

(iv) P-D controller:

- The proportional plus derivative controller produces an opp signal consisting of two terms.
- (i) proportional to error signal
 - (ii) proportional to the derivative of the i/p error signal.

$$P_d(t) \propto [e(t) + \frac{d}{dt} e(t)]$$

$$P_d(t) = K_p e(t) + K_p T_d \frac{d}{dt} e(t)$$

$K_p \rightarrow$ proportional gain

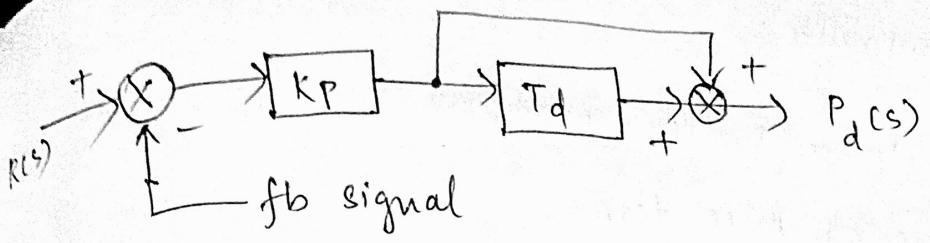
$T_d \rightarrow$ derivative time

$$\rightarrow \text{on, LT, } P_d(s) = K_p E(s) + K_p T_d s E(s)$$

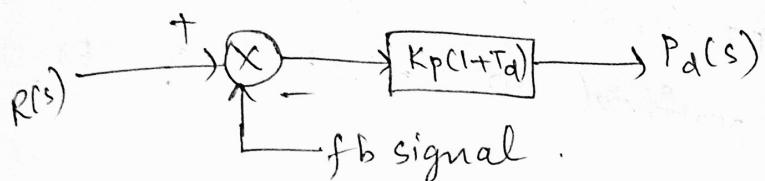
$$= E(s) [K_p + K_p T_d]$$

$$P_d(s) = E(s) [K_p (1 + T_d)]$$

$$\frac{P_d(s)}{E(s)} = K_p (1 + T_d)$$



↓



→ The derivative control acts on the rate of change of error & its action is effective during transient periods and does not produce effective correction on constant error.

→ Hence the derivative controller is never used alone, but it is employed in association with proportional and integral controllers.

→ The derivative controller does not affect the steady state error directly but initiates an early correction action and tends to increase the stability of the S/m.

→ But it amplifies noise signals & may cause a saturation effect in the actuator.

→ The derivative control action is adjusted by varying the derivative time, hence it is called as rate control.

(v) P-I-D controller:-

→ The PID controller produces an op signal consisting of three terms:

- (a) proportional to $e(t)$
- (b) proportional to integral of $e(t)$
- (c) proportional to derivative of $e(t)$.

$$\rightarrow P_{id}(t) \propto [e(t) + \int e(t) dt + \frac{d}{dt} e(t)]$$

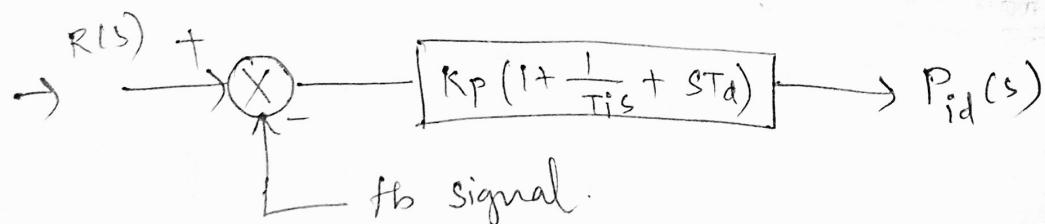
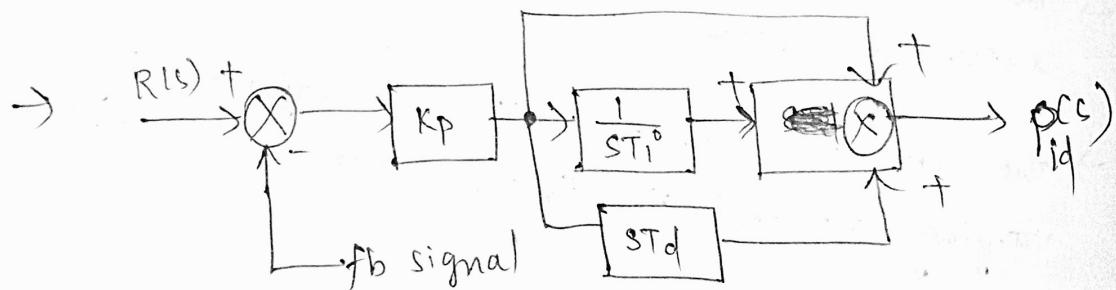
$$P_{id}(t) = K_p e(t) + \frac{K_p}{T_i} \int e(t) dt + K_p T_d \frac{d}{dt} e(t)$$

→ on, L.T

$$P_{id}(s) = K_p E(s) + \frac{K_p}{T_i} \frac{1}{s} E(s) + K_p T_d s E(s).$$

$$P_{id}(s) = E(s) K_p \left(1 + \frac{1}{s T_i} + s T_d \right)$$

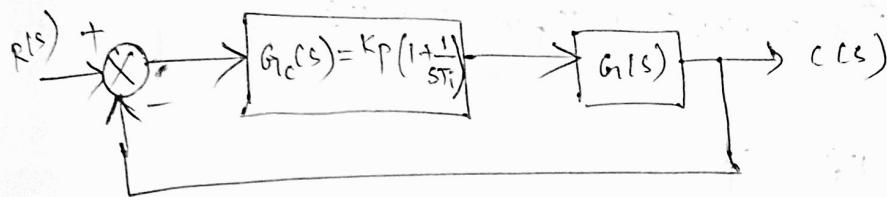
$$\frac{P_{id}(s)}{E(s)} = K_p \left(1 + \frac{1}{s T_i} + s T_d \right)$$



- the proportional controller stabilizes the gain but produces a steady state error.
- the Integral controller reduces or eliminates the steady state error.
- The derivative controller reduces the rate of change of error.

Effect of PI & PD controllers :-

→ PI controller



$G_c(s)$ → controller transfer func.

$$G_c(s) \rightarrow \text{open loop transfer func.} = \frac{\omega_n^2}{s(s + 2\zeta\omega_n)}$$

$$\begin{aligned} \text{CLTF} \Rightarrow \frac{C(s)}{R(s)} &= \frac{G_c(s) G(s)}{1 + G_c(s) G(s) H(s)} \\ &= \frac{K_p \left(1 + \frac{1}{sT_i}\right) \left(\frac{\omega_n^2}{s^2 + 2\zeta\omega_n s}\right)}{1 + K_p \left(\frac{sT_i + 1}{sT_i}\right) \left(\frac{\omega_n^2}{s^2 + 2\zeta\omega_n s}\right)} \end{aligned}$$

$$\begin{aligned} &= \frac{K_p \left(\frac{sT_i + 1}{sT_i}\right) \left(\frac{\omega_n^2}{s^2 + 2\zeta\omega_n s}\right)}{sT_i \left(s^2 + 2\zeta\omega_n s\right) + K_p (sT_i + 1) (\omega_n^2)} \\ &\quad \frac{}{sT_i \left(s^2 + 2\zeta\omega_n s\right)} \end{aligned}$$

$$= \frac{K_p \omega_n^2 (1 + sT_i)}{s^3 T_i + 2\zeta \omega_n s^2 T_i + K_p \cdot T_i s \omega_n^2 + K_p \omega_n^2}$$

$$= \frac{K_p \omega_n^2 (1 + sT_i)}{T_i (s^3 + 2\zeta \omega_n s^2 + K_p \omega_n^2 s + \frac{K_p \omega_n^2}{T_i})}$$

$$\frac{C(s)}{R(s)} = \frac{K_i^0 \omega_n^2 (1 + sT_i)}{s^3 + 2\zeta \omega_n s^2 + K_p \omega_n^2 s + K_i^0 \omega_n^2}$$

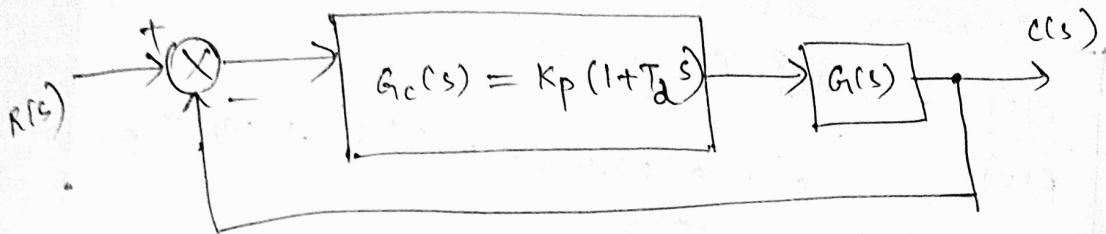
where $K_i^0 = \frac{K_p}{T_i}$

→ PI controller introduces one zero. ~~hence~~^{Also} the order increases by one. Increase in the order of the system results in less stable sys.

→ In $G_c(s) G(s)$, the PI controller increases the type number by one. The increase in type no. results in low steady state error.

PD controller :-

the proportional plus derivative controller, block diagram is,



$$G(s) = \frac{\omega_n^2}{s(s+2\zeta\omega_n)} \Rightarrow \text{OLTF}$$

$$\begin{aligned} \rightarrow G_c(s) G(s) &\Rightarrow \text{TF of PD} \\ G_c(s) G(s) &= K_p (1 + T_d s) \times \frac{\omega_n^2}{s(s+2\zeta\omega_n)} \\ &= \frac{K_p \omega_n^2 (1 + T_d s)}{s(s+2\zeta\omega_n)} \end{aligned}$$

$$\begin{aligned} \rightarrow \text{CLTF} &= \frac{G_c(s) G(s)}{1 + G_c(s) G(s)} \\ &= \frac{(K_p \omega_n^2 (1 + T_d s)) / s(s+2\zeta\omega_n)}{1 + \frac{K_p \omega_n^2 (1 + T_d s)}{s(s+2\zeta\omega_n)}} \end{aligned}$$

$$\begin{aligned} \text{CLTF} &= \frac{K_p \omega_n^2 (1 + T_d s)}{s^2 + 2\zeta\omega_n s + K_p \omega_n^2 (1 + T_d s)} \\ \left[\frac{C(s)}{R(s)} \right] &= \frac{\omega_n^2 (K_p + K_p T_d s)}{s^2 + 2\zeta\omega_n s + \omega_n^2 (K_p + K_p T_d s)} \end{aligned}$$

$$= \frac{\omega_n^2 (K_p + K_d s)}{s^2 + 2\zeta\omega_n s + \omega_n^2 (K_p + K_d s)}$$

$$\boxed{\frac{C(s)}{R(s)} = \frac{\omega_n^2 (K_p + K_d s)}{s^2 + s(2\zeta\omega_n + \omega_n^2 K_d) + \omega_n^2 K_p}}$$

where $K_d = K_p T_s$ & $\zeta' = (\zeta + \frac{\omega_n K_d}{2})$

→ PD-controller introduces a zero in the s/m & increase the damping ratio. The addition of zero may increase the peak overshoot & reduce the rise time.

→ But use in the damping ratio, use the peak-overshoot & hence compensated.

$$\left[\because M_p = e^{-\zeta\pi/\sqrt{1-\zeta^2}} \right]$$

$\& t_p = \pi/\omega_d$

→ There is no increase in the type no. of the s/m in PD-controller. Hence PD-controller will not modify the steady state error.

Qblms:

1) Find out the position, velocity and acceleration error w-efficienti for the following unity fb s/m/s having forward loop transfer function $G(s)$

as

$$\frac{K}{s^2(s^2 + 8s + 100)}$$

sofn

$$G(s) = \frac{K}{s^2(s^2 + 8s + 100)}$$

$$H(s) = 1$$

$$K_p = \lim_{s \rightarrow 0} G(s) H(s)$$

$$= \lim_{s \rightarrow 0} \frac{K}{s^2(s^2 + 8s + 100)}$$

$$\boxed{K_p = \infty}$$

$$K_v = \lim_{s \rightarrow 0} s G(s) H(s)$$

$$= \lim_{s \rightarrow 0} \frac{K}{s(s^2 + 8s + 100)}$$

$$\boxed{K_v = \infty}$$

$$K_a = \lim_{s \rightarrow 0} \frac{K}{(s^2 + 8s + 100)}$$

$$\boxed{K_a = K/100}$$

2) A unity fb sm has $G(s) = \frac{10}{(s+1)}$. Find the steady state error and the generalized error co-efficient for $r(t) = t$.

Soln.

$$c_0 = \frac{1}{1 + K_p}$$

$$c_1 = \frac{1}{K_V}$$

$$c_2 = \frac{1}{K_a}$$

$$c_n = \lim_{s \rightarrow 0} \frac{d^n}{ds^n} F(s)$$

$$F(s) = \frac{1}{1 + G(s) H(s)}$$

$$= \frac{1}{1 + \left(\frac{10}{s+1}\right)}$$

$$F(s) = \frac{(s+1)}{(s+11)}$$

$$c_0 = \lim_{s \rightarrow 0} F(s) \Rightarrow \boxed{\frac{1}{11} = c_0}$$

$$K_p = \lim_{s \rightarrow 0} G(s) H(s)$$

$$= \lim_{s \rightarrow 0} \frac{10}{s+1}$$

$$\boxed{K_p = 10}$$

$$K_V = \lim_{s \rightarrow 0} s G(s) H(s)$$

$$K_V = 0$$

$$K_a = \lim_{s \rightarrow 0} s^2 G(s) H(s)$$

$$\boxed{K_a = 0}$$

$$c_1 = \lim_{s \rightarrow 0} \frac{d}{ds} \left(\frac{s+1}{s+11} \right) = \lim_{s \rightarrow 0} \frac{(s+11)(1) - (s+1)(1)}{(s+11)^2}$$

$$= \lim_{s \rightarrow 0} \frac{s+11 - s - 1}{(s+11)^2} = \lim_{s \rightarrow 0} \frac{10}{(s+11)^2}$$

$$c_1 = \boxed{\frac{10}{121}}$$

$$c_2 = \lim_{s \rightarrow 0} 10 \left(-2 \times (s+11)^{-3} \right)$$

$$= \lim_{s \rightarrow 0} \frac{-20}{(s+11)^3}$$

$$= \boxed{-\frac{20}{11^3}}$$

$$c_2 = \boxed{-20/11^3}$$

Steady state error:

$$e_{ss} = \lim_{s \rightarrow 0} s E(s) \quad E(s) = \frac{R(s)}{1 + G(s)H(s)}$$

$$= \lim_{s \rightarrow 0} \frac{s \left(\frac{1}{s^2} \right)}{1 + \frac{10}{(s+1)}}$$

$$= \lim_{s \rightarrow 0} \frac{1/(s+1)}{s(s+1+10)}$$

$$= \lim_{s \rightarrow 0} \frac{(s+1)}{s(s+11)}$$

$$e_{ss} = \boxed{\infty}$$

3) The open loop tfx function of a unity fb ctrl s/m
 is $G(s) = \frac{9}{(s+1)}$, using the generalized error series
 determine the error signal and steady state error
 of the s/m when the s/m is excited by $3t^2/2$.

Ans

$$G(s) = \frac{9}{(s+1)}$$

$$H(s) = 1$$

$$r(t) = \frac{3t^2}{2} \Rightarrow R(s) = \frac{3}{2} \times \frac{2!}{s^3} = \frac{3}{s^3}$$

$$e(t) = c_0 r(t) + c_1 r'(t) + \frac{c_2}{2!} r''(t) + \dots$$

$$c_0 = \lim_{s \rightarrow 0} F(s) = \lim_{s \rightarrow 0} \frac{1}{1 + G(s)H(s)}$$

$$= \lim_{s \rightarrow 0} \frac{1}{1 + \left(\frac{9}{s+1}\right)}$$

$$= \lim_{s \rightarrow 0} \frac{s+1}{s+10}$$

$$c_0 = \frac{1}{10}$$

$$c_1 = \lim_{s \rightarrow 0} \frac{d}{ds} F(s) \Rightarrow \lim_{s \rightarrow 0} \frac{(s+10) - (s+1)}{(s+10)^2}$$

$$= \lim_{s \rightarrow 0} \frac{9}{(s+10)^2}$$

$$c_1 = \frac{9}{100}$$

$$c_2 = \lim_{s \rightarrow 0} \frac{9(-2)}{(s+10)^3}$$

$$c_2 = -\frac{18}{10^3}$$

$$g(t) = \frac{3t^2}{2}$$

$$g'(t) = \frac{3}{2} \times 2t = 3t$$

$$g''(t) = 3$$

$$e(t) = \frac{1}{10} \times \frac{3t^2}{2} + \frac{9}{100} \times 3t + \left(-\frac{18}{10^3} \times \frac{1}{2} \times 3 \right)$$

$$e(t) = \frac{3}{20} t^2 + \frac{27}{100} t - \frac{27}{10^3}$$

$$e(t) = 0.15t^2 + 0.27t - 0.027$$

$$e_{ss} = \lim_{t \rightarrow \infty} e(t)$$

$$e_{ss} = \infty$$