

Topology optimization of lattice materials with nonlinear elasticity law

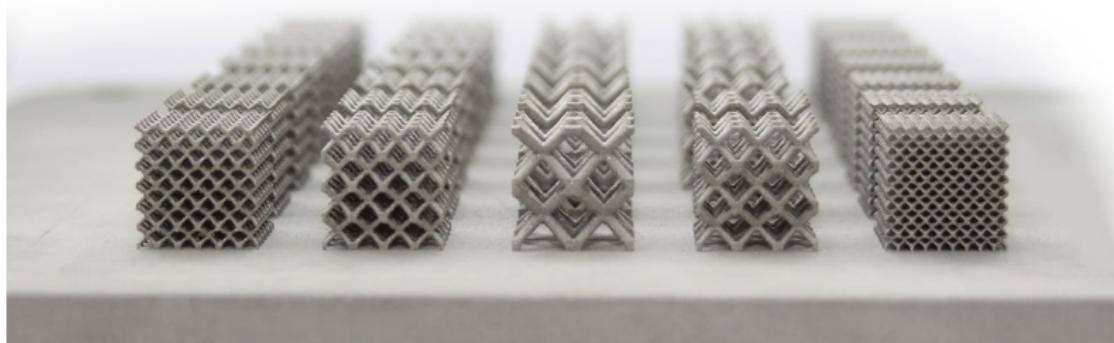
Teresa Babini
Manfred Nesti

Tutors: Prof. S. Perotto, Prof. S. Micheletti, Dr. N. Ferro

Numerical Analysis for Partial Differential Equations
Politecnico di Milano

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Lattice structures and metamaterials



Design lattices with linear elastic law

Weak form of the modified linear elasticity equation:

$$\text{find } \mathbf{u} \in U = \left\{ \mathbf{v} \in (H^1(\Omega))^2 : \mathbf{u} = 0 \text{ on } \Gamma_D \right\}$$

s.t.

$$a(\mathbf{u}, \mathbf{v}) = C(\mathbf{v}) \quad \forall \mathbf{v} \in U$$

with

$$a(\mathbf{u}, \mathbf{v}) = \int_{\Omega} \sigma_p(\mathbf{u}) : \varepsilon(\mathbf{v}) \, d\mathbf{x}$$

$$C(\mathbf{v}) = \int_{\Gamma_N} \mathbf{f} \cdot \mathbf{v} \, d\gamma$$

$$\sigma_p(\mathbf{u}) = \rho^p \sigma(\mathbf{u})$$

Topology Optimization

Algorithm 1: SIMP on a fixed grid

Result: ρ

Input: TOL, kmax, ρ_{\min} , α ;

Set: $\rho_h^0 \leftarrow 1$, $k \leftarrow 0$, err $\leftarrow 1 + TOL$

while $err > TOL$ & $k < kmax$ **do**

1. $\rho_h^{k+1} \leftarrow \text{IPOPT}(\rho_h^k, \rho_{\min}, Mit = 10, \alpha, \dots);$
2. $\rho_h^{k+1} \leftarrow \text{HELMHOLTZ}(\rho_h^{k+1}, \tau);$
3. $err \leftarrow \|\rho_h^{k+1} - \rho_h^k\|_\infty;$
4. $k \leftarrow k + 1;$

end

Anisotropic mesh adaptivity

Algorithm 2: SIMPATY: SIMP with AdaptiviT^Y

Result: ρ

Input: CTOL, MTOL, kmax, ρ_{\min} , \mathcal{T}_h^0 , α ;

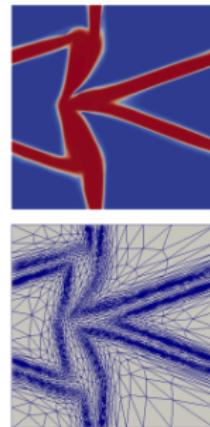
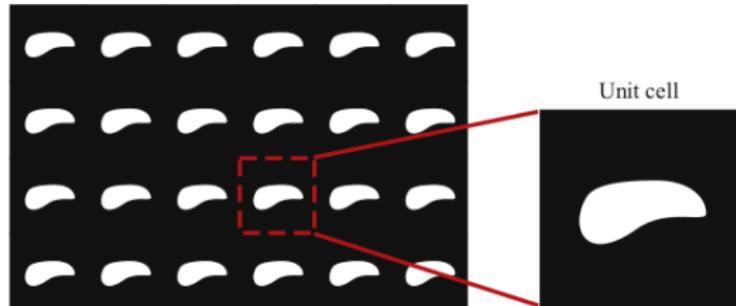
Set: $\rho_h^0 \leftarrow 1$, $k \leftarrow 0$, errC $\leftarrow 1 + TOL$

while $errC > TOL$ & $k < kmax$ **do**

1. $\rho_h^{k+1} \leftarrow IPOPT(\rho_h^k, \rho_{\min}, Mit = nk, \alpha, \dots);$
2. $\mathcal{T}_h^{k+1} \leftarrow adaptmesh(\mathcal{T}_h^k, \rho_h^{k+1}, MTOL, method);$
3. $errC \leftarrow |\#\mathcal{T}_h^{k+1} - \#\mathcal{T}_h^k| / \#\mathcal{T}_h^k;$
4. $k \leftarrow k + 1;$

end

Homogenization applied to linear elasticity law



$$\int_Y E_{ijpq} \varepsilon_{pq}^{*,kl} \varepsilon_{ij}(v) dY = \int_Y E_{ijpq} \varepsilon_{pq}^{0,kl} \varepsilon_{ij}(v) dY \quad \forall v \in V \quad (1)$$

$$E_{ijkl}^H = \frac{1}{|Y|} \int_Y E_{pqrs} \left(\varepsilon_{pq}^{0,kl} - \varepsilon_{pq}^{*,kl} \right) \left(\varepsilon_{rs}^{0,ij} - \varepsilon_{rs}^{*,ij} \right) dY \quad (2)$$

$$J = \sum_{ijkl} \left(E_{ijkl}^H(\rho) - E_{ijkl}^W \right)^2 \quad (3)$$

TO problem

Find ρ such that $\min_{\rho \in L^\infty(Y)} J(\rho)$ is achieved under constraints

- ① State equation for nonlinear material is satisfied by $\mathbf{u}(\rho)$
- ② + Periodicity conditions
- ③ $\int_Y \rho \, dY \leq \alpha |Y|$
- ④ $\rho_{\min} \leq \rho \leq 1$

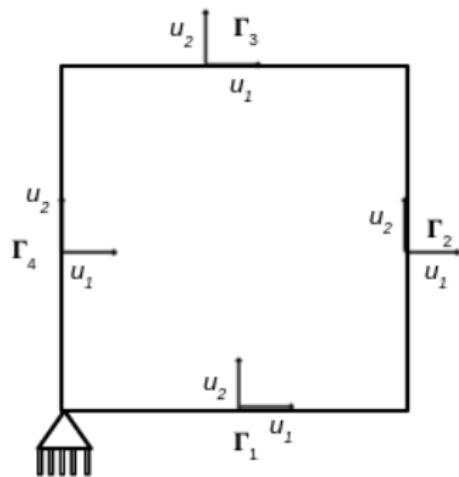
$$J(\mathbf{u}) = \frac{1}{2} (c(\mathbf{u}) - c^*)^2 = \frac{1}{2} (\nu(\mathbf{u}) - \nu^*)^2$$

Design lattices with nonlinear elastic law

- Boundary conditions and Poisson's ratio ν
- Nonlinear model
- Lagrange method for IPOPT
- Tests to validate the model
- Final algorithm and parameters tuning

Design lattices with nonlinear elastic law

Poisson's ratio



$$\begin{cases} \mathbf{u} \cdot \mathbf{n} = u_1 & = 0 \quad \text{on } \Gamma_1 \\ \mathbf{u} \cdot \mathbf{n} = u_2 & = 0 \quad \text{on } \Gamma_4 \\ u_1 & = d_1 \quad \text{on } \Gamma_2 \\ \frac{\partial \Psi(\mathbf{u})}{\partial \mathbf{u}} \cdot \mathbf{n} & = 0 \quad \text{on } \Gamma_3 \end{cases}$$

Poisson's ratio is computed with

$$\nu_{12} = -\frac{\int_{\Gamma_3} u_2 - \int_{\Gamma_1} u_2}{d_1}$$

where d_1 is the traction imposed at the right boundary and $u_2 = 0$ on Γ_1 because of symmetry conditions

Design lattices with nonlinear elastic law

Nonlinear model

Linear model

$$\Psi(\rho, \mathbf{u}) = \sigma_\rho(\mathbf{u}) : \varepsilon(\mathbf{u}) = \frac{1}{2} \lambda_L (E_{kk})^2 + \mu E_{ij} E_{ij}$$

In our study we have used

$$\Psi(\rho, \mathbf{u}) = \frac{\lambda_L}{2} (J - 1)^2 + \mu E_{ij} E_{ij}$$

to circumvent the drawbacks of the Kirchhoff-St.Venant model under excessive compression (formula (6d) from ref. [2])

Design lattices with nonlinear elastic law

Lagrange method

Lagrange functional:

$$\mathcal{L}(\rho, \mathbf{u}, \boldsymbol{\lambda}) = J(\mathbf{u}) + \int_Y \rho^p \frac{\partial \Psi(\mathbf{u})}{\partial \mathbf{u}} \boldsymbol{\lambda} dY$$

By requiring that the Gateaux derivatives of \mathcal{L} with respect to the variables $\rho, \mathbf{u}, \boldsymbol{\lambda}$ evaluated at the solution $(\hat{\rho}, \hat{\mathbf{u}}, \hat{\boldsymbol{\lambda}})$ vanish for any test function properly chosen, we obtain the state equation , the adjoint equation and the gradient of the cost function.

Design lattices with nonlinear elastic law

State equation

To retrieve the state equation, we imposed

$$\frac{\partial \mathcal{L}}{\partial \lambda} \left(\hat{\rho}, \hat{\mathbf{u}}, \hat{\lambda} \right) \varphi = 0 \quad \forall \varphi \in V$$

Find $\hat{\mathbf{u}} \in V$ such that

$$\int_Y \hat{\rho}^p \frac{\partial \Psi(\hat{\mathbf{u}})}{\partial \mathbf{u}} \varphi dY = 0 \quad \forall \varphi \in V$$

Newton tangent problem

Given $\mathbf{u}^0 \quad \forall k = 0, 1, \dots$ up to convergence, solve:

$$\begin{cases} \frac{\partial}{\partial \mathbf{u}} \left[\int_Y \hat{\rho}^p \frac{\partial \Psi(\mathbf{u}^k)}{\partial \mathbf{u}} \delta \mathbf{u} dY \right] \varphi = - \int_Y \hat{\rho}^p \frac{\partial \Psi(\mathbf{u}^k)}{\partial \mathbf{u}} \mathbf{u}^k \varphi dY \quad \forall \varphi \in V \\ \mathbf{u}^{k+1} = \mathbf{u}^k + \delta \mathbf{u} \end{cases} \quad (4)$$

Design lattices with nonlinear elastic law

Adjoint problem

The adjoint equation in the optimization procedure has been derived imposing $\frac{\partial \mathcal{L}}{\partial \mathbf{u}} \left(\hat{\rho}, \hat{\mathbf{u}}, \hat{\boldsymbol{\lambda}} \right) \psi = 0 \quad \forall \psi \in V$

Dual problem

Find $\hat{\boldsymbol{\lambda}} \in V$ such that

$$\frac{\partial}{\partial \mathbf{u}} \left(\int_Y \rho^p \frac{\partial \psi(\hat{\mathbf{u}})}{\partial \mathbf{u}} \hat{\boldsymbol{\lambda}} dY \right) \psi + \frac{\partial J(\mathbf{u})}{\partial \mathbf{u}} \psi = 0 \quad \forall \psi \in V \quad (5)$$

$$\frac{\partial J(\mathbf{u})}{\partial \mathbf{u}} \psi = \frac{-(\nu_{12} - \nu^*)}{d_1} \int_{\Gamma_3} \psi_2$$

Design lattices with nonlinear elastic law

Gradient of J

Derivative of the Lagrange functional with respect to the control variable:

$$\frac{\partial \mathcal{L}(\hat{\rho}, \hat{\mathbf{u}}, \hat{\boldsymbol{\lambda}})}{\partial \rho} (\hat{\rho}, \hat{\mathbf{u}}, \hat{\boldsymbol{\lambda}}) v = \int_Y p \hat{\rho}^{p-1} v \frac{\partial \Psi(\hat{\mathbf{u}})}{\partial \mathbf{u}} \hat{\boldsymbol{\lambda}} dY \quad (6)$$

Example of possible filter inside IPOPT

$$\bar{\rho} = \frac{\tanh(\beta\eta) + \tanh(\beta(\rho - \eta))}{\tanh(\beta\eta) + \tanh(\beta(1 - \eta))} \quad p \bar{\rho}^{p-1} \frac{\partial \bar{\rho}}{\partial \rho} v = p \bar{\rho}^{p-1} \frac{1}{\tanh(\beta\eta) + \tanh(\beta(1 - \eta))} \frac{\beta}{\cosh(\beta(\hat{\rho} - \eta))^2} v$$

Validation of the model

Poisson's coefficient computation

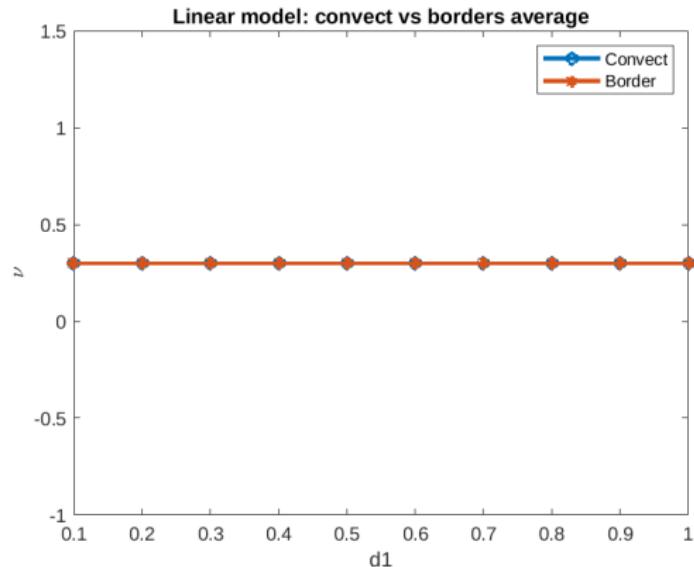
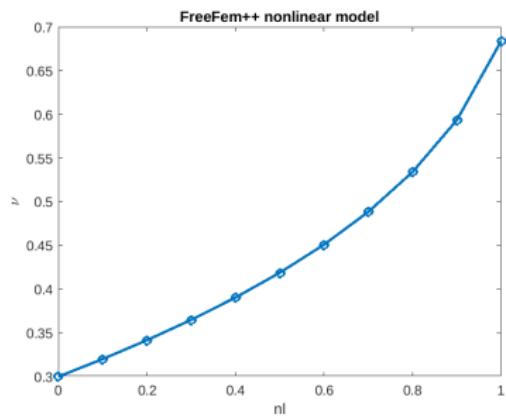


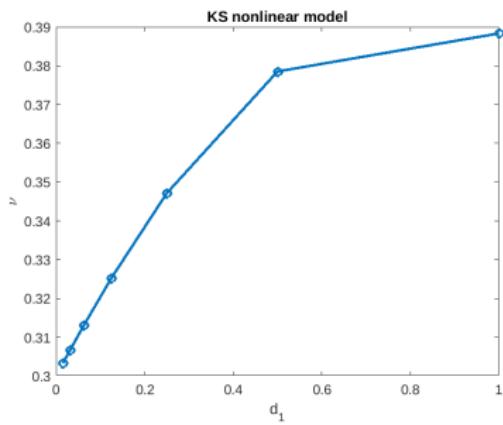
Figure: Check on the linear model for the computation of Poisson's ratio

Validation of the model

Nonlinear models



(a) FreeFem++ nonlinear model



(b) KS nonlinear model

Figure: Check on the nonlinear model

Validation of the model

GradJ and Newton's method

$$\left\| \frac{[F(\mathbf{u} + \varepsilon \mathbf{d}\mathbf{u}) - F(\mathbf{u} - \varepsilon \mathbf{d}\mathbf{u})]}{2\varepsilon} - \text{Jac}(\mathbf{u}) \right\|_{L^\infty} = 9.09059e-08$$

$$\left\| \frac{J(\rho + \varepsilon d\rho) - J(\rho - \varepsilon d\rho)}{2\varepsilon} - \text{gradJ}(\rho) \right\|_{L^\infty} = 7.18473e-12$$

Final algorithm and parameters tuning

Algorithm 3: Final Algorithm

Result: ρ

Input: CTOL, MTOL, maxit, ρ_{\min} , \mathcal{T}_h^0 , α ;

Set: ρ_h^0 , $k \leftarrow 0$, errC $\leftarrow 1 + TOL$

while $errC > TOL$ & $k < maxit$ **do**

1. $p^{k+1} \leftarrow p_{\max} - 2e^{-k/2}$
2. $\rho_h^{k+1} \leftarrow IPOPT(\rho_h^k, \rho_{\min}, Mit = IPOPTmaxiter, tol = IPOPTtol, \dots);$
3. $\rho_h^{k+1} \leftarrow HELMHOLTZ(\rho_h^{k+1}, \tau);$
4. $\mathcal{T}_h^{k+1} \leftarrow adaptmesh(\mathcal{T}_h^k, \rho_h^{k+1}, MTOL, method);$
5. $\rho_h^{k+1} \leftarrow HEAVISIDE(\rho_h^{k+1}, \beta_H);$
6. $\rho_h^{k+1} \leftarrow SIGMUND(\rho_h^{k+1}, \beta = \beta^k, \eta = \eta^k);$
7. $errC \leftarrow |\#\mathcal{T}_h^{k+1} - \#\mathcal{T}_h^k| / \#\mathcal{T}_h^k;$
8. $k \leftarrow k + 1;$

end

Optimized materials obtained

Initial density

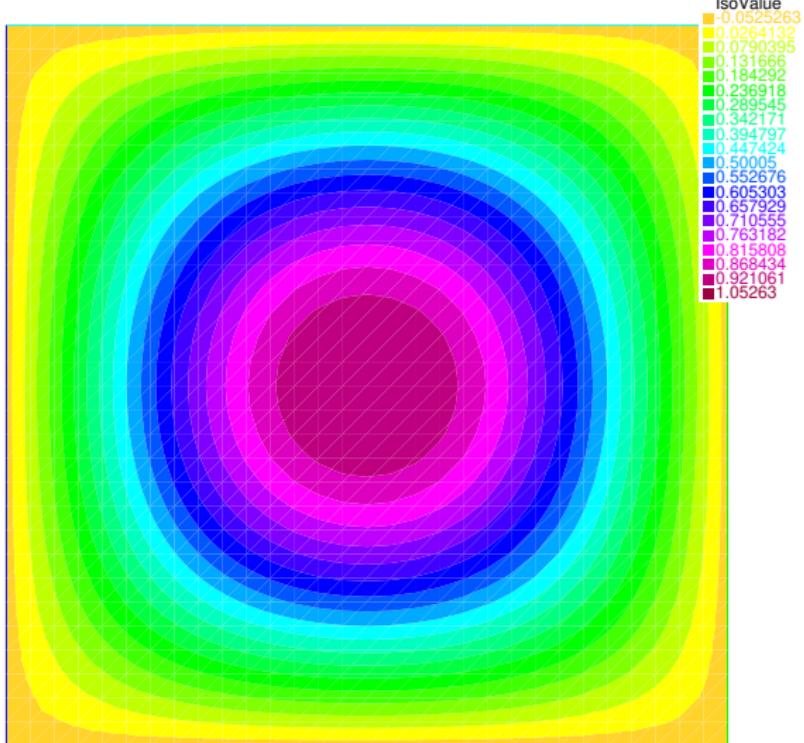


Figure: Initial density

Optimized materials obtained

Density preSig0

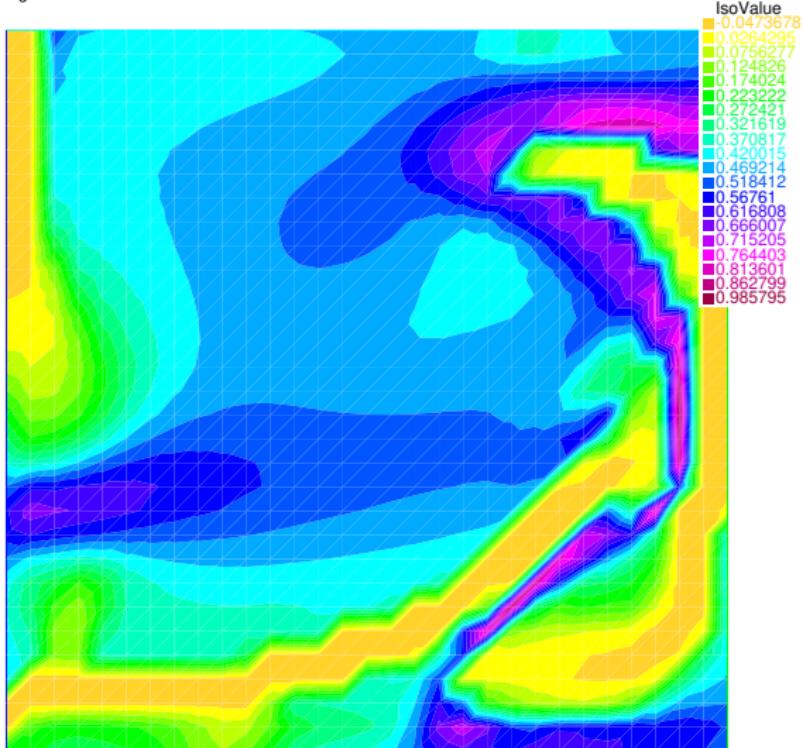
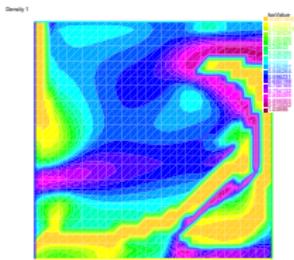
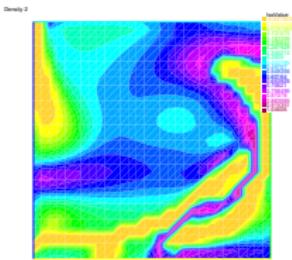


Figure: Density after the first IPOPT cycle

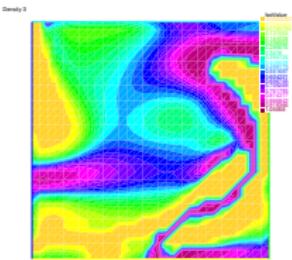
Optimized materials obtained



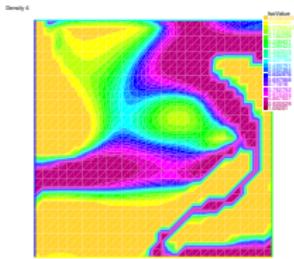
(a) $ii = 1$



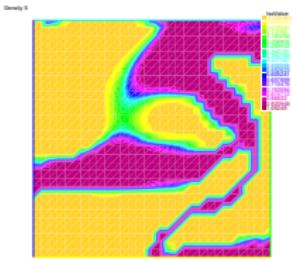
(b) $ii = 2$



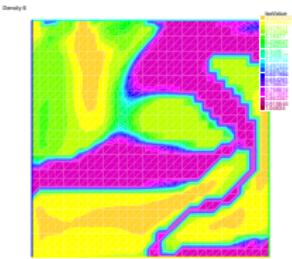
(c) $ii = 3$



(d) $ii = 4$



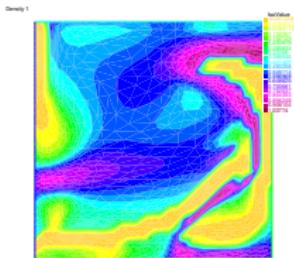
(e) $ii = 5$



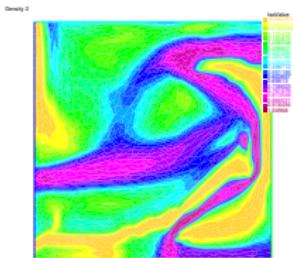
(f) $ii = 6$

Figure: Structure with increasing Sigmund filters parameters

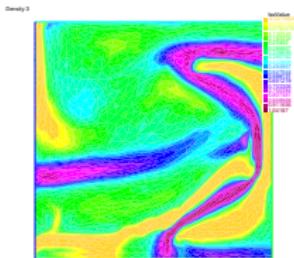
Optimized materials obtained



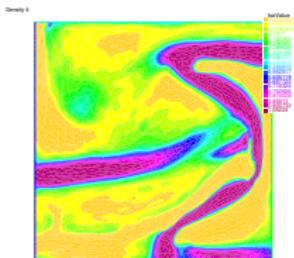
(a) $\text{ii} = 1$



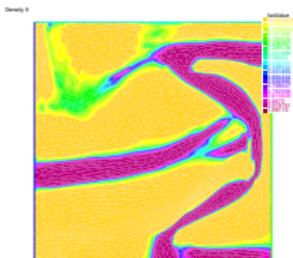
(b) $\text{ii} = 2$



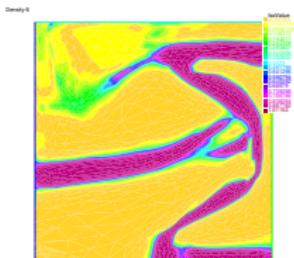
(c) $\text{ii} = 3$



(d) $\text{ii} = 4$



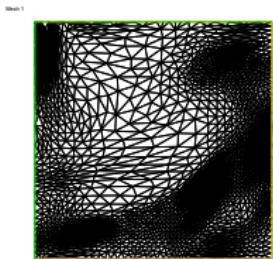
(e) $\text{ii} = 5$



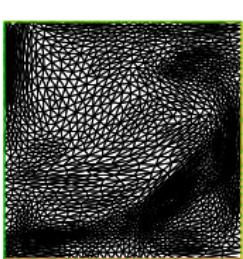
(f) $\text{ii} = 6$

Figure: Structure with increasing Sigmund filters parameters and grid adaptation

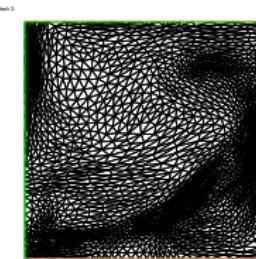
Optimized materials obtained



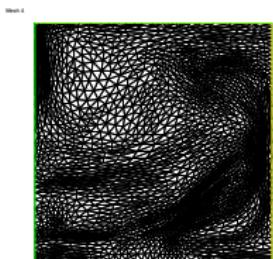
(a) $\text{ii} = 1$



(b) $\text{ii} = 2$



(c) $\text{ii} = 3$



(d) $\text{ii} = 4$



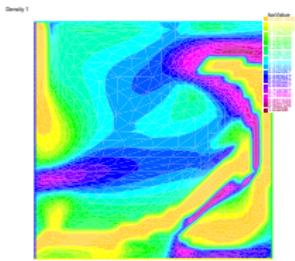
(e) $\text{ii} = 5$



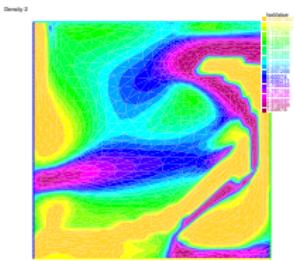
(f) $\text{ii} = 6$

Figure: Mesh of structures with increasing Sigmund filters parameters and grid adaptation

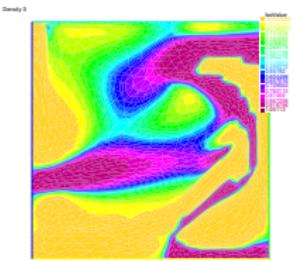
Optimized materials obtained



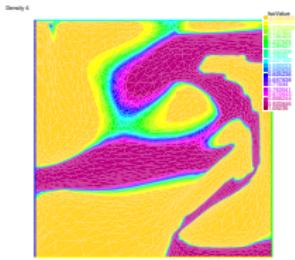
(a) $\text{ii} = 1$



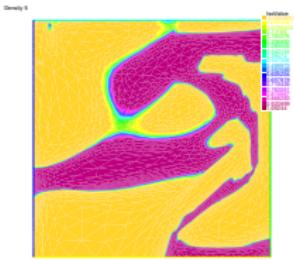
(b) $\text{ii} = 2$



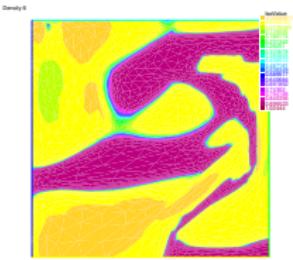
(c) $\text{ii} = 3$



(d) $\text{ii} = 4$



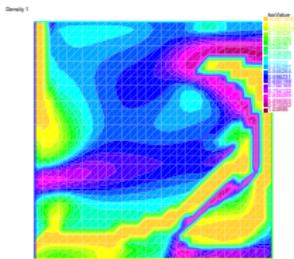
(e) $\text{ii} = 5$



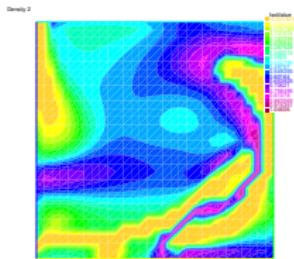
(f) $\text{ii} = 6$

Figure: Structure with fixed $\eta = 0.5$ and grid adaptation

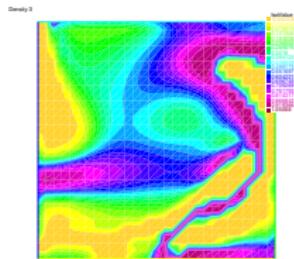
Optimized materials obtained



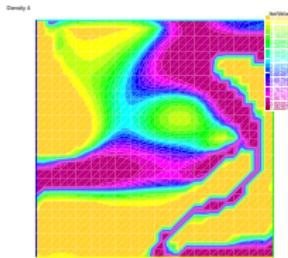
(a) $ii = 1$



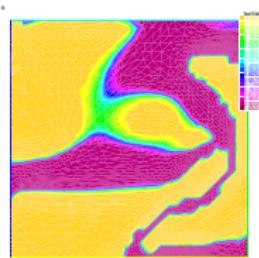
(b) $ii = 2$



(c) $ii = 3$



(d) $ii = 4$

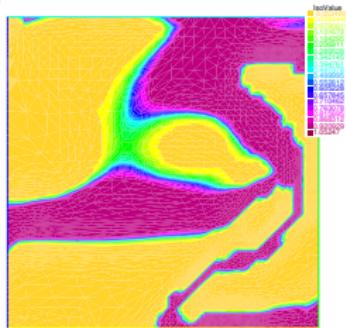


(e) $ii = 5$

Figure: Final structure optimization

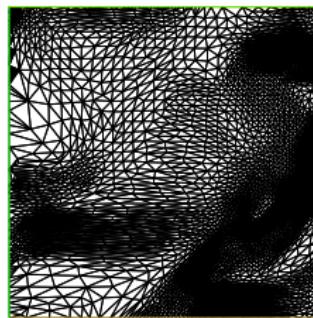
Conclusions

Density 5



(a) Final structure

Mesh 5



(b) Final mesh

Figure: Final structure and mesh

Conclusions

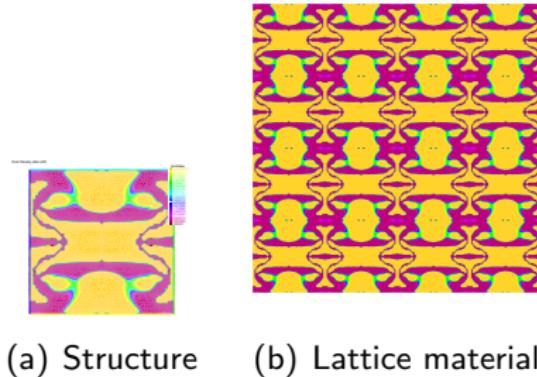


Figure: Reflected (2×2) final structure and lattice material

- Poisson's ratio computed on 2×2 cells: $\nu = -1.35916$
- Model reliability validated
- Big issue of parameters tuning: problem specific
- Future studies: extend to other TO problems and to 3D setting

Essential bibliography

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