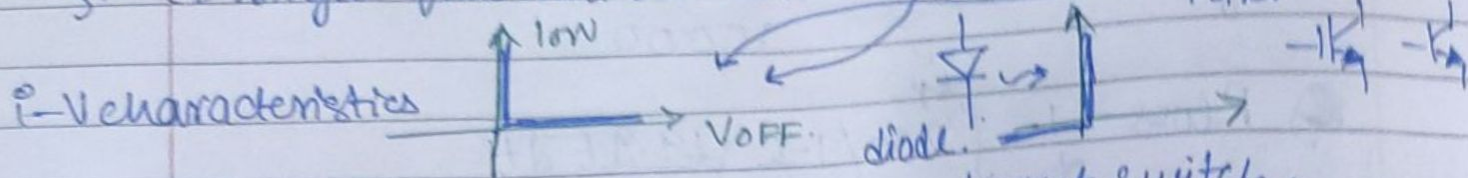
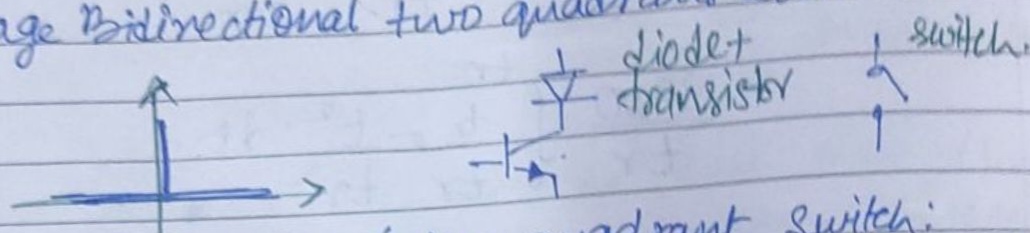


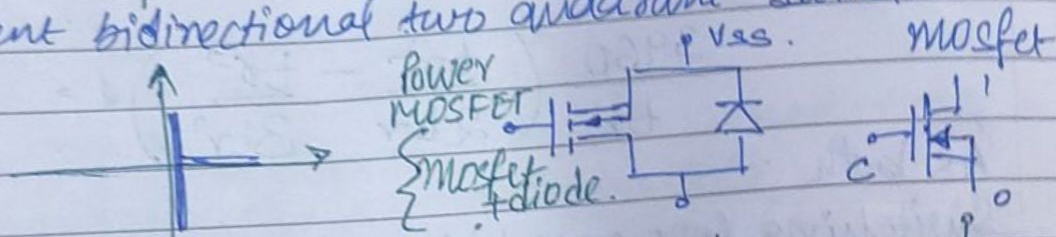
Q1. (A) single quadrant switch. = Bipolar Junction Transistor, (BJT) 1 diode.



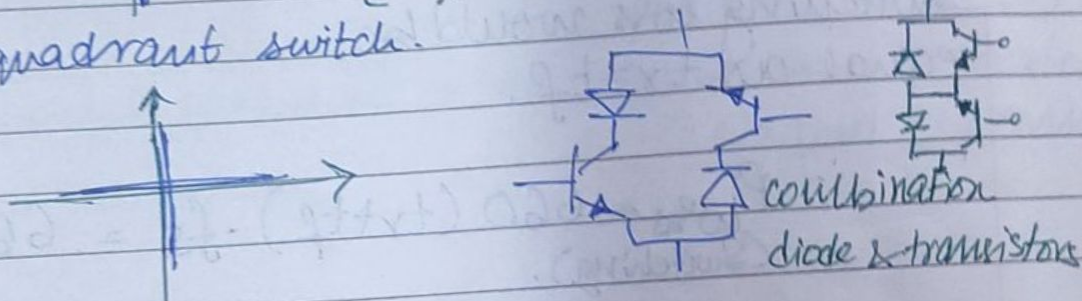
(B) voltage bidirectional two quadrant switch.



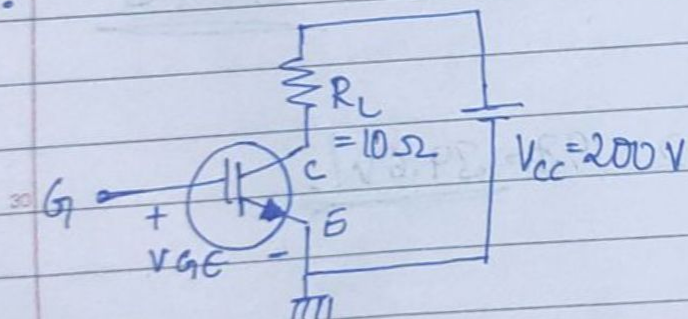
(C) current bidirectional two quadrant switch:



(d) four quadrant switch.



Q2.



$$t_{ON} = 3\mu s$$

$$t_{OFF} = 3\mu s$$

$$D = 0.7$$

$$V_{CE} = 2V$$

$$f_s = 1kHz$$

$$T_s = \frac{V_G}{f_s} = 1ms$$

(A) Avg load current

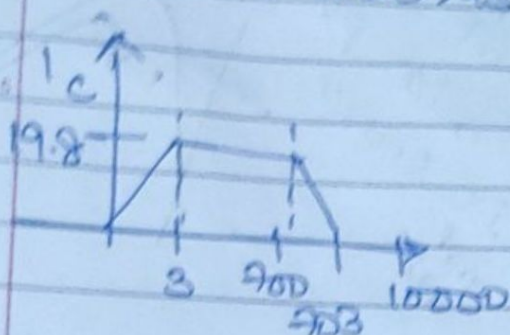
(B) Conduction loss

(C) switching loss.

Q2. (A) $T_B = \frac{1}{f_s} = 1 \text{ ms.}$

$t = 0.7 \text{ ms}$
 $= 700 \mu\text{s.}$

$I_C = \frac{250 - 2}{10}$
 $= 19.8 \text{ A.}$



$I_{C \text{ avg}} = \frac{1}{2} (703 + 697) \times \frac{19.8}{10000} = 1.386 \text{ A.}$

$P_{\text{loss}} = \frac{1}{T_B} \int_0^{T_B} 200 \left(\frac{t}{T_B} \right) + \frac{19.8 t}{T_B} dt.$

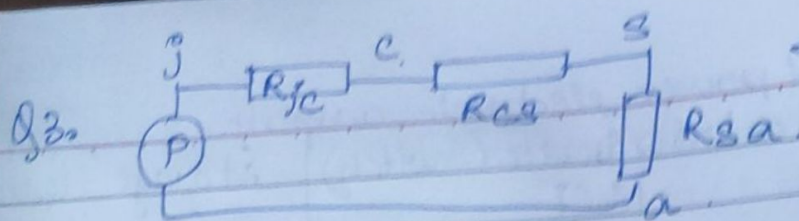
$= \frac{3960}{T_B} \int_0^{T_B} \frac{t}{T_B} - \frac{t^2}{T_B^2} dt.$

$= \frac{3960}{T_B} \left(\frac{t T_B^2}{2 T_B} - \frac{t^3}{3 T_B^2} \right) = \frac{3960}{6} = 660 \text{ W.}$

As both
 Switching loss would be
 equal as $t_r = t_f$.

$\therefore P_{\text{loss (Switching)}} = 660 (t_r + t_f) \cdot f_s = 660 \times 6 \times 10^3$
 $= 3.96 \times 10^6 \times 10^3 = \underline{\underline{3.96}}$

3) $P_{\text{loss (C)}} = V_{CE} \times I_C = 2 \times 19.8 = \underline{\underline{39.6 \text{ W.}}}$



Thermal equivalent circuit.

$T_c = 110^\circ\text{C}$, $T_a = 25^\circ\text{C}$, $T_{\text{max}} = 125^\circ\text{C}$, $R_{sa} = 0.5^\circ\text{C/W}$,
 $R_{ca} = 0.6^\circ\text{C/W}$, $R_{ja} = 0.72^\circ\text{C/W}$.

$$\begin{aligned}
 P_{\text{loss}} &= \frac{T_j - T_a}{R_{ja}} = \frac{T_c - T_a}{R_{ca}} = \frac{T_s - T_a + T_c - T_s}{R_{ca}} \\
 &= \frac{R_{cs} P_{\text{loss}} + R_{sa} P_{\text{loss}}}{R_{ca}}
 \end{aligned}$$

$$\begin{aligned}
 R_{ca} &= R_{cs} + R_{sa} \\
 R_{cs} &= 0.1^\circ\text{C/W}
 \end{aligned}$$

$$\frac{T_s - T_a}{R_{sa}} = \frac{T_c - T_s}{R_{cs}}$$

$$\frac{T_s - 25}{0.5} = \frac{110 - T_s}{0.1}$$

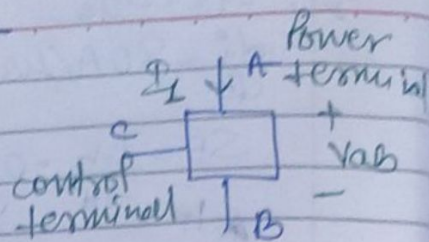
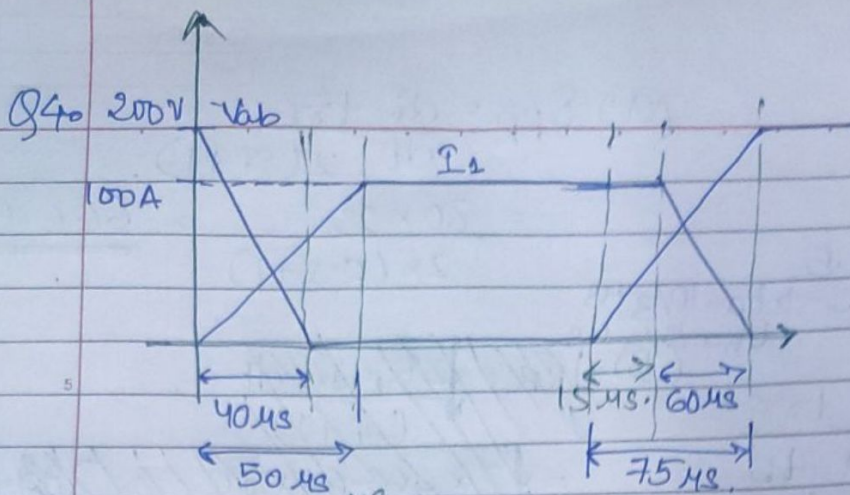
$$6T_s = 585$$

$$T_s = 97.5^\circ\text{C}$$

$$T_s = 97.5^\circ\text{C/W}$$

$$\begin{aligned}
 R_{je} &= R_{ja} - R_{cs} - R_{sa} \\
 &= 0.72 - 0.1 - 0.5
 \end{aligned}$$

$$R_{je} = 0.12^\circ\text{C/W}$$



(A) $E_{ON} = \int_0^{40 \mu s} V_{ab} I_1 dt \Rightarrow I_1 = \frac{100}{50 \times 10^{-6}} t$
 $V_{ab} = 200 \left(1 - \frac{t}{40 \times 10^{-6}}\right)$

$$E_{ON} = \int_0^{4 \times 10^{-5}} 200 \left(\frac{100t}{5 \times 10^{-5}}\right) \times \left(1 - \frac{t}{4 \times 10^{-5}}\right) dt$$

$$= \frac{2 \times 10^4}{5 \times 10^{-5}} \int_0^{4 \times 10^{-5}} \left(t - \frac{t^2}{4 \times 10^{-5}}\right) dt$$

$$= 4 \times 10^8 \left(\frac{(40 \times 10^{-6})^2}{2} - \frac{(40 \times 10^{-6})^3}{3 \times (40 \times 10^{-6})} \right)$$

$$= 4 \times 10^8 (4 \times 10^{-5})^2$$

$$= \frac{4 \times 16 \times 10^{8-10}}{6} = \frac{64 \times 10^{-2}}{6} = \underline{\underline{0.1066 \text{ J}}}$$

Q4(B).

$$V_{ab} = \frac{200}{75} \times 10^6 t = \frac{8 \times 10^6 t}{3}$$

$$t_1 = 100 \quad t \leq 15 \mu s$$

$$= 100 - \frac{100}{60} \times 10^6 t \quad 15 \leq t$$

$$\Rightarrow \left(100 - \frac{5}{3} \times 10^6 t \right)$$

$$E_{OFF} = \frac{1}{R} \int_0^{t_{OFF}} V_{ab} I_1 dt$$

$$= \int_0^{15 \mu s} \frac{8 \times 10^8}{3} t dt + \int_{15 \mu s}^{75 \mu s} \frac{8 \times 10^6 t}{3} \left(100 - \frac{5}{3} \times 10^6 t \right) dt$$

$$= \frac{8 \times 10^8}{3} \left[\frac{(15 \times 10^{-6})^2}{2} + \int_{15 \mu s}^{75 \mu s} \left(t - \frac{5}{3} \times 10^4 t^2 \right) dt \right]$$

$$= 3 \times 10^{-2} + \frac{8 \times 10^8}{3} \left[\frac{(75 \times 10^{-6} - 15 \times 10^{-6})}{(60 \times 10^{-6})(90 \times 10^{-6})} + \frac{5 \times 10^4}{3 \times 3} \left[\frac{(75 \times 10^{-6})^3}{3} - \frac{(15 \times 10^{-6})^3}{3} \right] \right]$$

$$Q_p = 3 \times 10^{-2} + \frac{8}{9} \times 10^8 [2.7 \times 10^{-10} + 2325 \times 10^{-12}]$$

$$= 3 \times 10^{-2} + \frac{8}{9} \times 5025 \times 10^{-4}$$

$$\underline{E_{off} = 137 \text{ J}}$$

$$(C) \text{ Total energy} = (1.37 + 0.1067) \text{ J}$$

$$= \underline{1.4767 \text{ J}}$$

$$(D) T = \frac{1}{f_{smax}}$$

$$\frac{1.4767}{T} = 1 \text{ K.}$$

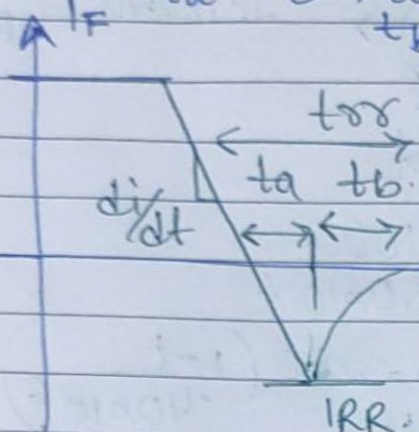
$$f_{smax} = \frac{10^3}{1.4767} = \underline{677.18 \text{ Hz}}$$

Q5. $t_{rr} = 5 \mu s$
 $\frac{di}{dt} = 80 A/\mu s$

(a) $I_{RR} = \frac{di}{dt} \frac{t_{rr}^2}{2(SF+1)}$
 $= \frac{80 \times 25}{2 \times (0.5+1)} = \underline{\underline{666.67 C}}$

$SF = \frac{t_b}{t_a} = 0.5$

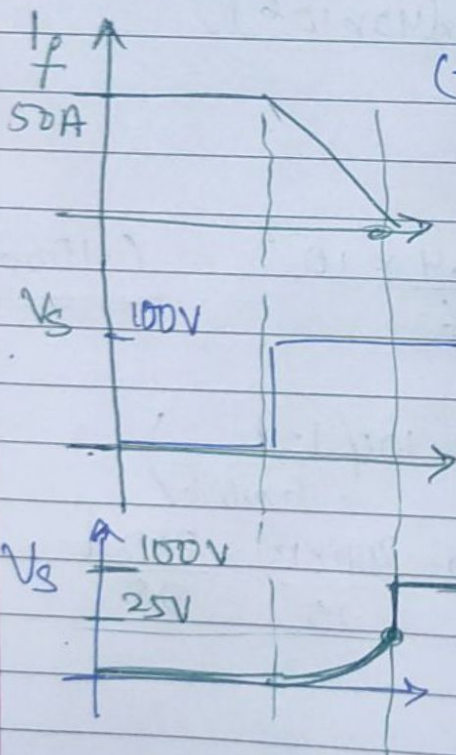
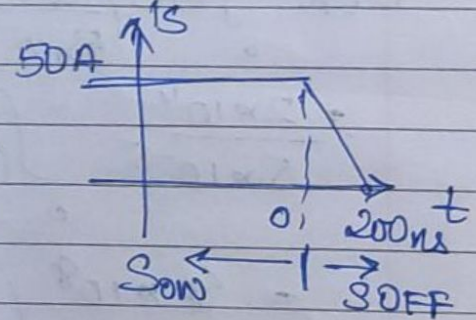
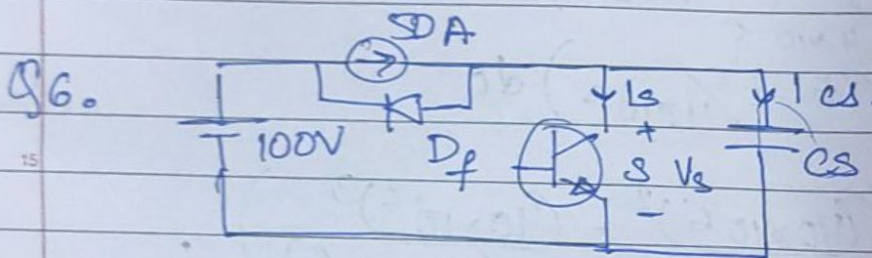
$t_a = 10/3 \mu s$
 $t_b = 5/3 \mu s$



(b) $I_{RR} = \frac{di}{dt} \frac{t_{rr}^2}{2(SF+1)}$
 $= \frac{80 \times 25}{2 \times (0.5+1)} = \underline{\underline{666.67 C}}$

OR $\frac{di}{dt} = \frac{I_{RR}}{t_a}$ $\therefore I_{RR} = \frac{800}{3} = \underline{\underline{266.66 A}}$

$C = \frac{1}{2} t_{rr} I_{RR} = 666.67 \mu F$



(A) without snubber capacitor

(B) snubber capacitance = $0.2 \mu F$
 $I_L = I_s + I_c$
 $= I_L (1 - \frac{t}{t_f}) + I_c$

As $t = t_f$
 $V_s = \frac{I_L t_f}{2C} = 25 V$

$I_c = I_L t / t_f$
 $V_s = V_c = \frac{1}{C} \int_0^{t_f} I_L t / t_f dt$
 $= \frac{I_L}{C t_f} \cdot \frac{t^2}{2}$

Q6.

(C)

$$C = \frac{50 \times 200 \times 10^{-9}}{200} = 50 \text{ nF}$$

$$C = 50 \text{ nF}$$

$$\frac{V_{\text{source}}}{I_{\text{smax}} - I_L} < R < \frac{V_{\text{CEmin}}}{I_C}$$

$$R < \frac{200 \times 10^{-9}}{50 \times 5 \times 10^{-9}}$$

$$R < 0.8 \Omega$$

$$\frac{V_{\text{source}}}{I_{\text{smax}} - I_L} < R$$

$$\frac{100}{I_{\text{smax}} - 50} < 0.8$$

$I_{\text{smax}} > 175 \text{ A}$.
maximum allowed
collector current in BJT.

$$\frac{100}{0.8} < I_{\text{smax}} - 50$$

- Q7. (A) practical power electronic converter: (Filter)
- | | |
|-------------------------------------|---------------------------------|
| Power Semiconductor Device (Switch) | Storage Element |
| - Diode | - Capacitor |
| - MOSFET | - Inductor |
| - IGBT | |
| - Thyristor | Other components |
| - SiC devices | - Heat sink cooling arrangement |
| - GaN devices | - Driver circuit |

(B) Advantages of wide Bandgap switching devices:

- wide Bandgap switching devices results in high Breakdown voltage so that it can operate at high voltages.
Power Electronic prefer high breakdown voltage semiconductors.
 - These devices also have excellent thermal stability to operate on high temperatures. (In comparison with Si, Ge, GaAs).
 - They also have critical electrical field strength which result in low ON state resistance hence conduction loss can be reduced.
 - More bandgap makes switch less sensitive to high frequency spikes and transients.
 - Example: SiC (Silicon Carbide), GaN (Gallium Nitride).
- (C) Isolation requirement of driver circuit w.r.t converter circuit diagram.

Q7 (E) MOSFET: Metal Oxide Semiconductor Field Effect Transistor
IGBT: Insulate Gate Bipolar Transistor
BJT: Bipolar Junction Transistor
SCR: Silicon Controlled Rectifier
IGCT: Integrated Gate Commutated Thyristor
GTO: Gate Turn-Off thyristor.

Q7 (D). (i) Day-to-Day life. (ii) Emerging Applications

- Power Bank (charge phones)	- Electric vehicles (TESLA)
- Solar photovoltaic	- Electric submarine
- HVDC (High voltage Direct current)	- Electric Aircrafts.