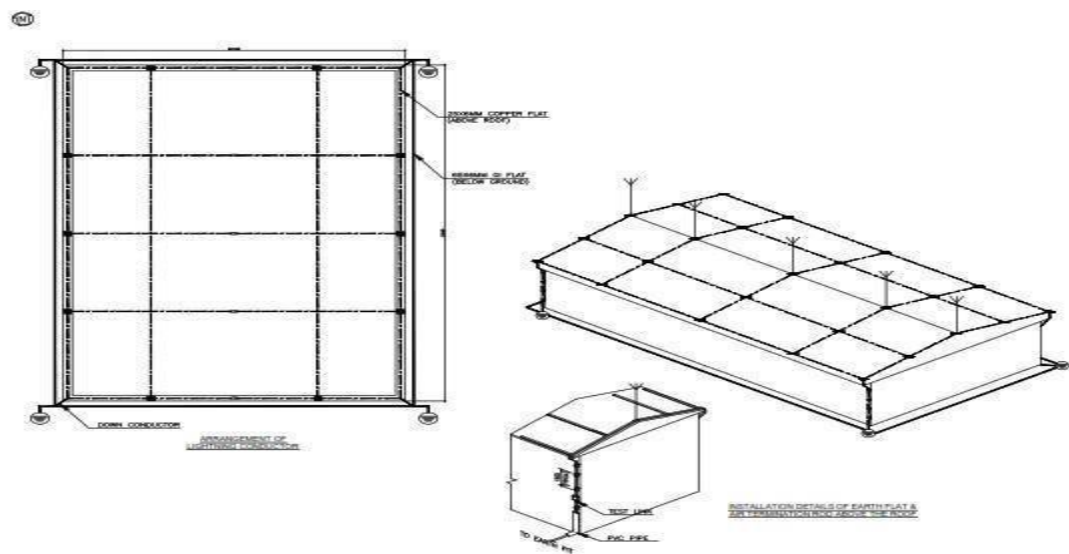
The principal function of a motor starter is to start and stop the respective motor connected with specially designed electromechanical switches which are similar in some ways to relays. The main difference between a relay and a starter is that a starter has overload protection for the motor that is missing in a relay.

Different types of motor starters are as follows:

- Direct-On-Line Starter
- Rotor Resistance Starter
- Stator Resistance Starter
- Auto Transformer Starter

19th May2021: Discribing about Earthing system and Lighting Protection.

10	Discribing about Earthing system and Lighting Protection.	Plant Earthing system	Lighting Protection materials
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Topic details: Discribing about Earthing system and Lighting Protection.

Lightning protection required for high rise structures and important buildings against lightning currents during thunder storms. Primarily Lightning protection system calculations are done based on soil resistivity, conductor material, coverage structure / Building to determine whether lightning protection is required or not.

20th May2021: Lighting or illumination systems and calculations.

11	Lighting or Illumination systems and Calculations	Lighting or illumination systems	Lighting calculations
----	---	----------------------------------	-----------------------

Topic details: Lighting or Illumination systems and Calculations.

All outdoor lighting fittings shall be connected with armoured PVC cable of suitable no. of cores and size. Necessary type and no. of junction boxes shall be provided for branch connections. Indoor light fittings shall be connected with FRLS PVC wires laid in cable trunks or conduits.

Inputs required: Equipment and cable routing layouts, lighting calculations, Design basis for type of light fittings to be used, required lux levels

Lighting calculations software: Dialux, Chalmrite, Calculux, Relux, Luxicon,

CG Lux Applicable Standards: IS 6665: Code of practice for industrial



lighting, IS 3646: Code

of practice for interior illumination, IEC 60598: Luminaires, IEC 62493: Assessment of lighting equipment related to human exposure to electromagnetic field

Deliverables: Indoor Lighting layouts, socket outlet layouts, Street lighting and area lighting layouts. BOQ.

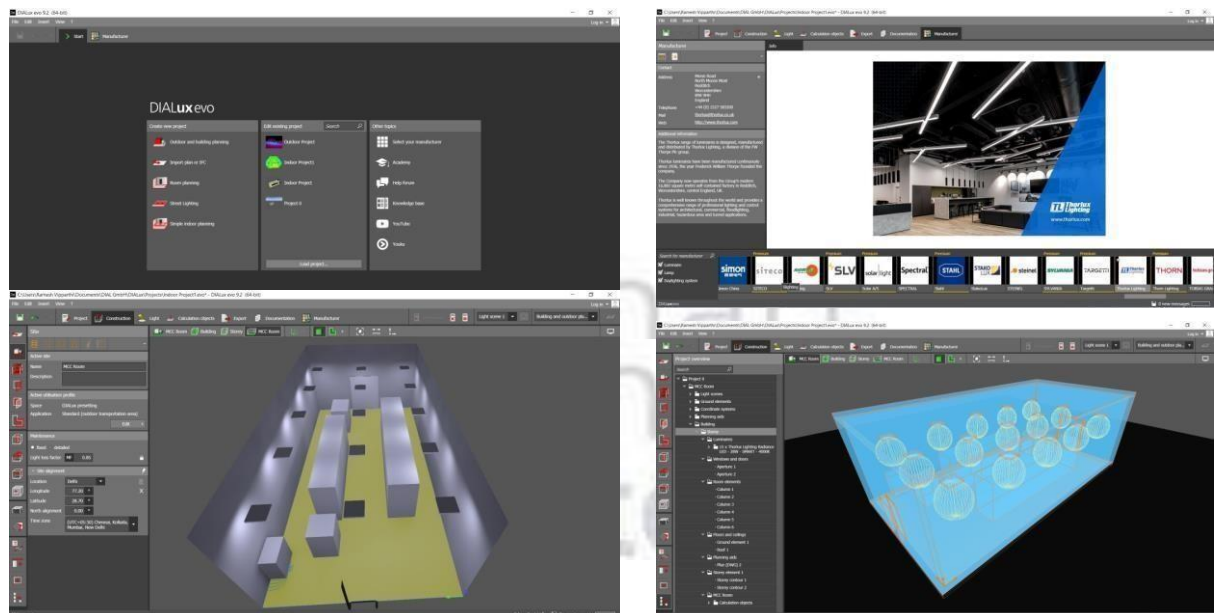
Types of light fittings: Industrial, flame proof type (EX d), increased safety type (Ex e).

21th May2021: Lighting or illumination systems using DIALUX software.

12	Lighting or Illumination using DIALUX software	Lighting or illumination systems	Operation of dialux software
----	--	----------------------------------	------------------------------

Topic details: Lighting or Illumination Calculations using DIALUX software.

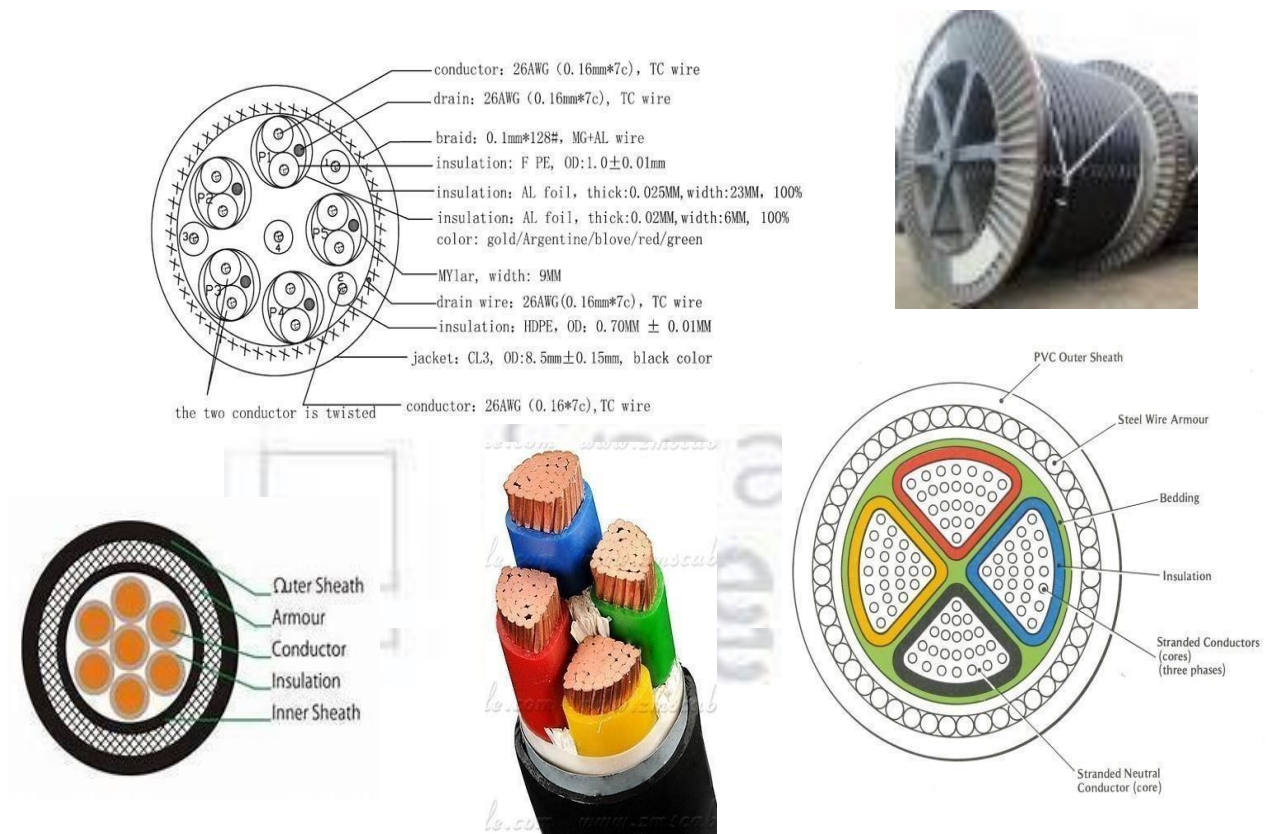
Here we are using this Dialux evo 5.9.2 software windows to construct the power plant and we can perform the operation from this software.



24th May2021: Cabling and their calculations and types.

13	Cabling and their types and claculations	Cabling calculations	Types of cabling materials
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Topic details: Cabling and their types and claculations .



Electrical cables must be properly supported to relieve mechanical stresses on the conductors, and protected from harsh conditions such as abrasion which might degrade the insulation.

Cables generally laid in the cable trays above ground, direct buried underground and in metallic or PVC conduits. Derating factors may be applicable for each type of cable laying conditions.

25th May2021: Cabling calculations and Cable gland selection.

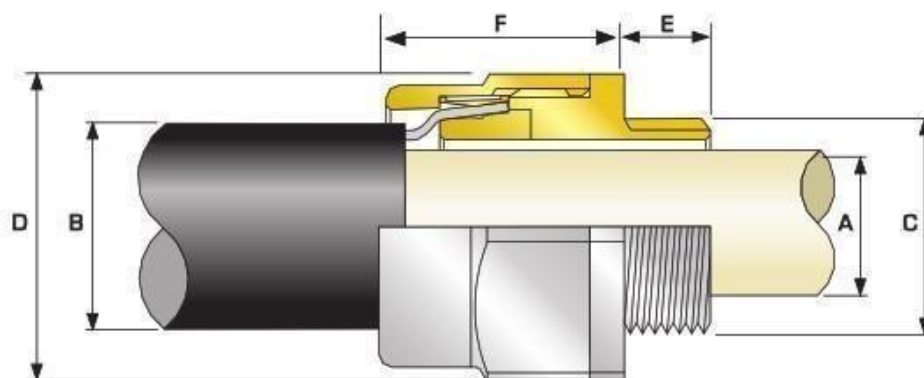
14	Cabling calculations and cable gland selection	Cabling calculations	Cable gland selection
----	--	----------------------	-----------------------

Topic details: Cable sizing calculation and cable gland selection.

Inputs required: Load List, Design basis, Electrical equipment layout, cable schedule, vendor catalogues for cable tray.

Cable tray sizing shall be performed for each branch of cable tray routing up to the load point. Results shall be checked with specified limits mentioned in design basis.

Cable gland:



Cable Gland Selection Table

Refer to illustration at the top of the page.

Cable Gland Size	Available Entry Threads "C" (Alternate Metric Thread Lengths Available)		Cable Bedding Diameter "A"	Overall Cable Diameter "B"	Armour Range		Across Flats "D"	Across Corners "D"	Protrusion Length "F"
	Metric	Thread Length (Metric) "E"	Max	Max	Min	Max	Max	Max	
20S16	M20	10.0	8.7	13.2	0.8	1.25	24.0	26.4	35.2
20S	M20	10.0	11.7	15.9	0.8	1.25	24.0	26.4	32.2
20	M20	10.0	14.0	20.9	0.8	1.25	30.5	33.6	30.6
25	M25	10.0	20.0	26.2	1.25	1.6	36.0	39.6	36.4
32	M32	10.0	26.3	33.9	1.6	2.0	46.0	50.6	32.6
40	M40	15.0	32.2	40.4	1.6	2.0	55.0	60.5	36.6
50S	M50	15.0	38.2	46.7	2.0	2.5	60.0	66.0	39.6
50	M50	15.0	44.1	53.1	2.0	2.5	70.1	77.1	39.1
63S	M63	15.0	50.0	59.4	2.0	2.5	75.0	82.5	52.0
63	M63	15.0	56.0	65.9	2.0	2.5	80.0	88.0	49.8
75S	M75	15.0	62.0	72.1	2.0	2.5	90.0	99.0	63.7
75	M75	15.0	68.0	78.5	2.5	3.0	100.0	110.0	57.3
90	M90	24.0	80.0	90.4	3.15	4.0	114.3	125.7	66.6

28 th May2021: Load calculations and Transformer sizing calculations

Calculation for Transformer Capacity

1.0 Example of calculation for Transformer Capacity

1.1 Calculation for assumed load

Assumed loads used for this example are as follows:

	KW	KVAR	KVA	
a. Continuous load	144.25	122.5	185.48	... [i]
b. Intermittent load / Diversity Factor	4.78	4.5	6.54	... [ii]
c. Standby load required as assumed load	45.22	35.1	55.34	... [iii]
Max. Consumed load = [i] + 30X [ii] + 10X [iii]	158.3	127.4	197.87	
Future expansion load [20X capacity]	31.1	25.5	38.41	
Total Load =	189.4	152.9	236.28	

1.2 Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load	=	197.4	KVA
Spare capacity	=	33.4	KVA
Required capacity	=	230.8	KVA
Transformer rated capacity	=	300	KVA

1.3 Voltage regulation check

During starting or deceleration of max. capacity motor [3400 KW], while all the other loads running, the voltage regulation is as follows:

$P_1 = 300 \text{ KVA}$ [X2] = 4 k Ratio X/R = 4.5 [refer table]

Hours, $X_R =$ = 2.215 X

$XX =$ = 3.33 X

$P_1 = 30 \text{ KW loading} \times K = 5$ k C = 1 k Cos $\phi = 0.78$ k Eff. = 0.91 k Cos $\phi_0 = 0.25$

$P_2 =$ = 255.539 KVA

Cos $\phi_1 = 0.25$, Corresponding to Angle $\phi =$ 75.5225 Degrees for which Sin $\phi =$ 0.97

$P_1 =$ 454 KVA k PD in KW is = 117.74 k P_1 in Kvar = 34.4 Cos $\phi_2 =$ 0.788

Cos $\phi_1 = 0.25$, Corresponding to Angle $\phi =$ 75.5225 Degrees, for which Sin $\phi =$ 0.97

$P_{11} =$ = 184.478 KW

$P_{12} =$ = 333.34 KVAR

$P_2 =$ = 385.287 KVA

Cos $\phi_2 =$ 0.47834, where as Sin $\phi_2 =$ 0.882

Voltage Regulation = = 5.1 X Selected Transformer rating is adequate.

1.4 Selection of rated capacity

Here 300KVA Transformer rating selected.

29th May2021: DG set calculations

16	DG set calculations
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DG SIZING CALCULATIONS		
Design Data		
Rated Voltage	415	KV
Power Factor (Cos ϕ)	0.74	Req
Efficiency	0.85	Req
Running kVA of load motor (Cos ϕ = 0.85)	48	KVA
Starting current ratio of motor	5	[Considering starting method as Soft starter]
Starting kVA of the largest motor (Running kVA of load motor \times Starting current ratio of motor)	240	KVA
Power load of DG set in KVA (Total operating load in KVA - Running kVA of load motor)	168	KVA
A Continuous operation under load - P1		
Capacity of DG set based on continuous operation under load P1	168	KVA
B Transient Voltage Dip during starting of load motor P2		
Total momentary load in KVA (Starting kVA of the load motor - Power load of DG set in KVA)	438	KVA
Subtransient Reactance of Generator (X $_d'$)	7.51X	[Assumed]
Transient Reactance of Generator (X $_d$)	18.865X	[Assumed]
X $_d''$ - [X $_d'$ - X $_d$]/2	5.67875	
Transient Voltage Dip	15X	[Max]
Transient Voltage dip during Soft starter starting of Load motor P2 - Total momentary load in KVA \times X $_d''$ \times [1 - Transient Voltage Dip] [Transient Voltage Dip]	253	KVA
C Overload capacity P3		
Capacity of DG set required considering overload capacity		
Total momentary load in KVA	438	KVA
overload capacity of DG (K) [Ref: IS/IEC 60094-1, Clause 5.3.2]	158X	
Capacity of DG set required considering overload capacity (P3) - Total momentary load in KVA overload capacity of DG (K)	287	KVA
Considering the load motor amongst P1, P2 and P3		
Continuous operation under load - P1	168	KVA
Transient Voltage dip during Soft starter starting of Load motor P2	253	KVA
Overload capacity P3	287	KVA
Considering the load motor amongst P1, P2 and P3	287	KVA
Hence, Existing Generator 287 KVA is adequate to cater the loads as per scheduled loads		
NOTE: VOLTAGE DIP CONSIDERED - 15X		

Topic details:

Transformer and DG set calculations, types, sizing or selections

2nd june2021: Calculations of Earthing and Lighting protection.

17	Calculation of Earthing and Lighting protection calculations	Earthing calculations	Lighting protection calculation
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Topic details:

Earthing calculation

	#	
Maximum line-to-ground fault in kA for 4 sec	15	
Earthing material [Earth rod & earth strip]	G1	
Depth of each flat bar in meter	B.5	
Average depth / length of Earth rod in meters	4.5	
Soil resistivity @ meter	15	
Radiated temperature in deg C	55	
Flat dimension [earth grid] L x B in meters	75 155	
Number of earth rods in nos.	6	
Earth electrode sizing: As - Required annular cross section in sq.mm $S_g = A_s \times \sqrt{\frac{TCAP(10^{-4})}{\rho_s \ln(R_2/R_1)}} \cdot Z_{Lg} \left[\frac{(R_p + T_m)}{(K_p + T_e)} \right]$		
Us - Thermal coefficient of resistivity at 28 °C	0.0032	
Pv - Resistivity of ground annular at 28 °C	28.18	
Ts - Radiated Temperature in °C	58	
L - RMS Fault current in kA - 5B KA	15	
Ie - Short circuit current duration sec	1	
Thermal capacity factor, TCAP J/[cm ³ .°C]	3.53	
Tm - Maximum allowable temperature for copper annular, in °C	415	
Kk - Factor at °C	255	
The data taken from IEEE 80-2000, Clause 41.3, Table-1 for solid steel rod:		
TS - As'	0.123	
As - Required annular cross section in sq.mm	422	
Earth rod dia in mm	12	
Earth rod dia [including 25% corrosion allowance] in mm	16	
Earth Flat sizing: As - Required annular cross section in sq.mm $S_g = A_s \times \sqrt{\frac{TCAP(10^{-4})}{\rho_s \ln(R_2/R_1)}} \cdot Z_{Lg} \left[\frac{(R_p + T_m)}{(K_p + T_e)} \right]$		
Us - Thermal coefficient of resistivity at 28 °C	0.0032	
Pv - Resistivity of ground annular at 28 °C	28.18	
Ts - Radiated Temperature in °C	58	
L - RMS Fault current in kA - 5B KA	15	
Ie - Short circuit current duration sec	1	
Thermal capacity factor, TCAP J/[cm ³ .°C]	3.53	
Tm - Maximum allowable temperature for copper annular, in °C	415	
Kk - Factor at °C	255	
The data taken from IEEE 80-2000, Clause 41.3, Table-1 for solid steel rod:		
TS - As'	0.123	
As - Required annular cross section in sq.mm	422	
Earth Flat area in mm	12	
Earth Flat area [including 25% corrosion allowance] in mm	16	
Selectd Flat size W' * Thk in sq mm	28	
Rq - Grid resistance Grid resistance can be calculated using Eq. 52 of IEEE 80 $R_{eq} = \rho \left\{ \left[\frac{1}{L} + \frac{1}{\sqrt{D} \pi A} \right] \left[1 + \frac{1}{1+h} \frac{1}{\sqrt{D} \pi A} \right] \right\}$		
p - Soil resistivity in @meter-	15	
L - Total buried length of ground annular in meter	428	
b - Depth of burial in meter	8.5	
A - Grid area in sq. meter	18125	
R - Grid resistance	0.003	

Earthing calculation

The data taken from IEEE 90-3000, Clause 11.3, Table-1 for clad steel rod:	
K0 - Factor of OC	383
TW - Maximum allowable temperature for copper conductor in OC	418
Thermal capacity factor, TCVF η (cm ² /°C)	383
IC - Short circuit current duration sec	
I ² - RMS fault current in kA = 20 kA	14
TA - Ambient Temperature in °C	22
bl - Resistivity of Ground conductor at 30 OC	30.10
al - Thermal co-efficient of resistivity at 30 OC	0.0025
	$I^R = A^2 \times \left[\frac{I^{20} \times 10^{20} \times b^2}{1.7 \times TCVF \times T \times 10^{-4}} \right] \times 10^4 \left[\frac{K^0 + 1}{K^0 + 1.7} \right]$
	$I^R = A^2 \times \left[\frac{I^{20} \times 10^{20} \times b^2}{1.7 \times TCVF \times T \times 10^{-4}} \right] \times 10^4 \left[\frac{K^0 + 1}{K^0 + 1.7} \right]$
AC - Required conductor cross section in sq.mm	
Earth pit sizing:	
Earth rod dia (including 32% corrosion allowance) in mm	12
Earth rod dia in mm	15
AC - Required conductor cross section in sq.mm	114
14 = AC *	0.153
The data taken from IEEE 90-3000, Clause 11.3, Table-1 for clad steel rod:	
K0 - Factor of OC	383
TW - Maximum allowable temperature for copper conductor in OC	418
Thermal capacity factor, TCVF η (cm ² /°C)	383
IC - Short circuit current duration sec	
I ² - RMS fault current in kA = 20 kA	14
TA - Ambient Temperature in °C	22
bl - Resistivity of Ground conductor at 30 OC	30.10
al - Thermal co-efficient of resistivity at 30 OC	0.0025
AC - Required conductor cross section in sq.mm	
Earth electrode sizing:	
Number of earth rods in nos	6
Pit dimensions (earth rod) L x B in meters	32
Ambient temperature in deg C	32
Soil resistivity Ohm-met	12
Average depth of earth rod in meters	4.2
Depth of earth pit in meters	0.2
Earth rod dia in mm	91
Maximum line-to-ground fault in kA for 1 sec	14
Earth connection	
Welding joint	

18	Cable sizing and cable tray sizing calculations	Cable sizing calculations	Cable tray calculation
----	---	---------------------------	------------------------

Cable sizing and cable tray sizing calculations for LV cables and MV/HV cables.

[illegible]Page 22 of 23

Conclusion

We have been taught many aspects of engineering activities during the EPC stages for all electrical and related other disciplines also.

Feedback

Smart Bridge

They conduct summer internships, work shops, debates, hackthons, technical sessions.

Method of conducting program

Online virtual program with presentation slides and explanation on the topic and practical usage of topic and with some examples.

Program highlights

It is for the detailed design of any industrial sectors.

Material

The material was good .

Benefits

It has been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

ASSIGNMENT-1

ELECTRICAL LOAD CALCULATIONS LV MCC

[illegible]

DG SIZING CALCULATIONS - VTV -3281 -LIT-9511-EL-CAL-002

Design Data

Rated Voltage	6.6	KV
Power factor (CosØ)	0.91	Assumed
Efficiency	0.94	Assumed
Total operating load on DG set in kVA at 0.91 power factor	#REF!	KVA (Refer Annexure-1 Electrical Load schedule)
Last motor to start in the sequence - load in KW	350	KW
Running kVA of last motor (CosØ= 0.91)	409	KVA
Starting current ratio of motor	4	(Considering starting method as Soft starter)
Starting KVA of the last motor (Running kVA of last motor X Starting current ratio of motor)	1637	KVA
Base load of DG set in KVA (Total operating load in kVA – Running kVA of last motor)	#REF!	KVA

A Continous operation under load -P1

Capacity of DG set based on continuous operation under load P1	#REF!	KVA
--	-------	-----

B Transient Voltage dip during Soft starter starting of Last motor P2

Total momentary load in KVA (Starting KVA of the last motor+Base load of DG set in KVA)	#REF!	KVA
Subtransient Reactance of Generator (Xd'')	14.91%	(Assumed)
Transient Reactance of Generator (Xd')	21.065%	(Assumed)
$X_d''' = (X_d'' + X_d') / 2$	0.179875	
Transient Voltage Dip (Ref: Job specification (Electrical) PC00167-GL-8001, 1.10.07,V)	15%	(Max)
Transient Voltage dip during Soft starter starting of Last motor $P2 = \text{Total momentary load in KVA} \times X_d''' \times \frac{1 - \text{Transient Voltage Dip}}{1}$ (Transient Voltage Dip)	#REF!	KVA

C Overload capacity P3

Capacity of DG set required considering overload capacity		
Total momentary load in KVA	#REF!	KVA
overcurrent capacity of DG (K) (Ref: IS/IEC 60034-1, Clause 9.3.2)	150%	
Capacity of DG set required considering overload capacity (P3) = $\frac{\text{Total momentary load in KVA}}{\text{overcurrent capacity of DG (K)}}$	#REF!	KVA

Considering the last value amongst P1, P2 and P3

Continous operation under load -P1	#REF!	KVA
Transient Voltage dip during Soft starter starting of Last motor P2	#REF!	KVA
Overload capacity P3	#REF!	KVA
Considering the last value amongst P1, P2 and P3	#REF!	KVA
Selected Generator Size	3750	KVA

ASSIGNMENT-3 Calculation for Transformer Capacity

1.0 Example of calculation for Transformer Capacity

1.1 Calculation for consumed load

Consumed loads used for this example are as follows :

	kW	kVar	kVA	
a. Continuous load	144.56	122.5	189.48	--- (i)
b. Intermittent load / Diversity Factor	4.78	4.5	6.54	--- (ii)
c. Stand-by load required as consumed load	43.22	36.1	56.34	--- (iii)

Max. Consumed load = ((i) + 30% (ii) + 10% (iii)) =	150.3	127.4	197.07
Future expansion load (20% capacity)	30.1	25.5	39.41
Total Load =	180.4	152.9	236.49

1.2 Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load	=	197.1	kVA
Spare capacity	=	39.4	kVA
Required capacity	=	236.5	kVA
Transformer rated capacity	=	300	kVA

1.3 Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW) , while all the other loads running , the voltage regulation is as follows :

$$P_T = 300 \text{ KVA} \quad (\%Z) = 4 \quad \& \text{ Ratio } X/R = 1.5 \text{ (refer table)}$$

$$\text{Hence , } \%R = 2.219 \%$$

$$\%X = 3.33 \%$$

$$P_M = 30 \text{ KW having (K = 6 \& C = 1 \& Cos } \theta = 0.78 \& \text{ Eff. } \eta = 0.91 \& \text{ Cos } \theta_s = 0.25)$$

$$P_s = 253.593 \text{ KVA}$$

$$\text{Cos } \theta_s = 0.25, \text{ Corresponding to Angle } \theta_s = 75.5225 \text{ Degrees for which Sin } \theta_s = 0.97$$

$$P_B = 151 \text{ KVA} \quad \& \text{ PB in KW is } 117.78 \quad \& \quad P_B \text{ in Kvar } = 94.4 \quad \therefore \text{ Cos } \theta_B = 0.780$$

$$\text{Cos } \theta_B = 0.85, \text{ Corresponding to Angle } \theta_B = 38.7394 \text{ Degrees, for which Sin } \theta_B = 0.63$$

$$P_{CP} = 181.178 \text{ KW}$$

$$P_{CQ} = 339.94 \text{ KVAR}$$

$$P_C = 385.207 \text{ KVA}$$

$$\text{Cos } \theta_C = 0.47034, \text{ where as Sin } \theta_C = 0.882$$

$$\text{Voltage Regulation } \% = 5.1 \%$$

Selected Transformer rating is adequate.

Result: During starting of max. capacity motor, while all other loads are running , the voltage regulation at Transformer secondary terminals shall be approx. 5.1% which meets the criteria to maintain less than 15% voltage regulation.

1.4 Selection of rated capacity

Hence 300kVA Transformer rating selected.

ASSIGNMENT-4 EARTHING CACULATIONS

8

Maximum line-to-ground fault in kA for 1 sec	15
Earthing material (Earth rod & earth strip)	GI
Depth of earth flat burrial in meter	0.5
Average depth / length of Earth rod in meters	4.5
Soil resistivity Ω-meter	15
Ambient temperature in deg C	55
Plot dimensions (earth grid) L x B in meters	75
Number of earth rods in nos.	6

Earth electrode sizing:

Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c \times \sqrt{\left[\frac{TCAP \times 10^{-4}}{t_c \times \alpha_r \times \rho_r} \right] \times \ln \left[\frac{K_0 + T_m}{K_0 + T_a} \right]}$$

αr - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρr - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
Ilg - RMS fault current in kA = 50 KA	15
tc - Short circuit current duration sec	1
Thermal capacity factor, TCAP J/(cm3.oC)	3.93
Tm - Maximum allowable temperature for copper conductor, in oC	419
K0 - Factor at oC	293
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:	
15 = Ac *	0.123
Ac - Required conductor cross section in sq.mm	122
Earth rod dia in mm	12
Earth rod dia (including 25% corrosion allowance) in mm	16

ASSIGNMENT-4 EARTHING CALCULATIONS

Earth flat sizing:

Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c \times \sqrt{\left[\frac{TCAP \times 10^{-4}}{t_c \times \alpha_r \times \rho_r} \right] \times \ln \left[\frac{K_0 + T_m}{K_0 + T_a} \right]}$$

αr - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρr - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
Ilg - RMS fault current in kA = 50 KA	15
tc - Short circuit current duration sec	1
Thermal capacity factor, TCAP J/(cm3.oC)	3.93
Tm - Maximum allowable temperature for copper conductor, in oC	419
K0 - Factor at oC	293
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:	

	15 = Ac *	0.123
Ac - Required conductor cross section in sq.mm		122
Earth flat area in mm		12
Earth flat area (including 25% corrosion allowance) in mm		16
Selected flat size W * Thk in sq mm		20

R_g - Grid resistance

Grid resistance can be calculated using Eq. 52 of IEEE 80

ρ - Soil resistivity in Ω -meter=	15
L - Total buried length of ground conductor in meter	420
h - Depth of burial in meter	0.5
A - Grid area in sq. meter	10125

R_g - Grid resistance 0.102

R_r - Earth Electrode resistance

Grid resistance can be calculated using Eq. 55 of IEEE 80

$$R_r = \frac{\rho}{2 \times \pi \times n_r \times L_r} \left\{ \left[\frac{4 \times L}{b} \right] - 1 + \frac{2 \times k_1 \times L_r}{\sqrt{A}} \left(\sqrt{n} - 1 \right) \right\}$$

ρ - Soil resistivity in Ω -meter, 16.96	15
n - No of earth electrodes	6
L_r - Length of earth electrode in meter	4.5
b - Diameter of earth electrode in meter	0.020
k_1 - co-efficient	1
A - Area of grid in square metre	10125

R_r - Earth Electrode resistance 5.50927

Grounding system resistance

Grounding system resistance can be calculated using equation 53 of IEEE 80 as follows:

$$R_s = \frac{R_g \times R_2 - R_m^2}{R_g + R_2 - 2R_m}$$

R_m - Mutual ground resistance between the group of ground conductors, R_g and group of electrodes, R_r in Ω . Neglected R_m , since this is for homogenous soil

R_s - Total earthing system resistance 0.100

ASSIGNMENT-5 LIGHTING CALCULATIONS

8

Location	Rajkot
Building	Concrete, School
Type of Building	Triangle Roofs (c)
Building Length (L)	15
Building breadth (W)	6
Building Height (H)	7

Risk Factor Calculation

1 Collection Area (A_c)

$$A_c = (2 * L * W) + (3.14 * 537.86)$$

2 Probability of Being Struck (P)

$$P = A_c * N_g * 10^{-6} = 0.00026893$$

3 Overall weighing factor

a) Use of structure (A)	=	1.7
b) Type of construction (B)	=	1.7
c) Contents or consequential effects (C)	=	1.7
d) Degree of isolation (D)	=	1.0
e) Type of country (E)	=	0.3
Wo - Overall weighing factor	=	$A * B * C * D * E$
	=	1.474

4 Overall Risk Factor

Po	=	$P * W_o$
Po	=	0.000396376
Pa	=	10^{-5}

As per clause no. 9.7 of BS- 6651, suggested acceptable risk factor (Po) has been taken as 10^{-5}
 Since $P_o > P_a$ lightning protection required.

5 Air Terminations

Perimeter of the building	=	$2(L+W)$
	=	42

6 Down Conductors

Perimeter of building	=	42
No. of down conductors based on perimeter	=	2

Hence 2 nos. of Down conductors have been selected.

Size of Down conductor	=	20 X 2.5 mm Ga
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(As per BS6651, lightning currents have very short duration, therefore thermal factors are of little consequence in deciding the cross-section of the conductor. The minimum size

ASSIGNMENT-6 CABLE SIZING																																		
S.NO.	Description	Equipment No.	Description	Consumed Load KW	Load Rating	Voltage (V)	No. of	Full Load	Motor Starting	Load P.F. Running	SIN Φ Running	Motor P.F. Starting	SIN Φ Starting	Type	No. of Runs	No. of Cores	Size, mm2	Current Rating	Derating factor	Derating factor	Derating factor	Derating factor	Overall Derating	Derated Current	Cable Length	Cable Resistance	Cable Reactance	Voltage drop	Voltage drop	Voltage drop	Voltage drop	Cable size	OD of Cable	Gland size
3	LV MCC	PU2315	Silica filter feed pump	28.83	30.00	415	3	50.1	300.82	0.8	0.6	0.8	0.5	2	1	4.0	16	85	0.98	0.9	1	1	0.882	75.0	95	1.4700	0.0815	10.10	2.43	60.23	14.51	OK	18	20
4	LV MCC	PU2322A	Soft water pump	8.37	9.20	415	3	14.6	87.34	0.8	0.6	0.8	0.5	2	1	4.0	10	66	0.98	0.9	1	1	0.882	58.2	95	2.3400	0.0852	4.61	1.11	27.51	6.63	OK	18	20s
5	LV MCC	PU 2314A	Absorbesnt/Neutral oil pump	7.21	7.50	415	3	12.5	75.23	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	60	9.4800	0.1007	9.96	2.40	59.69	14.38	OK	16	20s
6	LV MCC	PU2324	Citric Acid Tank pump	29.11	30.00	415	3	50.6	303.74	0.8	0.6	0.8	0.5	2	1	4.0	16	85	0.98	0.9	1	1	0.882	75.0	85	1.4700	0.0815	9.13	2.20	54.41	13.11	OK	21	20s
7	LV MCC	PU2333	Slop Oil pump	29.34	30.00	415	3	51.0	306.14	0.8	0.6	0.8	0.5	2	1	4.0	16	85	0.98	0.9	1	1	0.882	75.0	75	1.4700	0.0815	8.12	1.96	48.39	11.66	OK	21	20s
8	LV MCC	PU 2322B	Soft water pump-Stand by	29.34	30.00	415	3	51.0	306.14	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	105	0.9300	0.0816	7.36	1.77	43.69	10.53	OK	22	20s
9	LV MCC	PU2321A	Lye/Simplex Metering Pump	12.60	15.00	415	3	21.9	131.47	0.8	0.6	0.8	0.5	2	1	4.0	10	66	0.98	0.9	1	1	0.882	58.2	100	2.3400	0.0852	7.30	1.76	43.60	10.51	OK	18	20s
10	LV MCC	PU2321B	Lye storage tank pump	1.23	1.50	415	3	2.1	12.83	0.8	0.6	0.8	0.5	2	1	4.0	10	66	0.98	0.9	1	1	0.882	58.2	100	2.3400	0.0852	0.71	0.17	4.26	1.03	OK	18	20s
11	LV MCC	PU2305	Feed Pump(Separator)	2.83	3.00	415	3	4.9	29.53	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	2.05	0.49	12.26	2.96	OK	18	20
12	LV MCC	PU2332	Soap Stock Pump	2.12	2.20	415	3	3.7	22.12	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	110	9.4800	0.1007	5.37	1.29	32.17	7.75	OK	16	20s
13	LV MCC	MX2305	Mixer	2.12	2.20	415	3	3.7	22.12	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0		3.9400	0.0902	1.54	0.37	9.19	2.21	OK	18	20
14	LV MCC	MX2308	Mixer	7.72	9.20	415	3	13.4	80.66	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	105	3.9400	0.0902	7.84	1.89	46.90	11.30	OK	18	20
15	LV MCC	CF2312	Separator	2.81	3.00	415	3	4.9	29.32	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	85	0.9300	0.0816	0.57	0.14	3.39	0.82	OK	22	32
16	LV MCC	BW2313	Blower	2.81	3.00	415	3	4.9	29.32	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	95	9.4800	0.1007	6.15	1.48	36.83	8.87	OK	16	20s
17	LV MCC	RV 2314	Rotary valve	4.91	5.50	415	3	8.5	51.23	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	65	9.4800	0.1007	7.35	1.77	44.03	10.61	OK	16	20s
18	LV MCC	SC2314	Screw conveyor			415	3	0.0	0.00	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	65	9.4800	0.1007	0.00	0.00	0.00	0.00	OK	16	20s
19	LV MCC	AG2324A	citric acid tan agitator			415	3	0.0	0.00	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	85	9.4800	0.1007	0.00	0.00	0.00	0.00	OK	16	20s
20	LV MCC	AG2305	citric oil rection vessel agitator			415	3	0.0	0.00	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	75	0.9300	0.0816	75	#REF!	0.00	0.00	#REF!	22	20s
21	LV MCC	AG2309	lye oil reaction vessel agitator			415	3	0.0	0.00	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	65	9.4800	0.1007	0.00	0.00	0.00	0.00	OK	16	20s
22	LV MCC	AG2310	lye oil reaction vessel agitator			415	3	0.0	0.00	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	65	9.4800	0.1007	0.00	0.00	0.00	0.00	OK	16	20s
23	LV MCC	AG2321A	lye tank agitator			415	3	0.0	0.00	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	115	9.4800	0.1007	0.00	0.00	0.00	0.00	OK	16	20s
24	LV MCC	AG2321B	lye tank agitator			415	3	0.0	0.00	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	115	9.4800	0.1007	0.00	0.00	0.00	0.00	OK	16	20s
25	LV MCC	AG2314	Soap adsorbant tank agitator			415	3	0.0	0.00	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	65	9.4800	0.1007	0.00	0.00	0.00	0.00	OK	16	20s
26	LV MCC	AG2300	Crude oil tank agitator			415	3	0.0	0.00	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	115	9.4800	0.1007	0.00	0.00	0.00	0.00	OK	16	20s
27	LV MCC	APFC	APFC PANEL			415	3	0.0		0.8	0.6			2	1	3.0	25	122	0.98	0.9	1	1	0.882	107.6	30	0.9300	0.0816	0.00	0.00	0.00	0.00	OK	22	25

Basis:

1. Overall derating factor k = k1 x k2 x k3 x k4
- K1=Rating factor for variation in air/ground temperature
- K2=Rating factor for depth of laying
- K3=Rating factor for spacing between two circuits
- K4=Rating factor for variation in thermal resistivity of the soil
2. LT Motors : Running Voltage Drop = 3%, Starting Voltage Drop = 15%
3. Cable type:
- TYPE 1: Al Conductor, XLPE Insulated, Armoured, PVC outer sheathed
- TYPE 2: Cu Conductor, XLPE Insulated, Armoured, PVC outer sheathed
4. Effect of Frequency Variation ± 5%
5. Combined Effect of Voltage & Frequency Variation ±10%

ASSIGNMENT-7

LT CABLES									
CABLE TRAY: FROM		LT-4		TO	LT-5				
Sr. No.	Cable Route (From-To)	Type & Cable Size	Size of Cable (mm2)	No. of Cable	Overall Diameter of each Cable (mm)	Sum of Cable OD (mm)	Self Weight of Cable (Kg/Mt)	Total Weight of Cable (Kg/Mt)	Remarks
1	PU2315	4	16	1	21	21	1	1	
2	PU2322A	4	10	1	18	18	0.9	0.9	
3	PU 2314A	4	2.5	1	16	16	0.5	0.5	
4	PU2316	4	16	1	21	21	1	1	
5	PU2322A	4	16	1	21	21	1	1	
6	PU 2314A	4	25	1	22	22	1.4	1.4	
7	PU2317	4	10	1	18	18	0.9	0.9	
8	PU2322A	4	10	1	18	18	0.9	0.9	
9	PU 2314A	4	6	1	18	18	0.7	0.7	
10	PU2318	4	2.5	1	16	16	0.5	0.5	
11	PU2322A	4	6	1	18	18	0.7	0.7	
12	PU 2314A	4	6	1	18	18	0.7	0.7	
13	PU2319	4	25	1	22	22	1.4	1.4	
14	PMCC-2 TO AUXILIARY PANEL-2(A/C)	4	2.5	1	16	16	0.5	0.5	
15	PMCC-2 TO COOLING TOWER DOSING SYSTEM PACKAGE	4	2.5	1	16	16	0.5	0.5	