# Macroeconomics A; EI056

Technical appendix: The real business cycles (RBC) model

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# 1 Building blocks of the model

Consider a closed economy where output is produced using labor and capital:

$$Y_t = (K_t)^{\alpha} (A_t L_t)^{1-\alpha} \qquad ; \qquad 0 < \alpha < 1$$
 (1)

where A is an exogenous stochastic productivity parameter. Output can be consumed, used by the government, or invested:

$$Y_t = C_t + G_t + I_t$$

Capital depreciates at a rate  $\delta$ , so the capital dynamics are:

$$K_{t+1} = (1 - \delta) K_t + I_t \tag{2}$$

Output is produced by a firm. At period t the firms buys  $K_t$  units of capital from the consumers at a price 1 (the capital good and the consumption goods are the same). It borrows at a real interest rate  $r_t$  to finance this purchase. At the end of the period the firms sell the remaining units of capital,  $(1 - \delta) K_t$ , to the consumers. The firm's profits are then:

$$\Pi_t = (K_t)^{\alpha} (A_t L_t)^{1-\alpha} - w_t L_t - [(1+r_t) - (1-\delta)] K_t$$

where w is the real wage. The maximization of profits with respect to labor and capital leads to:

$$\frac{\partial \Pi_t}{\partial L_t} = 0 \Rightarrow w_t = (1 - \alpha) \left(\frac{K_t}{A_t L_t}\right)^{\alpha} A_t \tag{3}$$

$$\frac{\partial \Pi_t}{\partial K_t} = 0 \Rightarrow r_t = \alpha \left(\frac{K_t}{A_t L_t}\right)^{\alpha - 1} - \delta \tag{4}$$

The economy is subjected to shocks in government spending and productivity who fluctuate

around some average values:

$$\ln\left(A_{t}\right) - \ln\left(\bar{A}\right) = \hat{A}_{t} = \rho_{A}\hat{A}_{t-1} + \varepsilon_{A,t} \tag{5}$$

$$\ln(G_t) - \ln(\bar{G}) = \hat{G}_t = \rho_G \hat{G}_{t-1} + \varepsilon_{G,t}$$
(6)

where  $\rho_A$  and  $\rho_G$  are the persistence of shocks (both are between -1 and 1).

The representative consumer maximizes an intertemporal utility in consumption and leisure:

$$U_{t} = E_{t} \sum_{s=0}^{\infty} \frac{1}{(1+\rho)^{s}} \left[ \ln C_{t+s} + b \ln (1 - L_{t+s}) \right]$$

where C and L are consumption and labor. We consider constant population of size 1. The utility is maximized subject to the budget constraint:

$$C_t + I_t = w_t L_t + [(1 + r_t) - (1 - \delta)] K_t - T_t$$
(7)

where T denotes lump-sum taxes. We assume that the government runs a balances budget, so  $T_t = G_t$ . The consumer earns money from wages and renting out capital to firms, pay taxes, and uses her disposable income to consume and invest in capital. Using (2), we write (7) as:

$$C_t + K_{t+1} = w_t L_t + (1 + r_t) K_t - G_t \tag{8}$$

As there is uncertainty, the future variables need to be indexes not only by time, but also by the state of nature in which the economy can find itself in the future. We index the possible states at time t+s by  $x_{t+s}$ . The probability of being in state  $x_{t+s}$  is  $\pi(x_{t+s})$ , and the value of a variable z in that state is  $z(x_{t+s})$ . From the point of view of the current period, the consumer maximizes the expected utility, which we write as the sum across state weighted by their probability:

$$E_{t} \sum_{s=0}^{\infty} \frac{1}{(1+\rho)^{s}} \left[ \ln C_{t+s} + b \ln (1 - L_{t+s}) \right]$$

$$= \sum_{x_{t+s}} \pi (x_{t+s}) \left( \sum_{s=0}^{\infty} \frac{1}{(1+\rho)^{s}} \left[ \ln C (x_{t+s}) + b \ln (1 - L (x_{t+s})) \right] \right)$$

$$= \sum_{s=0}^{\infty} \frac{1}{(1+\rho)^{s}} \sum_{x_{t+s}} \pi (x_{t+s}) \left[ \ln C (x_{t+s}) + b \ln (1 - L (x_{t+s})) \right]$$

The budget constraint in a specific state of nature at t + s is:

$$C(x_{t+s}) + K(x_{t+s+1}) = w(x_{t+s}) L(x_{t+s}) + (1 + r(x_{t+s})) K(x_{t+s}) - G(x_{t+s})$$

The optimization is then written as the following Lagrangian:

$$\mathcal{L} = \sum_{s=0}^{\infty} \frac{1}{(1+\rho)^{s}} \sum_{x_{t+s}} \pi(x_{t+s}) \left\{ \begin{array}{c} \ln(C(x_{t+s})) + b \ln(1 - L(x_{t+s})) \\ -\varphi(x_{t+s}) \left[ K(x_{t+s+1}) + C(x_{t+s}) + G(x_{t+s}) \\ -w(x_{t+s}) L(x_{t+s}) - (1 + r(x_{t+s})) K(x_{t+s}) \end{array} \right] \right\}$$

We now take the first-order conditions, focusing on variables at time t and t+1 for simplicity. The first-order condition with respect to current consumption is:

$$0 = \frac{\partial \mathcal{L}}{\partial C(x_t)}$$

$$0 = \frac{1}{C(x_t)} - \varphi(x_t)$$

$$\frac{1}{C(x_t)} = \varphi(x_t)$$

where we used  $\pi(x_t) = 1$  as at period t we know which state we are in. The first-order condition with respect to future consumption in a specific state is:

$$0 = \frac{\partial \mathcal{L}}{\partial C(x_{t+1})}$$

$$0 = \frac{1}{1+\rho} \pi(x_{t+1}) \left\{ \frac{1}{C(x_{t+1})} - \varphi(x_{t+1}) \right\}$$

$$\frac{1}{C(x_{t+1})} = \varphi(x_{t+1})$$

The first-order condition with respect to current labor is:

$$0 = \frac{\partial \mathcal{L}}{\partial L(x_t)}$$

$$0 = -\frac{b}{1 - L(x_t)} + \varphi(x_t) w(x_t)$$

$$\frac{b}{1 - L(x_t)} = \varphi(x_t) w(x_t)$$

The first-order condition with respect to future labor in a specific state is:

$$0 = \frac{\partial \mathcal{L}}{\partial L(x_{t+1})}$$

$$0 = \frac{1}{1+\rho} \pi(x_{t+1}) \left\{ -\frac{b}{1-L(x_{t+1})} + \varphi(x_{t+1}) w(x_{t+1}) \right\}$$

$$\frac{b}{1-L(x_{t+1})} = \varphi(x_{t+1}) w(x_{t+1})$$

Finally, we write the first-order condition with respect to capital  $K(x_{t+1})$ . Note that this future capital stock is determined in period t and will apply to all possible states of nature in period t+1:

$$0 = \frac{\partial \mathcal{L}}{\partial K(x_{t+1})}$$

$$0 = -\varphi(x_t) + \frac{1}{1+\rho} \sum_{x_{t+1}} \pi(x_{t+1}) \varphi(x_{t+1}) (1+r(x_{t+1}))$$

$$\varphi(x_t) = \frac{1}{1+\rho} \sum_{x_{t+1}} \pi(x_{t+1}) \varphi(x_{t+1}) (1+r(x_{t+1}))$$

As the state of nature is known at time t, we can denote variables simply by the time subscript (for instance  $w(x_t) = w_t$ ). Combining the first order conditions with respect to current labor and consumption gives the labor supply:

$$\frac{b}{1 - L_t} = w_t \varphi_t$$

$$\frac{b}{1 - L_t} = w_t \frac{1}{C_t}$$

$$w_t = \frac{b}{1 - L_t} C_t$$
(9)

The expectation of a variable is the sum of its values across states of natures time the probabilities of these states:

$$E_t z_{z+1} = \sum_{x_{t+1}} \pi(x_{t+1}) z(x_{t+1})$$

Combining the optimality conditions with respect to capital and consumptions, we get the Euler condition:

$$\varphi_{t} = E_{t}\varphi_{t+1} \frac{1 + r_{t+1}}{1 + \rho} 
\frac{1}{C_{t}} = E_{t} \left[ \frac{1}{C_{t+1}} \frac{1 + r_{t+1}}{1 + \rho} \right]$$
(10)

Combining (3)-(4) with (9)-(10), we compute two of the key relations, namely the Euler and the labor market equilibrium:

$$\frac{b}{1 - L_t} C_t = w_t = (1 - \alpha) \left( \frac{K_t}{A_t L_t} \right)^{\alpha} A_t$$

$$\frac{1}{C_t} = E_t \left[ \frac{1 + r_{t+1}}{1 + \rho} \frac{1}{C_{t+1}} \right]$$

$$= E_t \left[ \frac{1}{C_{t+1}} \left( \frac{1 + \alpha \left( \frac{K_{t+1}}{A_{t+1} L_{t+1}} \right)^{\alpha - 1} - \delta}{1 + \rho} \right) \right]$$
(12)

(1) and (8) imply:

$$K_{t+1} = w_t L_t + (1 + r_t) K_t - G_t - C_t$$

$$= w_t L_t + (r_t + \delta) K_t + (1 - \delta) K_t - G_t - C_t$$

$$= (1 - \alpha) \left(\frac{K_t}{A_t L_t}\right)^{\alpha} A_t L_t + \alpha \left(\frac{K_t}{A_t L_t}\right)^{\alpha - 1} K_t + (1 - \delta) K_t - G_t - C_t$$

$$= (K_t)^{\alpha} (A_t L_t)^{1 - \alpha} + (1 - \delta) K_t - G_t - C_t$$
(13)

The model is summarized by (11)-(13) and the shocks (5)-(6)

Investment is computed from the capital accumulation (2)

$$I_t = K_{t+1} - (1 - \delta) K_t$$

$$\frac{I_t}{K_t} = \frac{K_{t+1}}{K_t} - (1 - \delta)$$

# 2 The steady state

## 2.1 Analytical results

We start by solving for the steady state, where we denote variables with an upper bar. We start by writing (12) as:

$$\frac{1}{\bar{C}} = \frac{1}{\bar{C}} \frac{1 + \alpha \left(\frac{\bar{K}}{A\bar{L}}\right)^{\alpha - 1} - \delta}{1 + \rho}$$

$$1 = \frac{1 + \alpha \left(\frac{\bar{K}}{A\bar{L}}\right)^{\alpha - 1} - \delta}{1 + \rho}$$

This implies:

$$\bar{k} = \frac{\bar{K}}{\bar{A}\bar{L}} = \left(\frac{\alpha}{\rho + \delta}\right)^{\frac{1}{1 - \alpha}} \tag{14}$$

(11) is then written as:

$$\frac{b}{1-\bar{L}}\bar{C} = (1-\alpha)\left(\bar{k}\right)^{\alpha}\bar{A}$$

The labor input is thus:

$$\bar{L} = 1 - \frac{b}{(1-\alpha)(\bar{k})^{\alpha}} \frac{\bar{C}}{\bar{A}}$$
(15)

(13) is written as:

$$\bar{K} = (1 - \delta) \bar{K} + (\bar{K})^{\alpha} (\bar{A}\bar{L})^{1-\alpha} - \bar{C} - \bar{G}$$

$$1 = (1 - \delta) + (\frac{\bar{A}\bar{L}}{\bar{K}})^{1-\alpha} - \frac{\bar{C}}{\bar{K}} - \frac{\bar{G}}{\bar{K}}$$

$$0 = (\bar{k})^{\alpha - 1} - \delta - \frac{\bar{C}}{\bar{K}} - \frac{\bar{G}}{\bar{K}}$$
(16)

Investment is written as:

$$\frac{I_t}{K_t} = \frac{K_{t+1}}{K_t} - (1 - \delta)$$

$$\frac{\bar{I}}{\bar{K}} = \delta$$

(3) and (4) imply:

$$w_t = (1 - \alpha) (\bar{k})^{\alpha} \bar{A}$$

$$r_t = \bar{r} = \alpha (\bar{k})^{\alpha - 1} - \delta = \rho$$
(17)

#### 2.2 Calibration

The various expressions can be calibrated using some key variables in the data. We set values of  $\alpha$  and  $\delta$ . Taking the average real interest rate in the data  $\bar{r}$  then gives  $\bar{k}$  from (17):

$$\bar{k} = \left(\frac{\alpha}{\bar{r} + \delta}\right)^{\frac{1}{1 - \alpha}}$$

Combining this with (14) we solve for  $\rho$  as:  $e^{\rho} = 1 + \bar{r}$ .

Recall that the production function is:

$$Y_t = (K_t)^{\alpha} (A_t L_t)^{1-\alpha}$$

$$\frac{\bar{Y}}{\bar{K}} = (\bar{k})^{\alpha-1} = \frac{\bar{r} + \delta}{\alpha}$$

Next, we set the steady state ratio of government consumption to GDP,  $\bar{G}/\bar{Y}$  and compute:

$$\frac{\bar{G}}{\bar{K}} = \frac{\bar{G}}{\bar{Y}}\frac{\bar{Y}}{\bar{K}} = \frac{\bar{G}}{\bar{Y}}\frac{\bar{r} + \delta}{\alpha}$$

(16) gives  $\bar{C}/\bar{K}$ :

$$\frac{\bar{C}}{\bar{K}} = \left(\bar{k}\right)^{\alpha - 1} - \delta - \frac{\bar{G}}{\bar{K}}$$

# 3 Log linearization

We expand the variables around the steady growth path. Define tilde variables as log deviations:

$$\hat{X}_t = \frac{X_t - \bar{X}}{\bar{X}}$$

(5)-(6) are already in the right form:

$$\hat{A}_t = \rho_A \hat{A}_{t-1} + \varepsilon_{A,t} \qquad ; \qquad \hat{G}_t = \rho_G \hat{G}_{t-1} + \varepsilon_{G,t}$$

The left-hand side of (11) is linearized as follows:

$$\begin{split} \frac{b}{1-L_t}C_t &= \frac{b}{1-\bar{L}}\bar{C} + \frac{b}{1-\bar{L}}\left(C_t - \bar{C}\right) - b\bar{C}\left(\frac{1}{1-\bar{L}}\right)^2(-1)\left(L_t - \bar{L}\right) \\ &= \frac{b}{1-\bar{L}}\bar{C} + \frac{b}{1-\bar{L}}\bar{C}\frac{C_t - \bar{C}}{\bar{C}} - \frac{b}{1-\bar{L}}\bar{C}\frac{1}{1-\bar{L}}(-1)\bar{L}\frac{L_t - \bar{L}}{\bar{L}} \\ &= \frac{b}{1-\bar{L}}\bar{C}\left(1 + \frac{C_t - \bar{C}}{\bar{C}} + \frac{\bar{L}}{1-\bar{L}}\frac{L_t - \bar{L}}{\bar{L}}\right) \\ &= \frac{b}{1-\bar{L}}\bar{C}\left(1 + \hat{C}_t + \frac{\bar{L}}{1-\bar{L}}\hat{L}\right) \end{split}$$

The right-hand side of (11) is linearized as follows:

$$(1-\alpha)\left(\frac{K_{t}}{A_{t}L_{t}}\right)^{\alpha}A_{t}$$

$$= (1-\alpha)\left(\bar{k}\right)^{\alpha}\bar{A} + (1-\alpha)\left(\bar{k}\right)^{\alpha}\left(A_{t} - \bar{A}\right)$$

$$+ (1-\alpha)\bar{A}\alpha\left[\left(\bar{k}\right)^{\alpha-1}\frac{K_{t} - \bar{K}}{\bar{A}\bar{L}} - \left(\bar{k}\right)^{\alpha-1}\bar{k}\frac{1}{\bar{A}}\left(A_{t} - \bar{A}\right)\right]$$

$$- (1-\alpha)\bar{A}\alpha\left(\bar{k}\right)^{\alpha-1}\bar{k}\frac{1}{\bar{L}}\left(L_{t} - \bar{L}\right)$$

$$= (1-\alpha)\left(\bar{k}\right)^{\alpha}\bar{A}\left(1 + \frac{A_{t} - \bar{A}}{\bar{A}}\right)$$

$$+ (1-\alpha)\bar{A}\alpha\left[\left(\bar{k}\right)^{\alpha}\frac{K_{t} - \bar{K}}{\bar{K}} - \left(\bar{k}\right)^{\alpha}\frac{A_{t} - \bar{A}}{\bar{A}} - \left(\bar{k}\right)^{\alpha}\frac{L_{t} - \bar{L}}{\bar{L}}\right]$$

$$= (1-\alpha)\left(\bar{k}\right)^{\alpha}\bar{A}\left(1 + \hat{A}_{t} + \alpha\left[\hat{K}_{t} - \hat{A}_{t} - \hat{L}_{t}\right]\right)$$

$$= (1-\alpha)\left(\bar{k}\right)^{\alpha}\bar{A}\left(1 + (1-\alpha)\hat{A}_{t} + \alpha\hat{K}_{t} - \alpha\hat{L}_{t}\right)$$

(11) is then:

$$\frac{b}{1 - L_t} C_t = (1 - \alpha) \left(\frac{K_t}{A_t L_t}\right)^{\alpha} A_t$$

$$\frac{b}{1 - \bar{L}} \bar{C} \left(1 + \hat{C}_t + \frac{\bar{L}}{1 - \bar{L}} \hat{L}_t\right) = (1 - \alpha) \left(\bar{k}\right)^{\alpha} \bar{A} \left(1 + (1 - \alpha) \hat{A}_t + \alpha \hat{K}_t - \alpha \hat{L}_t\right)$$

$$\hat{C}_t + \frac{\bar{L}}{1 - \bar{L}} \hat{L}_t = (1 - \alpha) \hat{A}_t + \alpha \hat{K}_t - \alpha \hat{L}_t$$

$$\hat{C}_t + \left(\frac{\bar{L}}{1 - \bar{L}} + \alpha\right) \hat{L}_t = (1 - \alpha) \hat{A}_t + \alpha \hat{K}_t$$
(18)

Next turn to (13). The left hand side is expanded as:

$$K_{t+1} = \bar{K} + K_{t+1} - \bar{K}$$

$$= \bar{K} + \bar{K} \frac{K_{t+1} - \bar{K}}{\bar{K}}$$

$$= \bar{K} \left( 1 + \hat{K}_{t+1} \right)$$

The right-hand side of (13) is expanded as:

$$(1 - \delta) K_{t} + (K_{t})^{\alpha} (A_{t}L_{t})^{1-\alpha} - C_{t} - G_{t}$$

$$= (1 - \delta) \bar{K} + (\bar{K})^{\alpha} (\bar{A}\bar{L})^{1-\alpha} - \bar{C} - \bar{G} + (1 - \delta) (K_{t} - \bar{K})$$

$$+ \alpha (\bar{K})^{\alpha-1} (\bar{A}\bar{L})^{1-\alpha} (K_{t} - \bar{K}) + (1 - \alpha) (\bar{K})^{\alpha} (\bar{A}\bar{L})^{-\alpha} \bar{L} (A_{t} - \bar{A})$$

$$+ (1 - \alpha) (\bar{K})^{\alpha} (\bar{A}\bar{L})^{-\alpha} \bar{A}\bar{L} (L_{t} - \bar{L}) - (C_{t} - \bar{C}) - (G_{t} - \bar{G})$$

$$= (1 - \delta) \bar{K} + (\bar{K})^{\alpha} (\bar{A}\bar{L})^{1-\alpha} - \bar{C} - \bar{G} + (1 - \delta) \bar{K} \frac{K_{t} - \bar{K}}{\bar{K}}$$

$$+ \alpha (\bar{K})^{\alpha} (\bar{A}\bar{L})^{1-\alpha} \frac{K_{t} - \bar{K}}{\bar{K}} + (1 - \alpha) (\bar{K})^{\alpha} (\bar{A}\bar{L})^{1-\alpha} \frac{A_{t} - \bar{A}}{\bar{A}}$$

$$+ (1 - \alpha) \left(\bar{K}\right)^{\alpha} \left(\bar{A}\bar{L}\right)^{1-\alpha} \frac{L_t - \bar{L}}{\bar{L}} - \bar{C}\frac{C_t - \bar{C}}{\bar{C}} - \bar{G}\frac{G_t - \bar{G}}{\bar{G}}$$

$$= (1 - \delta) \bar{K} + (\bar{K})^{\alpha} \left(\bar{A}\bar{L}\right)^{1-\alpha} - \bar{C} - \bar{G} + (1 - \delta) \bar{K}\hat{K}_t$$

$$+ (\bar{K})^{\alpha} \left(\bar{A}\bar{L}\right)^{1-\alpha} \left[\alpha\hat{K}_t + (1 - \alpha)\hat{A}_t + (1 - \alpha)\hat{L}_t\right] - \bar{C}\hat{C}_t - \bar{G}\hat{G}_t$$

Putting both sides together, (13) becomes:

$$K_{t+1} = (1 - \delta) K_t + (K_t)^{\alpha} (A_t L_t)^{1-\alpha} - C_t - G_t$$

$$\bar{K} \left( 1 + \hat{K}_{t+1} \right) = (1 - \delta) \bar{K} + (\bar{K})^{\alpha} (\bar{A}\bar{L})^{1-\alpha} - \bar{C} - \bar{G} + (1 - \delta) \bar{K}\hat{K}_t$$

$$+ (\bar{K})^{\alpha} (\bar{A}\bar{L})^{1-\alpha} \left[ \alpha \hat{K}_t + (1 - \alpha) \hat{A}_t + (1 - \alpha) \hat{L}_t \right] - \bar{C}\hat{C}_t - \bar{G}\hat{G}_t$$

$$\bar{K}\hat{K}_{t+1} = (1 - \delta) \bar{K}\hat{K}_t + (\bar{K})^{\alpha} (\bar{A}\bar{L})^{1-\alpha} \left[ \alpha \hat{K}_t + (1 - \alpha) \hat{A}_t + (1 - \alpha) \hat{L}_t \right]$$

$$- \bar{C}\hat{C}_t - \bar{G}\hat{G}_t$$

$$\bar{K}\hat{K}_{t+1} = \bar{K} \left[ (1 - \delta) \hat{K}_t + (\bar{k})^{\alpha-1} \left[ \alpha \hat{K}_t + (1 - \alpha) \hat{A}_t + (1 - \alpha) \hat{L}_t \right] \right]$$

$$- \bar{K} \left[ \frac{\bar{C}}{\bar{K}} \hat{C}_t + \frac{\bar{G}}{\bar{K}} \hat{G}_t \right]$$

$$\hat{K}_{t+1} = (1 - \delta) \hat{K}_t + (\bar{k})^{\alpha-1} \left[ \alpha \hat{K}_t + (1 - \alpha) \hat{A}_t + (1 - \alpha) \hat{L}_t \right]$$

$$- \frac{\bar{C}}{\bar{K}} \hat{C}_t - \frac{\bar{G}}{\bar{K}} \hat{G}_t$$

$$\hat{K}_{t+1} = \eta_{KK} \hat{K}_t + \eta_{KA} \hat{A}_t + \eta_{KC} \hat{C}_t + \eta_{KL} \hat{l}_t + \eta_{KG} \hat{G}_t$$

$$(19)$$

where:

$$\eta_{KK} = (1 - \delta) + (\bar{k})^{\alpha - 1} \alpha = 1 + \bar{r}$$

$$\eta_{KA} = (\bar{k})^{\alpha - 1} (1 - \alpha) = (\bar{r} + \delta) \frac{1 - \alpha}{\alpha}$$

$$\eta_{KC} = -\frac{\bar{C}}{\bar{K}}$$

$$\eta_{KL} = \eta_{KA}$$

$$\eta_{KG} = -\frac{\bar{G}}{\bar{K}}$$

The left-hand side of (12) is expanded as:

$$\frac{1}{C_t} = \frac{1}{\bar{C}} - \left(\frac{1}{\bar{C}}\right)^2 \left(C_t - \bar{C}\right)$$

$$= \frac{1}{\bar{C}} - \frac{1}{\bar{C}} \frac{C_t - \bar{C}}{\bar{C}} = \frac{1}{\bar{C}} \left(1 - \hat{C}_t\right)$$

The right-hand side of 12) is expanded as:

$$e^{-\rho}E_t\left[\frac{1}{c_{t+1}}\left(1+\alpha\left(\frac{K_{t+1}}{A_{t+1}L_{t+1}}\right)^{\alpha-1}-\delta\right)\right]$$

$$= e^{-\rho} E_{t} \left[ \frac{1}{\overline{C}} \left( 1 + \alpha \left( \bar{k} \right)^{\alpha - 1} - \delta \right) \right]$$

$$+ e^{-\rho} \left( 1 + \alpha \left( \bar{k} \right)^{\alpha - 1} - \delta \right) E_{t} \left[ - \left( \frac{1}{\overline{C}} \right)^{2} \left( C_{t+1} - \bar{C} \right) \right]$$

$$+ e^{-\rho} E_{t} \left[ \frac{1}{\overline{C}} \alpha \left( \alpha - 1 \right) \left[ \begin{array}{c} \left( \bar{k} \right)^{\alpha - 2} \frac{K_{t+1} - \bar{K}}{A\bar{L}} - \left( \bar{k} \right)^{\alpha - 2} \bar{k} \frac{A_{t+1} - \bar{A}}{A}}{- \left( \bar{k} \right)^{\alpha - 2} \bar{k} \frac{L_{t+1} - \bar{L}}{\bar{L}}} \right] \right]$$

$$= e^{-\rho} E_{t} \left[ \frac{1}{\overline{C}} \left( 1 + \alpha \left( \bar{k} \right)^{\alpha - 1} - \delta \right) \right]$$

$$- e^{-\rho} \frac{1}{\overline{C}} \left( 1 + \alpha \left( \bar{k} \right)^{\alpha - 1} - \delta \right) E_{t} \frac{C_{t+1} - \bar{C}}{\bar{C}}$$

$$+ e^{-\rho} \frac{1}{\overline{C}} \alpha \left( \alpha - 1 \right) \left( \bar{k} \right)^{\alpha - 1} E_{t} \left[ \frac{K_{t+1} - \bar{K}}{\bar{K}} - \frac{A_{t+1} - \bar{A}}{\bar{A}} - \frac{L_{t+1} - \bar{L}}{\bar{L}} \right]$$

$$= e^{-\rho} E_{t} \left[ \frac{1}{\overline{C}} \left( 1 + \alpha \left( \bar{k} \right)^{\alpha - 1} - \delta \right) \right]$$

$$- e^{-\rho} \frac{1}{\overline{C}} \left( 1 + \alpha \left( \bar{k} \right)^{\alpha - 1} - \delta \right) E_{t} \hat{C}_{t+1}$$

$$+ e^{-\rho} \frac{1}{\overline{C}} \alpha \left( \alpha - 1 \right) \left( \bar{k} \right)^{\alpha - 1} E_{t} \left[ \hat{K}_{t+1} - \hat{A}_{t+1} - \hat{L}_{t+1} \right]$$

Combining both sides (12) becomes:

$$\begin{split} \frac{1}{C_{t}} &= e^{-\rho} E_{t} \left[ \frac{1}{c_{t+1}} \left( 1 + \alpha \left( \bar{k} \right)^{\alpha - 1} - \delta \right) \right] \\ \frac{1}{\bar{C}} \left( 1 - \hat{C}_{t} \right) &= e^{-\rho} E_{t} \left[ \frac{1}{\bar{C}} \left( 1 + \alpha \left( \bar{k} \right)^{\alpha - 1} - \delta \right) \right] \\ &- e^{-\rho} \frac{1}{\bar{C}} \left( 1 + \alpha \left( \bar{k} \right)^{\alpha - 1} - \delta \right) E_{t} \hat{C}_{t+1} \\ &+ e^{-\rho} \frac{1}{\bar{C}} \alpha \left( \alpha - 1 \right) \left( \bar{k} \right)^{\alpha - 1} E_{t} \left[ \hat{K}_{t+1} - \hat{A}_{t+1} - \hat{L}_{t+1} \right] \\ -\hat{C}_{t} &= -E_{t} \hat{C}_{t+1} + e^{-\rho} \alpha \left( \alpha - 1 \right) \left( \bar{k} \right)^{\alpha - 1} E_{t} \left[ \hat{K}_{t+1} - \hat{A}_{t+1} - \hat{L}_{t+1} \right] \\ \hat{C}_{t} &= E_{t} \hat{C}_{t+1} - e^{-\rho} \alpha \left( \alpha - 1 \right) \left( \bar{k} \right)^{\alpha - 1} E_{t} \left[ \hat{K}_{t+1} - \hat{A}_{t+1} - \hat{L}_{t+1} \right] \\ \hat{C}_{t} &= E_{t} \hat{C}_{t+1} - \frac{\alpha \left( \alpha - 1 \right) \left( \bar{k} \right)^{\alpha - 1}}{1 + \alpha \left( \bar{k} \right)^{\alpha - 1} - \delta} E_{t} \left[ \hat{K}_{t+1} - \hat{A}_{t+1} - \hat{L}_{t+1} \right] \end{split}$$

Recall that along the steady growth path the real interest is:

$$\bar{r} = \alpha \left(\bar{k}\right)^{\alpha - 1} - \delta$$

We then write the Euler relation as:

$$\hat{C}_{t} = E_{t} \hat{C}_{t+1} - \frac{1}{1 + \alpha \left(\bar{k}\right)^{\alpha - 1} - \delta} \alpha \left(\alpha - 1\right) \left(\bar{k}\right)^{\alpha - 1} E_{t} \left[\hat{K}_{t+1} - \hat{A}_{t+1} - \hat{L}_{t+1}\right]$$

$$\hat{C}_{t} = E_{t}\hat{C}_{t+1} - \frac{1}{1+\bar{r}}\alpha (\alpha - 1) (\bar{k})^{\alpha - 1} E_{t} \left[\hat{K}_{t+1} - \hat{A}_{t+1} - \hat{L}_{t+1}\right] 
\hat{C}_{t} = E_{t}\hat{C}_{t+1} + \frac{\bar{r} + \delta}{1+\bar{r}} (1-\alpha) E_{t} \left[\hat{K}_{t+1} - \hat{A}_{t+1} - \hat{L}_{t+1}\right]$$
(20)

Investment is expanded as follows:

$$\begin{split} \frac{I_{t}}{K_{t}} &= \frac{K_{t+1}}{K_{t}} - (1 - \delta) \\ \frac{\bar{I}}{\bar{K}} + \frac{I_{t} - \bar{I}}{\bar{K}} - \frac{\bar{I}}{\bar{K}} \frac{K_{t} - \bar{K}}{\bar{K}} &= 1 - (1 - \delta) + \frac{K_{t+1} - \bar{K}}{\bar{K}} - \frac{K_{t} - \bar{K}}{\bar{K}} \\ \frac{\bar{I}}{\bar{K}} \frac{I_{t} - \bar{I}}{\bar{I}} - \frac{\bar{I}}{\bar{K}} \frac{K_{t} - \bar{K}}{\bar{K}} &= \frac{K_{t+1} - \bar{K}_{t+1}}{\bar{K}_{t+1}} - \frac{K_{t} - \bar{K}_{t}}{\bar{K}_{t}} \\ \frac{\bar{I}}{\bar{K}} \left( \hat{I}_{t} - \hat{K}_{t} \right) &= \hat{K}_{t+1} - \hat{K}_{t} \\ \hat{I}_{t} - \hat{K}_{t} &= \frac{1}{\delta} \left( \hat{K}_{t+1} - \hat{K}_{t} \right) \\ \hat{I}_{t} - \hat{K}_{t} &= \frac{1}{\delta} \left( (\eta_{KK} - 1) \hat{K}_{t} + \eta_{KA} \hat{A}_{t} + \eta_{KC} \hat{C}_{t} + \eta_{KL} \hat{I}_{t} + \eta_{KG} \hat{G}_{t} \right) \\ \hat{I}_{t} &= \left( 1 + \frac{1}{\delta} \left( \eta_{KK} - 1 \right) \right) \hat{K}_{t} \\ &+ \frac{1}{\delta} \left( \eta_{KA} \hat{A}_{t} + \eta_{KC} \hat{C}_{t} + \eta_{KL} \hat{I}_{t} + \eta_{KG} \hat{G}_{t} \right) \end{split}$$

# 4 Solution with undetermined coefficients

## 4.1 Analytical steps

The model is summarized by (18)-(20) and (5)-(6):

$$\begin{split} \hat{C}_t + \left(\frac{\bar{L}}{1 - \bar{L}} + \alpha\right) \hat{L}_t &= (1 - \alpha) \, \hat{A}_t + \alpha \hat{K}_t \\ \hat{K}_{t+1} &= \eta_{KK} \hat{K}_t + \eta_{KA} \hat{A}_t + \eta_{KC} \hat{C}_t + \eta_{KL} \hat{L}_t + \eta_{KG} \hat{G}_t \\ \hat{C}_t &= E_t \hat{C}_{t+1} + \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) \, E_t \left[ \hat{K}_{t+1} - \hat{A}_{t+1} - \hat{L}_{t+1} \right] \\ \hat{A}_t &= \rho_A \hat{A}_{t-1} + \varepsilon_{A,t} \\ \hat{G}_t &= \rho_G \hat{G}_{t-1} + \varepsilon_{G,t} \end{split}$$

There are three state variables:  $\hat{A}$ ,  $\hat{G}$  and  $\hat{K}$  and two control variables:  $\hat{C}$  and  $\hat{L}$ . The endogenous variables should then be linear functions of the state variables, with coefficients to be determined:

$$\hat{C}_{t} = a_{CK}\hat{K}_{t} + a_{CA}\hat{A}_{t} + a_{CG}\hat{G}_{t}$$

$$\hat{L}_{t} = a_{LK}\hat{K}_{t} + a_{LA}\hat{A}_{t} + a_{LG}\hat{G}_{t}$$

$$\hat{K}_{t+1} = b_{KK}\hat{K}_{t} + b_{KA}\hat{A}_{t} + b_{KG}\hat{G}_{t}$$

From (18) we write:

$$\begin{split} \hat{C}_t &= -\left(\frac{\bar{L}}{1-\bar{L}} + \alpha\right) \hat{L}_t + (1-\alpha) \, \hat{A}_t + \alpha \hat{K}_t \\ a_{CK} \hat{K}_t + a_{CA} \hat{A}_t + a_{CG} \hat{G}_t &= -\left(\frac{\bar{L}}{1-\bar{L}} + \alpha\right) \left[a_{LK} \hat{K}_t + a_{LA} \hat{A}_t + a_{LG} \hat{G}_t\right] + (1-\alpha) \, \hat{A}_t + \alpha \hat{K}_t \end{split}$$

This implies three restrictions on the coefficients:

$$a_{CK} = -\left(\frac{\bar{L}}{1-\bar{L}} + \alpha\right) a_{LK} + \alpha$$

$$a_{CA} = -\left(\frac{\bar{L}}{1-\bar{L}} + \alpha\right) a_{LA} + (1-\alpha)$$

$$a_{CG} = -\left(\frac{\bar{L}}{1-\bar{L}} + \alpha\right) a_{LG}$$
(21)

From (19) we write:

$$\begin{split} \hat{K}_{t+1} &= \eta_{KK} \tilde{K}_t + \eta_{KA} \hat{A}_t + \eta_{KC} \hat{C}_t + \eta_{KL} \hat{L}_t + \eta_{KG} \hat{G}_t \\ b_{KK} \hat{K}_t + b_{KA} \hat{A}_t + b_{KG} \hat{G}_t &= \eta_{KK} \tilde{K}_t + \eta_{KA} \hat{A}_t + \eta_{KC} \left[ a_{CK} \hat{K}_t + a_{CA} \hat{A}_t + a_{CG} \hat{G}_t \right] \\ &+ \eta_{KL} \left[ a_{LK} \hat{K}_t + a_{LA} \hat{A}_t + a_{LG} \hat{G}_t \right] + \eta_{KG} \hat{G}_t \end{split}$$

Using (21) to substitute for the coefficients on consumption, this implies three restrictions:

$$b_{KK} = \eta_{KK} + \eta_{KC}a_{CK} + \eta_{KL}a_{LK}$$

$$= \eta_{KK} + \eta_{KC}\alpha + \left[\eta_{KL} - \eta_{KC}\left(\frac{\bar{L}}{1 - \bar{L}} + \alpha\right)\right]a_{LK}$$

$$b_{KA} = \eta_{KA} + \eta_{KC}a_{CA} + \eta_{KL}a_{LA}$$

$$= \eta_{KA} + \eta_{KC}\left(1 - \alpha\right) + \left[\eta_{KL} - \eta_{KC}\left(\frac{\bar{L}}{1 - \bar{L}} + \alpha\right)\right]a_{LA}$$

$$b_{KG} = \eta_{KC}a_{CG} + \eta_{KL}a_{LG} + \eta_{KG}$$

$$= \eta_{KG} + \left[\eta_{KL} - \eta_{KC}\left(\frac{\bar{L}}{1 - \bar{L}} + \alpha\right)\right]a_{LG}$$

$$(22)$$

Given  $a_{LK}$ ,  $a_{LA}$  and  $a_{LG}$  (21)-(22) allow us to compute  $a_{CK}$ ,  $a_{CA}$  and  $a_{CG}$  and  $b_{KK}$ ,  $b_{KA}$  and  $b_{KG}$ .

We now turn to (20):

$$\hat{C}_{t} = E_{t}\hat{C}_{t+1} + \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) E_{t} \left[ \hat{K}_{t+1} - \hat{A}_{t+1} - \hat{L}_{t+1} \right]$$

$$a_{CK}\hat{K}_{t} + a_{CA}\hat{A}_{t} + a_{CG}\hat{G}_{t} = E_{t} \left[ a_{CK}\hat{K}_{t+1} + a_{CA}\hat{A}_{t+1} + a_{CG}\hat{G}_{t+1} \right]$$

$$+ \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) E_{t} \left[ \hat{K}_{t+1} - \hat{A}_{t+1} - a_{LK}\hat{K}_{t+1} - a_{LA}\hat{A}_{t+1} - a_{LG}\hat{G}_{t+1} \right]$$

$$a_{CK}\hat{K}_{t} + a_{CA}\hat{A}_{t} + a_{CG}\hat{G}_{t} = \left[ a_{CA} - \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) (1 + a_{LA}) \right] E_{t}\hat{A}_{t+1}$$

$$+ \left[ a_{CG} - \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) a_{LG} \right] E_t \hat{G}_{t+1}$$

$$+ \left[ a_{CK} + \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) [1 - a_{LK}] \right] E_t \hat{K}_{t+1}$$

Using (5)-(6) this becomes:

$$\begin{split} &a_{CK}\hat{K}_{t} + a_{CA}\hat{A}_{t} + a_{CG}\hat{G}_{t} \\ &= \left[a_{CA} - \frac{\bar{r} + \delta}{1 + \bar{r}}\left(1 - \alpha\right)\left(1 + a_{LA}\right)\right]\rho_{A}\hat{A}_{t} \\ &\quad + \left[a_{CG} - \frac{\bar{r} + \delta}{1 + \bar{r}}\left(1 - \alpha\right)a_{LG}\right]\rho_{G}\hat{G}_{t} \\ &\quad + \left[a_{CK} + \frac{\bar{r} + \delta}{1 + \bar{r}}\left(1 - \alpha\right)\left[1 - a_{LK}\right]\right]E_{t}\hat{K}_{t+1} \\ &= \left[a_{CA} - \frac{\bar{r} + \delta}{1 + \bar{r}}\left(1 - \alpha\right)\left(1 + a_{LA}\right)\right]\rho_{A}\hat{A}_{t} + \left[a_{CG} - \frac{\bar{r} + \delta}{1 + \bar{r}}\left(1 - \alpha\right)a_{LG}\right]\rho_{G}\hat{G}_{t} \\ &\quad + \left[a_{CK} + \frac{\bar{r} + \delta}{1 + \bar{r}}\left(1 - \alpha\right)\left[1 - a_{LK}\right]\right]\left[b_{KK}\hat{K}_{t} + b_{KA}\hat{A}_{t} + b_{KG}\hat{G}_{t}\right] \end{split}$$

This implies three restrictions:

$$a_{CK} = \left[ a_{CK} + \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) [1 - a_{LK}] \right] b_{KK}$$

$$a_{CA} = \left[ a_{CA} - \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) (1 + a_{LA}) \right] \rho_A + \left[ a_{CK} + \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) [1 - a_{LK}] \right] b_{KA}$$

$$a_{CG} = \left[ a_{CG} - \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) a_{LG} \right] \rho_G + \left[ a_{CK} + \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) [1 - a_{LK}] \right] b_{KG}$$

Using (21)-(22) the last two of these restrictions become:

$$\begin{aligned} 0 &= \left(\frac{\bar{L}}{1-\bar{L}} + \alpha\right) a_{LA} - (1-\alpha) \\ &+ \left[ -\left(\frac{\bar{L}}{1-\bar{L}} + \alpha + \frac{\bar{r}+\delta}{1+\bar{r}} (1-\alpha)\right) a_{LA} + \frac{1-\delta}{1+\bar{r}} (1-\alpha) \right] \rho_A \\ &+ \left[ -\left(\frac{\bar{L}}{1-\bar{L}} + \alpha + \frac{\bar{r}+\delta}{1+\bar{r}} (1-\alpha)\right) a_{LK} + \alpha + \frac{\bar{r}+\delta}{1+\bar{r}} (1-\alpha) \right] \\ &\times \left[ \eta_{KA} + \eta_{KC} (1-\alpha) + \left[ \eta_{KL} - \eta_{KC} \left(\frac{\bar{L}}{1-\bar{L}} + \alpha\right) \right] a_{LA} \right] \end{aligned}$$

and:

$$0 = \left(\frac{\bar{L}}{1-\bar{L}} + \alpha\right) a_{LG}$$

$$-\left(\frac{\bar{L}}{1-\bar{L}} + \alpha + \frac{\bar{r}+\delta}{1+\bar{r}} (1-\alpha)\right) a_{LG} \rho_{G}$$

$$+ \left[-\left(\frac{\bar{L}}{1-\bar{L}} + \alpha + \frac{\bar{r}+\delta}{1+\bar{r}} (1-\alpha)\right) a_{LK} + \alpha + \frac{\bar{r}+\delta}{1+\bar{r}} (1-\alpha)\right]$$

$$\times \left[ \eta_{KG} + \left[ \eta_{KL} - \eta_{KC} \left( \frac{\bar{L}}{1 - \bar{L}} + \alpha \right) \right] a_{LG} \right]$$

These two relations give linear solutions for  $a_{LA}$  and  $a_{LG}$  conditional on  $a_{LK}$ .

The first of the two restrictions is a quadratic polynomial in  $a_{LK}$ :

$$0 = \left(\frac{\bar{L}}{1-\bar{L}} + \alpha\right) a_{LK} - \alpha$$

$$+ \left[ -\left(\frac{\bar{L}}{1-\bar{L}} + \alpha + \frac{\bar{r}+\delta}{1+\bar{r}} (1-\alpha)\right) a_{LK} + \alpha + \frac{\bar{r}+\delta}{1+\bar{r}} (1-\alpha) \right]$$

$$\times \left[ \eta_{KK} + \eta_{KC} \alpha + \left[ \eta_{KL} - \eta_{KC} \left(\frac{\bar{L}}{1-\bar{L}} + \alpha\right) \right] a_{LK} \right]$$

We pick the value of  $a_{LK}$  such that  $b_{KK}$  is smaller than one, so the system converges back to the steady state.

#### 4.2 A numerical illustration

We take the following parameters:

$$\alpha = \frac{1}{3}, \ \delta = 0.025, \ \rho_A = \rho_G = 0.95, \ \bar{r} = 0.015, \ \frac{\bar{G}}{\bar{Y}} = 0.2, \ \bar{L} = \frac{1}{3}$$

These values imply the following:

The numerical values of the various coefficients are then:

$$\eta_{KK} = 1.015$$
 ;  $\eta_{KA} = 0.08$  ;  $\eta_{KC} = -0.071$   
 $\eta_{KL} = 0.08$  ;  $\eta_{KG} = -0.024$ 

And:

$$a_{CK} = 0.61$$
 ;  $a_{CA} = 0.37$  ;  $a_{CG} = -0.12$    
 $a_{LK} = -0.33$  ;  $a_{LA} = 0.35$  ;  $a_{LG} = 0.15$    
 $b_{KK} = 0.95$  ;  $b_{KA} = 0.08$  ;  $b_{KG} = -0.004$ 

## 5 Solution with Blanchard and Kahn

#### 5.1 Overall system

The model can be solved using the matrix representation that we used with the Ramsey model. We recall the linear system (18)-(20) and (5)-(6):

$$\hat{C}_{t} + \left(\frac{\bar{L}}{1 - \bar{L}} + \alpha\right) \hat{L}_{t} = (1 - \alpha) \hat{A}_{t} + \alpha \hat{K}_{t} 
\hat{K}_{t+1} = \eta_{KK} \hat{K}_{t} + \eta_{KA} \hat{A}_{t} + \eta_{KC} \hat{C}_{t} + \eta_{KL} \hat{L}_{t} + \eta_{KG} \hat{G}_{t} 
\hat{C}_{t} = E_{t} \hat{C}_{t+1} + \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) E_{t} \left[ \hat{K}_{t+1} - \hat{A}_{t+1} - \hat{L}_{t+1} \right] 
\hat{A}_{t} = \rho_{A} \hat{A}_{t-1} + \varepsilon_{A,t} 
\hat{G}_{t} = \rho_{G} \hat{G}_{t-1} + \varepsilon_{G,t}$$

where:

$$\eta_{KK} = 1 + \bar{r}$$

$$\eta_{KA} = \eta_{KL} = (\bar{r} + \delta) \frac{1 - \alpha}{\alpha}$$

$$\eta_{KC} = -\frac{\bar{C}}{\bar{K}}$$

$$\eta_{KG} = -\frac{\bar{G}}{\bar{K}}$$

Before writing a matrix system, we need one more step- Notice that the first equation of the system (the labor market clearing) only contains variables at time t and none at time t+1. This will lead to a problem of non-invertible matrix. To avoid this, we write labor for this condition as:

$$\hat{L}_t = \frac{(1-\alpha)}{\frac{\bar{L}}{1-\bar{L}} + \alpha} \hat{A}_t + \frac{\alpha}{\frac{\bar{L}}{1-\bar{L}} + \alpha} \hat{K}_t - \frac{1}{\frac{\bar{L}}{1-\bar{L}} + \alpha} \hat{C}_t$$

$$\hat{L}_t = \eta_{LA} \hat{A}_t + \eta_{LK} \hat{K}_t + \eta_{LC} \hat{C}_t$$

We can then write the system in a tighter form:

$$\hat{K}_{t+1} = (\eta_{KK} + \eta_{KL}\eta_{LK}) \, \hat{K}_t + (\eta_{KA} + \eta_{KL}\eta_{LA}) \, \hat{A}_t + (\eta_{KC} + \eta_{KL}\eta_{LC}) \, \hat{C}_t + \eta_{KG} \hat{G}_t$$

$$\hat{C}_t = \left(1 - \eta_{LC} \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha)\right) E_t \hat{C}_{t+1} + \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) E_t \left[ (1 - \eta_{LK}) \, \hat{K}_{t+1} - (1 + \eta_{LA}) \, \hat{A}_{t+1} \right]$$

$$\hat{A}_{t+1} = \rho_A \hat{A}_t + \varepsilon_{A,t+1}$$

$$\hat{G}_{t+1} = \rho_G \hat{G}_t + \varepsilon_{G,t+1}$$

This shows that when using the method you first need to "tighten" the system to avoid issues of non-invertible matrices.

The vectors of state variables, control variables, and shocks are:

$$S_t = \left| egin{array}{c} \hat{K}_t \\ \hat{A}_t \\ \hat{G}_t \end{array} \right| \hspace{0.5cm} ; \hspace{0.5cm} P_t = \left| \hat{C}_t \right| \hspace{0.5cm} ; \hspace{0.5cm} V_{t+1} = \left| egin{array}{c} arepsilon_{A,t+1} \\ arepsilon_{G,t+1} \end{array} \right|$$

They system is (X and Y are 4x4 matrices and Z is a 4x2 matrix):

$$X \left| \begin{array}{c} S_{t+1} \\ E_t P_{t+1} \end{array} \right| = Y \left| \begin{array}{c} S_t \\ P_t \end{array} \right| + Z V_{t+1}$$

where:

$$X = \begin{vmatrix} 1 & 0 & 0 & 0 & 0 \\ \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) (1 - \eta_{LK}) & -\frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) (1 + \eta_{LA}) & 0 & 1 - \eta_{LC} \frac{\bar{r} + \delta}{1 + \bar{r}} (1 - \alpha) \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{vmatrix}$$

$$Y = \begin{vmatrix} \eta_{KK} + \eta_{KL} \eta_{LK} & \eta_{KA} + \eta_{KL} \eta_{LA} & \eta_{KG} & \eta_{KC} + \eta_{KL} \eta_{LC} \\ 0 & 0 & 0 & 1 \\ 0 & \rho_A & 0 & 0 \\ 0 & 0 & \rho_G & 0 \end{vmatrix}$$

$$Z = \begin{vmatrix} 0 & 0 \\ 0 & 0 \\ 1 & 0 \\ 0 & 1 \end{vmatrix}$$

We rewrite the system as:

$$X \begin{vmatrix} S_{t+1} \\ E_t P_{t+1} \end{vmatrix} = Y \begin{vmatrix} S_t \\ P_t \end{vmatrix} + ZV_{t+1}$$

$$\begin{vmatrix} S_{t+1} \\ E_t P_{t+1} \end{vmatrix} = X^{-1}Y \begin{vmatrix} S_t \\ P_t \end{vmatrix} + X^{-1}ZV_{t+1}$$

$$\begin{vmatrix} S_{t+1} \\ E_t P_{t+1} \end{vmatrix} = A \begin{vmatrix} S_t \\ P_t \end{vmatrix} + BV_{t+1}$$

$$\begin{vmatrix} S_{t+1} \\ E_t P_{t+1} \end{vmatrix} = C^{-1}\Lambda C \begin{vmatrix} S_t \\ P_t \end{vmatrix} + BV_{t+1}$$

where  $\Lambda$  is the diagonal matrix of eigenvalues of A and C the matrix of eigenvectors (in the rows). We split $CA = \Lambda C$  along the lines of state and control variables::

$$\Lambda C = \left| \begin{array}{cc} J_1 & 0 \\ 0 & J_2 \end{array} \right| \left| \begin{array}{cc} C_{11} & C_{12} \\ C_{21} & C_{22} \end{array} \right|$$

where  $J_1$  is a 3x3 matrix,  $J_2$  is a 1x1 matrix,  $C_{11}$  is a 3x3 matrix,  $C_{12}$  is a 3x1 matrix,  $C_{21}$  is a 1x3 matrix,  $C_{22}$  is a 1x1 matrix. We also define:

$$Q_t = C \begin{vmatrix} S_t \\ P_t \end{vmatrix} = \begin{vmatrix} C_{11}S_t + C_{12}P_t \\ C_{21}S_t + C_{22}P_t \end{vmatrix} = \begin{vmatrix} Q_{1,t} \\ Q_{2,t} \end{vmatrix}$$

where  $Q_{1,t}$  is a 3x1 vector and  $Q_{1,t}$  is a 1x1 vector.

### 5.2 Solving for control variables

Take the expectation of the system from the point of view of t:

$$\left| \begin{array}{c} E_t S_{t+1} \\ E_t P_{t+1} \end{array} \right| = C^{-1} \Lambda C \left| \begin{array}{c} S_t \\ P_t \end{array} \right|$$

The eigenvalues in  $J_1$  are smaller than 1 and the ones in  $J_2$  are larger than one (we should of course ensure that this is indeed the case). We can write:

$$C \begin{vmatrix} E_t S_{t+1} \\ E_t P_{t+1} \end{vmatrix} = \Lambda C \begin{vmatrix} S_t \\ P_t \end{vmatrix}$$

$$E_t Q_{t+1} = \Lambda Q_t$$

$$\begin{vmatrix} E_t Q_{1,t+1} \\ E_t Q_{2,t+1} \end{vmatrix} = \begin{vmatrix} J_1 & 0 \\ 0 & J_2 \end{vmatrix} \begin{vmatrix} Q_{1,t} \\ Q_{2,t} \end{vmatrix}$$

Take the bottow row of this system:

$$E_t Q_{2,t+1} = J_2 Q_{2,t}$$

As  $J_2 > 1$  this is explosive, unless  $Q_{2,t} = 0$ :

$$0 = Q_{2,t}$$

$$0 = C_{21}S_t + C_{22}P_t$$

$$P_t = -(C_{22})^{-1}C_{21}S_t$$

This gives the control variables as a function of the state variables.

### 5.3 Solving for state variables

Take the top row of the systemt in expected terms:

$$E_{t}Q_{1,t+1} = J_{1}Q_{1,t}$$

$$C_{11}E_{t}S_{t+1} + C_{12}E_{t}P_{t+1} = J_{1}\left[C_{11}S_{t} + C_{12}P_{t}\right]$$

$$\left[C_{11} - C_{12}\left(C_{22}\right)^{-1}C_{21}\right]E_{t}S_{t+1} = J_{1}\left[C_{11} - C_{12}\left(C_{22}\right)^{-1}C_{21}\right]S_{t}$$

$$E_t S_{t+1} = (\Omega)^{-1} J_1 \Omega S_t = D S_t$$

where:  $\Omega = C_{11} - C_{12} (C_{22})^{-1} C_{21}$ .

The state variables are also affected by shocks. This component is drawn directly from the initial matrix system:

$$\begin{vmatrix} S_{t+1} \\ E_t P_{t+1} \end{vmatrix} = C^{-1} \Lambda C \begin{vmatrix} S_t \\ P_t \end{vmatrix} + B V_{t+1}$$
$$\begin{vmatrix} S_{t+1} \\ E_t P_{t+1} \end{vmatrix} = \begin{vmatrix} E_t S_{t+1} \\ E_t P_{t+1} \end{vmatrix} + B V_{t+1}$$

This implies:

$$\begin{array}{lcl} S_{t+1} & = & E_t S_{t+1} + B_T V_{t+1} \\ \\ S_{t+1} & = & D S_t + F V_{t+1} \end{array}$$

where  $B_T$  are the top rows of B, taking as many rows as they are state variables.