

**SRI VENKATESWARA COLLEGE OF ENGINEERING AND  
TECHNOLOGY  
(AUTONOMOUS)**

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**DEPARTMENT OF MECHANICAL ENGINEERING**

# **HEAT TRANSFER LAB OBSERVATON**

**Name of the student:** \_\_\_\_\_

**Roll Number:** \_\_\_\_\_ **Branch:** \_\_\_\_\_

**Name of the Laboratory:** \_\_\_\_\_

**Year & Sem:** \_\_\_\_\_ **Academic Year:** \_\_\_\_\_

**HEAT TRANSFER LAB MANUAL**

**LIST OF EXPERIMENTS**

1. Composite wall apparatus
2. Critical heat flux apparatus
3. Heat transfer in drop and film wise condensation apparatus
4. Emissivity measurement of radiating surfaces apparatus
5. Heat transfer by forced convection apparatus
6. Heat pipe demonstration apparatus
7. Thermal conductivity of insulating powder apparatus
8. Lagged pipe apparatus
9. Heat transfer by natural convection apparatus
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11. Heat transfer from pin-fin apparatus
12. Stefan Boltzmann apparatus
13. Thermal conductivity of metal rod apparatus
14. Study of two phase flow apparatus
15. Experiment on Transient heat conduction apparatus

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## **COMPOSITE WALL APPARATUS**

### **AIM:**

To find out total thermal resistance and total thermal conductivity of composite wall.

### **DESCRIPTION:**

The apparatus consists of central heater sandwiched between the slabs of MS, Asbestos and Wood, which forms composite structure. The whole structure is well tightened make perfect contact between the slabs. A dimmer stat is provided to vary heat input of heaters and it is measured by a digital volt meter and ammeter. Thermocouples are embedded between interfaces of slabs. A digital temperature indicator is provided to measure temperature at various points.

### **SPECIFICATION:**

1. Slab assembly arranged symmetrically on both sides of the Heater.
2. Heater coil type of 250-Watt capacity.
3. Dimmer stat open type, 230V, 0-5 amp, single phase.
4. Volt meter range 0-270V
5. Ammeter range 0-20A
6. Digital temperature indicator range 0-800<sup>0</sup> c
7. Thermocouple used: Teflon coated, Chromal - Alumal
8. Slab diameter of each =150 mm.
9. Thickness of mild steel = 10 mm.
10. Thickness of Asbestos = 6 mm.
11. Thickness of wood= 10 mm.

### **PROCEDURE:**

1. Start the main switch.

2. By adjusting the dimmer knob give heat input to heater. (Say 60V).
3. Wait for about 20 -30 min. approximately to reach steady state.
4. Take the readings of all (8) thermocouples.
5. Tabulate the readings in observation table.
6. Make dimmer knob to “zero” position and then put main switch off.
7. Repeat the procedure for different heat input.

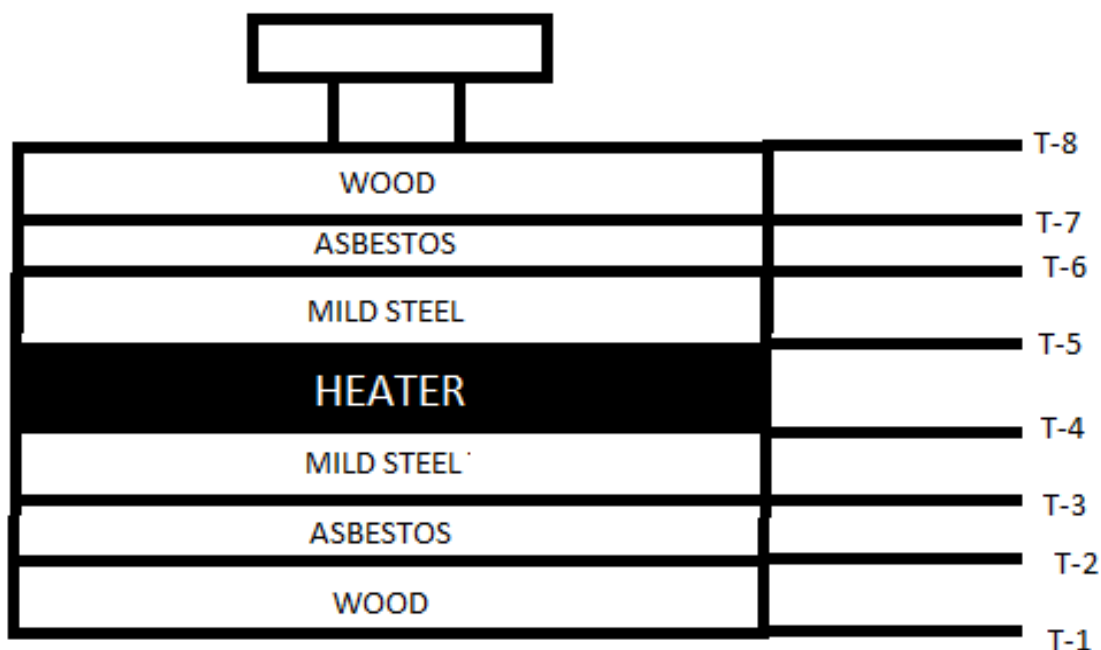


Fig :- COMPOSITE WALL

### OBSERVATION TABLE:

Sl. No	V Volts	I amps	T <sub>1</sub> °C	T <sub>2</sub> °C	T <sub>3</sub> °C	T <sub>4</sub> °C	T <sub>5</sub> °C	T <sub>6</sub> °C	T <sub>7</sub> °C	T <sub>8</sub> °C
1.										
2.										
3.										

### FORMULAE:

1. Heat input  $Q = \frac{V \times I}{2} \text{ Watts} \dots\dots\dots$

$$T_{Wood} = \frac{T_1 + T_8}{2} \text{ } ^\circ\text{C} \dots\dots\dots$$

$$T_{Asbestos} = \frac{T_2 + T_7}{2} \text{ } ^\circ\text{C} \dots\dots\dots$$

$$T_{Mildsteel} = \frac{T_3 + T_6}{2} \text{ } ^\circ\text{C} \dots\dots\dots$$

$$T_{Heater} = \frac{T_4 + T_5}{2} \text{ } ^\circ\text{C} \dots\dots\dots$$

2. Area of Slab

$$A = \frac{\pi d^2}{4} m^2 \text{ (Where “d” is diameter of slab= 300 mm)}$$

3. Thermal Resistance of Slab ( R )

$$R = \frac{T_{heater} - T_{wood}}{Q} \text{ } ^\circ\text{C/W}$$

4. Thermal Conductivity ( K )

$$K = \frac{Q \times t}{A(T_{heater} - T_{wood}) m - k} \text{ (Where “t” is total thickness of slab=26mm)}$$

**PRECAUTIONS:**

1. Keep the dimmer stat to zero before starting the experiment.
2. While removing plates do not disturb thermocouples.
3. Use the selector switch knob and dimmer knob gently.

**RESULT:**

1. Total thermal resistance of composite wall =.....
2. Total thermal conductivity of composite wall=.....

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## **CRITICAL HEAT FLUX APPARATUS**

### **AIM:**

To study the phenomenon of the boiling heat transfer and to plot the graph of heat flux versus temperature difference.

### **APPARATUS:**

It consists of a cylindrical glass container, the test heater and a heater coil for initial heating of water in the container. This heater coil is directly connected to the mains and the test heater is also connected to the mains via a Dimmer stat and an ammeter is connected in series to the current while a voltmeter across it to read the voltage.

The glass container is kept on the table. The test heater wire can be viewed through a magnifying lens. Figure enclosed shows the set up.

### **SPECIFICATIONS:**

- |   |                                  |
|---|----------------------------------|
| 1. Length of Nichrome wire                    | $L = 52 \text{ mm}$              |
| 2. Diameter of Nichrome wire                  | $D = 0.25 \text{ mm (33 gauge)}$ |
| 3. Distilled water quantity                   | $= 4 \text{ liters}$             |
| 4. Thermometer range                          | $: 0 - 100 ^\circ\text{C}$       |
| 5. Heating coil capacity (bulk water heater ) | $: 2 \text{ kW}$                 |
| 6. Dimmer stat                                |                                  |
| 7. Ammeter                                    |                                  |
| 8. Voltmeter                                  |                                  |

## THEORY:

When heat is added to a liquid surface from a submerged solid surface which is at a temperature higher than the saturation temperature of the liquid, it is usual that a part of the liquid to change phase. This change of phase is called 'boiling'. If the liquid is not flowing and present in container, the type of boiling is called as 'pool boiling'. Pool boiling is also being of various types depending upon the temperature difference between the surfaces of liquid. The different types of zones are as shown in the figure A. The heat flux supplied to the surface is plotted against  $(T_w - T_s)$  where  $T_s$  is the temperature of the submerged solid and ' $T_w$ ' is the saturation temperature of the liquid at exposed pressure. The boiling curve can be divided into three regions:

- I. Natural convection region
- II. Nucleate boiling region
- III. Film boiling region

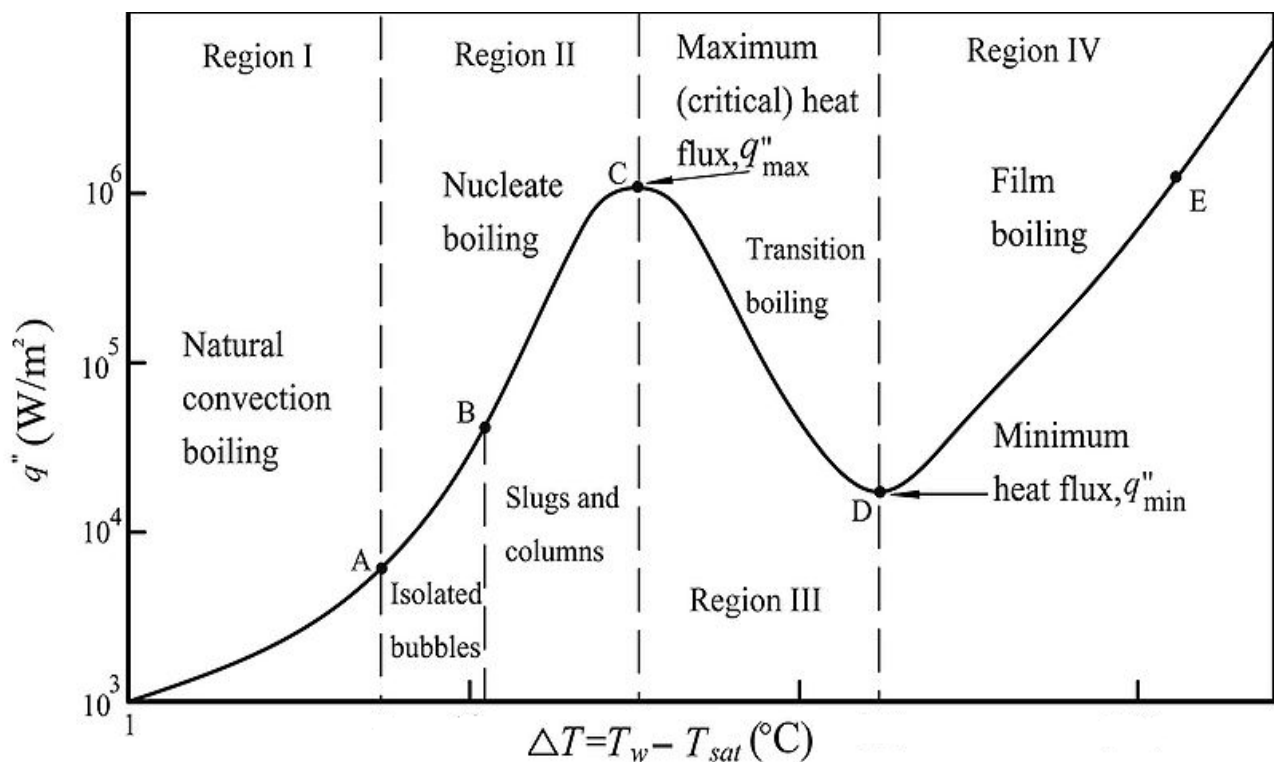


Figure A TYPICAL POOL BOILING CURVE

As temperature difference  $(T_w - T_s)$  is very small ( $1^{\circ}\text{C}$  or so), the liquid near to the surface gets slightly superheated and rises up to the surface. The heat



transfer from the heating surface to the liquid is similar to that by natural convection and hence this region is called 'natural convection region'.

When  $(T_w - T_s)$  becomes a few degrees, vapor bubble start forming at some discrete locations of the heating surface and we enter into 'Nucleate boiling region'. Region II consists of two parts. In the first part, the bubbles formed are very few in number and before reaching the top liquid surface, they get condensed. In second part, the rate of bubble formation as well as the locations where they are formed increases with increase in temperature difference. A stage is finally reached when the rate of formation of bubbles is so high that they start coalesce and blanket the surface with a vapor film. This is the beginning of region III since the vapor has got very low thermal conductivity, the formation of vapor film on the heating surface suddenly increases the temperature beyond the melting point of the submerged surface and as such the end of 'Nucleate boiling' is important and its limiting condition is known as critical heat flux point or burn out point.

The pool boiling phenomenon up to critical heat flux point can be visualized and studied with the help of apparatus described above.

### **PROCEDURE:**

1. Distilled water of about 5 liters is taken into the glass container.
2. The test heater (Nichrome wire) is connected across the studs and electrical connections are made.
3. The heaters are kept in submerged position.
4. The bulk water is switched on and kept on, until the required bulk temperature of water is obtained. (Say  $40^{\circ}\text{C}$  )
5. The bulk water heater coil is switched off and test heater coil is switched on.
6. The boiling phenomenon on wire is observed as power input to the test heater coil is varied gradually.
7. The voltage is increased further and a point is reached when wire breaks (melts) and at this point voltage and current are noted.
8. The experiment is repeated for different values of bulk temperature of water. (Say  $60^{\circ}\text{C}$ , and  $80^{\circ}\text{C}$ ).

**OBSERVATION TABLE:**

Sl. No	Bulk water Temperature in $^{\circ}\text{C}$ 'T <sub>w</sub> '	Specimen temperature in $^{\circ}\text{C}$ 'T <sub>s</sub> '	Voltage 'V' in Volt	Current 'I' in Amps	Heat Input 'Q' in watt	Critical heat Flux $q = Q/A$ In $\text{W/m}^2$
1						
2						
3						
4						
5						
6						
7						
8						
9						
10						
11						
12						
13						
14						
15						
16						
17						
18						
19						
20						
21						
22						
23						
24						
25						
26						

**MODEL CALCULATIONS:**

- a. Area of Nichrome wire  $A = \pi \times D \times L =$  \_\_\_\_\_
- b. Heater input  $Q = V \times I =$  \_\_\_\_\_
- c. Critical heat flux  $q = Q/A =$  \_\_\_\_\_

**PRECAUTIONS:**

1. All the switches and Dimmer stat knob should be operated gently.
2. When the experiment is over, bring the Dimmer stat to zero position.
3. Run the equipment once in a week for better performance.
4. Do not switch on heaters unless distilled water is present in the container.

**RESULT:**

The phenomenon of the boiling heat transfer is studied and plotted the graph of the heat flux versus temperature difference and critical heat flux is calculated.

Critical heat flux  $q =$ -----

**Date:**

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## **HEAT TRANSFER IN DROP AND FILM WISE CONDENSATION**

### **AIM:**

To determine the experimental and theoretical heat transfer coefficient for drop wise and film wise condensation.

### **INTRODUCTION:**

Condensation of vapor is needed in many of the processes, like steam condensers, refrigeration etc. When vapor comes in contact with surface having temperature lower than saturation temperature, condensation occurs. When the condensate formed wets the surface, a film is formed over surface and the condensation is film wise condensation. When condensate does not wet the surface, drops are formed over the surface and condensation is drop wise condensation

### **APPARATUS:**

The apparatus consists of two condensers, which are fitted inside a glass cylinder, which is clamped between two flanges. Steam from steam generator enters the cylinder through a separator. Water is circulated through the condensers. One of the condensers is with natural surface finish to promote film wise condensation and the other is chrome plated to create drop wise condensation. Water flow is measured by a Rota meter. A digital temperature indicator measures various temperatures. Steam pressure is measured by a pressure gauge. Thus heat transfer coefficients in drop wise and film wise condensation can be calculated.

### **SPECIFICATIONS:**

Heater	: Immersion type, capacity 2kW
Voltmeter	: Digital type, Range 0-300v
Ammeter	: Digital type, Range 0-20 amps
Dimmer stat	: 0-240 V, 2 amps
Temperature Indicator	: Digital type, 0-800°C

Thermocouple Used : Teflon coated, Chromal - Alupal (Ch-Al)  
Diameter of copper tube d=16 mm  
Length of copper tube L= 300 mm  
Maximum Capacity of boiler : 2kg/cm<sup>2</sup>

### **EXPERIMENTAL PROCEDURE:**

1. Fill up the water in the steam generator and close the water-filling valve.
2. Start water supply through the condensers.
3. Close the steam control valve, switch on the supply and start the heater.
4. After some time, steam will be generated. Close water flow through one of the condensers.
5. Open steam control valve and allow steam to enter the cylinder and pressure gauge will show some reading.
6. Open drain valve and ensure that air in the cylinder is expelled out.
7. Close the drain valve and observe the condensers.
8. Depending upon the condenser in operation, drop wise or film wise condensation will be observed.
9. Wait for some time for steady state, and note down all the readings.
10. Repeat the procedure for the other condenser.

### **OBSERVATIONS:**

‘V’ Volt	‘I’ Amp	Thermocouple readings (0C)								Volume flow rate of water, V cc/min
		T <sub>1</sub>	T <sub>2</sub>	T <sub>3</sub>	T <sub>4</sub>	T <sub>5</sub>	T <sub>6</sub>	T <sub>7</sub>	T <sub>8</sub>	

Water inlet temperature -T<sub>1</sub>

Copper tube surface temperature (Film wise condensation) -T<sub>2</sub>

Copper specimen chamber steam temperature - T<sub>3</sub>

Gold tube surface temperature (Drop wise condensation) -T<sub>4</sub>

Gold specimen chamber steam temperature - T<sub>5</sub>

Steam Inlet temperature - T<sub>6</sub>

Copper tube Water outlet temperature - T<sub>7</sub>

Gold tube Water outlet temperature - T<sub>8</sub>

## CALCULATIONS:

(FILM WISE & DROP WISE CONDENSATION)

Water flow  $m_w =$  kg/sec

Water inlet temperature  $=$  °C

Water outlet temperature  $=$  °C

( $T_8$  for drop-wise condensation and  $T_7$  for film-wise condensation)

Heat carried away by the water,

$Q = m_w \cdot c_p \cdot (T_{7 \text{ or } 8} - T_1)$  Watts

$Q = \dots\dots\dots$  Watts

Where  $c_p =$  Specific heat of water  $= 4.2 \times 10^3$  J / Kg-K

Surface area of the condenser,  $A = \pi dL$  m<sup>2</sup>

Experimental heat transfer coefficient,  $h = \frac{Q}{A(T_s - T_w)}$  W / m<sup>2</sup> °C

(for both film wise and drop wise condensation)

Where  $T_s =$  Temperature of steam ( $T_3$  or  $T_5$ )

$T_w =$  Condenser wall temperature ( $T_2$  or  $T_4$ )

Theoretically, for film wise condensation

$$h = 0.943 \left[ \frac{h_{fg} \cdot \rho^2 \cdot g \cdot k^3}{(T_s - T_w) \cdot \mu \cdot L} \right]^{0.25}$$

Where

$h_{fg} =$  Latent heat of steam at  $T_s$  J/kg

(Take from temperature tables in steam tables)

$\rho =$  Density of water, Kg / m<sup>3</sup>

$g =$  Gravitational acceleration, m / sec<sup>2</sup>

$k =$  Thermal conductivity of water W / m° C

$\mu =$  Viscosity of water, N.s/m<sup>2</sup>

$L =$  Length of condenser = 0.15 m

Above values at mean temperature,  $T_m = \frac{(T_s + T_w)}{2}$  °C (from data book)

(For drop wise condensation, determine experimental heat transfer coefficient only) In film wise condensation, film of water acts as barrier to heat transfer whereas, in case of drop formation, there is no barrier to heat transfer, Hence heat transfer coefficient in drop wise condensation is much greater than film wise condensation, and is preferred for condensation. But practically, it is difficult to prolong the drop wise condensation and after a period of condensation the surface becomes wetted by the liquid. Hence slowly film wise condensation starts.

### **PRECAUTIONS:**

1. Operate all the switches and controls gently
2. Never allow steam to enter the cylinder unless the water is flowing through condenser.
3. Always ensure that the equipment is earthed properly before switching on the supply.

### **RESULTS:**

Thus we studied and compared the drop wise and film wise condensation.

#### **1. Film wise condensation:**

Experimental average heat transfer coefficient =

Theoretical average heat transfer coefficient =

#### **2. Drop wise condensation:**

Experimental average heat transfer coefficient =

Theoretical average heat transfer coefficient =

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## **EMISSIVITY MEASUREMENT OF RADIATING SURFACES**

### **AIM:**

To determine the emissivity of given test plate surface.

### **THEORY:**

Any hot body maintained by a constant heat source, loses heat to surroundings by conduction, convection and radiation. If two bodies made of same geometry are heated under identical conditions, the heat loss by conduction and convection can be assumed same for both the bodies, when the difference in temperatures between these two bodies is not high. In such a case, when one body is black & the other body is gray from the values of different surface temperatures of the two bodies maintained by a constant power source emissivity can be calculated. The heat loss by radiation depends on

- a) Characteristic of the material
- b) Geometry of the surface and
- c) Temperature of the surface

The heat loss by radiation when one body is completely enclosed by the other body is given by

$$Q = \frac{\sigma A_1 (T_1^4 - T_2^4)}{\frac{1}{\varepsilon} + \frac{A_1}{A_2} \left[ \frac{1}{\varepsilon_2} - 1 \right]}$$

If a body is losing heat to the surrounding atmosphere, then the area of atmosphere  $A_2 \gg$  area of body  $A_1$ . Thus if anybody is losing heat by radiation to the surrounding atmosphere equation (1) takes the form.

$$Q = \sigma A_1 (T_1^4 - T_2^4)$$

Where

$\sigma$  = Stefan Boltzmann constant =  $5.6697 \times 10^{-8}$  W/m<sup>2</sup> K<sup>4</sup>

$A_1$  = Surface area in m<sup>2</sup>

$\varepsilon$  = Emissivity



$T_1$  = surface temperature of the body in K and

$T_2$  = surrounding atmospheric temperature in K

Let us consider a black body & a gray body with identical geometry being heated under identical conditions, assuming conduction & convection heat loss to remain the same.

Let  $Q_b$  and  $Q_g$  be the heat supplied to black & gray bodies respectively. If heat input to both the bodies are same,

$$Q_b = Q_g$$

Assuming, heat loss by conduction and convection from both bodies to remain same.

Heat loss by radiation by the black body = Heat loss by radiation by the gray body

$$\sigma A_b \varepsilon_b (T_b^4 - T_a^4) = \sigma A_g \varepsilon_g (T_g^4 - T_a^4)$$

As geometry of two bodies are identical  $A = A_g = A_b$  and  $\varepsilon_b = 1$  for black body.

Therefore,  $\varepsilon_g = \frac{(T_b^4 - T_a^4)}{(T_g^4 - T_a^4)}$

Where

Suffix 'b' stands for black body,

Suffix 'g' stands for gray body,

Suffix 'c' stands for chamber.

### **DESCRIPTION:**

The experimental set up consists of two circular aluminium plates of identical dimensions. One of the plates is made black by applying a thick layer of lamp black while the other plate whose emissivity is to be measured is a gray body. Heating coils are provided at the bottom of the plates. The plates are mounted on asbestos cement sheet and kept in an enclosure to provide undisturbed natural convection condition. Three thermocouples are mounted on each plate to measure the average temperature. One thermocouple is in the chamber to measure the ambient temperature or chamber air temperature. The heat input can be varied with

the help of variac for both the plates , that can be measured using digital volt and ammeter.

### **SPECIFICATIONS:**

Specimen material	: Aluminum
Specimen Size	: $\phi$ 150 mm, 10 mm thickness (gray & black body)
Voltmeter	: Digital type, 0-300v
Ammeter	: Digital type, 0-3 amps
Dimmer stat	: 0-240 V, 2 amps
Temperature Indicator	: Digital type, 0-300°C, K type
Thermocouple Used	: 7 nos.
Heater	: Sand witched type Nichrome heater, 400 W

### **PROCEDURE:**

1. Switch on the electric mains.
2. Operate the dimmer stat very slowly and give same power input to both the heater Say 60 V by using (or) operating cam switches provided panel.
3. When steady state is reached note down the temperatures  $T_1$  to  $T_7$  by rotating the temperature selection switch gently.
4. Also note down the volt & ammeter reading
5. Repeat the experiment for different heat inputs.

### **OBSERVATION TABLE:**

Sl. No.	Heater input		Temperature of black surface °C			Temperature of gray surface °C			Chamber Temp °C
	V	I	$T_1$	$T_2$	$T_3$	$T_5$	$T_6$	$T_7$	$T_4$
1.									
2.									
3.									

### **SPECIMEN CALCULATIONS:**

1. Temperature of the black body  $T_b = \frac{(T_1 + T_2 + T_3)}{3} + 273.15 \text{ K}$

2. Temperature of the gray body  $T_g = \frac{(T_5 + T_6 + T_7)}{3} + 273.15 \text{ K}$

3. Temperature of the Chamber  $T_c = (T_7 + 273.15) \text{ K}$

4. Heat input to the coils  $Q = V \times I \text{ watt}$

5. Emissivity of gray body  $\epsilon_g = \epsilon_b \left[ \frac{(T_b^4 - T_c^4)}{(T_g^4 - T_c^4)} \right]$

### **Result:**

Emissivity of the black body is greater than gray body.

The emissivity of the test plate (gray body) surface is determined =.....

**Date:**  
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## **HEAT TRANSFER BY FORCED CONVECTION**

### **AIM:**

To determine the convective heat transfer coefficient and the rate of heat transfer by forced convection for flow of air inside a horizontal pipe.

### **THEORY:**

Convective heat transfer between a fluid and a solid surface takes place by the movement of fluid particles relative to the surface. If the movement of fluid particles is caused by means of external agency such as pump or blower that forces fluid over the surface, then the process of heat transfer is called forced convection.

In convectional heat transfer, there are two flow regions namely laminar & turbulent. The non-dimensional number called Reynolds number is used as the criterion to determine change from laminar to turbulent flow. For smaller value of Reynolds number viscous forces are dominant and the flow is laminar and for larger value of Reynolds numbers the inertia forces become dominant and the flow is turbulent. Dittus –Boelter correlation for fully developed turbulent flow in circular pipes is,

$$N_u = 0.023 (Re)^{0.8} (Pr)^n \quad \text{(from data book)}$$

Where

$n = 0.4$  for heating of fluid

$n = 0.3$  for cooling of fluid

$$\text{Nusselt number} = N_u = \frac{hd}{k}$$

$$Re = \text{Reynolds Number} = \frac{Vd}{\nu}$$

$$Pr = \text{Prandtl Number} = \frac{\mu C_p}{k}$$

### **DESCRIPTION OF THE APPARATUS:**

The apparatus consists of a blower to supply air. The air from the blower passes through a flow passage, heater and then to the test section. Air flow is

measured by an orifice meter placed near the test section. A heater placed around the tube heats the air, heat input is controlled by a dimmer stat. Temperature of the air at inlet and at outlet are measured using thermocouples. The surface temperature of the tube wall is measured at different sections using thermocouples embedded in the walls. Test section is enclosed in a asbestos rope where the circulation of rope is avoid the heat loss to outside.

### **PROCEDURE:**

1. Start the blower after keeping the valve open, at desired rate.
2. Put on the heater and adjust the voltage to a desired value and maintain it as constant
3. Allow the system to stabilize and reach a steady state.
4. Note down all the temperatures  $T_1$  to  $T_7$ , voltmeter and ammeter readings, and manometer readings.
5. Repeat the experiment for different heat input and flow rates.

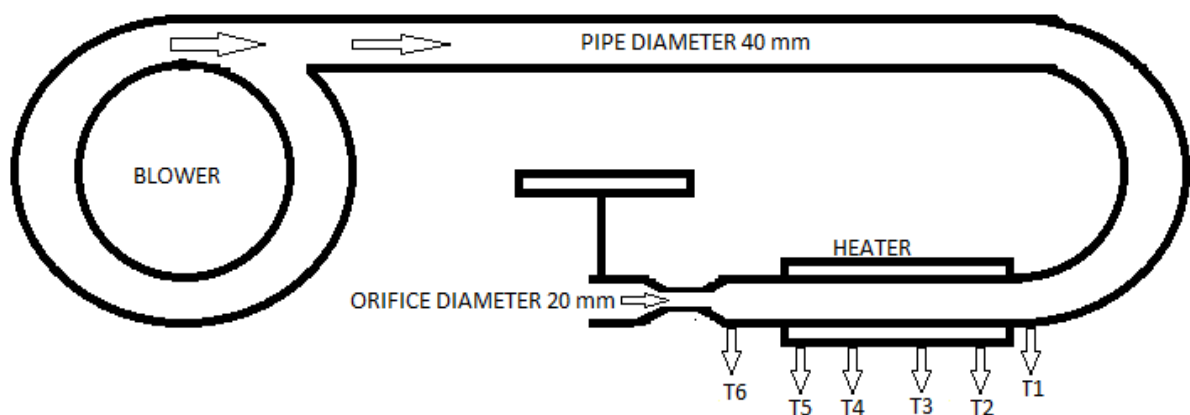


Fig:- FORCED CONVECTION APPARATUS

### **SPECIFICATIONS:**

Specimen	: Copper Tube
Size of the Specimen	: I.D. 25mm x 300mm long
Heater	: Externally heated, Nichrome wire Band Heater
Ammeter	: Digital type, 0-20amps, AC
Voltmeter	: Digital type, 0-300volts, AC

Dimmer stat for heating Coil : 0-230v, 2amps  
 Thermocouple Used : 7 nos.  
 Centrifugal Blower : Single Phase 230v, 50 hz, 3000rpm  
 Manometer : U-tube with water as working fluid  
 Orifice diameter, 'd<sub>2</sub>' : 20 mm  
 G. I pipe diameter, 'd<sub>1</sub>' : 40 mm  
 Coefficient of discharge : 0.62  
 Length of the tube : 500 mm

### **OBSERVATION TABLE:**

Sl. No	Heater input Q (Watts)			Diff. in Mano meter reading h <sub>m</sub> mm	Air temp. °C		Tube surface Temperature °C				
	V volt	I amp	V X I		Inlet T <sub>1</sub>	Outlet T <sub>7</sub>	T <sub>2</sub>	T <sub>3</sub>	T <sub>4</sub>	T <sub>5</sub>	T <sub>6</sub>
1.											
2.											
3.											

### **MODEL CALCULATIONS:**

#### **Method -I:**

1. Velocity of the air in the tube  $V_a = \frac{Q}{a_1}$

Discharge of the air in the tube  $Q = \frac{C_d a_1 a_2 \sqrt{2gh_m}}{\sqrt{a_1^2 - a_2^2}}$

Where

Coefficient of discharge C<sub>d</sub>= 0.62

Area of GI pipe  $a_1 = \frac{\pi}{4} d_1^2$  → d<sub>1</sub> is diameter of the GI pipe = 40mm.

Area of Orifice  $a_2 = \frac{\pi}{4} d_2^2$  → d<sub>2</sub> is diameter of the Orifice = 20mm.

h<sub>m</sub> Differential manometer reading .

2. Properties of air are taken at temperature  $T_f = \frac{T_h + T_s}{2}$

Average surface temperature of the tube  $T_h = \frac{T_2 + T_3 + T_4 + T_5}{4}$

Mean temperature of air  $T_s = \frac{T_1 + T_6}{2}$

3. Reynolds Number  $R_e = \frac{V_a d_1}{\nu}$   
 ( $\nu = \text{Kinematic Viscosity}$  From data book at  $T_f$ )

4. Nusselt number  $Nu = 0.023 R_e^{0.8} P_r^{0.3}$   
 ( $P_r = \text{Prandtl number}$  from data book at  $T_f$ )

5. Nusselt number  $N_u = \frac{h d_1}{k}$

6. Forced convective heat transfer co-efficient  $h = \frac{N_u k}{d_1}$  W/m<sup>2</sup> - K  
 ( $k = \text{thermal conductivity}$  from data book at  $T_f$ )

### **Method -II:**

From Newton's Law of Cooling:

1. Rate of heat transfer  $Q = hA(T_h - T_s)$

Where

Amount of heat supplied  $Q = V \times I$  Watts

Surface area of the pipe  $A = \pi d_1 L$

Forced convective heat transfer co-efficient  $h = \frac{Q}{\pi d_1 L (T_h - T_s)}$  W/m<sup>2</sup> - K

### **PRECAUTIONS:**

1. Never switch on main power supply before ensuring that all on/off switches given on the panel are at off position
2. Never run the apparatus if power supply is less than 180 or above 200 volts.

### **RESULT:**

The convective heat transfer coefficient and the rate of heat transfer by forced convection for flow of air inside a horizontal pipe has been determined.

1. The convective heat transfer coefficient by forced convection  $h = \dots\dots\dots$
2. The rate of heat transfer by forced convection  $Q = \dots\dots\dots$

**Date:**  
**Exp No:**

## **HEAT PIPE DEMONSTRATION**

### **AIM:**

To compare the performance characteristics of a heat pipe with two other geometrically similar pipes of copper and stainless steel.

### **THEORY:**

The performance of heat pipes can be studied by measuring the temperature distributed along the length of the pipe and heat transfer characteristics of each pipe under steady state for each heat pipe.

Energy input to heater in time  $\Delta t$

$$Q = V \times I \Delta t$$

Heat transferred to water

$$Q_w = M_w C_w (T_{\text{final}} - T_{\text{initial}})$$

### **PROCEDURE:**

- 1) Fill the known quantity (500ml) of water in three heat sinks and measure its initial temperatures.
- 2) Switch on the mains and supply the same power input to each heater equipped with three pipes.
- 3) Wait for steady state conditions, and note down the readings of thermocouples connected to pipes.
- 4) Measure the final temperature of water in three heat sinks.
- 5) Repeat the experiment for different heat input.

### **SPECIFICATIONS**

Standard heat pipe: A

Inside Diameter of the pipe	= 24 mm
Outside Diameter of the pipe	= 28 mm
Length of pipes	= 300 mm.



**OBSERVATION TABLES:****Quantity of the water in the out let-500ml****I. STAIN LESS STEEL PIPE**

Sl. No	Heat input		Readings of thermocouple along pipe °C				Temperature of water °C	
	V	I	T <sub>1</sub>	T <sub>2</sub>	T <sub>3</sub>	T <sub>4</sub>	inlet	outlet
1.								
2.								
3.								

**II. COPPER PIPE**

SL No	Heat input		Readings of thermocouple along pipe °C				Temperature of water °C	
	V	I	T <sub>5</sub>	T <sub>6</sub>	T <sub>7</sub>	T <sub>8</sub>	inlet	outlet
1.								
2.								
3.								

**III. HEAT PIPE**

SL No	Heat input		Readings of thermocouple along pipe °C				Temperature of water °C	
	V	I	T <sub>9</sub>	T <sub>10</sub>	T <sub>11</sub>	T <sub>12</sub>	inlet	outlet
1.								
2.								
3.								

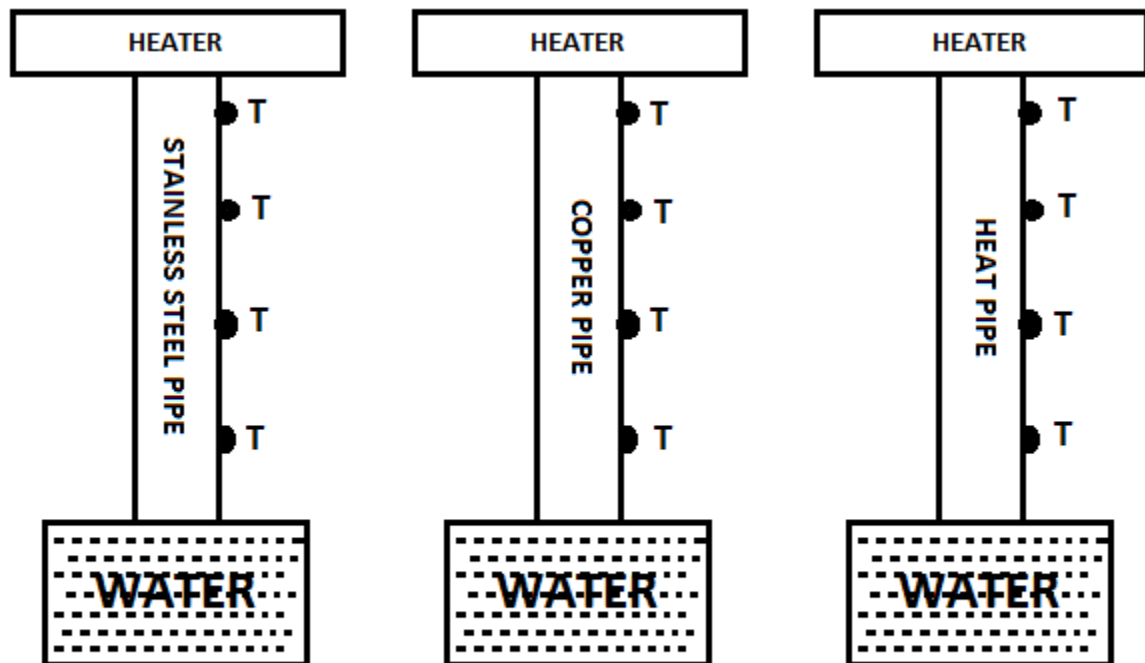


Fig:HEAT PIPE DEMONSTRATAR

### MODEL CALCULATIONS:

#### 1. Stain less steel Pipe

Energy input to heater in time  $\Delta t$

$$Q = V \times I \times \Delta t$$

Heat transferred to water,

$$Q_w = M_w C_w (T_{\text{final}} - T_{\text{initial}})$$

$$T_1 = \text{_____}^{\circ}\text{C} \quad T_2 = \text{_____}^{\circ}\text{C} \quad T_3 = \text{_____}^{\circ}\text{C} \quad T_4 = \text{_____}^{\circ}\text{C}$$

#### 2. Copper Pipe

Energy input to heater in time  $\Delta t$

$$Q = V \times I \times \Delta t$$

Heat transferred to water,

$$Q_w = M_w C_w (T_{\text{final}} - T_{\text{initial}})$$

$$T_5 = \text{_____}^{\circ}\text{C} \quad T_6 = \text{_____}^{\circ}\text{C} \quad T_7 = \text{_____}^{\circ}\text{C} \quad T_8 = \text{_____}^{\circ}\text{C}$$

#### 3. Standard heat Pipe

Energy input to heater in time  $\Delta t$

$$Q = V \times I \times \Delta t$$

Heat transferred to water,

$$Q_w = M_w C_w (T_{\text{final}} - T_{\text{initial}})$$

$T_9 = \text{_____}^{\circ}\text{C}$     $T_{10} = \text{_____}^{\circ}\text{C}$     $T_{11} = \text{_____}^{\circ}\text{C}$     $T_{12} = \text{_____}^{\circ}\text{C}$

**RESULT:**

The performance characteristics of a heat pipe with two other geometrically similar pipes of copper and stainless steel has been determined.

**Date:**  
**Exp No:**

## **THERMAL CONDUCTIVITY OF INSULATING POWDER**

### **AIM:**

To determine the thermal conductivity of insulating powder at various heat inputs.

### **THEORY:**

#### **FORIER LAW OF HEAT CONDUCTION:**

A Materials having lower thermal conductivity are called insulators. Examples for good conductors include all metals. While asbestos, magnesia, glass wool etc., are some the examples for insulators.

The radial heat conduction for single hollow sphere transferring heat from inside to outside is given by

$$Q = \frac{4k\pi \cdot r_i r_o (T_i - T_o)}{r_o - r_i}$$

This law states that rate of heat flow through a surface is directly proportional to the area normal to the surface and the temperature gradient across the surface.

$$Q \propto \frac{dT}{dX}$$

$$Q = -kA \frac{dT}{dX}$$

Negative sign indicates that the heat flows from higher temperature to the lower temperature. K is called the thermal conductivity.

#### **THERMAL CONDUCTIVITY:**

This can be defined as the amount of heat that can flow per unit time across a unit cross sectional area when the temperature gradient is unity. The units of thermal conductivity are w/m-K. Materials having higher thermal conductivity are called conductors while those

**Where:**

$Q$	= rate of heat transfer in watts	= $V \times I$
$k$	= Thermal conductivity w/m-k	
$r_i$	= radius of inner sphere in meters	
$r_o$	= radius of outer sphere in meters	
$T_i$	=Temperature of the inner sphere	
$T_o$	=Temperature of the outer sphere	

### **DESCRIPTION OF APPARATUS:**

The apparatus consists of two concentric copper spheres. Heating coils is provided in the inner sphere. The space between the inner and outer spheres are filled by the insulating powder whose thermal conductivity is to be determined. The power supply to the heating coils is adjusted by using dimmer stat. Chromel - Alumel thermocouples are used to record the temperatures. Thermocouples 1 to 6 are embedded on the surface of inner sphere and 7 to 12 are embedded on the outer shell surface.

### **SPECIFICATIONS:**

1. Radius of inner sphere = 50mm
2. Radius of outer sphere = 100 mm
3. Voltmeter 0-300V & Ammeter 0-5amps.
4. Dimmer stat – 2 amps.
5. Temperature indicator 0-300<sup>0</sup>c

### **PROCEDURE:**

1. Connect the unit to an AC source 240 V 5amps and switch on the MCB.
2. Operate the dimmer stat slowly to increase the heat input to the heater and adjust the voltage to any desired voltage (do not exceed 150V).
3. Maintain the same heat input throughout the experiment until the temperature reaches a steady state.

4. Note down the following readings provided in the Observation table.
5. Repeat the experiment for other heat inputs.

**OBSERVATION TABLE:**

Sl. No.	Heat Input		Inner Surface temp C						Outer Surface temp C					
	V	A	T <sub>1</sub>	T <sub>2</sub>	T <sub>3</sub>	T <sub>4</sub>	T <sub>5</sub>	T <sub>6</sub>	T <sub>7</sub>	T <sub>8</sub>	T <sub>9</sub>	T <sub>10</sub>	T <sub>11</sub>	T <sub>12</sub>
1.														
2.														
3.														

$$\text{Average } T_i = \frac{T_1 + T_2 + T_3 + T_4 + T_5 + T_6}{6} \text{ } ^\circ\text{C}$$

$$\text{Average } T_o = \frac{T_7 + T_8 + T_9 + T_{10} + T_{11} + T_{12}}{6} \text{ } ^\circ\text{C}$$

$$k = \frac{Q(r_o - r_i)}{4\pi r_i r_o (T_i - T_o)} \text{ w /mK}$$

**GRAPH:**

Plot the graph K vs Heat Input

**PRECAUTIONS:**

4. Keep the dimmer stat to zero before starting the experiment.
5. Take readings at study state condition only.
6. Use the selector switch knob and dimmer knob gently.

**RESULT:**

The thermal conductivity of insulating powder at various heat inputs has been determined.

**Date:**  
**Exp No:**

## **LAGGED PIPE**

### **AIM**

To determine thermal conductivity of different insulating materials, Overall heat transfer coefficient of lagged pipe and thermal resistance.

### **APPARATUS**

The apparatus consists of three concentric pipes mounted on suitable stand. The hollow space of the innermost pipe consists of the heater. Between first two cylinders the insulating material with which lagging is to be done is filled compactly. Between second and third cylinders, another material used for lagging is filled. The third cylinder is concentric to other outer cylinder. The thermocouples are attached to the surface of cylinders appropriately to measure the temperatures. The input to the heater is varied through a dimmerstat .

### **SPECIFICATIONS:**

Diameter of heater rod  $d_H = 20$  mm

Diameter of heater rod with asbestos lagging  $d_A = 40$ mm

Diameter of heater rod with asbestos and saw dust lagging  $d_S = 80$ mm

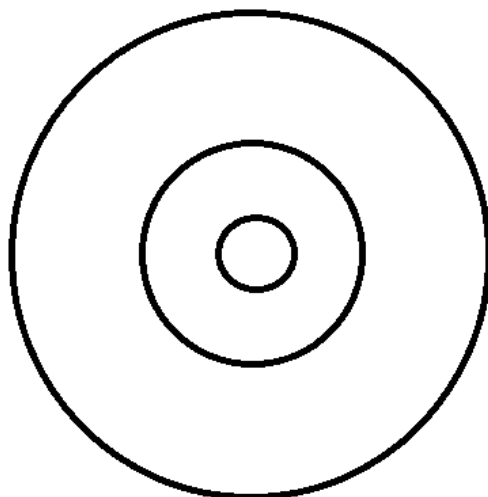
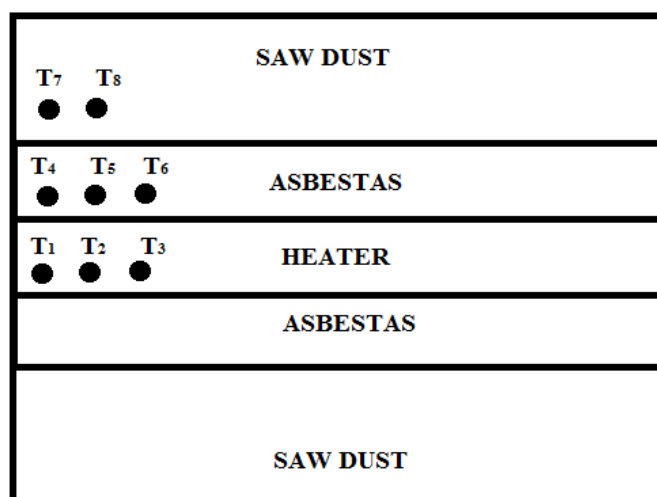
Effective length of the cylinder  $l = 500$ mm.

### **PROCEDURE:**

1. Switch on the unit and check if channels of temperature indicator showing proper change temperature.
2. Switch on the heater using the regulator and keep the power input at some particular value.
3. Allow the unit to stabilize for about 20 to 30 minutes
4. Now note down the ammeter reading, voltmeter reading, which gives the heat input, temperatures 1,2,3 are the temperature of heater rod, 4,5,6 are the

temperatures on the asbestos layer, 7 and 8 are the temperatures on the sawdust lagging.

5. The average temperature of each cylinder is taken for calculation.
6. The temperatures are measured by thermocouple with multipoint digital temperature indicator.
7. The experiment may repeat for different heat inputs.



**Fig: Lagged pipe Apparatus**

### **OBSERVATIONS:**

Sl. No	V Volt	I amps	Heater Temp( $T_H$ )				Asbestos Temp( $T_A$ )				Sawdust Temp( $T_S$ )		
			$T_1$	$T_2$	$T_3$	$(T_H)_{Avg}$	$T_4$	$T_5$	$T_6$	$(T_A)_{Avg}$	$T_7$	$T_8$	$(T_S)_{Avg}$
1													
2													
3													



## CALCULATIONS:

### 1. Mean readings

$$(T_H)_{Aveg} = \frac{T_1 + T_2 + T_3}{3} \text{ } ^\circ C$$

$$(T_A)_{Aveg} = \frac{T_4 + T_5 + T_6}{3} \text{ } ^\circ C$$

$$(T_S)_{Aveg} = \frac{T_7 + T_8}{2} \text{ } ^\circ C$$

### 2. Temperature difference

$$\nabla T_1 = (T_H)_{Aveg} - (T_A)_{Aveg}$$

$$\nabla T_2 = (T_H)_{Aveg} - (T_S)_{Aveg}$$

### 3. Heat flow $Q=VI$

### 4. Thermal conductivity of Asbestos lagging

$$k_{Asbestos} = \frac{Q \ln(r_2 / r_1)}{2\pi L \Delta T_1} \text{ W / mK}$$

### 5. Thermal conductivity of Asbestos lagging

$$k_{Sawdust} = \frac{Q \ln(r_3 / r_2)}{2\pi L \Delta T_2} \text{ W / mK}$$

### 6. Overall heat transfer coefficient

$$U = \frac{1}{r_1} \left( \frac{1}{\left[ \frac{1}{k_1} \ln \frac{r_2}{r_1} + \frac{1}{k_2} \ln \frac{r_3}{r_2} \right]} \right) \frac{W}{m^2 k}$$

### 7. Thermal resistance of Asbestos $R_{Asbestos} = \frac{\Delta T_1}{Q} \text{ k / W}$

### 8. Thermal resistance of Sawdust $R_{Sawdust} = \frac{\Delta T_2}{Q} \text{ k / W}$

### **PRECAUTIONS:**

- 1) Keep dimmer stat to ZERO position before start.
- 2) Increase voltage gradually.
- 3) Keep the assembly undisturbed while testing.
- 4) While removing or changing the lagging materials do not disturb the thermocouples.
- 5) Do not increase voltage above 150V
- 6) Operate selector switch of temperate indicator gently.

**RESULTS:** Thermal conductivity of different insulating materials, Overall heat transfer coefficient of lagged pipe and thermal resistance has been determined.

1. Thermal conductivity of asbestos powder lagging  $k_{Asbestos} = \dots\dots\dots$
2. Thermal conductivity of sawdust lagging  $k_{Sawdust} = \dots\dots\dots$
3. Overall heat transfer coefficient  $U = \dots\dots\dots$
4. Thermal resistance of Asbestos  $R_{Asbestos} = \dots\dots\dots$
5. Thermal resistance of Sawdust  $R_{Sawdust} = \dots\dots\dots$

**Date:**  
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## **HEAT TRANSFER BY NATURAL CONVECTION**

### **AIM:**

To find out heat transfer coefficient and heat transfer rate from vertical cylinder in natural convection.

### **THEORY:**

Natural convection heat transfer takes place by movement of fluid particles on solid surface caused by density difference between the fluid particles on account of difference in temperature. Hence there is no external agency forcing fluid over the surface. It has been observed that the fluid adjacent to the surface gets heated, resulting in thermal expansion of the fluid and reduction in its density. Subsequently a buoyancy force acts on the fluid causing it to flow up the surface. Here the flow velocity is developed due to difference in temperature between fluid particles.

The following empirical correlations may be used to find out the heat transfer coefficient for vertical cylinder in natural convection.

$$Nu = 0.53(Gr.Pr)^{\frac{1}{4}} \text{ for } Gr.Pr < 10^5$$

$$Nu = 0.56(Gr.Pr)^{\frac{1}{4}} \text{ for } 10^5 < Gr.Pr < 10^8$$

$$Nu = 0.13(Gr.Pr)^{\frac{1}{3}} \text{ for } 10^8 < Gr.Pr < 10^{12}$$

Where,

$$Nu = \text{Nusselt number} = \frac{hL}{k}$$

$$Gr = \text{Grashof number} = \frac{L^3 \beta g (T_s - T_a)}{\nu^2}$$

$$Pr = \text{Prandtl number} = \frac{\mu C_p}{k}$$

$\beta$  = Coefficient of Volumetric expansion (or) temperature co-efficient of thermal conductivity in  $\frac{1}{K}$

For ideal gases  $\beta = \frac{1}{T_f}$

Where 'T<sub>f</sub>' is the absolute film temperature at which the properties are taken.

### **SPECIFICATIONS:**

Specimen	: Stainless Steel tube,
Size of the Specimen	: Outer diameter 45mm, 500mm length
Heater	: Nichrome wire type heater along its length
Thermocouples used	: 6nos.
Ammeter	: Digital type, 0-2amps, AC
Voltmeter	: Digital type, 0-300volts, AC
Dimmer stat for heating coil	: 0-230 V, 2 amps, AC power
Enclosure with acrylic door	: For visual display of test section (fixed)

### **APPARATUS:**

The apparatus consists of a stainless steel tube fitted in a rectangular duct in a vertical position. The duct is open at the top and bottom and forms an enclosure and serves the purpose of undisturbed surroundings. One side of the duct is made of acrylic sheet for visualization. A heating element is kept in the vertical tube, which heats the tube surface. The heat is lost from the tube to the surrounding air by natural convection. Digital temperature indicator measures the temperature at different points with the help of seven temperature sensors, including one for measuring surrounding temperature. The heat input to the heater is measured by Digital Ammeter and Digital Voltmeter and can be varied by a dimmer stat.

### **PROCEDURE:**

1. Ensure that all ON/OFF switches given on the panel are at OFF position.
2. Ensure that variac knob is at zero position, provided on the panel.
3. Now switch on the main power supply (220 V AC, 50 Hz).

4. Switch on the panel with the help of mains ON/OFF switch given on the panel.
5. Fix the power input to the heater with the help of variac, voltmeter and ammeter provided.
6. Take thermocouple, voltmeter & ammeter readings when steady state is reached.
7. When experiment is over, switch off heater first.
8. Adjust variac to zero position.
9. Switch off the panel with the help of Mains On/Off switch given on the panel.
10. Switch off power supply to panel.

**TABULAR COLUMN:**

Sl. No.	V Volts	I Amps	Thermocouple readings °C					
			T <sub>2</sub>	T <sub>3</sub>	T <sub>4</sub>	T <sub>5</sub>	Chamber	
							Lower T <sub>1</sub>	Upper T <sub>6</sub>
1.								
2.								
3.								

**CALCULATIONS:**

1. Temperature of vertical cylinder wall  $T_w = \frac{T_2 + T_3 + T_4 + T_5}{4} + 273.15 \text{ } ^\circ\text{K} = \dots\dots\dots$

2. Surrounding ambient temperature  $T_\infty = \frac{T_1 + T_6}{2} = \dots\dots\dots + 273.15 \text{ } ^\circ\text{K}$

3. Obtain the properties of air at a mean temperature of  $T_f = \frac{T_w + T_\infty}{2} \text{ } ^\circ\text{K}$

4. Volumetric coefficient of thermal expansion  $\beta = \frac{1}{T_f}$

5. Rayleigh Number  $Ra = Gr.Pr$

6. Grashof Number,  $Gr = \frac{L^3 \beta g (T_w - T_\infty)}{\nu^2}$

Where,

Pr= Prandtl number (from Data book at  $T_f$ ).....

$\nu$  = kinematic viscosity..... m<sup>2</sup>/sec (from Data book at  $T_f$ )

7. Nusselt Number 
$$Nu = \frac{hL}{k}$$

The following correlations are used to find Nusselt Number

$$Nu = 0.53(Gr.Pr)^{\frac{1}{4}} \text{ for } Gr.Pr < 10^4$$

$$Nu = 0.59(Gr.Pr)^{\frac{1}{4}} \text{ for } 10^4 < Gr.Pr < 10^9$$

$$Nu = 0.10(Gr.Pr)^{\frac{1}{3}} \text{ for } 10^9 < Gr.Pr$$

8. Free convective heat transfer coefficient

$$h = \frac{Nu.k}{L} \text{ W/m}^2\text{-K}$$

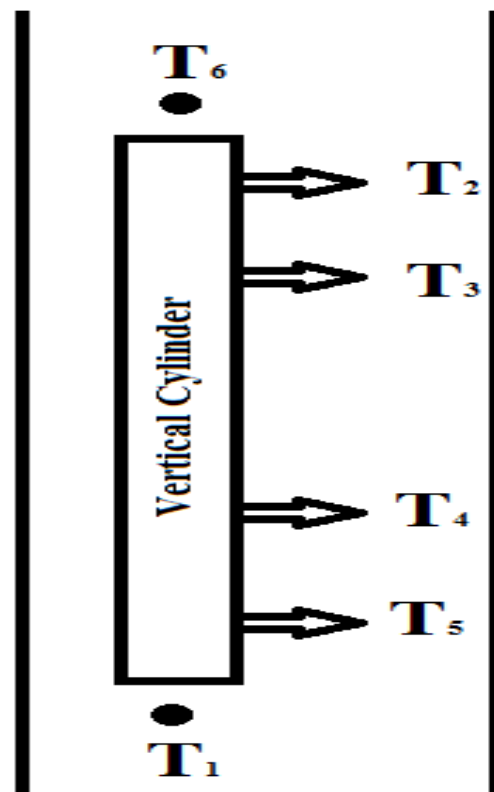
9. Heat transfer rate by convection

$$Q_c = h A (T_w - T_\infty)$$

$$Q_c = h \pi d L (T_w - T_\infty) \quad \text{watt}$$

10. Heat Input to the coil

$$Q_i = V \times I \quad \text{watts}$$



**Fig: Natural Convection Apparatus**

**PRECAUTIONS:**

1. Never switch on the main power supply before ensuring that all on / off switches give on the panel are at off position.
2. Never run the apparatus if power supply is less than 180 or above 200 Volts.
3. Make sure that convection should conduct in closed container.
4. Before switch on the main supply observer that the dimmer is in zero position.

**RESULT:**

The convective heat transfer coefficient and heat transfer rate from vertical cylinder in natural convection has been determined.

1. Convective heat transfer coefficient=.....
2. Heat transfer rate=.....

**Date:**  
**Exp No:**

## **PARALLEL FLOW AND COUNTER FLOW HEAT EXCHANGER**

### **AIM:**

To determine LMTD, effectiveness and overall heat transfer coefficient for parallel and counter flow heat exchanger

### **SPECIFICATIONS:**

Length of heat exchanger	L	=2440 mm
Inner copper tube	ID	=12 mm
	OD	=15 mm
Outer GI tube	ID	=40 mm
Geyser capacity		=1 Lt, 3 kW

### **THEORY:**

Heat exchanger is a device in which heat is transferred from one fluid to another. Common examples of heat exchangers are:

- i. Condensers and boilers in steam plant
- ii. Inter coolers and pre-heaters
- iii. Automobile radiators
- iv. Regenerators

### **CLASSIFICATION OF HEAT EXCHANGERS:**

#### **1. Based on the nature of heat exchange process:**

- i. Direct contact type – Here the heat transfer takes place by direct mixing of hot and cold fluids
- ii. Indirect contact heat exchangers – Here the two fluids are separated through a metallic wall. ex. Regenerators, Recuperators etc

#### **2. Based on the relative direction of fluid flow:**



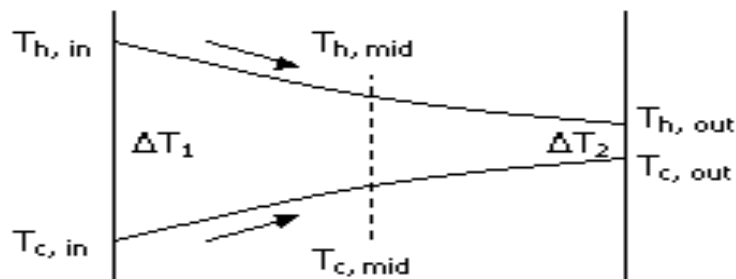
- i. Parallel flow heat exchanger – Here both hot and cold fluids flow in the same direction.
- ii. Counter flow heat exchanger – Here hot and cold fluids flow in opposite direction.
- iii. Cross-flow heat exchangers – Here the two fluids cross one another.

### **LOGARITHMIC MEAN TEMPERATURE DIFFERENCE (LMTD):**

This is defined as that temperature difference which, if constant, would give the same rate of heat transfer as usually occurs under variable conditions of temperature difference.

#### **FOR PARALLEL FLOW:**

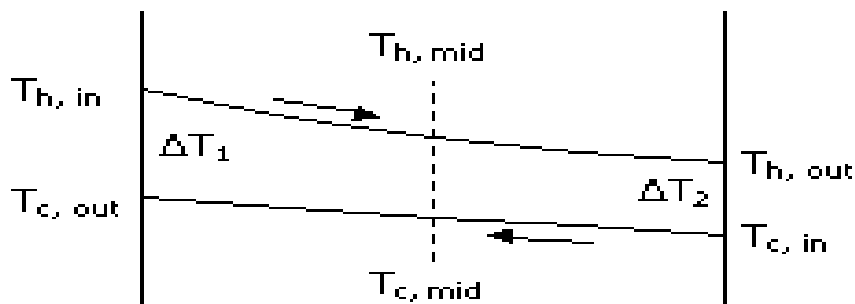
Where



Length of the TUBE

$$\text{LMTD} = \frac{(T_{ho} - T_{co}) - (T_{hi} - T_{ci})}{\ln\left(\frac{T_{ho} - T_{co}}{T_{hi} - T_{ci}}\right)} = \frac{\theta_2 - \theta_1}{\ln\left(\frac{\theta_2}{\theta_1}\right)}$$

#### **For Counter flow:**



Length of the TUBE

$$\text{LMTD} = \frac{(T_{hi} - T_{ci}) - (T_{ho} - T_{ci})}{\ln\left(\frac{T_{hi} - T_{co}}{T_{ho} - T_{ci}}\right)} = \frac{\theta_2 - \theta_1}{\ln\left(\frac{\theta_2}{\theta_1}\right)}$$

$T_{ho}$  = Outlet temperature of hot fluid

$T_{co}$  = Outlet temperature of cold fluid

$T_{hi}$  = Inlet temperature of hot fluid

$T_{ci}$  = Inlet temperature of cold fluid

### **OVERALL HEAT TRANSFER COEFFICIENT:**

The rate of heat transfer between hot and cold fluid is given by

$$Q = U_o A_o / \text{LMTD}$$

Where,

$U_o$  is overall heat transfer coefficient based on outer surface area of tubes, W/m<sup>2</sup>-K

$A_o$  is the total outer surface area of tubes, m<sup>2</sup>

### **EFFECTIVENESS:**

Effectiveness of a heat exchanger is defined as the ratio of actual heat transfer rate to the theoretical maximum possible heat transfer rate.

$$\text{Effectiveness: } \varepsilon = \frac{Q}{Q_{\max}}$$

It can be shown that

$$\varepsilon = \frac{T_{hi} - T_{ho}}{T_{hi} - T_{ci}} \quad \text{if } m_h c_h < m_c c_c$$

And

$$\varepsilon = \frac{T_{co} - T_{ci}}{T_{hi} - T_{ci}} \quad \text{if } m_c c_c < m_h c_h$$

Where,

$m_h$  and  $m_c$  are the mass flow rate of hot and cold fluids respectively in kg/s;

$c_h$  and  $c_c$  are the specific heat of hot and cold fluids respectively in J/kg-K.

### **DESCRIPTION OF THE APPRATUS:**

The apparatus consists of a concentric tube heat exchanger. The hot fluid namely hot water is obtained from the Geyser (heater capacity 3 kW) & it flows through the inner tube. The cold fluid i.e. cold water can be admitted at any one of the ends enabling the heat exchanger to run as a parallel flow or as a counter flow exchanger. Measuring jar used for measure flow rate of cold and hot water. This can be adjusted by operating the different valves provided. Temperature of the fluid can be measured using thermocouples with digital display indicator. The outer tube is provided with insulation to minimize the heat loss to the surroundings.

### **PROCEDURE:**

1. First switch ON the unit panel
2. Start the flow of cold water through the annulus and run the exchanger as counter flow or parallel flow.
3. Switch ON the geyser provided on the panel & allow to flow through the inner tube by regulating the valve.
4. Adjust the flow rate of hot water and cold water by using rotameters & valves.
5. Keep the flow rate same till steady state conditions are reached.
6. Note down the temperatures on hot and cold water sides. Also note the flow rate.
7. Repeat the experiment for different flow rates and for different temperatures.

The same method is followed for parallel flow also.

### **OBSERVATION TABLE:**

#### **PARALLEL FLOW**

Sl. No.	Hot water flow rate $m_h$ , kg/s	Cold water flow rate $m_c$ , kg/s	Temperature of cold water in °C		Temp. of hot water in °C	
			Inlet $T_{ci}$	Outlet $T_{co}$	Inlet $T_{hi}$	Outlet $T_{ho}$
1.						
2.						
3.						

### COUNTER FLOW

Sl. No.	Hot water flow rate $m_h$ , kg/s	Cold water flow rate $m_c$ , kg/s	Temperature of cold water in °C		Temp. of hot water in °C	
			Inlet $T_{ci}$	Outlet $T_{co}$	Inlet $T_{hi}$	Outlet $T_{ho}$
1.						
2.						
3.						

### EQUATIONS USED:

1. Heat transfer from hot water

$$Q_h = m_h C_{ph} (T_{hi} - T_{ho}) \text{ watts}$$

$m_h$  = mass flow rate of hot water kg/sec

$C_{ph}$  = Specific heat of hot water = 4186.8 J kg-K

2. Heat gain by the cold fluid

$$Q_c = m_c C_{pc} (T_{co} - T_{ci}) \text{ watts}$$

$m_c$  = Mass flow of cold fluid, kg/s

$C_{pc}$  = Specific heat of cold fluid = 4186.8 J/kg -K

3. 
$$Q = \frac{Q_h + Q_c}{2} \text{ watts}$$

$$LMTD = \frac{\theta_2 - \theta_1}{\ln\left(\frac{\theta_2}{\theta_1}\right)}$$

$\theta_1 = T_{hi} - T_{ci}$  and  $\theta_2 = T_{ho} - T_{co}$  for parallel flow heat exchanger

$\theta_1 = T_{ho} - T_{ci}$  and  $\theta_2 = T_{hi} - T_{co}$  for counter flow heat exchanger

5. Overall heat transfer coefficient based on outside surface area of inner tube

$$U_o = \frac{Q}{A_o \cdot LMTD} \quad \text{W/m}^2 \text{ } ^\circ\text{K}$$

Where,

$$A_o = \pi d_o l \quad \text{m}^2$$

$$d_o = \text{Outer diameter of the tube} = 0.0125 \text{ m}$$

$$L = \text{length of the tube} = 1.5 \text{ m}$$

6. Effectiveness:

Find  $C_h = m_h c_{ph}$  and  $C_c = m_c c_{pc}$

$$\text{Effectiveness} = \frac{T_{hi} - T_{ho}}{T_{hi} - T_{ci}} \quad \text{if } C_h < C_c$$

$$\text{And Effectiveness} = \frac{T_{co} - T_{ci}}{T_{hi} - T_{ci}} \quad \text{if } C_c < C_h$$

This is applicable both for Parallel and counter flow heat exchanger

7. Effectiveness using NUMBER OF TRANSFER UNIT (NTU) method

$$\text{i) } NTU = \frac{U_o A_o}{C_{\min}}$$

Note: if  $C_h < C_c$  then  $C_h = C_{\min}$ ,  $C_c = C_{\max}$

And if  $C_c < C_h$  then  $C_c = C_{\min}$ ,  $C_h = C_{\max}$

ii) Effectiveness of parallel flow heat exchanger

$$\varepsilon = \frac{1 - e^{-NTU \left[ 1 + \frac{C_{\min}}{C_{\max}} \right]}}{1 + \frac{C_{\min}}{C_{\max}}}$$

iii) Effectiveness of counter flow heat exchanger

$$\varepsilon = \frac{1 - e^{-NTU \left[ 1 - \frac{C_{\min}}{C_{\max}} \right]}}{1 - \frac{C_{\min}}{C_{\max}} e^{-NTU \left[ 1 - \frac{C_{\min}}{C_{\max}} \right]}}$$

**RESULT:**

The overall heat transfer coefficient of parallel flow and counter flow heat exchangers has been determined.

**Date:**  
**Exp No:**

## **HEAT TRANSFER FROM PIN-FIN APPARATUS**

### **AIM:**

To determine the temperature of a pin-fin for forced convection and to find fin efficiency and effectiveness.

### **SPECIFICATIONS:**

Length of the fin, 'L'	= 145mm
Diameter of the fin, 'd <sub>f</sub> '	= 12mm
Diameter of the orifice, 'd <sub>o</sub> '	= 20 mm
Width of the duct, 'W'	= 150 mm
Breadth of the duct, 'B'	= 100 mm
Coefficient of discharge of the orifice, 'C <sub>d</sub> '	= 0.62
Density of manometric fluid (water)	= 1000 kg/m <sup>3</sup>

### **THEORY:**

The heat transfer from a heated surface to the ambient surrounding is given by the relation,  $q = h A \Delta T$ . In this relation  $h_c$  is the convective heat transfer coefficient,  $\Delta T$  is the temperature difference &  $A$  is the area of heat transfer. To increase  $q$ ,  $h$  may be increased or surface area may be increased. In some cases it is not possible to increase the value of heat transfer coefficient & the temperature difference  $\Delta T$  & thus the only alternative is to increase the surface area of heat transfer. The surface area is increased by attaching extra material in the form of rod (circular or rectangular) on the surface where we have to increase the heat transfer rate. "This extra material attached is called the extended surface or fin."

The fins may be attached on a plane surface, and then they are called plane surface fins. If the fins are attached on the cylindrical surface, they are called circumferential fins. The cross section of the fin may be circular, rectangular, triangular or parabolic.

**Temperature distribution along the length of the fin:**

$$\frac{\theta}{\theta_0} = \frac{T - T_\infty}{T_0 - T_\infty} = \frac{\cosh[m(L - x)]}{\cosh(mL)}$$

Where

$T$  = Temperature at any distance  $x$  on the fin

$T_0$  = Temperature at  $x = 0$

$T_\infty$  = Ambient temperature

$L$  = Length of the fin

$$m = \sqrt{\frac{h_c P}{kA}}$$

Where

$h$  = convective heat transfer coefficient

$P$  = Perimeter of the fin

$A$  = area of the fin

$K$  = Thermal conductivity of the fin

**Rate of heat flow for end insulated condition:**

$$Q = \theta_0 \sqrt{h_c P k A} \tanh(mL)$$

Effectiveness of a fin is defined as the ratio of the heat transfer with fin to the heat transfer from the surface without fins.

$$\varepsilon = \frac{\theta_0 (\sqrt{h P k A}) \tanh(mL)}{h A \theta_0}$$

$$\varepsilon = \left( \sqrt{\frac{P k}{h A}} \right) \tanh(mL)$$

The efficiency of a fin is defined as the ratio of the actual heat transferred by the fin to the maximum heat transferred by the fin if the entire fin area were at base temperature.

$$\eta_f = \frac{\theta_0 (\sqrt{h P k A}) \tanh(mL)}{h P L \theta_0}$$

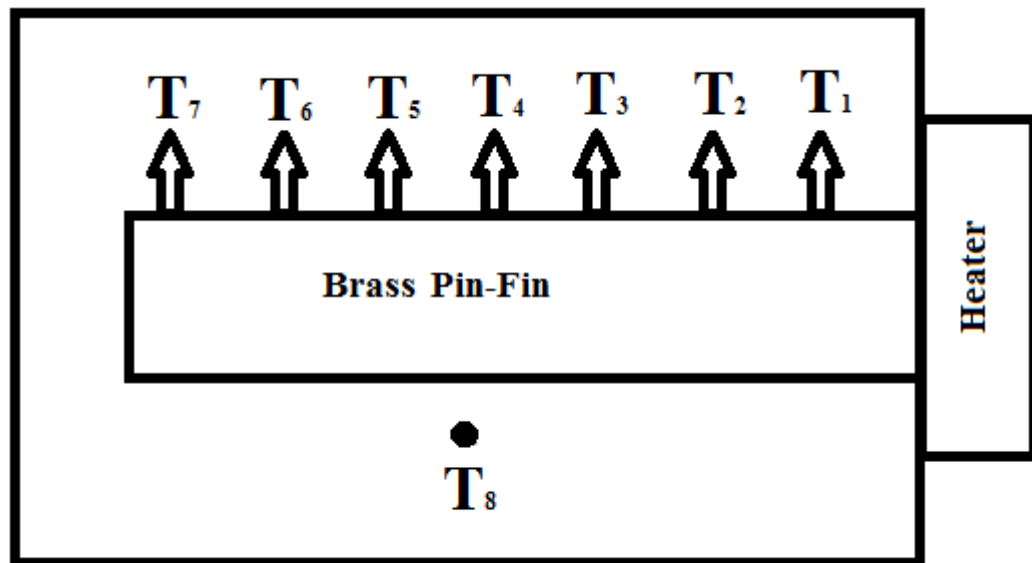
$$\eta_f = \frac{\tanh(mL)}{mL}$$

**PROCEDURE:**

1. Connect the equipment to electric power supply.
2. Keep the thermocouple selector switch to zero position.

3. Turn the dimmer stat clockwise and adjust the power input to the heater to the desired value and switch on the blower.
4. Set the air-flow rate to any desired value by adjusting the difference in water levels in the manometer and allow the unit to stabilize.
5. Note down the temperatures,  $T_1$  to  $T_6$  from the thermocouple selector switch.

Note down the difference in level of the manometer and repeat the experiment for different power inputs to the heater.



**Fig: Pin-Fin apparatus**

### CALCULATIONS:

7. Velocity of the air in the tube  $V_a = \frac{Q}{a_1}$

Discharge of the air in the tube  $Q = \frac{C_d a_1 a_2 \sqrt{2gh_m}}{\sqrt{a_1^2 - a_2^2}}$

Where

Coefficient of discharge  $C_d = 0.62$

Area of Pipe  $a_1 = \frac{\pi}{4} d_1^2 \rightarrow d_1$  is diameter of the pipe = 40mm.

Area of Orifice  $a_2 = \frac{\pi}{4} d_2^2 \rightarrow d_2$  is diameter of the Orifice = 20mm.

$h_m$  Differential manometer reading .

8. Properties of air are taken at temperature  $T_f = \frac{T_w + T_\infty}{2}$

Where



Average surface temperature of the Pin-fin

$$T_{avg} = T_w = \frac{T_1 + T_2 + T_3 + T_4 + T_5 + T_6 + T_7}{7}$$

Ambient temperature of air in Duct  $T_\infty = T_8$

9. Reynolds Number  $Re_D = \frac{V_a \cdot d_f}{\nu}$   
 ( $\nu = \text{Kinematic Viscosity}$  From data book at  $T_f$ )  
 ( $Pr = \text{Prandtl number}$  from data book at  $T_f$ )

10. Nusselt number  $Nu = C Re_D^m Pr^{0.333}$

For

$Re_D = 0.4$	to 4.0	$C = 0.989$	$m = 0.33$
$Re_D = 4$	to 40	$C = 0.911$	$m = 0.385$
$Re_D = 40$	to 4000	$C = 0.683$	$m = 0.466$
$Re_D = 4000$	to 40,000	$C = 0.293$	$m = 0.618$
$Re_D = 40,000$	to 400,000	$C = 0.27$	$m = 0.805$

11. Nusselt number  $Nu = \frac{h d_f}{k}$

12. Forced convective heat transfer co-efficient  $h = \frac{Nu k}{d_f}$   $W/m^2 - K$   
 ( $k = \text{thermal conductivity}$  from data book at  $T_f$ )

13. Rate of heat transfer  $Q_c = h A (T_w - T_\infty)$

$$Q_c = h \pi d L (T_w - T_\infty) \quad \text{watt}$$

14. Temperature distribution is given by

$$\frac{T - T_\infty}{T_0 - T_\infty} = \frac{\cosh(m(L - X))}{\cosh(mL)}$$

15. Therefore  $T = T_8 + [T_1 - T_8] \times \left[ \frac{\cosh(m(L - X))}{\cosh(mL)} \right]$

Distance x, m	Temperature from Experiment °C	Temperature °C from calculation
$x_1 = 0.02$	$T_{0.02} =$	$T_{0.02} =$
$x_2 = 0.04$	$T_{0.04} =$	$T_{0.04} =$
$x_3 = 0.06$	$T_{0.06} =$	$T_{0.06} =$
$x_4 = 0.08$	$T_{0.08} =$	$T_{0.08} =$
$x_5 = 0.10$	$T_{0.1} =$	$T_{0.1} =$

$x_6 = 0.12$	$T_{0.12} =$	$T_{0.12} =$
$x_7 = 0.14$	$T_{0.14} =$	$T_{0.14} =$

16. Efficiency of fin  $\eta_f = \frac{\tanh(mL)}{mL}$

Where  $L =$  Length of the Fin = 145mm

$$m = \sqrt{\frac{hP}{k_{brass}A}}$$

$h =$  Convective heat transfer coefficient  $\text{W/m}^2\text{-K}$

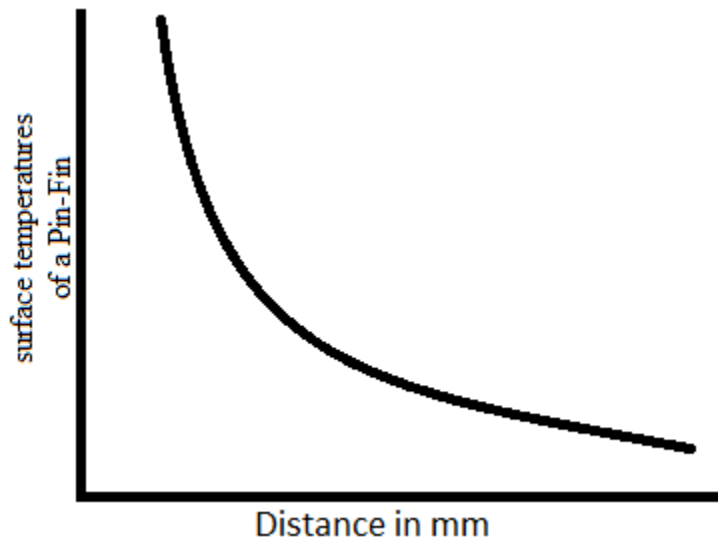
$P =$  Perimeter of the Fin ( $\pi d_f$ )

$A =$  Cross-sectional area of the Fin  $A = \frac{\pi}{4} d_f^2$

$k_{brass} =$  Thermal conductivity of brass = 110.7 W/m-K

17. Effectiveness of fin  $\varepsilon = \left( \sqrt{\frac{Pk}{hA}} \right) \tanh(mL)$

**GRAFF:** surface temperature of Pin-Fin Vs Distance (location of thermocouples on Pin-Fin)



### **PRECAUTIONS:**

3. Never switch on main power supply before ensuring that all on/off switches given on the panel are at off position
4. Never run the apparatus if power supply is less than 180 or above 200 volts.

### **RESULT:**

The temperature distribution of a pin – fin for forced convection efficiency and effectiveness has been determined.

1. Temperature distribution of a pin fin is given by

Distance x, m	Temperature from Experiment °C	Temperature °C from calculation
$x_1 = 0.02$	$T_{0.02} =$	$T_{0.02} =$
$x_2 = 0.04$	$T_{0.04} =$	$T_{0.04} =$
$x_3 = 0.06$	$T_{0.06} =$	$T_{0.06} =$
$x_4 = 0.08$	$T_{0.08} =$	$T_{0.08} =$
$x_5 = 0.10$	$T_{0.1} =$	$T_{0.1} =$
$x_6 = 0.12$	$T_{0.12} =$	$T_{0.12} =$
$x_7 = 0.14$	$T_{0.14} =$	$T_{0.14} =$

2. Efficiency of Pin-Fin=.....

3. Effectiveness of Pin-Fin=.....

**Date:**  
**Exp No:**

## **STEFAN BOLTZMANN APPARATUS**

### **AIM:**

To determine the value of Stefan Boltzmann constant for radiation heat transfer.

### **APPARATUS:**

Hemisphere, Heater, Temperature indicator, Stopwatch.

### **THEORY:**

Stefan Boltzmann law states that the total emissive power of a perfect black body is proportional to fourth power of the absolute temperature of black body surface.

$$E_b = \sigma T^4$$

Where

$$\sigma = \text{Stefan Boltzmann constant} = 5.6697 \times 10^{-8} \text{ W/(m}^2 \text{ K}^4\text{)}$$

### **DESCRIPTION:**

The apparatus consists of a flanged copper hemisphere fixed on a flat non-conducting plate. A test disc made of copper is fixed to the plate. Thus the test disc is completely enclosed by the hemisphere. The outer surface of the hemisphere is enclosed in a vertical water jacket used to heat the hemisphere to a suitable constant temperature. Three Cr-Al thermocouples are attached at three strategic places on the surface of the hemisphere to obtain the temperatures. The disc is mounted on an ebonite rod which is fitted in a hole drilled at the center of the base plate. Another Cr-Al thermocouple is fixed to the disc to record its temperature. Fill the water in the SS water container with immersion heater kept on top of the panel.

### **SPECIFICATIONS:**

Specimen material	:	Copper
Size of the disc	:	ϕ 20mm x 0.5mm thickness
Base Plate	:	ϕ 250mm x 12mm thickness (hylam)

Heater	:	1.5 kW capacity, immersion type
Copper Bowl	:	$\phi$ 200mm
Digital temperature indicator	:	0 -199.9° C
Thermocouples used	:	3 nos. on hemisphere
Stop Watch	:	Digital type
Overhead Tank	:	SS, approx. 12 liter capacity
Water Jacket	:	$\phi$ 230 mm, SS
Mass of specimen, 'm'	:	5 gm
Specific heat of the disc $C_p$	:	0.38 kJ/kg K

### **PROCEDURE:**

1. Remove the test disc before starting the experiment.
2. Allow water to flow through the hemisphere, Switch on the heater and allow the hemisphere to reach a steady state temperature.
3. Note down the temperatures  $T_1, T_2$  &  $T_3$ . The average of these temperatures is the hemisphere temperature  $T_h$ .
4. Insert the test disc at the bottom of the hemisphere and lock it. Start the stop clock simultaneously.
5. Note down the temperature of the test disc at an interval of about 15 sec for about 15 to 20 minutes.

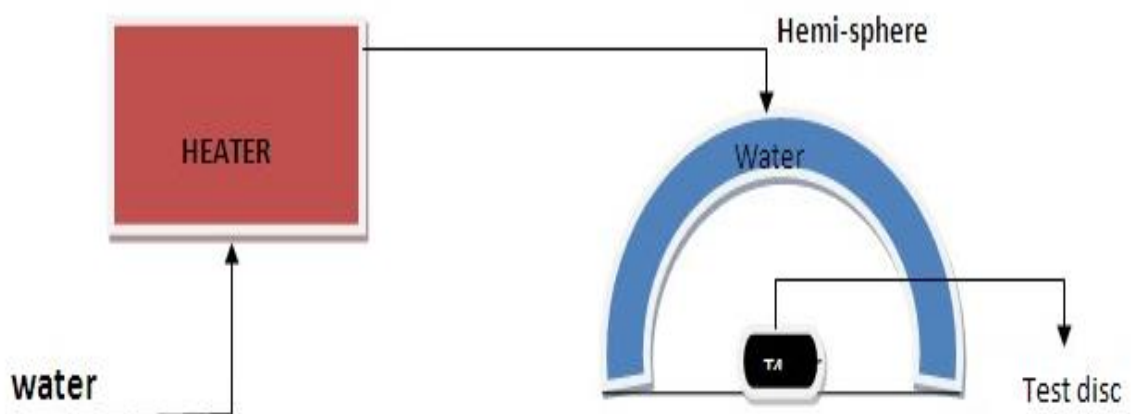


FIG: STEFAN BOLTZMANN APPARATUS

**OBSERVATION TABLE:**

Let  $T_d$  = Temperature of the disc before inserting into the plate in K

Thermocouple	Temperature of the copper hemisphere ° C
$T_1$	
$T_2$	
$T_3$	
$T_h$ Average of $T_1$ , $T_2$ and $T_3$ =	

Temperature – time response of test disc:

Time 't' sec	Temperature $T_d$ ° C	Time 't' sec	Temperature $T_d$ ° C

**CALCULATIONS:**

1. Plot the graph of temperature of the disc v/s time to obtain the slope (dT/dt) of the line, which passes through/nearer to all points.
2. Average temperature of the hemisphere

$$T_h = \frac{T_1 + T_2 + T_3}{3} + 273.15$$

3.  $T_d =$  Temperature of the disc before inserting to  
Test chamber ° K (ambient)

4. Rate of change of heat capacity of the disc =  $mC_p \frac{dT}{dt}$

Net energy radiated on the disc =  $\sigma A_d (T_h^4 - T_d^4)$

Where

$A_d =$  area of the disc =  $\frac{\pi}{4} d^2$  in  $m^2$

$d =$  20 mm

$C_p =$  specific heat of copper = 0.38 kJ/kg–K

Rate of change of heat capacity of the disc = Net energy radiated on the disc

$$mC_p \frac{dT}{dt} = \sigma A_d (T_{avg}^4 - T_d^4)$$

Thus 'σ' can be evaluated as shown

$$\sigma = \frac{mC_p \frac{dT}{dt}}{A_d (T_{avg}^4 - T_d^4)}$$

**Result:** The experiment on Stefan Boltzmann apparatus has been conducted and the value of Stefan Boltzmann constant is determined.

**Date:**  
**Exp No:**

## **THERMAL CONDUCTIVITY OF METAL ROD**

### **AIM:**

To determine the thermal conductivity of given metal rod.

### **THEORY:**

From Fourier's law of heat conduction

$$Q = -kA \frac{dT}{dx}$$

where

$Q$  = Rate of heat conducted, W

$A$  = Area of heat transfer, m<sup>2</sup>

$k$  = Thermal conductivity of the material, W/m-K

$\frac{dT}{dx}$  = Temperature gradient

Thermal conductivity is a property of the material and may be defined as the amount of heat conducted per unit time through unit area, when a temperature difference of unit degree is maintained across unit thickness.

### **DESCRIPTION OF THE APPARATUS:**

The apparatus consists of a brass rod, one end of which is heated by an electric heating coil while the other end projects into the cooling water jacket. The rod is insulated with glass wool to minimize the radiation and convection loss from the surface of the rod and thus ensure nearly constant temperature gradient throughout the length of the rod. The temperature of the rod is measured at five different locations. The heater is provided with a dimmerstat for controlling the heat input. Water is circulated through the jacket and its flow rate and temperature rise can be measured.

### **SPECIFICATIONS :**

Specimen material	:	Brass rod
Size of the Specimen	:	φ20 mm, 450mm long
Cylindrical shell	:	300mm long



Voltmeter	:	Digital type, 0-300volt, AC
Ammeter	:	Digital type, 0-20amp, AC
Dimmer for heating Coil	:	0-230v, 12amps
Heater	:	Band type Nichrome heater, 250 W
Thermocouple used	:	11 nos.
Temperature indicator	:	Digital type, 0-200 <sup>0</sup> c, Cr-Al

### **PRODEDURE:**

1. Power supply is given to the apparatus.
2. Give heat input to the heater by slowly rotating the dimmer and adjust the voltage to say 60 V, 80 V, etc
3. Start the cooling water supply through the jacket and adjust its flow rate so that the heat is taken away from the specimen constantly.
4. Allow sufficient time for the apparatus to reach steady state.
5. Take readings of voltmeter and ammeter.
6. Note the temperatures along the length of the specimen rod at 5 different locations.
7. Note down the inlet & outlet temperatures of cooling water and measure the flow rate of water.
8. Repeat the experiment for different heat inputs.

### **OBSERVATION TABLE:**

‘V’ Volt	‘I’ Amp	Metal rod thermocouple reading (0C)									Water temp (0C)		Volume flow rate of water, V cc/min
											In let	Ou tlet	
		T <sub>1</sub>	T <sub>2</sub>	T <sub>3</sub>	T <sub>4</sub>	T <sub>5</sub>	T <sub>6</sub>	T <sub>7</sub>	T <sub>8</sub>	T <sub>9</sub>	T <sub>10</sub>	T <sub>11</sub>	
1.													
2.													
3.													

### **CALCULATION:**

Plot the variation of temperature along the length of the rod. From the graph, obtain  $dT/dx$ , which is the slope of the straight line passing through/near to the

points in the graph. Assuming no heat loss, heat conducted through the rod = heat carried away by the cooling water

$$kA \frac{dT}{dx} = m_f C_p (T_{11} - T_{10})$$

Where, 'k' = thermal conductivity of metal rod, (W/m-K)

'A' = Cross sectional area of metal rod =  $\pi d^2/4$  (m<sup>2</sup>)

'd' = diameter of the specimen = 20 mm

'C<sub>p</sub>' = Specific heat of water = 4.187 kJ/kg-K

Thus, the thermal conductivity 'k' of metal rod can be evaluated.

$$k = \frac{m_f C_p (T_{11} - T_{10})}{A \frac{dT}{dx}}$$

### **GRAPH:**

Plot the graph Distance vs Temperature.
---

### **PRECAUTIONS:**

7. Keep the dimmer stat to zero before starting the experiment.
8. Take readings at study state condition only.
9. Use the selector switch knob and dimmer knob gently.

### **RESULT:**

The thermal conductivity of given metal rod has been determined.

Date:

Exp No:

## **TWO PHASE HEAT TRANSFER APPARATUS**

### **AIM:**

To Study the Two Phase heat transfer phenomena for pool boiling of water.

### **THEORY:**

Two phase heat transfer is a mode of heat transfer that occurs because of vaporization. Vaporization is a process in which a substance is changed from liquid to vapour state. Pool boiling takes place when a liquid is confined in a container and a heater is submerged in the liquid.

### **BOILING REGIMES:**

Consider that the rate of heat convection, heat transfer for the system is expressed analytically by the **Newton's equation**:

$$Q = h A \Delta t \text{----- (1)}$$

Where 'h' is the heat transfer coefficient, 'A' is area involved in heat transfer and  $\Delta t$  is some well defined temperature difference, The difference between the temperature of the solid and the mean temperature of fluid at the limit of the thermal boundary layer, An analogous equation issued for boiling heat transfer.

$$\frac{\dot{Q}}{A} = h \Delta t \text{----- (2)}$$

Where  $q'' = \dot{Q}/A$  is called the heat flux and h the boiling heat transfer coefficient.  $t_w$  is the wall superheat or surface temperature.  $\Delta t$  which is defined as difference between the wall temperature of the heating surface and saturation temperature of the liquid  $t_s$ .

$$\Delta t = t_w - t_s \text{----- (3)}$$

### **DESCRIPTION:**

The main apparatus is fitted on MS tube frame consisting of a glass column with a sample holding sump with a heater and drain valve at the bottom and a

helical condenser, with water inlet and outlet , a safety valve, and a feed valve at the top and the unit is made leak proof with necessary flange connections.

The panel consists of voltmeter, ammeter, temperature indicator, dimmer, thermocouple selector switch, toggle switch for pump, Rotameter. Below the table a water sump fitted with pump is provided to circulate water through the helical condenser coil, a bypass is also provided for the pump to safety guard the motor.

**PROCEDURE:**

1. Fill the sample holding sump with sample of about 250ml (approx) through the feed valve provided on top of the column (ensure that the drain valve provided at the bottom is closed) and close the feed valve after filling.
2. Ensure that the dimmer is 'OFF', thermocouple selector switch at any position; the pump toggle switch is 'OFF'.
3. Connect the three pin plug top to 230V, 50, 5 amps power supply socket with proper earthing.
4. Fill water into the water sump provided below the table.
5. Open the bypass valve fully and also open the Rota meter valve.
6. Switch 'ON' the toggle switch for pump.
7. Observe water falling into the sump through bypass.
8. Slowly turn the bypass valve clock wise and observe the Rota meter float to rise.
9. Set the water flow rate to any desired value indicated by the Rota meter.
10. Turn the dimmer clockwise and set the power input to the heater at the minimum possible limit by observing the volt and ammeter ( $V \times I = W$ ) and note the readings.
11. Note down the temperatures indicated by the temperature indicator by turning the thermocouple selector switch clockwise step by step.
12. Bring back the thermocouple selector switch to any position.

13. Increase the power input to the heater by lowest possible value (increasing of the power output to the heater should be made at a known interval time) record the readings.
14. Record the temperatures indicated at each step  $T_1$  &  $T_2$ .
15. Repeat increasing of power input to the heater and recording the temperatures at an interval of time till the sample start boiling.
16. Tabulate all the readings and calculate.
17. After the experiment is over turn the dimmer anticlockwise to 'ZERO' position. Also bring back thermocouple selector switch to any position allow the water circulation pump to work for some time, switch 'OFF' the pump switch, drain the sample by opening the drain valve and close the drain valve after draining.

#### **EXPERIMENT APPARATUS:**

The apparatus consists of a vertical glass cylinder, in which liquid WATER boils. Inside the glass cylinder a copper-condensing coil is placed. At the bottom of the glass column a copper bowl heater electrically by a heating coil. Cooling water is circulated through the condenser by means of pump. Water flow control is achieved through valve  $V_1$  Rota meter gives an indication of water flow rate.

Thermocouple  $T_1$ , measures the temperature in the heating pad a  $T_2$  measures the liquid and temperature. Voltmeter 'V' and Ammeter 'A' measure the heater input voltage and current respectively.

#### **THERMOCOUPLE DETAILS:**

$T_1$ =Heater temperature

$T_2$ =Liquid temperature

$T_3$ =Vapour temperature

$T_4$ =Water inlet temperature to coil

$T_5$ =Water outlet temperature from coil

**OBSERVATION TABLE:**

Sl. No	Volts (V)	amps (I)	T <sub>1</sub>	T <sub>2</sub>	T <sub>3</sub>	T <sub>4</sub>	T <sub>5</sub>	Volume flow rate of water, cc/min
1.								
2.								
3.								

**CALCULATIONS:**

Heat input  $Q = V \times I$  watts

Heat transfer area  $A = \frac{\pi}{4} D^2 \text{ m}^2$

Where  $D =$  Dia of copper bowl  $= 100\text{mm}$

Heat flux  $\dot{Q} = Q/A \text{ w/m}^2$

$$\Delta t = T_1 - T_2$$

**GRAPH:**

Plot the graph $Q$ vs $\Delta t$ .
------------------------------------

**PRECAUTIONS:**

10. Keep the dimmer stat to zero before starting the experiment.
11. Take readings at study state condition only.
12. Use the selector switch knob and dimmer knob gently.

**RESULT:** Hence the study of boiling heat transfer for pool boiling of WATER is studied. The two phase heat transfer of phenomenon for cool boiling of water is studied and graph is plotted between the heat flux and temperature.

**Date:**

**Exp No:**

## **UNSTEADY STATE HEAT TRANSFER**

### **AIM:**

To obtain the specimen temperature at any interval of time by theoretical methods and observe the heating and cooling curves of unsteady state.

### **INTRODUCTION:**

Unsteady state designates a phenomenon which is time dependent. Conduction of heat in unsteady state refers to transient conditions where in, heat flow and temperature distribution at any point of system varies with time. Transient conditions occur in heating or cooling of metal billets, cooling of IC engine cylinder, brick and vulcanization of rubber.

### **DESCRIPTION:**

Unsteady state heat transfer equipment has oil check which is at top of oil heater. Thermocouple No.1 is located inside the specimen No.2 thermocouple measures the atmospheric temperature. No.3 thermocouple measures the oil temperature.

Digital temperature indicator indicates respective temperatures of thermocouples as we select it by selector switch. Heater ON/OFF toggle switch and buzzer ON/OFF toggle switch is provided on the control panel.

### **SPECIFICATIONS:**

- |                                  |                      |
|----------------------------------|----------------------|
| 1. D.C Buzzer                    | : 10-30 volt         |
| 2. Oil Heater                    | : 1 kW               |
| 3. Digital temperature indicator | : 1200C <sup>0</sup> |
| 4. Thermocouple                  | : Al-Cr type         |
| 5. Specimens material            | : Copper             |
| 6. Fuse                          | : 4 Amps.            |

### **EXPERIMENTATION:**

Obtain the specimen temperature at any interval of time by practical and by theoretical methods and observe the heating and cooling curves of unsteady state.

### **PROCEDURE:**

1. Put ON the mains switch.
2. Fill the oil jar up to  $\frac{3}{4}^{th}$  of its height.
3. Insert the thermocouple in jar having tag No.3.
4. Keep thermocouple No.2 near to the specimen inside the transparent chamber.
5. Start the oil heater by putting heater's toggle switch in downward direction.
6. Keep selector switch No.3 and observe oil temperature.
7. When the oil temperature reaches up to  $95^{\circ}\text{C}$  insert specimen in oil jar. At the same time note down the specimen temperature and start the stop watch.
8. Note down the specimen reading for every 30 sec. Check the oil temperature by selecting No.3 on selector switch.
9. Take the readings of specimen temperature till it comes nearly too hot oil temperature.
10. Now put the specimen inside the rectangular chamber. At the same time put OFF the heater.
11. Take the atmospheric temperature by selecting No.2 and specimen temperature. Note the specimen temperature reading till it comes closer to atmospheric temperature.
12. Put OFF the main switch.

### **OBSERVATIONS:**

- |                                     |   |
|-------------------------------------|---|
| 1. Specimen material                | : Copper                                      |
| 2. Thermal conductivity of copper,  | $k=386 \text{ W/m}^{\circ}\text{K}$ .         |
| 3. Coefficient of thermal expansion | $\alpha=17.7 \times 10^{-6}/^{\circ}\text{C}$ |
| 4. Specimen diameter,               | $d=30\text{mm}$                               |
| 5. Specimen length,                 | $l=30\text{mm}$                               |



**TABULATION:****In case of Heating:****In case of Cooling:**

Sl. No	Oil temperature $T_1$ in $^{\circ}\text{C}$	Specimen Temperature $T_3$ in $^{\circ}\text{C}$ at interval of 30 sec.	Time in second t	Sl. No	Atmospheric temperature $T_2$ in $^{\circ}\text{C}$	Specimen Temperature $T_3$ in $^{\circ}\text{C}$ at interval of 30 sec	Time in second t
1.	70		0	1.			0
2.			30	2.			30
3.			60	3.			60
4.			90	4.			90
5.			120	5.			120
6.			150	6.			150
7.			180	7.			180
8.			240	8.			240
9.			270	9.			270
10.			300	10.			300
11.			330	11.			330

**CALCULATION:**

Specimen material : Copper

Thermal conductivity of copper,  $k=386 \text{ W/m}^{\circ}\text{K}$ .Coefficient of thermal expansion  $\alpha=17.7 \times 10^{-6}/^{\circ}\text{C}$ Specimen diameter,  $d=30\text{mm}$ Specimen length,  $l=30\text{mm}$ Characteristic length for cylinder  $L= d/2$ Biot number  $Bi= \frac{hL}{k}$ Fourier number  $Fo= \frac{\alpha t}{L^2}$

$$\text{Mean temperature} = T = \frac{T_{\max} + T_{\min}}{2}$$

In case of cooling

$T_{\max}$ =specimen temperature just after the hot oil both

$T_{\min}$ = atmospheric temperature

In case of heating

$T_{\max}$ =hot oil temperature

$T_{\min}$ = specimen temperature before inserting into oil both

$$\frac{T - T_{\infty}}{T_0 - T_{\infty}} = e^{-(Bi \dots X \dots Fo)}$$

Where

$T$ = temperature of the specimen at time interval of 't' sec

$T_a$ = atmospheric temperature in 0C

$T_s$ =specimen temperature

In case of cooling

$T_a$ = atmospheric temperature

$T_s$ = specimen temperature

In case of heating

$T_a$ = Specimen temperature

$T_s$ = hot oil temperature

Obtain the temperature at any desired interval of the time

Plot the graph of temperature difference V/S time for heating and cooling

### **PRECAUTIONS:**

1. Keep the dimmer stat to zero before starting the experiment.
2. Operate the stop watch carefully.
3. Use the selector switch knob and dimmer knob gently.

### **RESULT:**

The specimen temperature at an interval of time by practical and by theoretical methods and observe the heating and cooling curves of unsteady state is observed.