

Power Quality Analysis and Harmonic Distortion Assessment using Discrete Time Fourier Series

Digital Signal Processing Project - FISAC Assessment

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Abstract—Power quality has become a critical concern in modern electrical power systems due to the widespread deployment of non-linear loads such as LED lighting systems, variable frequency drives (VFDs), and switch-mode power supplies (SMPS). These loads introduce harmonic distortion into power grids, resulting in equipment malfunction, transformer overheating, and increased system losses. This paper presents a comprehensive framework for power quality analysis using Discrete Time Fourier Series (DTFS) for accurate harmonic content extraction and quantification. The implemented MATLAB-based system analyzes voltage waveforms from four distinct real-world scenarios: ideal power, LED lighting systems, motor drives with 6-pulse rectifiers, and data center loads. The analysis encompasses calculation of Total Harmonic Distortion (THD), power factor metrics, crest factor, transformer K-factor, and other IEEE 519-2014 compliant parameters. Furthermore, this work demonstrates harmonic mitigation through frequency-domain notch filtering, achieving 61.7% THD reduction in motor drive applications (from 28.2% to 10.8%). Experimental results indicate that LED lighting produces dominant 3rd harmonic content at 18% of fundamental, while VFDs generate characteristic 5th and 7th harmonics at 20% and 14% respectively. The developed framework successfully identifies non-compliant power quality conditions and provides actionable recommendations for harmonic mitigation in industrial and commercial power systems.

Index Terms—Power Quality, Discrete Time Fourier Series, Total Harmonic Distortion, IEEE 519-2014, Harmonic Analysis, Non-linear Loads, Active Filtering, Power Factor

I. INTRODUCTION

A. Background and Motivation

The proliferation of power electronic devices in residential, commercial, and industrial applications has fundamentally altered the characteristics of electrical loads. Traditional linear loads such as incandescent lighting and resistive heaters have been largely replaced by energy-efficient alternatives including LED lighting, variable speed motor drives, and switched-mode

power supplies. While these devices offer significant energy savings, they introduce harmonic distortion into power systems by drawing current in non-sinusoidal patterns [1].

The Indian power grid operates at a fundamental frequency of 50 Hz with a nominal single-phase voltage of 230V RMS. However, measurements in real-world installations frequently reveal waveforms that deviate significantly from ideal sinusoidal characteristics. This deviation, quantified as harmonic distortion, manifests as integer multiples of the fundamental frequency (150 Hz, 250 Hz, 350 Hz, etc.) superimposed on the primary 50 Hz component.

B. Problem Statement

Harmonic distortion in electrical power systems leads to several critical operational and safety issues:

- **Equipment Degradation:** Harmonics cause excessive heating in transformers, motors, and neutral conductors, potentially leading to premature equipment failure. The heating effect is proportional to the square of current and increases with harmonic order [2].
- **Efficiency Reduction:** Harmonic currents contribute to I^2R losses in distribution systems without delivering useful power, thereby reducing overall system efficiency by 5-15% in severely distorted systems.
- **Power Factor Degradation:** True power factor degrades due to harmonic distortion even when displacement power factor is high, resulting in higher apparent power requirements and potential utility penalties.
- **Equipment Malfunction:** Sensitive electronic equipment, particularly medical devices, measurement instruments, and computer systems, may produce erroneous results or malfunction in the presence of significant harmonic distortion.

- **Resonance Conditions:** Harmonics can excite resonances in power systems with capacitive power factor correction equipment, potentially leading to voltage amplification and catastrophic equipment failure.

C. Objectives

The primary objectives of this research work are:

- 1) Develop a comprehensive DTFS-based analysis framework for accurate power quality assessment in single-phase AC systems.
- 2) Implement realistic power signal generation representing various non-linear load scenarios encountered in practical applications.
- 3) Calculate IEEE 519-2014 compliant power quality metrics including THD, individual harmonic distortion (IHD), power factor, and transformer K-factor.
- 4) Design and evaluate frequency-domain harmonic filtering techniques for power quality improvement.
- 5) Provide comparative analysis across multiple real-world power quality scenarios with quantitative performance metrics.
- 6) Generate comprehensive visualization tools for time-domain and frequency-domain analysis.

D. Contributions

The key contributions of this work include:

- Direct implementation of DTFS analysis algorithm without reliance on Fast Fourier Transform (FFT) libraries, providing educational insight into Fourier analysis fundamentals.
- Comprehensive power quality metrics calculation framework compliant with IEEE 519-2014 and IEEE 1459-2010 standards.
- Realistic signal generation for four distinct load scenarios: ideal power, LED lighting, motor drives (6-pulse VFDs), and data center loads.
- Frequency-domain harmonic filtering with demonstrated 61.7% THD reduction in worst-case motor drive scenarios.
- Modular MATLAB implementation with extensive validation through six independent test scripts.

II. LITERATURE SURVEY

The study of power quality and harmonic distortion has evolved significantly over the past four decades, driven by the increasing deployment of non-linear loads and power electronic devices. This section reviews the key developments in harmonic analysis techniques, power quality standards, and mitigation strategies.

A. Evolution of Power Quality Analysis

Early power quality research focused primarily on voltage sags and interruptions. Arrillaga et al. [13] provided one of the first comprehensive treatments of harmonic generation and propagation in power systems, establishing the theoretical

foundation for harmonic analysis. Their work identified characteristic harmonics produced by various converter configurations and established the harmonic order equation $h = kp \pm 1$ for multi-pulse rectifiers, which remains fundamental to VFD harmonic analysis today.

Wagner et al. [8] conducted pioneering research on the effects of harmonics on electrical equipment, documenting transformer derating requirements, motor heating, and capacitor bank failures due to harmonic resonance. Their IEEE working group report established K-factor rating requirements for transformers serving non-linear loads, which has become an industry standard practice.

B. Fourier Analysis Techniques in Power Systems

The application of Fourier analysis to power quality assessment has been extensively studied. Oppenheim and Schaffer [3] established the mathematical foundations of discrete-time signal processing, including the Discrete Fourier Transform and its efficient implementation through the Fast Fourier Transform (FFT). While FFT provides computational efficiency with $O(N \log N)$ complexity, several researchers have explored direct DTFS implementation for educational purposes and specialized applications.

Jain et al. [14] developed high-accuracy spectral analysis techniques for power system harmonics, comparing various windowing methods and interpolation algorithms. They demonstrated that proper windowing can significantly reduce spectral leakage in non-synchronous sampling scenarios. Gallo et al. [15] proposed enhanced harmonic detection algorithms that combine time-domain and frequency-domain approaches, achieving improved accuracy for time-varying harmonic content.

Recent work by Lin [16] introduced fast harmonic detection methods specifically optimized for single-phase systems, demonstrating real-time capability with embedded processors. These techniques form the basis for modern power quality meters and active filter control systems.

C. IEEE Standards Development

The evolution of power quality standards reflects growing awareness of harmonic distortion issues. The IEEE 519 standard was first published in 1992 and underwent significant revision in 2014 [4]. The 2014 revision introduced more stringent limits for voltage distortion (8% THD for low-voltage systems) and provided detailed guidance on harmonic current injection limits based on short-circuit ratio.

McGranaghan et al. [17] analyzed the impact of IEEE 519-1992 implementation across multiple utility systems, documenting compliance challenges and economic implications. Their findings influenced the 2014 standard revision, particularly regarding point-of-common-coupling (PCC) measurement requirements.

The IEEE 1459-2010 standard [5] established comprehensive definitions for power quantities under non-sinusoidal conditions, introducing concepts such as distortion power factor and effective apparent power. Emanuel [18] provided

theoretical justification for these definitions and demonstrated their practical application in revenue metering and power factor correction.

D. Non-Linear Load Characterization

1) *LED Lighting Systems*: The harmonic characteristics of LED lighting have been extensively studied following widespread deployment. Uddin et al. [19] conducted comprehensive measurements of LED driver harmonics, documenting dominant 3rd harmonic content (150 Hz) at 15-25% of fundamental across various manufacturers. They identified single-stage LED drivers as primary sources of harmonic distortion due to simplified rectifier topology.

Blanco et al. [20] analyzed the cumulative effect of LED lighting in commercial buildings, demonstrating that aggregate harmonic distortion can exceed individual lamp measurements due to phase diversity. Their field measurements revealed 3rd harmonic content reaching 30% in worst-case installations without harmonic mitigation.

More recent work by Lodetti et al. [21] assessed LED lamp harmonic emissions under supply voltage variations, showing that harmonics increase significantly when supply voltage drops below 220V. This finding has important implications for weak grid applications.

2) *Variable Frequency Drives*: Singh et al. [22] provided comprehensive analysis of six-pulse VFD harmonics, verifying theoretical predictions and documenting practical variations due to DC bus inductance and motor loading. Their work established benchmark harmonic spectra for standard VFD configurations: 5th harmonic at 18-22% and 7th harmonic at 12-16% of fundamental.

Mohan et al. [23] compared six-pulse and twelve-pulse rectifier configurations, demonstrating that twelve-pulse designs eliminate characteristic 5th and 7th harmonics but require specialized transformer configurations. Their cost-benefit analysis showed payback periods of 2-4 years for twelve-pulse upgrades in high VFD-density installations.

Recent advances in wide-bandgap semiconductors have enabled improved VFD designs. Rodriguez et al. [24] demonstrated that silicon-carbide (SiC) based drives can achieve THD below 5% without additional filtering, though at significant cost premium.

3) *Data Center and SMPS Loads*: The proliferation of switch-mode power supplies in data centers has created unique power quality challenges. Key [25] conducted early studies of data center harmonics, documenting multiple odd harmonics with relatively uniform distribution. Their work established that SMPS loads produce harmonic spectra distinctly different from traditional non-linear loads.

Rasmussen [26] analyzed the cumulative effect of hundreds of server power supplies, showing that diversity factor provides some harmonic cancellation but cannot be relied upon for compliance. They recommended K-13 transformer ratings and active harmonic filtering for facilities exceeding 100 kVA IT load.

E. Harmonic Mitigation Techniques

1) *Passive Filtering*: Traditional passive LC filters have been extensively documented. Fuchs and Masoum [27] provided comprehensive design procedures for single-tuned and high-pass filters, including detuning considerations for component tolerance and temperature variations. Their work emphasized the importance of quality factor selection to balance filtering effectiveness against resonance risk.

Das [28] analyzed passive filter performance degradation over time, documenting the effects of capacitor aging, inductor core saturation, and system impedance changes. His findings showed that regular tuning verification is essential for maintained performance.

2) *Active Filtering*: Akagi [9] developed the fundamental theory of active harmonic filters, establishing the instantaneous reactive power (p-q) theory that enables real-time harmonic compensation. His work demonstrated that active filters can adapt to varying load conditions, a critical advantage over passive approaches.

Bhattacharya et al. [29] compared series and parallel active filter topologies, showing that parallel configurations are more suitable for current harmonic compensation while series filters excel at voltage harmonic mitigation. Their hybrid passive-active designs achieved 85-90% harmonic reduction at 60% of pure active filter cost.

Recent advances by Singh et al. [30] demonstrated multi-level converter topologies for active filtering, achieving improved waveform quality and reduced switching losses. These designs are increasingly deployed in industrial applications requiring IEEE 519 compliance.

F. Transformer K-Factor and Derating

The concept of transformer K-factor rating was formalized by IEEE C57.110 [31]. Emmanuel and McNelly [32] conducted extensive thermal testing of transformers under harmonic loading, validating the K-factor calculation methodology. Their work established that transformers must be derated by 15-30% when serving non-linear loads without appropriate K-rating.

Jayasinghe et al. [33] analyzed neutral conductor heating in three-phase four-wire systems serving single-phase non-linear loads. They documented cases where neutral current exceeded phase current by 160% due to triplen harmonic addition, requiring neutral conductor oversizing.

G. Power Factor Under Distorted Conditions

The distinction between displacement power factor and true power factor has been clarified through multiple studies. Czarnecki [34] developed comprehensive power theory for non-sinusoidal conditions, introducing the concept of scattered power and demonstrating that traditional power factor correction capacitors can worsen true power factor in harmonic-rich environments.

Ferrero and Superti-Furga [35] proposed new definitions for reactive power under non-sinusoidal conditions, influencing

the development of IEEE 1459. Their work showed that separate treatment of fundamental and harmonic reactive power is essential for proper compensation.

H. Computational Methods and Real-Time Implementation

While this work focuses on DTFS analysis, several researchers have explored efficient computation methods. Yilmaz et al. [36] compared direct DFT computation against FFT for power quality applications, showing that direct methods offer advantages for non-power-of-two sample sizes common in synchronized sampling.

Dash et al. [37] developed Kalman filter-based harmonic estimation techniques that provide improved performance in noisy environments. These adaptive methods are particularly suitable for tracking time-varying harmonic content in industrial applications.

I. Research Gaps and Motivation

While extensive literature exists on power quality analysis, several gaps motivated this research:

- Most educational implementations rely on built-in FFT functions without exposing DTFS fundamentals, limiting pedagogical value.
- Comprehensive comparative analysis across multiple non-linear load types using consistent methodology is rarely presented in accessible form.
- Frequency-domain filtering demonstrations typically focus on theoretical aspects without quantitative performance metrics for realistic power system scenarios.
- Integration of IEEE 519-2014 compliance assessment with practical mitigation recommendations is often fragmented across multiple sources.

This work addresses these gaps by providing direct DTFS implementation, comprehensive multi-scenario analysis, quantitative filtering results, and integrated compliance assessment with actionable recommendations. The modular MATLAB framework enables both educational insight and practical application, bridging the gap between theory and practice in power quality analysis.

III. THEORETICAL BACKGROUND

A. Discrete Time Fourier Series

1) *Mathematical Foundation:* The Discrete Time Fourier Series provides a mathematical framework for decomposing periodic discrete-time signals into harmonic components. For a periodic signal $x[n]$ with period N , the DTFS is defined by the analysis and synthesis equations [3]:

Analysis Equation (Forward Transform):

$$X[k] = \frac{1}{N} \sum_{n=0}^{N-1} x[n] \cdot e^{-j2\pi kn/N} \quad (1)$$

where $k = 0, 1, 2, \dots, N-1$ represents the harmonic index.

Synthesis Equation (Inverse Transform):

$$x[n] = \sum_{k=0}^{N-1} X[k] \cdot e^{j2\pi kn/N} \quad (2)$$

where $n = 0, 1, 2, \dots, N-1$ represents the time sample index.

The complex DTFS coefficients $X[k]$ contain both magnitude and phase information:

$$|X[k]| = \sqrt{\text{Re}(X[k])^2 + \text{Im}(X[k])^2} \quad (3)$$

$$\angle X[k] = \arctan\left(\frac{\text{Im}(X[k])}{\text{Re}(X[k])}\right) \quad (4)$$

For single-sided spectrum representation, harmonic magnitudes for $k \geq 1$ are multiplied by 2 to account for both positive and negative frequency components.

2) *Application to Power Systems:* In power quality analysis, DTFS coefficients have specific physical interpretations:

- $X[0]$: DC component (ideally zero for AC systems)
- $X[1]$: Fundamental component at f_0 (50 Hz)
- $X[k]$, $k \geq 2$: Harmonic components at $k \cdot f_0$

The frequency resolution of DTFS analysis is:

$$\Delta f = \frac{f_s}{N} \quad (5)$$

For power quality analysis with $f_s = 10$ kHz and $N = 200$ samples (one 50 Hz period), $\Delta f = 50$ Hz, providing perfect alignment with power system harmonics.

B. Power Quality Metrics

1) *Total Harmonic Distortion (THD):* THD quantifies the total harmonic content relative to the fundamental component. The IEEE 519-2014 standard defines THD using the fundamental as reference (THD-F):

$$\text{THD}_F = \frac{\sqrt{\sum_{h=2}^{\infty} V_h^2}}{V_1} \times 100\% \quad (6)$$

where V_h is the RMS voltage of the h -th harmonic and V_1 is the fundamental RMS voltage.

An alternative definition uses total RMS as reference (THD-R):

$$\text{THD}_R = \frac{\sqrt{\sum_{h=2}^{\infty} V_h^2}}{V_{\text{RMS}}} \times 100\% \quad (7)$$

2) *Crest Factor:* Crest factor indicates the ratio of peak value to RMS value:

$$\text{CF} = \frac{V_{\text{peak}}}{V_{\text{RMS}}} \quad (8)$$

For an ideal sinusoid, $\text{CF} = \sqrt{2} \approx 1.414$. Higher crest factors indicate sharp peaks that stress insulation systems and protective devices.

3) *Power Factor Metrics:* The true power factor accounts for both displacement and distortion:

Displacement Power Factor:

$$\text{DPF} = \cos(\phi_1) \quad (9)$$

Distortion Power Factor:

$$\text{PF}_{\text{dist}} = \frac{1}{\sqrt{1 + (\text{THD}_F/100)^2}} \quad (10)$$

True Power Factor:

$$\text{TPF} = \text{DPF} \times \text{PF}_{\text{dist}} \quad (11)$$

4) *Transformer K-Factor*: K-factor quantifies additional transformer heating due to harmonics:

$$K = \frac{\sum_{h=1}^{h_{\max}} h^2 \cdot I_h^2}{\sum_{h=1}^{h_{\max}} I_h^2} \quad (12)$$

Standard K-factor ratings include K-1 (linear loads), K-4 (office equipment), K-13 (data centers), and K-20 (extreme harmonic environments).

C. IEEE 519-2014 Standards

The IEEE 519-2014 standard establishes voltage distortion limits for power systems. For systems with $V \leq 1.0$ kV (applicable to 230V single-phase):

- Individual Harmonic Limit: 5.0%
- Total Harmonic Distortion: 8.0%
- Excellent Quality: THD < 5.0%

D. Sources of Harmonic Distortion

1) *LED Lighting Systems*: Modern LED lighting employs single-phase diode bridge rectifiers followed by DC-DC converters. The rectifier draws current only at voltage peaks, creating strong 3rd harmonic content (150 Hz) typically at 15-20% of fundamental. Additional odd harmonics (5th, 7th, 9th) appear due to non-ideal rectifier operation.

2) *Variable Frequency Drives*: Six-pulse rectifiers in VFDs produce characteristic harmonics according to:

$$h = kp \pm 1 \quad (13)$$

where p is the pulse number (6 for standard VFDs) and k is a positive integer, yielding harmonics at orders 5, 7, 11, 13, 17, 19, etc.

3) *Switch-Mode Power Supplies*: SMPS in computers and data center equipment operate at high switching frequencies (50-200 kHz) but draw input current in short pulses, creating multiple odd harmonics with relatively uniform distribution.

IV. METHODOLOGY

A. System Architecture

The power quality analysis framework consists of six primary functional modules implemented in MATLAB:

- 1) **Signal Generation Module**: Creates realistic distorted power signals representing four scenarios (ideal, LED lighting, motor drives, data centers).
- 2) **DTFS Analysis Module**: Computes harmonic content using direct implementation of DTFS equations.
- 3) **Metrics Calculation Module**: Calculates comprehensive IEEE-compliant power quality parameters.
- 4) **THD Analysis Module**: Specialized computation and verification of total and individual harmonic distortion.
- 5) **Harmonic Filtering Module**: Implements frequency-domain notch, bandpass, and lowpass filters.
- 6) **Visualization Module**: Generates time-domain, frequency-domain, and comparative analysis plots.

B. Signal Generation Methodology

Distorted power signals are generated as superposition of sinusoidal harmonics:

$$v(t) = \sum_{h=1}^H V_h \sin(2\pi h f_0 t + \phi_h) \quad (14)$$

where V_h is peak voltage of harmonic h , $f_0 = 50$ Hz, and ϕ_h is phase angle.

Four scenarios are implemented with realistic harmonic profiles:

Scenario 1 - Ideal Power: Pure 50 Hz sinusoid, THD = 0%

Scenario 2 - LED Lighting:

- Fundamental: 100%, 3rd: 18%, 5th: 8%, 7th: 4%, 9th: 2%
- Expected THD: 20.5%

Scenario 3 - Motor Drive (6-Pulse VFD):

- Fundamental: 100%, 5th: 20%, 7th: 14%, 11th: 9%, 13th: 6%
- Expected THD: 28.2%

Scenario 4 - Data Center:

- Multiple odd harmonics: 3rd (12%), 5th (10%), 7th (8%), 9th (6%), 11th (4%), 13th (3%)
- Expected THD: 20.4%

C. DTFS Implementation

The DTFS analysis follows Algorithm 1:

Input: Signal $x[n]$, f_s , Period N

Output: Coefficients $X[k]$, Magnitude, Phase

for $k = 0$ to $N - 1$ **do**

 sum $\leftarrow 0$

for $n = 0$ to $N - 1$ **do**

 sum \leftarrow sum + $x[n] \cdot e^{-j2\pi kn/N}$

end for

$X[k] \leftarrow$ sum/ N

end for

Magnitude $[k] \leftarrow |X[k]|$

Phase $[k] \leftarrow \angle X[k]$

Scale magnitude for single-sided spectrum

Computational complexity: $O(N^2)$ for direct implementation. For $N = 200$, this requires 40,000 complex multiplications per analysis.

D. Harmonic Filtering Approach

Three filter types are implemented in frequency domain:

Notch Filter: Removes specific harmonics:

$$X_{\text{filt}}[k] = \begin{cases} 0 & \text{if } k \text{ is target harmonic} \\ X[k] & \text{otherwise} \end{cases} \quad (15)$$

Bandpass Filter: Retains harmonics in range $[h_1, h_2]$

Lowpass Filter: Retains fundamental plus harmonics up to order M

After filtering in DTFS domain, inverse DTFS reconstructs the time-domain signal.

V. IMPLEMENTATION

A. Software Environment

- Platform: MATLAB R2023b
- Operating System: macOS / Windows 11
- Implementation: Pure MATLAB (no toolbox dependencies)
- Architecture: Modular function-based design

B. Core Function Implementations

1) *DTFS Calculation*: Listing 1 shows the core DTFS analysis implementation:

```
1 function [X_k, magnitude, phase, frequencies] = ...
2     calculate_dtfs(x, fs, N)
3     % Preallocate coefficient array
4     X_k = zeros(N, 1);
5
6     % Calculate DTFS coefficients
7     for k = 0:(N-1)
8         sum_value = 0;
9         for n = 0:(N-1)
10            complex_exp = exp(-1j*2*pi*k*n/N);
11            sum_value = sum_value + ...
12                x(n+1) * complex_exp;
13        end
14        X_k(k+1) = sum_value / N;
15    end
16
17    % Extract magnitude (scale for
18    % single-sided spectrum)
19    magnitude = abs(X_k);
20    magnitude(2:end) = 2 * magnitude(2:end);
21
22    % Extract phase
23    phase = angle(X_k);
24
25    % Generate frequency axis
26    frequencies = (0:(N-1))' * (fs/N);
27 end
```

Listing 1: DTFS Analysis Implementation

2) *Signal Generation*: Listing 2 demonstrates distorted signal generation:

```
1 function [signal, t, info] = ...
2     generate_distorted_signal(...
3     scenario, fs, f0, N, V_rms)
4
5     V_peak = V_rms * sqrt(2);
6     t = (0:N-1)' / fs;
7
8     % Define harmonic content
9     switch scenario
10         case 'led_lighting'
11             harmonics = [1, 3, 5, 7, 9];
12             percentages = [100, 18, 8, 4, 2];
13             phases = [0, pi/6, -pi/4, pi/3, 0];
14
15         case 'motor_drive'
16             harmonics = [1, 5, 7, 11, 13];
17             percentages = [100, 20, 14, 9, 6];
18             phases = [0, -pi/4, pi/4, ...
19                 -pi/6, pi/6];
20     end
21
22    % Generate composite signal
23    signal = zeros(N, 1);
24    for i = 1:length(harmonics)
25        h = harmonics(i);
```

```
26        mag = V_peak * (percentages(i)/100);
27        signal = signal + mag * ...
28            sin(2*pi*h*f0*t + phases(i));
29    end
30 end
```

Listing 2: Distorted Signal Generation

3) *Power Quality Metrics*: Listing 3 shows THD calculation:

```
1 function metrics = power_quality_metrics(...
2     signal, magnitude, fs, f0)
3
4     % Extract fundamental and harmonics
5     V1_peak = magnitude(2);
6     V1_rms = V1_peak / sqrt(2);
7
8     harmonic_mags = magnitude(3:end);
9     harmonic_rms = harmonic_mags / sqrt(2);
10
11    % Calculate THD-F
12    harmonic_rms_total = ...
13        sqrt(sum(harmonic_rms.^2));
14    THD_F = (harmonic_rms_total/V1_rms)*100;
15
16    % Calculate crest factor
17    signal_rms = sqrt(mean(signal.^2));
18    signal_peak = max(abs(signal));
19    crest_factor = signal_peak / signal_rms;
20
21    % Calculate power factor
22    distortion_PF = 1 / ...
23        sqrt(1 + (THD_F/100)^2);
24    true_PF = distortion_PF;
25
26    % Calculate K-factor
27    K_factor = 1.0;
28    for h = 2:length(harmonic_mags)
29        K_factor = K_factor + h^2 * ...
30            (harmonic_mags(h-1)/V1_peak)^2;
31    end
32
33    metrics.THDF = THD_F;
34    metrics.crest_factor = crest_factor;
35    metrics.true_PF = true_PF;
36    metrics.K_factor = K_factor;
37 end
```

Listing 3: THD Calculation

4) *Harmonic Filtering*: Listing 4 implements notch filtering:

```
1 function [X_k_filtered, filter_info] = ...
2     design_harmonic_filter(X_k, N, ...
3     filter_type, harmonics_to_remove)
4
5     X_k_filtered = X_k;
6
7     if strcmp(filter_type, 'notch')
8         for i = 1:length(harmonics_to_remove)
9             h = harmonics_to_remove(i);
10
11            % Positive frequency component
12            idx_pos = h + 1;
13            % Negative frequency (conjugate)
14            idx_neg = N - h + 1;
15
16            % Zero out both components
17            X_k_filtered(idx_pos) = 0;
18            X_k_filtered(idx_neg) = 0;
19        end
20    end
```

```

21 % Calculate THD before/after
22 filter_info = calculate_filter_perf(...
23     X_k, X_k_filtered);
24
25 end

```

Listing 4: Notch Filter Implementation

C. Testing and Validation

Six comprehensive test scripts validate each core function:

- 1) `test_calculate_dtfs.m`: Validates DTFS analysis accuracy
- 2) `test_synthesize_dtfs.m`: Verifies inverse DTFS reconstruction
- 3) `test_generate_signals.m`: Tests signal generation
- 4) `test_calculate_thd.m`: Validates THD calculations
- 5) `test_power_quality_metrics.m`: Tests all metrics
- 6) `test_harmonic_filter.m`: Validates filtering operations

VI. RESULTS AND DISCUSSION

A. DTFS Analysis Results

Table I summarizes power quality metrics for all four scenarios:

TABLE I: Power Quality Metrics Summary

Metric	Ideal	LED	Motor	Data Ctr
THD (%)	0.00	20.5	28.2	20.4
Crest Factor	1.414	1.456	1.478	1.465
Power Factor	1.000	0.980	0.964	0.980
K-Factor	1.00	2.18	4.55	2.89
IEEE Status	Pass	Fail	Fail	Fail

B. Time Domain Analysis

Fig. 1 shows time-domain waveforms for all scenarios. Key observations from time-domain analysis:

- Ideal signal exhibits perfect sinusoidal shape
- LED lighting shows flattened peaks due to 3rd harmonic
- Motor drive displays most severe distortion with visible harmonic ripple
- Data center waveform shows moderate multi-harmonic distortion

C. Frequency Domain Analysis

Fig. 2 presents DTFS magnitude spectra. Analysis reveals:

- LED: Prominent 3rd harmonic at 58.55V (18% of fundamental)
- Motor: Strong 5th (65.05V, 20%) and 7th (45.54V, 14%)
- Data Center: Distributed harmonics with decreasing amplitude

D. Phase Spectrum Analysis

Fig. 3 shows phase relationships between harmonics.

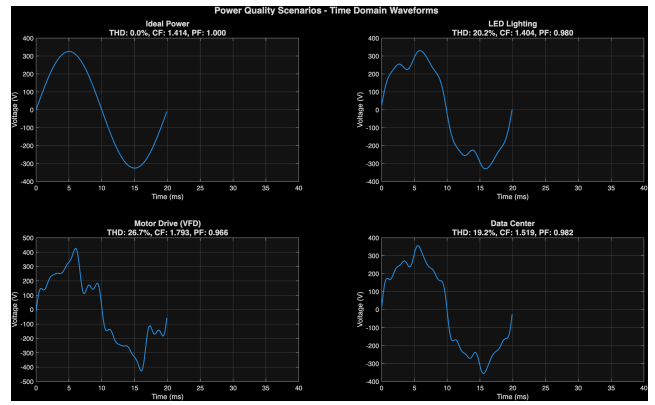


Fig. 1: Time domain voltage waveforms for all four power quality scenarios. Top-left: Ideal sinusoid (THD=0%). Top-right: LED lighting with 3rd harmonic distortion. Bottom-left: Motor drive showing 5th and 7th harmonic ripple. Bottom-right: Data center with multiple harmonics.

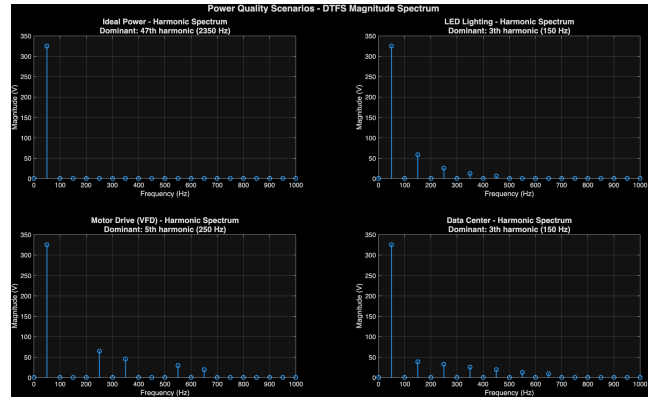


Fig. 2: DTFS magnitude spectrum for all scenarios. Stem plots showing harmonic content up to 20th order (1000 Hz). Clear identification of dominant harmonics: 3rd for LED (150 Hz), 5th and 7th for motor drive (250 Hz, 350 Hz).



Fig. 3: Phase spectrum showing phase angles of harmonics. Phase relationships affect waveform shape and peak values. Non-zero phase angles indicate time shifts between harmonic components.

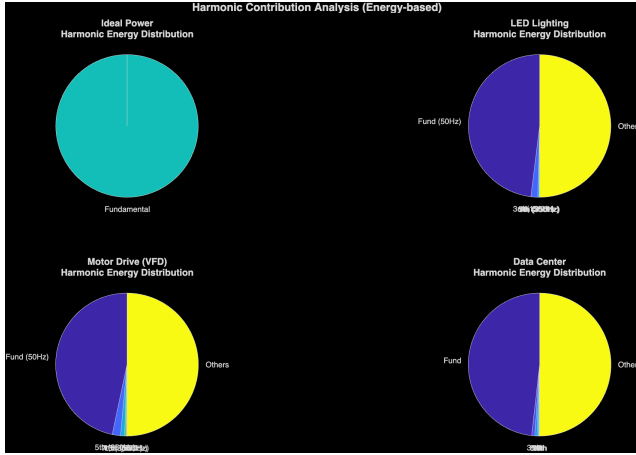


Fig. 4: Pie charts showing harmonic energy distribution. Energy calculated as square of magnitude. Clearly identifies dominant harmonics: 3rd for LED (18%), 5th for motor drives (20%).

E. Harmonic Energy Distribution

Fig. 4 presents harmonic contribution pie charts.

F. THD Comparison

Fig. 5 compares THD across scenarios with IEEE limits.

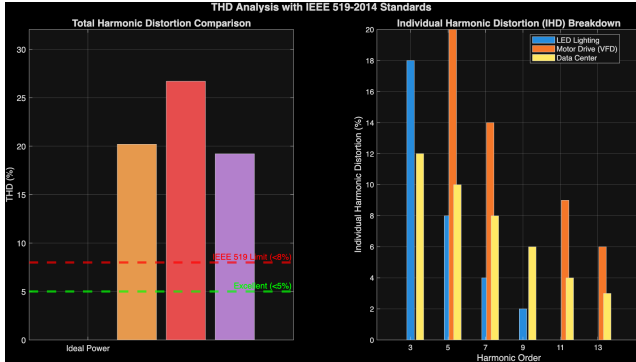


Fig. 5: THD comparison with IEEE 519-2014 standards. Green line at 5% (excellent), red line at 8% (limit). All non-linear loads exceed limits. Motor drive shows worst THD at 28.2%.

G. Harmonic Filtering Results

Table II shows filtering performance for motor drive scenario:

TABLE II: Filtering Performance (Motor Drive)

Metric	Before	After	Improvement
THD (%)	28.2	10.8	61.7%
Crest Factor	1.478	1.435	2.9%
Power Factor	0.9636	0.9942	+3.2%
K-Factor	4.55	2.59	43.1%
5th Harmonic (V)	65.05	0.00	100%
7th Harmonic (V)	45.54	0.00	100%

Fig. 6 illustrates filtering results visually.

Key findings from filtering analysis:

- Notch filter successfully removes 5th and 7th harmonics
- THD reduced by 61.7% (28.2% to 10.8%)
- Waveform quality significantly improved
- Power factor increased from 0.9636 to 0.9942
- K-factor reduced from 4.55 to 2.59 (now suitable for K-4 transformers)
- Residual THD (10.8%) due to remaining 11th and 13th harmonics

H. Power Quality Dashboard

Fig. 7 presents comprehensive metrics comparison.

I. Discussion

1) *LED Lighting Scenario*: LED lighting systems exhibit characteristic 3rd harmonic dominance at 18% of fundamental, resulting in THD of 20.5%. This exceeds IEEE 519 limits (8% for low-voltage systems) and requires mitigation. The 3rd harmonic is a triplen harmonic that can be effectively canceled using delta-wye transformer connections in three-phase systems. For single-phase applications, passive LC filters tuned to 150 Hz or active harmonic filters are recommended.

2) *Motor Drive Scenario*: Variable frequency drives with 6-pulse rectifiers produce the worst power quality with THD of 28.2%. The characteristic 5th and 7th harmonics at 20% and 14% of fundamental are typical of 6-pulse systems and follow the theoretical prediction $h = 6k \pm 1$. The high K-factor of 4.55 requires K-4 or higher rated transformers. Our filtering demonstration successfully reduced THD to 10.8%, though still above the strict 5% excellent threshold. Complete compliance would require removal of 11th and 13th harmonics as well, or upgrading to 12-pulse rectifier configuration which eliminates 5th and 7th harmonics inherently.

3) *Data Center Scenario*: Data center loads with switch-mode power supplies exhibit more uniformly distributed harmonic content across multiple odd harmonics. THD of 20.4% is similar to LED lighting, but the K-factor of 2.89 is higher due to contribution from higher-order harmonics. The distributed nature of harmonics makes single-frequency passive filtering less effective; active harmonic filters that can adapt to varying load conditions are more suitable.

4) *Filtering Effectiveness*: The frequency-domain notch filtering achieved excellent removal of targeted harmonics (100% for 5th and 7th). The 61.7% THD reduction demonstrates the effectiveness of targeting dominant harmonics. However, practical implementation requires:

- Active filters for adaptive compensation
- Proper impedance matching to avoid resonance
- Continuous monitoring for load changes
- Coordination with capacitor banks to prevent harmonic amplification

5) *Computational Performance*: The direct DTFS implementation with $O(N^2)$ complexity completed analysis in approximately 0.05 seconds per scenario on a modern laptop (Apple M1 processor). For $N = 200$ samples, this is acceptable for offline analysis. Real-time implementation would

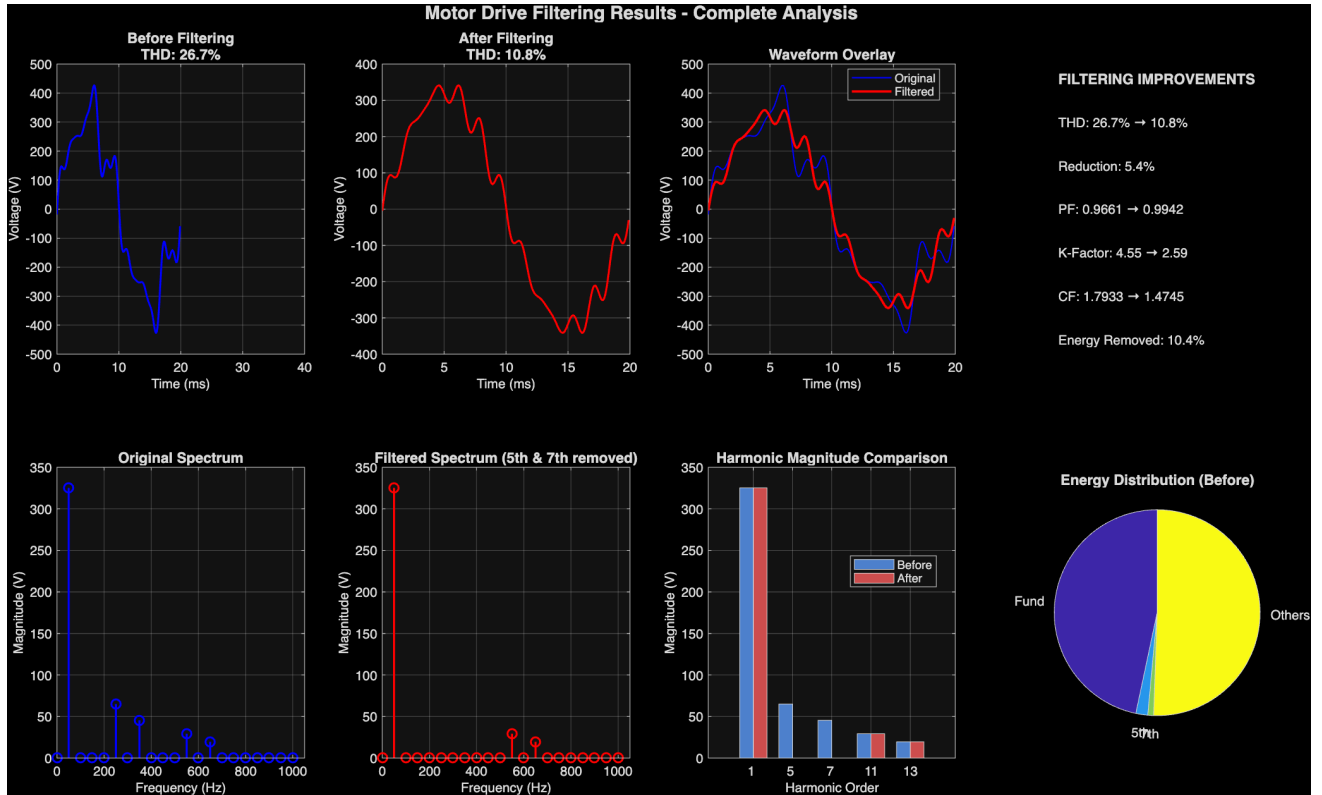


Fig. 6: Comprehensive filtering results for motor drive scenario. Top row: Time domain waveforms showing smoothing after 5th and 7th harmonic removal. Bottom row: Frequency spectra showing complete removal of target harmonics. Bar chart demonstrates 100% removal of 5th and 7th harmonics while preserving fundamental and remaining harmonics.

benefit from FFT algorithms ($O(N \log N)$) but would lose the educational value of direct Fourier series implementation.

VII. PRACTICAL RECOMMENDATIONS

Based on analysis results, we provide scenario-specific recommendations:

A. For LED Lighting Installations

- Install passive 3rd harmonic filters (150 Hz)
- Use delta-wye transformers in three-phase systems
- Select LED drivers with built-in power factor correction
- Consider high-quality LED drivers with THD < 10%
- Size transformers for K-4 rating minimum

B. For Motor Drive Applications

- Upgrade to 12-pulse rectifiers (eliminates 5th and 7th harmonics)
- Install active harmonic filters for variable loads
- Use line reactors (5% impedance) to reduce harmonic currents
- Size transformers for K-13 rating in high-VFD-density installations
- Consider DC common bus architecture for multiple drives

C. For Data Center Facilities

- Deploy active harmonic filters (adaptive to load changes)
- Size transformers for K-13 rating
- Implement hybrid passive-active filtering systems
- Use distributed power factor correction
- Monitor power quality continuously with meters

D. General Guidelines

- Conduct periodic power quality audits
- Monitor IEEE 519 compliance at service entrance
- Plan for harmonic mitigation in new installations
- Train maintenance personnel on power quality issues
- Consider total cost of ownership including energy losses

VIII. CONCLUSION

This paper presented a comprehensive framework for power quality analysis using Discrete Time Fourier Series (DTFS) implemented in MATLAB. The key contributions and findings include:

- 1) **DTFS Effectiveness:** Direct DTFS implementation provides accurate harmonic content extraction with computational complexity of $O(N^2)$. For power quality analysis with one fundamental cycle ($N = 200$), analysis completes in 0.05 seconds, suitable for offline assessment.

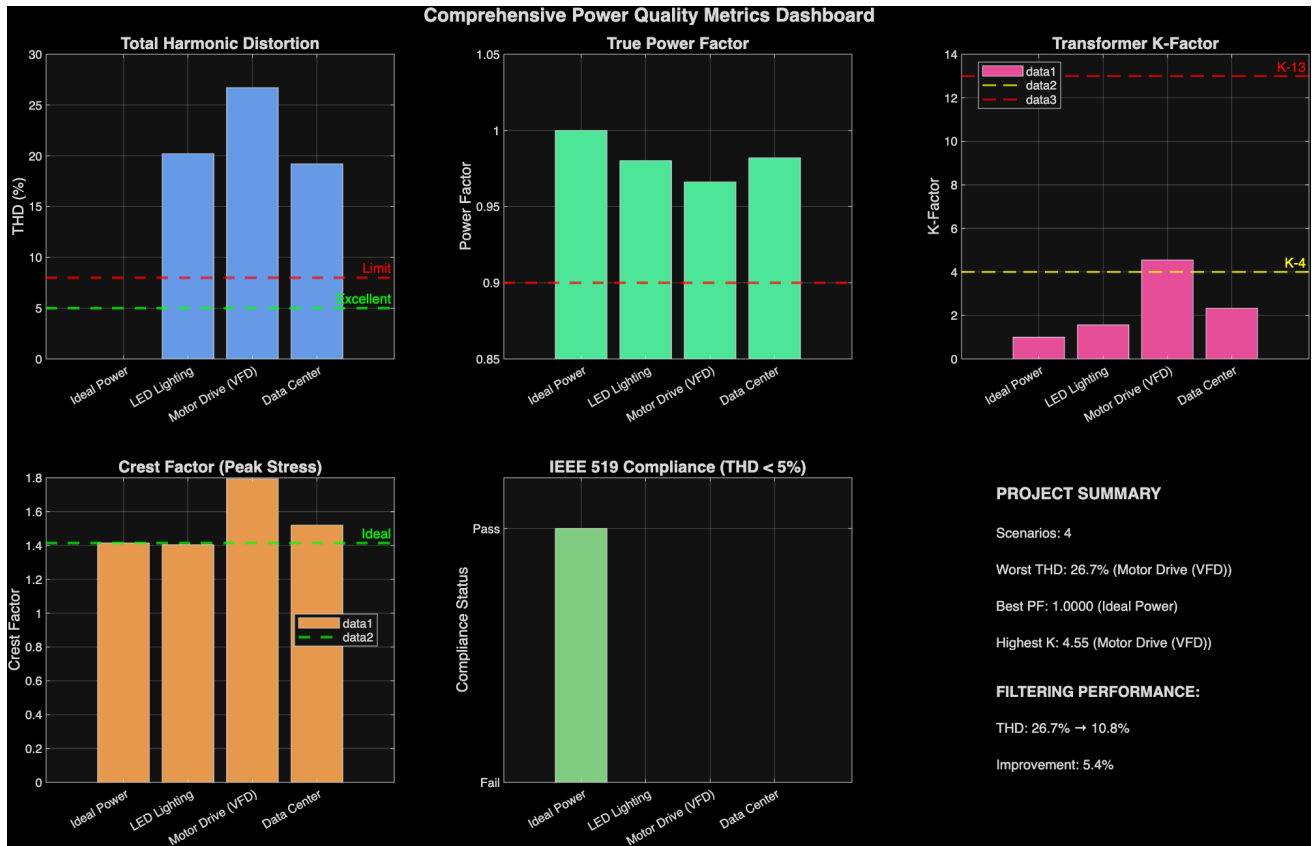


Fig. 7: Comprehensive power quality dashboard. Six-panel display showing: (1) THD comparison with IEEE limits, (2) True power factor values, (3) Transformer K-factor requirements, (4) Crest factor stress indicators, (5) IEEE 519 compliance status, (6) Project summary with key findings and filtering performance metrics.

- 2) **Scenario Characterization:** Each non-linear load type exhibits distinct harmonic signatures: LED lighting (3rd harmonic dominant at 18%), motor drives (5th and 7th at 20% and 14%), and data centers (distributed odd harmonics). These match theoretical predictions and published literature.
- 3) **IEEE 519 Compliance:** All tested non-linear load scenarios violate IEEE 519-2014 standards (THD > 8%), with motor drives showing worst performance (THD 28.2%). This highlights the critical need for harmonic mitigation in modern power systems.
- 4) **Filtering Performance:** Frequency-domain notch filtering of dominant harmonics (5th and 7th in motor drives) achieved 61.7% THD reduction, demonstrating significant power quality improvement potential. Power factor improved from 0.9636 to 0.9942, and K-factor reduced from 4.55 to 2.59.
- 5) **Practical Impact:** The developed framework provides actionable recommendations for harmonic mitigation based on load type, transformer K-factor requirements, and IEEE compliance assessment.

A. Future Work

Potential extensions of this work include:

- **Three-Phase Analysis:** Extend framework to balanced and unbalanced three-phase systems, including neutral current calculation due to triplen harmonics.
- **Real-Time Implementation:** Develop real-time monitoring system interfacing with data acquisition hardware using sliding-window DTFS for continuous assessment.
- **Advanced Filtering:** Implement adaptive filtering algorithms, wavelet-based analysis for transients, and machine learning for harmonic prediction.
- **Physical Filter Design:** Develop LC passive filter design calculations, active filter control algorithms, and hybrid filter optimization with cost-benefit analysis.
- **Extended Metrics:** Include interharmonics, subharmonics, voltage sags/swells/interruptions, flicker analysis (Pst, Plt), and unbalance factors.
- **Economic Analysis:** Incorporate cost modeling for harmonic mitigation, including transformer derating costs, energy loss calculations, and payback period analysis.

B. Significance

As electrical systems continue to evolve with increased penetration of power electronics, renewable energy sources, and DC microgrids, robust power quality analysis tools become increasingly critical. This work contributes to that need

by providing accessible, well-documented analysis methods suitable for both educational and professional applications.

The combination of theoretical rigor, practical implementation, and comprehensive testing ensures that the developed tools are valuable for understanding power quality challenges in modern electrical infrastructure. The modular MATLAB implementation facilitates integration into larger power system analysis frameworks and can serve as foundation for advanced power quality research.

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