

## Simple Digital Filters

- Later in the course we shall review various methods of designing frequency-selective filters satisfying prescribed specifications
- We now describe several low-order FIR and IIR digital filters with reasonable selective frequency responses that often are satisfactory in a number of applications

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## Simple FIR Digital Filters

- FIR digital filters considered here have integer-valued impulse response coefficients
- These filters are employed in a number of practical applications, primarily because of their simplicity, which makes them amenable to inexpensive hardware implementations

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## Simple FIR Digital Filters

### Lowpass FIR Digital Filters

- The simplest lowpass FIR digital filter is the 2-point moving-average filter given by

$$H_0(z) = \frac{1}{2}(1 + z^{-1}) = \frac{z+1}{2z}$$

- The above transfer function has a zero at  $z = -1$  and a pole at  $z = 0$
- Note that here the pole vector has a unity magnitude for all values of  $\omega$

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## Simple FIR Digital Filters

- On the other hand, as  $\omega$  increases from 0 to  $\pi$ , the magnitude of the zero vector decreases from a value of 2, the diameter of the unit circle, to 0
- Hence, the magnitude response  $|H_0(e^{j\omega})|$  is a monotonically decreasing function of  $\omega$  from  $\omega = 0$  to  $\omega = \pi$

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- The maximum value of the magnitude function is 1 at  $\omega = 0$ , and the minimum value is 0 at  $\omega = \pi$  i.e.,
- The frequency response of the above filter is given by

$$|H_0(e^{j\omega})| = 1, \quad |H_0(e^{j\pi})| = 0$$

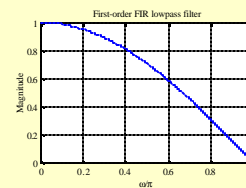
$$H_0(e^{j\omega}) = e^{-j\omega/2} \cos(\omega/2)$$

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## Simple FIR Digital Filters

- The magnitude response  $|H_0(e^{j\omega})| = \cos(\omega/2)$  can be seen to be a monotonically decreasing function of  $\omega$



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- The frequency  $\omega = \omega_c$  at which

$$\left| H_0(e^{j\omega_c}) \right| = \frac{1}{\sqrt{2}} \left| H_0(e^{j0}) \right|$$

is of practical interest since here the gain  $G(\omega_c)$  in dB is given by

$$\begin{aligned} G(\omega_c) &= 20 \log_{10} \left| H(e^{j\omega_c}) \right| \\ &= 20 \log_{10} \left| H(e^{j0}) \right| - 20 \log_{10} \sqrt{2} \cong -3 \text{ dB} \end{aligned}$$

since the dc gain  $G(0) = 20 \log_{10} \left| H(e^{j0}) \right| = 0$

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- Thus, the gain  $G(\omega)$  at  $\omega = \omega_c$  is approximately 3 dB less than the gain at  $\omega = 0$

- As a result,  $\omega_c$  is called the **3-dB cutoff frequency**

- To determine the value of  $\omega_c$  we set

$$\left| H_0(e^{j\omega_c}) \right|^2 = \cos^2(\omega_c / 2) = \frac{1}{2}$$

which yields  $\omega_c = \pi / 2$

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- The 3-dB cutoff frequency  $\omega_c$  can be considered as the passband edge frequency
- As a result, for the filter  $H_0(z)$  the passband width is approximately  $\pi/2$
- The stopband is from  $\pi/2$  to  $\pi$
- Note:  $H_0(z)$  has a zero at  $z = -1$  or  $\omega = \pi$ , which is in the stopband of the filter

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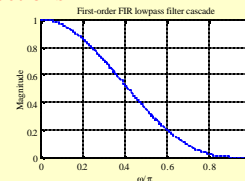
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## Simple FIR Digital Filters

- A cascade of the simple FIR filter

$$H_0(z) = \frac{1}{2}(1 + z^{-1})$$

results in an improved lowpass frequency response as illustrated below for a cascade of 3 sections



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- The 3-dB cutoff frequency of a cascade of  $M$  sections is given by

$$\omega_c = 2 \cos^{-1}(2^{-1/2M})$$

- For  $M = 3$ , the above yields  $\omega_c = 0.302\pi$
- Thus, the cascade of first-order sections yields a sharper magnitude response but at the expense of a decrease in the width of the passband

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- A better approximation to the ideal lowpass filter is given by a higher-order moving-average filter

- Signals with rapid fluctuations in sample values are generally associated with high-frequency components

- These high-frequency components are essentially removed by an moving-average filter resulting in a smoother output waveform

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## Simple FIR Digital Filters

### Highpass FIR Digital Filters

- The simplest highpass FIR filter is obtained from the simplest lowpass FIR filter by replacing  $z$  with  $-z$ .
- This results in

$$H_1(z) = \frac{1}{2}(1 - z^{-1})$$

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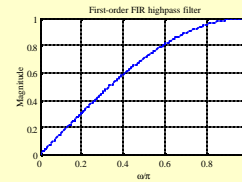
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- Corresponding frequency response is given by

$$H_1(e^{j\omega}) = j e^{-j\omega/2} \sin(\omega/2)$$

whose magnitude response is plotted below



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## Simple FIR Digital Filters

- The monotonically increasing behavior of the magnitude function can again be demonstrated by examining the pole-zero pattern of the transfer function  $H_1(z)$
- The highpass transfer function  $H_1(z)$  has a zero at  $z = 1$  or  $\omega = 0$  which is in the stopband of the filter

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## Simple FIR Digital Filters

- Improved highpass magnitude response can again be obtained by cascading several sections of the first-order highpass filter
- Alternately, a higher-order highpass filter of the form

$$H_1(z) = \frac{1}{M} \sum_{n=0}^{M-1} (-1)^n z^{-n}$$

is obtained by replacing  $z$  with  $-z$  in the transfer function of a moving average filter

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## Simple FIR Digital Filters

- An application of the FIR highpass filters is in moving-target-indicator (MTI) radars
- In these radars, interfering signals, called **clutters**, are generated from fixed objects in the path of the radar beam
- The clutter, generated mainly from ground echoes and weather returns, has frequency components near zero frequency (dc)

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- The clutter can be removed by filtering the radar return signal through a **two-pulse canceler**, which is the first-order FIR highpass filter  $H_1(z) = \frac{1}{2}(1 - z^{-1})$
- For a more effective removal it may be necessary to use a **three-pulse canceler** obtained by cascading two two-pulse cancelers

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## Simple IIR Digital Filters

### Lowpass IIR Digital Filters

- A first-order causal lowpass IIR digital filter has a transfer function given by

$$H_{LP}(z) = \frac{1-\alpha}{2} \left( \frac{1+z^{-1}}{1-\alpha z^{-1}} \right)$$

where  $|\alpha| < 1$  for stability

- The above transfer function has a zero at  $z = -1$  i.e., at  $\omega = \pi$  which is in the stopband

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## Simple IIR Digital Filters

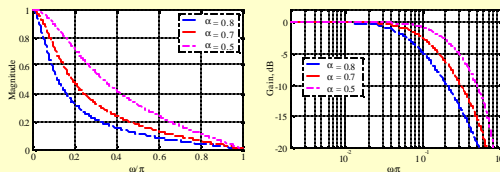
- $H_{LP}(z)$  has a real pole at  $z = \alpha$
- As  $\omega$  increases from 0 to  $\pi$ , the magnitude of the zero vector decreases from a value of 2 to 0, whereas, for a positive value of  $\alpha$ , the magnitude of the pole vector increases from a value of  $1-\alpha$  to  $1+\alpha$
- The maximum value of the magnitude function is 1 at  $\omega = 0$ , and the minimum value is 0 at  $\omega = \pi$

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- i.e.,  $|H_{LP}(e^{j0})| = 1$ ,  $|H_{LP}(e^{j\pi})| = 0$
- Therefore,  $|H_{LP}(e^{j\omega})|$  is a monotonically decreasing function of  $\omega$  from  $\omega = 0$  to  $\omega = \pi$  as indicated below



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- The squared magnitude function is given by

$$|H_{LP}(e^{j\omega})|^2 = \frac{(1-\alpha)^2(1+\cos\omega)}{2(1+\alpha^2-2\alpha\cos\omega)}$$

- The derivative of  $|H_{LP}(e^{j\omega})|^2$  with respect to  $\omega$  is given by

$$\frac{d}{d\omega} |H_{LP}(e^{j\omega})|^2 = \frac{-(1-\alpha)^2(1+2\alpha+\alpha^2)\sin\omega}{2(1-2\alpha\cos\omega+\alpha^2)^2}$$

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$d|H_{LP}(e^{j\omega})|^2/d\omega \leq 0$  in the range  $0 \leq \omega \leq \pi$  verifying again the monotonically decreasing behavior of the magnitude function

- To determine the 3-dB cutoff frequency we set

$$|H_{LP}(e^{j\omega_c})|^2 = \frac{1}{2}$$

in the expression for the square magnitude function resulting in

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$$\frac{(1-\alpha)^2(1+\cos\omega_c)}{2(1+\alpha^2-2\alpha\cos\omega_c)} = \frac{1}{2}$$

or

$$(1-\alpha)^2(1+\cos\omega_c) = 1+\alpha^2-2\alpha\cos\omega_c$$

which when solved yields

$$\cos\omega_c = \frac{2\alpha}{1+\alpha^2}$$

- The above quadratic equation can be solved for  $\alpha$  yielding two solutions

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- The solution resulting in a stable transfer function  $H_{LP}(z)$  is given by

$$\alpha = \frac{1 - \sin \omega_c}{\cos \omega_c}$$

- It follows from

$$|H_{LP}(e^{j\omega})|^2 = \frac{(1 - \alpha)^2 (1 + \cos \omega)}{2(1 + \alpha^2 - 2\alpha \cos \omega)}$$

that  $H_{LP}(z)$  is a BR function for  $|\alpha| < 1$

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## Simple IIR Digital Filters

### Highpass IIR Digital Filters

- A first-order causal highpass IIR digital filter has a transfer function given by

$$H_{HP}(z) = \frac{1 + a}{2} \left( \frac{1 - z^{-1}}{1 - az^{-1}} \right)$$

where  $|\alpha| < 1$  for stability

- The above transfer function has a zero at  $z = 1$  i.e., at  $\omega = 0$  which is in the stopband

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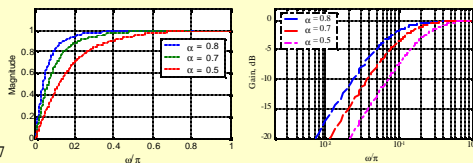
## Simple IIR Digital Filters

- Its 3-dB cutoff frequency  $\omega_c$  is given by

$$\alpha = (1 - \sin \omega_c) / \cos \omega_c$$

which is the same as that of  $H_{LP}(z)$

- Magnitude and gain responses of  $H_{HP}(z)$  are shown below



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- $H_{HP}(z)$  is a BR function for  $|\alpha| < 1$
- Example** - Design a first-order highpass digital filter with a 3-dB cutoff frequency of  $0.8\pi$

- Now,  $\sin(\omega_c) = \sin(0.8\pi) = 0.587785$  and  $\cos(0.8\pi) = -0.80902$

- Therefore

$$\alpha = (1 - \sin \omega_c) / \cos \omega_c = -0.5095245$$

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- Therefore,

$$\begin{aligned} H_{HP}(z) &= \frac{1 + a}{2} \left( \frac{1 - z^{-1}}{1 - az^{-1}} \right) \\ &= 0.245238 \left( \frac{1 - z^{-1}}{1 + 0.5095245 z^{-1}} \right) \end{aligned}$$

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## Simple IIR Digital Filters

### Bandpass IIR Digital Filters

- A 2nd-order bandpass digital transfer function is given by

$$H_{BP}(z) = \frac{1 - \alpha}{2} \left( \frac{1 - z^{-2}}{1 - \beta(1 + \alpha)z^{-1} + \alpha z^{-2}} \right)$$

- Its squared magnitude function is

$$\begin{aligned} |H_{BP}(e^{j\omega})|^2 &= \frac{(1 - \alpha)^2 (1 - \cos 2\omega)}{2[1 + \beta^2(1 + \alpha)^2 + \alpha^2 - 2\beta(1 + \alpha)^2 \cos \omega + 2\alpha \cos 2\omega]} \end{aligned}$$

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- $|H_{BP}(e^{j\omega})|^2$  goes to zero at  $\omega = 0$  and  $\omega = \pi$
- It assumes a maximum value of 1 at  $\omega = \omega_o$ , called the **center frequency** of the bandpass filter, where
 
$$\omega_o = \cos^{-1}(\beta)$$
- The frequencies  $\omega_{c1}$  and  $\omega_{c2}$  where  $|H_{BP}(e^{j\omega})|^2$  becomes 1/2 are called the **3-dB cutoff frequencies**

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## Simple IIR Digital Filters

- The difference between the two cutoff frequencies, assuming  $\omega_{c2} > \omega_{c1}$  is called the **3-dB bandwidth** and is given by

$$B_w = \omega_{c2} - \omega_{c1} = \cos^{-1}\left(\frac{2\alpha}{1+\alpha^2}\right)$$

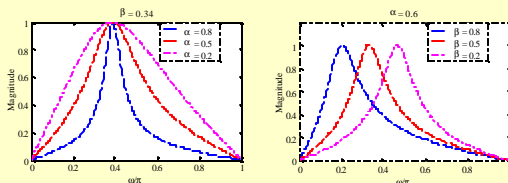
- The transfer function  $H_{BP}(z)$  is a BR function if  $|\alpha| < 1$  and  $|\beta| < 1$

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## Simple IIR Digital Filters

- Plots of  $|H_{BP}(e^{j\omega})|$  are shown below



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- **Example** - Design a 2nd order bandpass digital filter with center frequency at  $0.4\pi$  and a 3-dB bandwidth of  $0.1\pi$
- Here  $\beta = \cos(\omega_o) = \cos(0.4\pi) = 0.309017$  and

$$\frac{2\alpha}{1+\alpha^2} = \cos(B_w) = \cos(0.1\pi) = 0.9510565$$

- The solution of the above equation yields:  $\alpha = 1.376382$  and  $\alpha = 0.72654253$

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## Simple IIR Digital Filters

- The corresponding transfer functions are

$$H'_{BP}(z) = -0.18819 \frac{1 - z^{-2}}{1 - 0.7343424z^{-1} + 1.37638z^{-2}}$$

and

$$H''_{BP}(z) = 0.13673 \frac{1 - z^{-2}}{1 - 0.533531z^{-1} + 0.72654253z^{-2}}$$

- The poles of  $H'_{BP}(z)$  are at  $z = 0.3671712 \pm j1.11425636$  and have a magnitude  $> 1$

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## Simple IIR Digital Filters

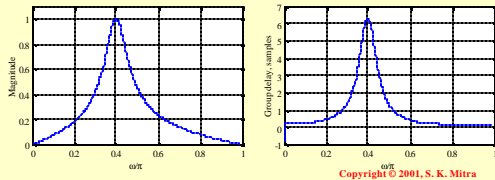
- Thus, the poles of  $H'_{BP}(z)$  are outside the unit circle making the transfer function unstable
- On the other hand, the poles of  $H''_{BP}(z)$  are at  $z = 0.2667655 \pm j0.8095546$  and have a magnitude of 0.8523746
- Hence  $H''_{BP}(z)$  is BIBO stable
- Later we outline a simpler stability test

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- Figures below show the plots of the magnitude function and the group delay of  $H_{BP}^n(z)$



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### Bandstop IIR Digital Filters

- A 2nd-order bandstop digital filter has a transfer function given by

$$H_{BS}(z) = \frac{1+\alpha}{2} \left( \frac{1-2\beta z^{-1}+z^{-2}}{1-\beta(1+\alpha)z^{-1}+\alpha z^{-2}} \right)$$

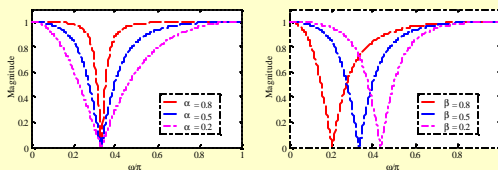
- The transfer function  $H_{BS}(z)$  is a BR function if  $|\alpha| < 1$  and  $|\beta| < 1$

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## Simple IIR Digital Filters

- Its magnitude response is plotted below



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- Here, the magnitude function takes the maximum value of 1 at  $\omega = 0$  and  $\omega = \pi$
- It goes to 0 at  $\omega = \omega_o$ , where  $\omega_o$ , called the **notch frequency**, is given by  $\omega_o = \cos^{-1}(\beta)$
- The digital transfer function  $H_{BS}(z)$  is more commonly called a **notch filter**

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## Simple IIR Digital Filters

- The frequencies  $\omega_{c1}$  and  $\omega_{c2}$  where  $|H_{BS}(e^{j\omega})|^2$  becomes 1/2 are called the **3-dB cutoff frequencies**
- The difference between the two cutoff frequencies, assuming  $\omega_{c2} > \omega_{c1}$  is called the **3-dB notch bandwidth** and is given by

$$B_w = \omega_{c2} - \omega_{c1} = \cos^{-1} \left( \frac{2\alpha}{1+\alpha^2} \right)$$

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## Simple IIR Digital Filters

### Higher-Order IIR Digital Filters

- By cascading the simple digital filters discussed so far, we can implement digital filters with sharper magnitude responses
- Consider a cascade of  $K$  first-order lowpass sections characterized by the transfer function

$$H_{LP}(z) = \frac{1-\alpha}{2} \left( \frac{1+z^{-1}}{1-\alpha z^{-1}} \right)^K$$

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## Simple IIR Digital Filters

- The overall structure has a transfer function given by

$$G_{LP}(z) = \left( \frac{1-\alpha}{2} \cdot \frac{1+z^{-1}}{1-\alpha z^{-1}} \right)^K$$

- The corresponding squared-magnitude function is given by

$$|G_{LP}(e^{j\omega})|^2 = \left[ \frac{(1-\alpha)^2(1+\cos\omega)}{2(1+\alpha^2-2\alpha\cos\omega)} \right]^K$$

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- To determine the relation between its 3-dB cutoff frequency  $\omega_c$  and the parameter  $\alpha$ , we set

$$\left[ \frac{(1-\alpha)^2(1+\cos\omega_c)}{2(1+\alpha^2-2\alpha\cos\omega_c)} \right]^K = \frac{1}{2}$$

which when solved for  $\alpha$ , yields for a stable  $G_{LP}(z)$ :

$$\alpha = \frac{1+(1-C)\cos\omega_c - \sin\omega_c\sqrt{2C-C^2}}{1-C+\cos\omega_c}$$

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where

$$C = 2^{(K-1)/K}$$

- It should be noted that the expression for  $\alpha$  given earlier reduces to

$$\alpha = \frac{1 - \sin\omega_c}{\cos\omega_c}$$

for  $K = 1$

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## Simple IIR Digital Filters

- Example** - Design a lowpass filter with a 3-dB cutoff frequency at  $\omega_c = 0.4\pi$  using a single first-order section and a cascade of 4 first-order sections, and compare their gain responses
- For the single first-order lowpass filter we have

$$\alpha = \frac{1 + \sin\omega_c}{\cos\omega_c} = \frac{1 + \sin(0.4\pi)}{\cos(0.4\pi)} = 0.1584$$

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- For the cascade of 4 first-order sections, we substitute  $K = 4$  and get

$$C = 2^{(K-1)/K} = 2^{(4-1)/4} = 1.6818$$

- Next we compute

$$\alpha = \frac{1 + (1-C)\cos\omega_c - \sin\omega_c\sqrt{2C-C^2}}{1-C+\cos\omega_c}$$

$$= \frac{1 + (1-1.6818)\cos(0.4\pi) - \sin(0.4\pi)\sqrt{2(1.6818) - (1.6818)^2}}{1-1.6818+\cos(0.4\pi)}$$

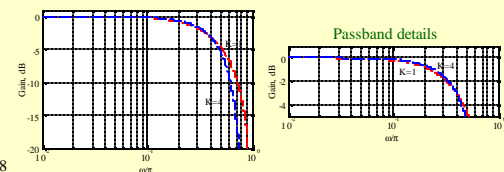
$$= -0.251$$

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## Simple IIR Digital Filters

- The gain responses of the two filters are shown below
- As can be seen, cascading has resulted in a sharper roll-off in the gain response



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