

Revisiting phenomena and instability mechanisms

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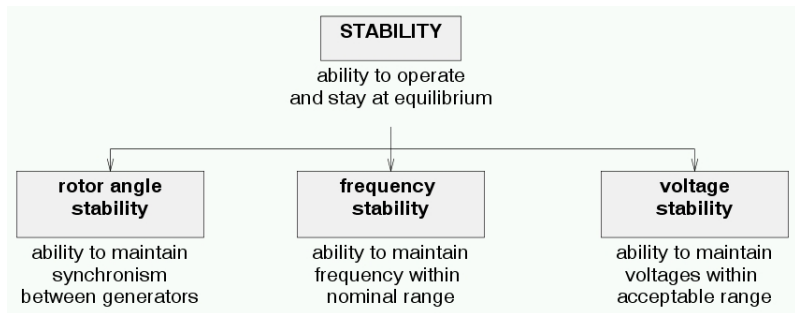
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Objectives

- definition and classification of power system stability notions
- qualitative explanation of instability mechanisms
- emphasis put on instability triggered by a large disturbance
- illustration from time simulations of a simple system

Main classification of stability problems



(Rotor) angle stability

- most of the electrical energy is generated by synchronous machines
- in normal system operation:
 - all synchronous machines have the same electrical speed $2\pi f$
 - the mechanical and electromagnetic torques acting on the rotating masses of each generator balance each other
 - the difference between the rotor angles of any two machines is constant = *synchronism*
- following a disturbance, there is an imbalance between the two torques and the rotor speed varies
- *rotor angle stability deals with the ability to keep synchronism after being subject to a disturbance*

Small-disturbance angle stability

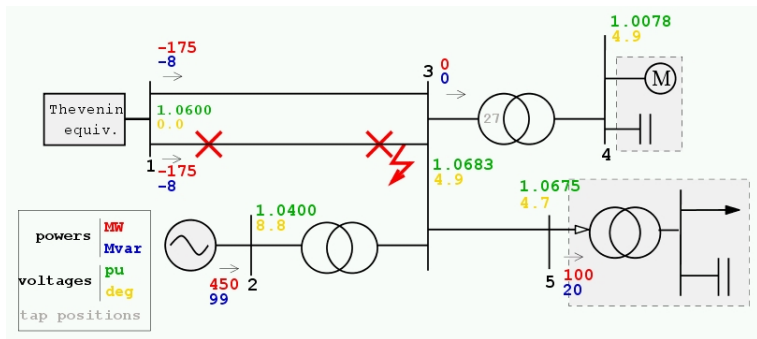
- *small-signal (or small-disturbance) angle stability deals with the ability of the system to keep synchronism after being subject to small disturbances*
- “small disturbances” are those for which the system equations can be linearized (around an equilibrium point)
- following small disturbances, the change in electromagnetic torque has two components:
 - *synchronizing torque* proportional to rotor angle deviation
 - *damping torque* proportional to rotor speed deviation
- a decrease in synchronizing torque will eventually lead to aperiodic instability (machine “going out of step”)
- a decrease in damping torque will eventually lead to oscillatory instability (growing oscillations)

Transient (angle) stability

- *transient (angle) stability deals with the ability of the system to keep synchronism after being subject to a large disturbance*
- typical “large” disturbances:
 - short-circuit cleared by opening of circuit breakers
 - more complex sequences in case of breaker failure, line autoreclosing, etc.
- synchronizing torque T_s is nonlinear function of rotor angle δ :
the larger $\Delta\delta$, the lower $\frac{\Delta T_s}{\Delta\delta}$ (“stiffness”)
- for large disturbances, this nonlinear effect must be taken into account
- unacceptable consequences of transient instability:
 - generators losing synchronism are tripped by protections
 - large angle swings create voltage dips disturbing customers

- small-signal angle stability:
 - depends on operating point and system parameters
 - does not depend on the disturbance (assumed infinitesimal and arbitrary)
 - is a necessary condition for operating a power system (small disturbances are always present !)
- transient stability:
 - depends on operating point, system parameters, AND the disturbance:
 - the system may be stable wrt disturbance D1 but not disturbance D2
 - if so, the system is *insecure* wrt D2, but as long as D2 does not happen, it can operate. . .

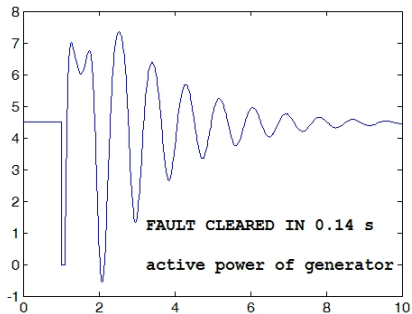
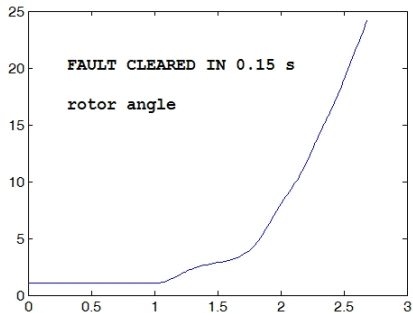
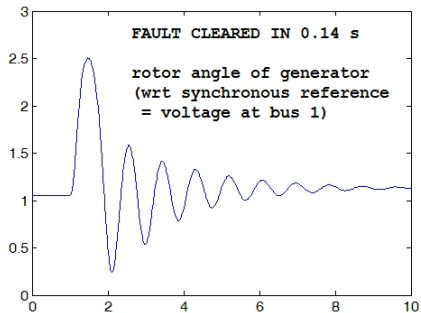
Transient stability - example



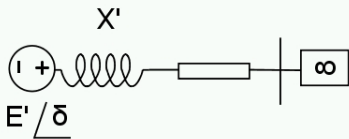
- synchronous generator (6th-order model) with Automatic Voltage Regulator (AVR), steam turbine and speed governor
- external system represented by Thévenin equivalent

short-circuit at $t = 1$ s, on line 1-3, near bus 3

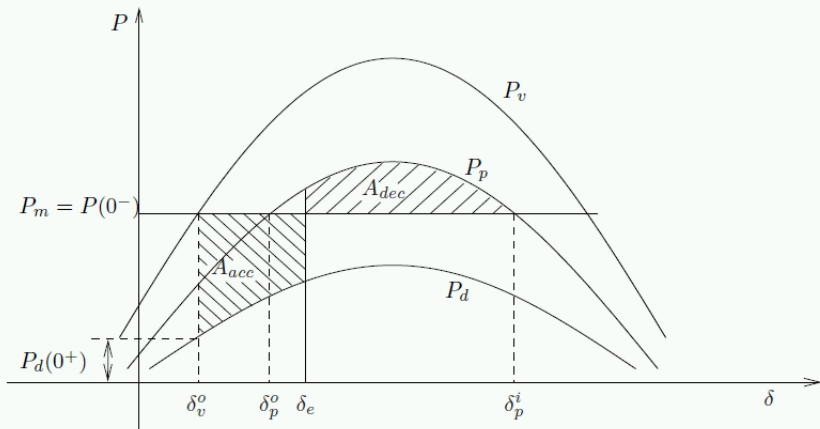
cleared by opening one circuit, after 0.14 and 0.15 s, respectively



Transient instability mechanism - equal-area criterion



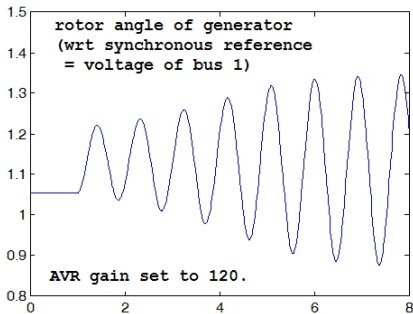
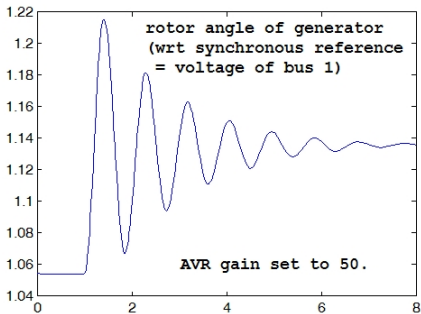
$$M \frac{d^2 \delta}{dt^2} = P_m - P(\delta)$$



Small-signal angle stability - example

same initial power flow

tripping of the line without short-circuit



with the AVR gain increased to 120, the post-disturbance equilibrium is almost the same but is oscillatory unstable

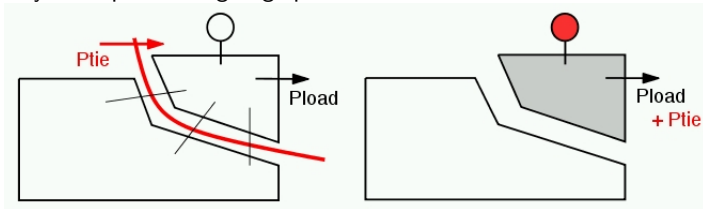
Not shown by this simple example: interarea oscillations

Frequency stability

- Electricity cannot be stored as such (in significant amount). It has to be converted into/from other forms of energy
- the active power balance $P_{gener} = P_{load} + P_{losses}$ must be satisfied at any time
- immediately after a disturbance:
 - generation deficit taken from kinetic energy of rotating masses in power plants \longrightarrow speed decrease \longrightarrow drop in frequency
 - generation excess given to rotating masses \longrightarrow speed increase \longrightarrow rise in frequency
- fastly, the speed deviation is corrected by *speed governors* adjusting the turbine control valves (to change the steam/water flow) = *primary frequency control*
- later on, frequency deviations left by primary control are corrected by *secondary frequency (or load frequency) control*
- together with deviations of tie-line power flows from schedule

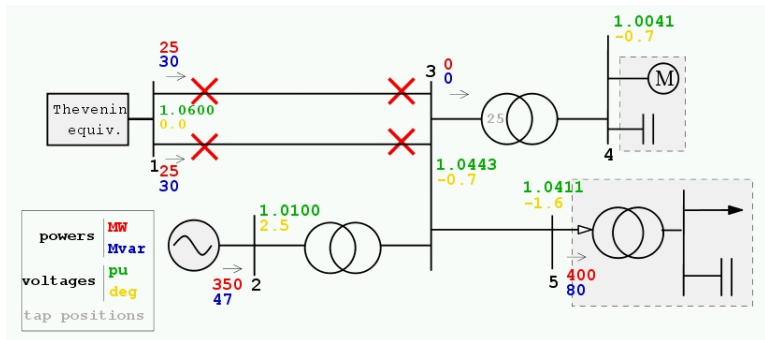
Frequency stability

- *Frequency stability deals with the ability of the system to keep frequency near its nominal value after a severe disturbance, with or without system split*
- in large interconnections:
 - frequency is controlled accurately
Example: sensitivity of UCTE system $\simeq 18,000$ MW/Hz
 - frequency instability of concern after:
 - a system split causing large power imbalance



- a severe loss of generation
Example: UCTE: maximum 3,000 MW

Frequency stability - example 1

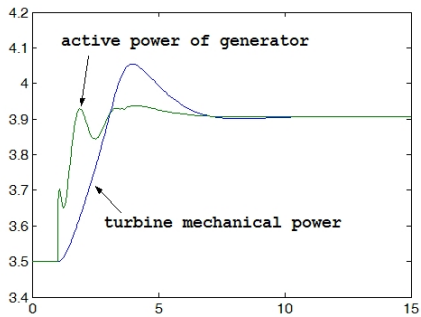
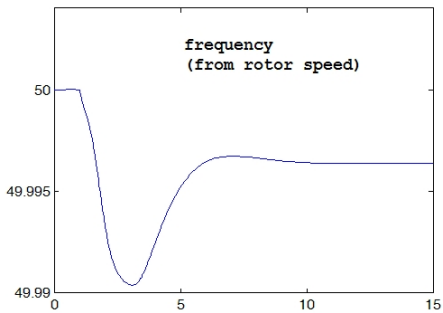


50 MW imported from equivalent system

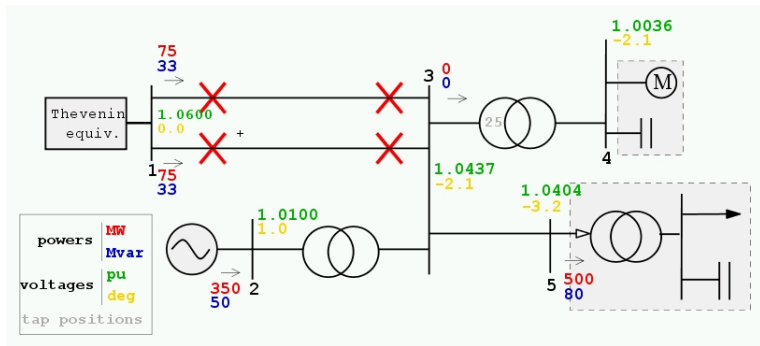
at $t = 1$ s, tripping of the double line

⇒ generator and load left isolated

generator driven by a turbine with 450 MW nominal power



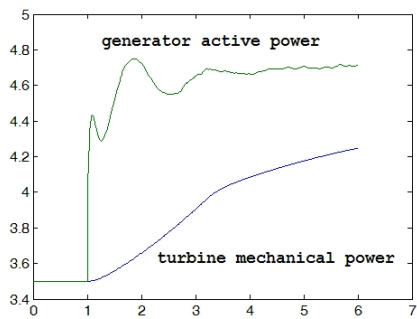
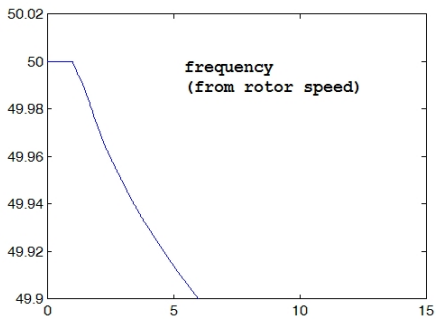
Frequency stability - example 2



same disturbance

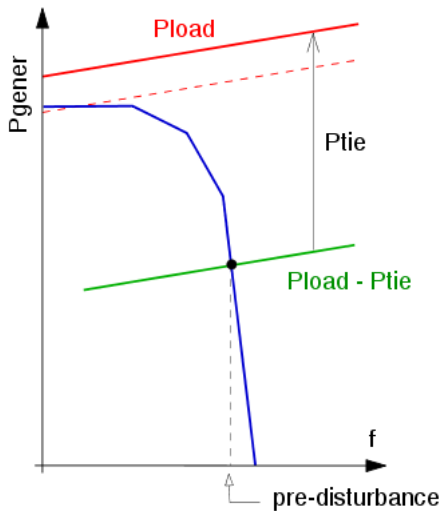
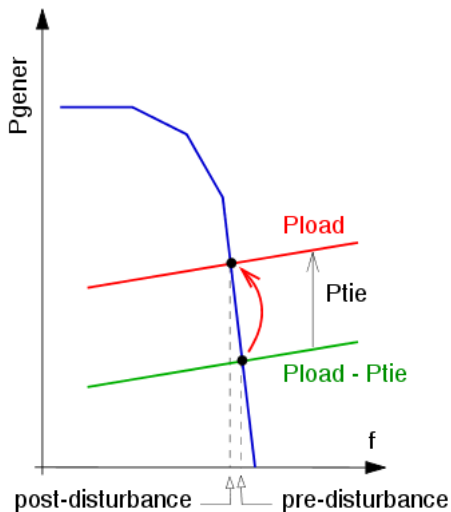
different operating point:

larger load and larger power import from equivalent system



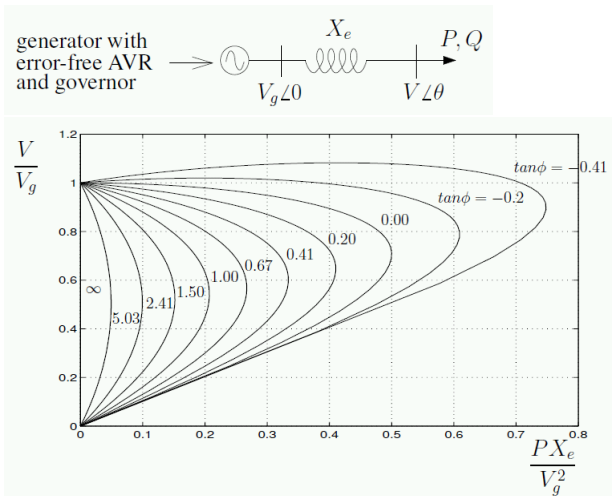
Frequency instability mechanism

combined steady-state characteristics
of turbines and speed governors in islanded network



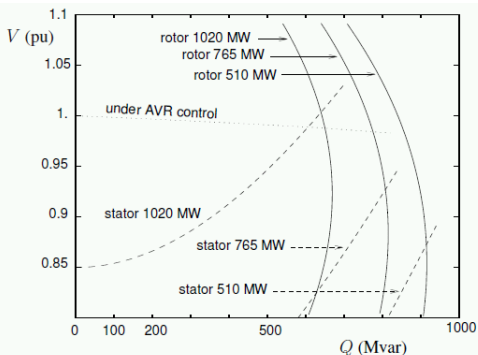
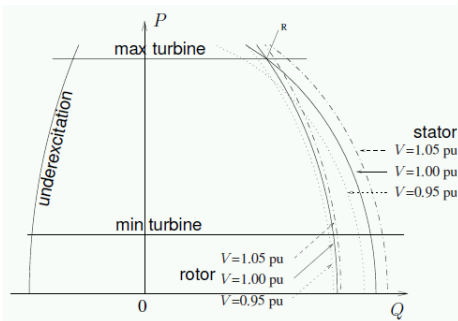
Voltage stability

- There is a maximum power that generators can deliver to loads through the network



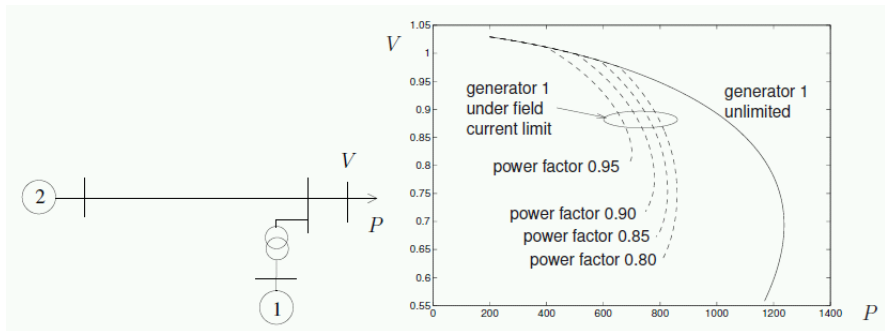
Voltage stability

- the reactive power production of a generator is limited by the thermal overload of the field winding
- when the OverExcitation limiter (OXL) is active the generator voltage is no longer controlled
- the stator (or armature) current may be also limiting



Voltage stability

- the reactive power limits of generators strongly impact the maximum power that can be delivered to loads



Voltage stability

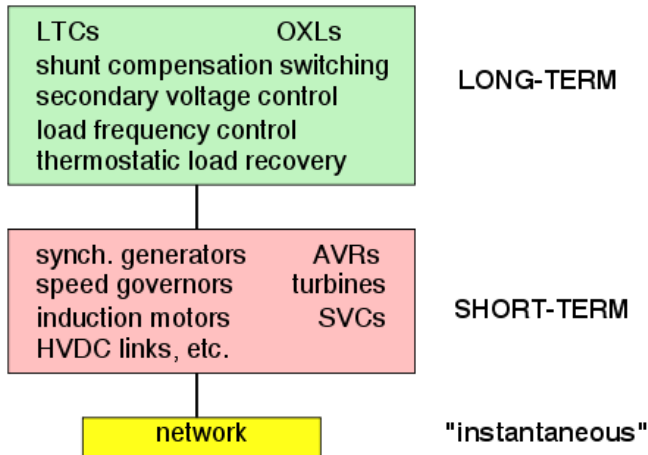
- after being subject to a voltage drop, some loads tend to restore their power consumption (close) to their pre-disturbance value

component	time scale	internal variable	equilibrium condition
induction motor	$\simeq 1$ second	motor speed	mechan. torque = electrom. torque
load tap changer	\simeq few minutes	transformer ratio	controlled voltage within deadband
thermostatically controlled load	\simeq few tens of minutes	amount of connected load	temperature within deadband

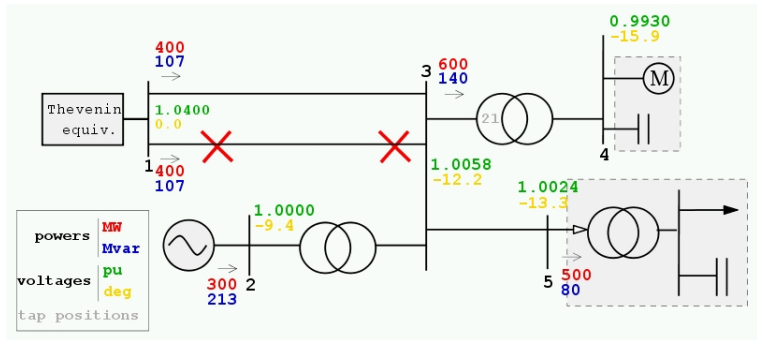
Voltage stability

- *Voltage stability deals with the ability of the system to keep voltages near their nominal values after a disturbance*
- voltage instability results from the inability of the combined transmission-generation system to provide the power requested by loads
- it is usually characterized by a monotonic decrease of system voltages
- it may develop in the short- as well as in the long-term time scale.

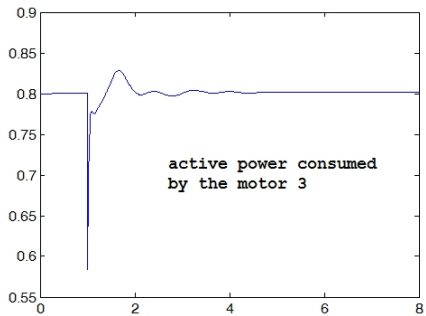
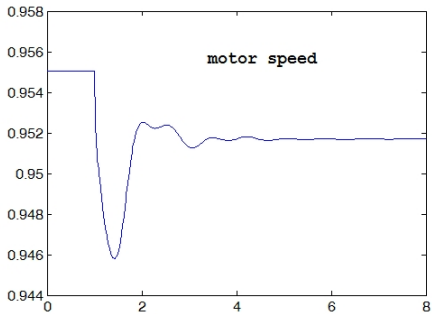
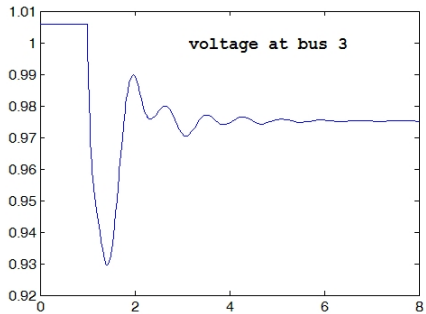
Time-scale decomposition



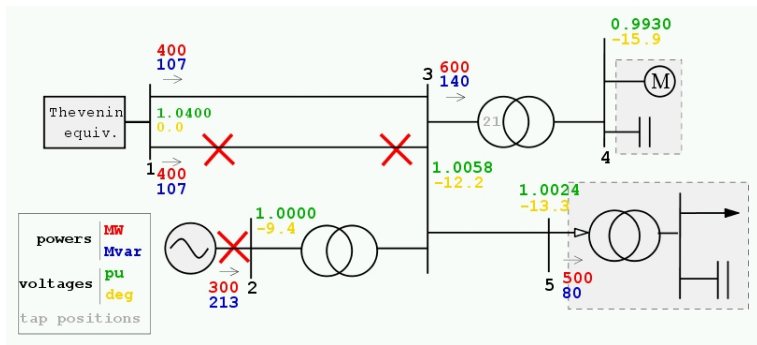
Short-term voltage stability - example 1



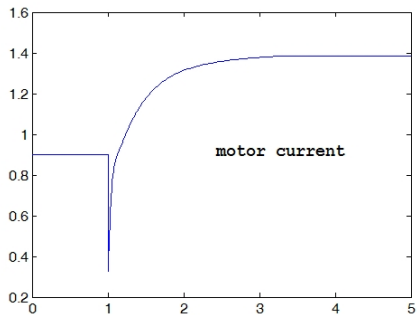
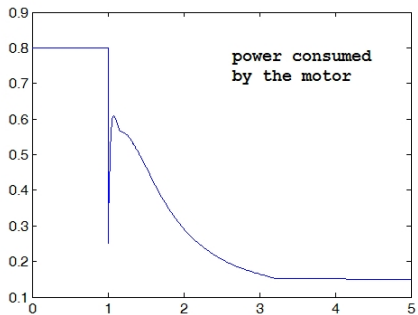
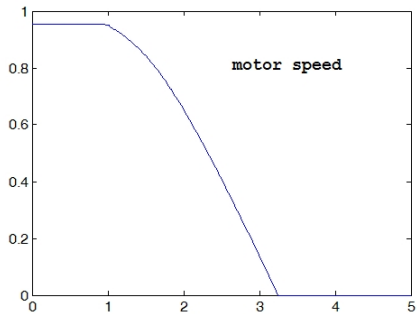
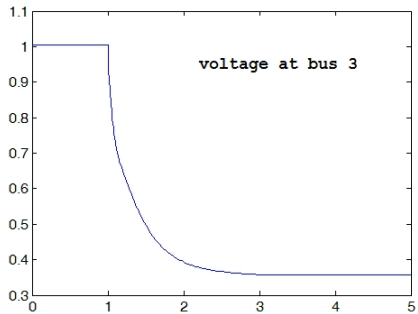
55 % induction motor load (single-motor equivalent)
at $t = 1$ s, tripping of one circuit of the line



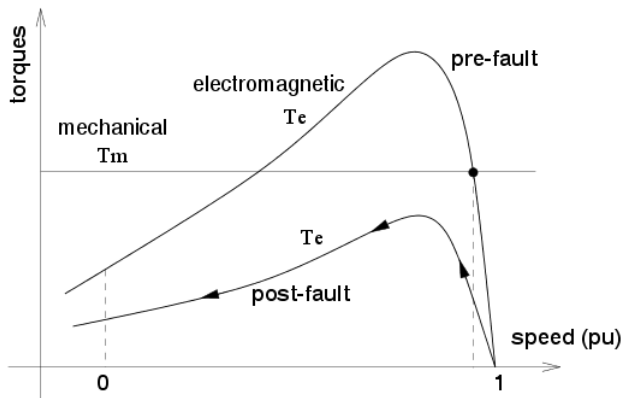
Short-term voltage stability - example 2



at $t = 1$ s, tripping of both the generator and one circuit of the line

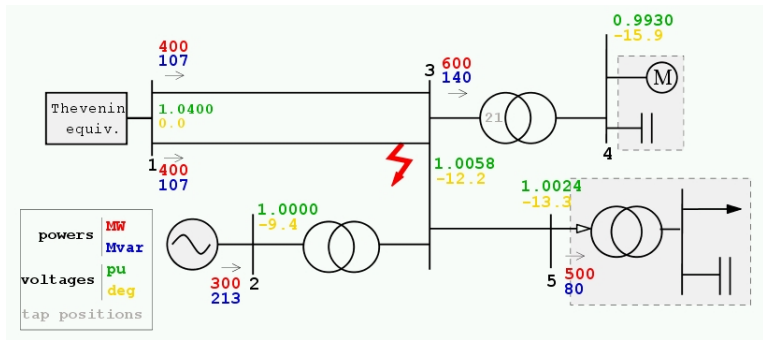


instability mechanism shown by motor speed-torque curves



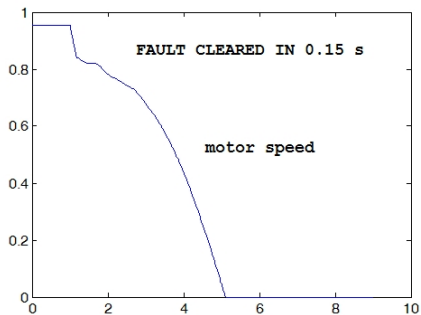
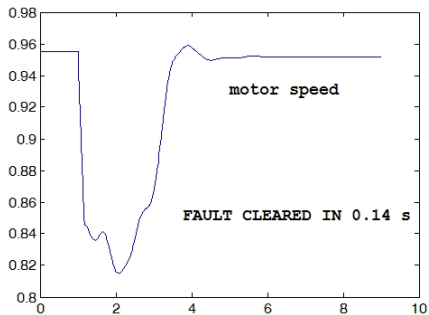
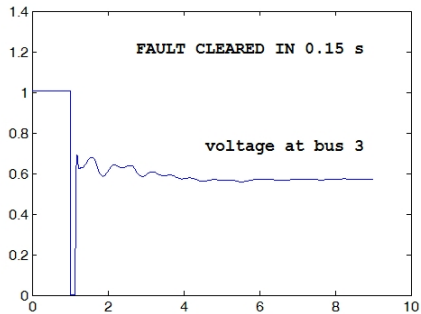
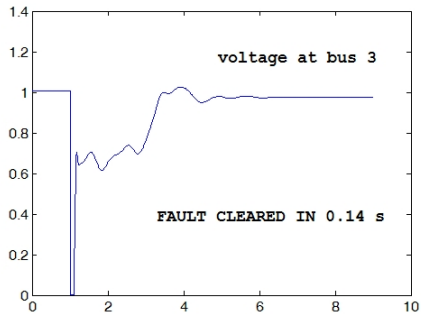
loss of short-term equilibrium

Short-term voltage stability - example 3

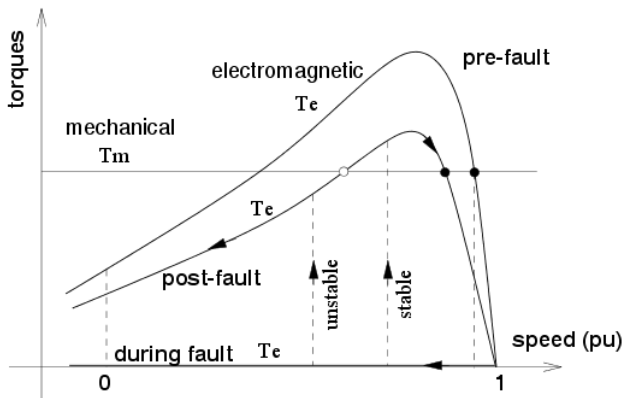


short-circuit at $t = 1$ s, on line 1-3, near bus 3

cleared by opening one circuit, after 0.14 and 0.15 s, respectively

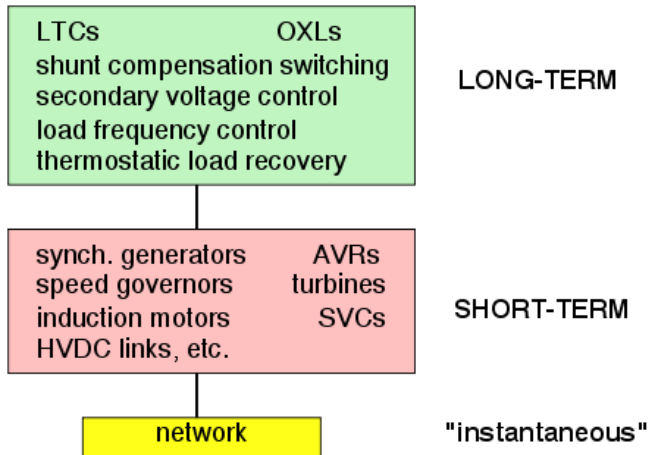


instability mechanism shown by motor speed-torque curves

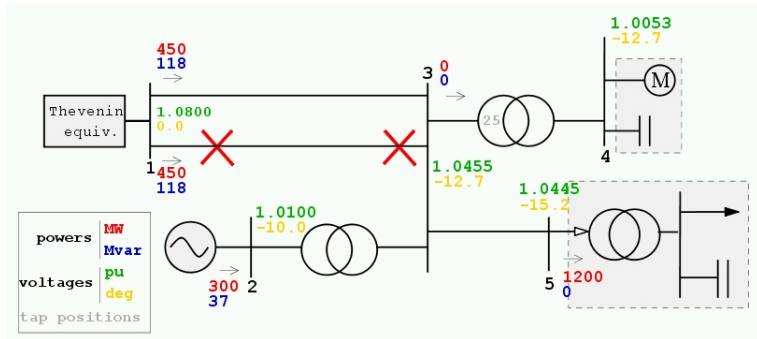


lack of attraction to post-fault stable equilibrium

Time-scale decomposition



Long-term voltage stability - example 1

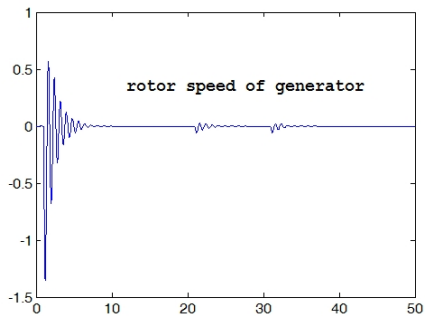
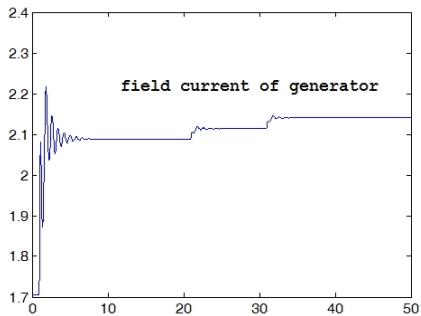
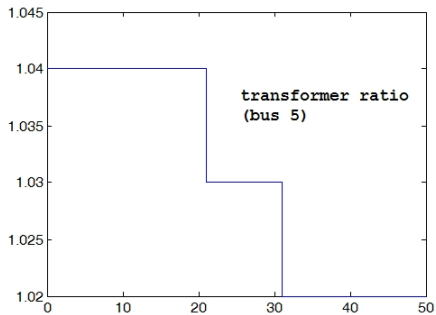
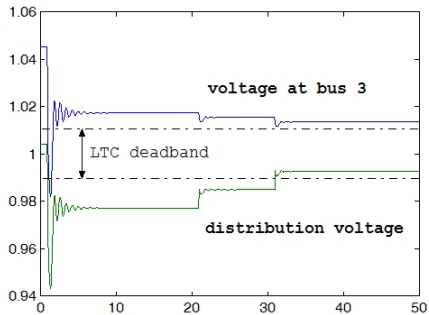


whole load with exponential model $P = \left(\frac{V}{V_0}\right)^{1.5}$ $Q = \left(\frac{V}{V_0}\right)^{2.5}$

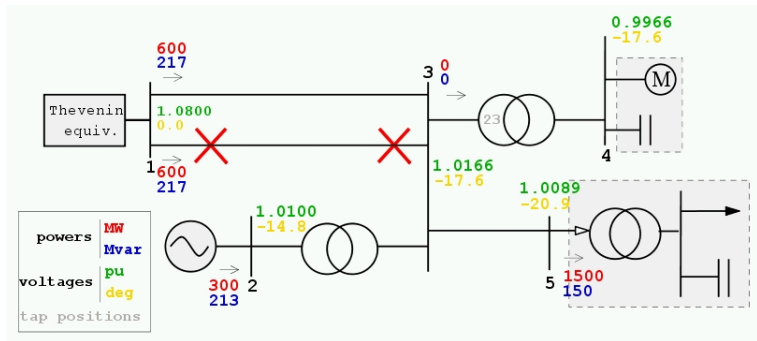
Load Tap Changer (LTC) controlling distribution voltage

generator equipped with field current limiter

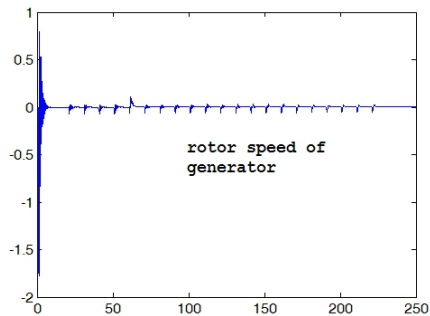
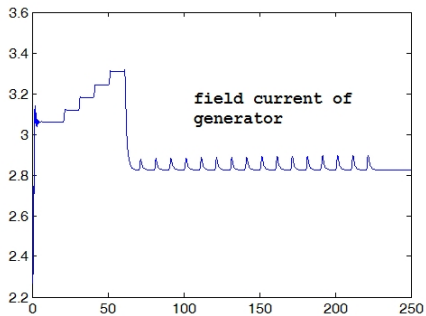
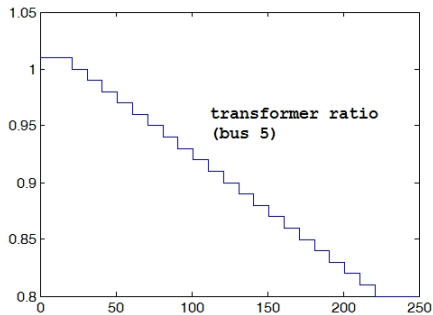
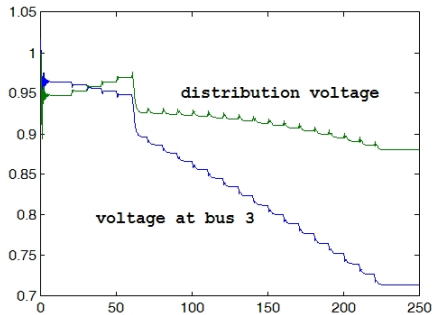
at $t = 1$ s, tripping of one circuit of the line



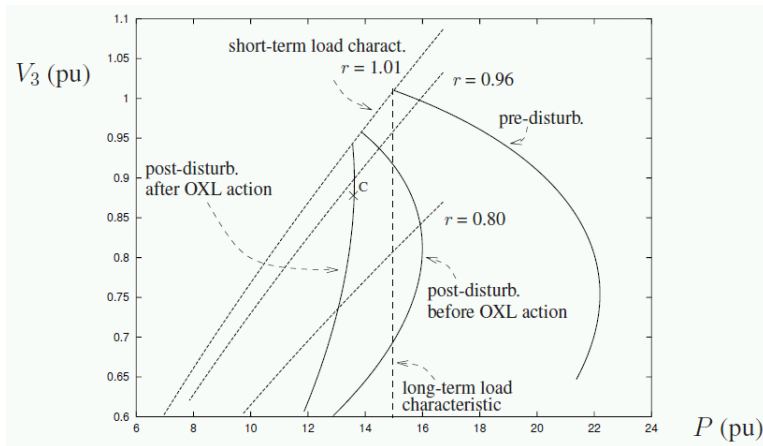
Long-term voltage stability - example 2



larger load
same disturbance

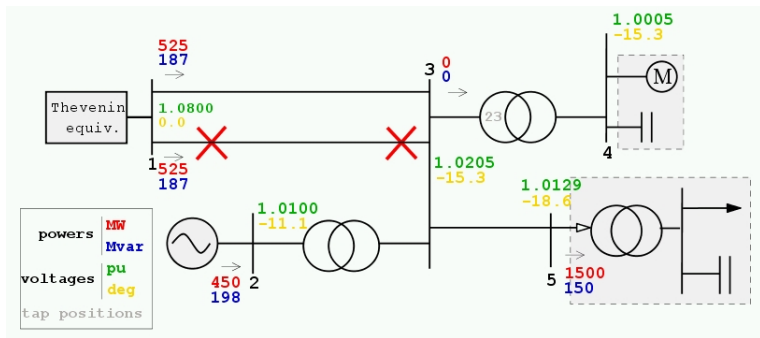


instability mechanism shown by PV curves

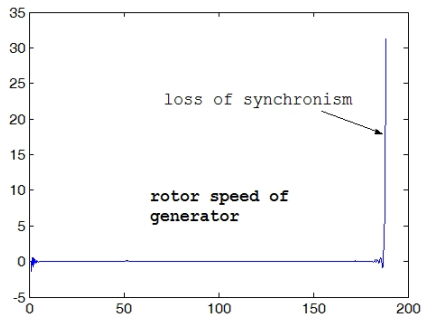
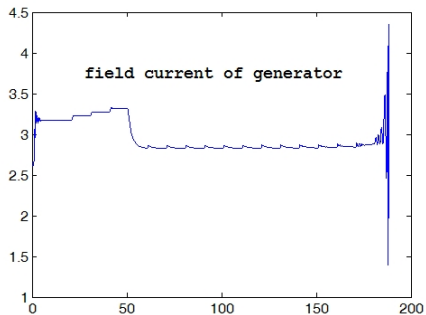
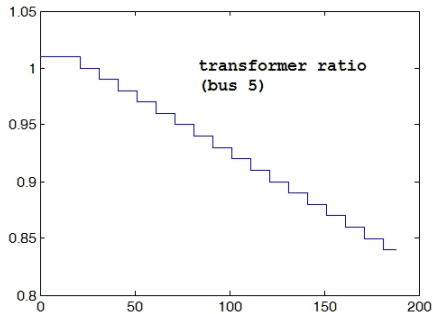
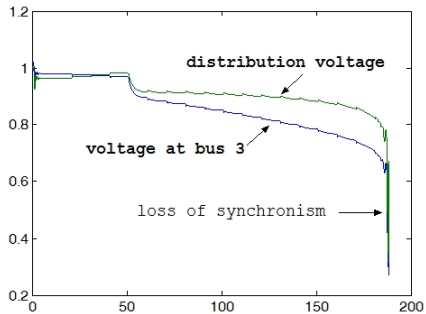


loss of equilibrium of long-term dynamics
pseudo-stabilization when LTC hits its limit
a case of “pure” long-term voltage instability

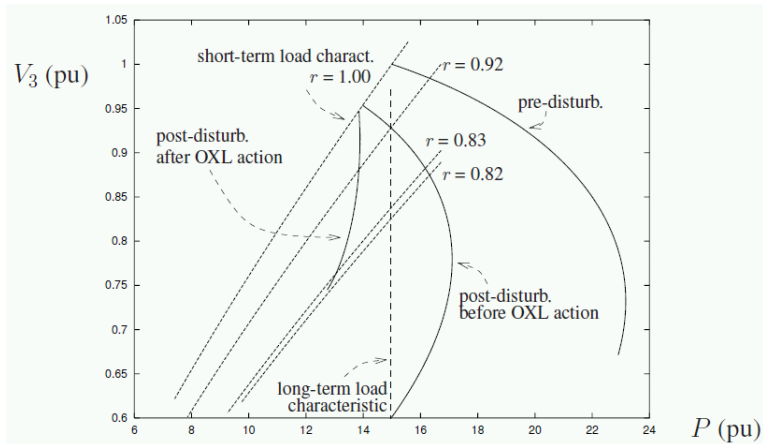
Long-term voltage stability - example 3



same load, larger production of generator
same disturbance

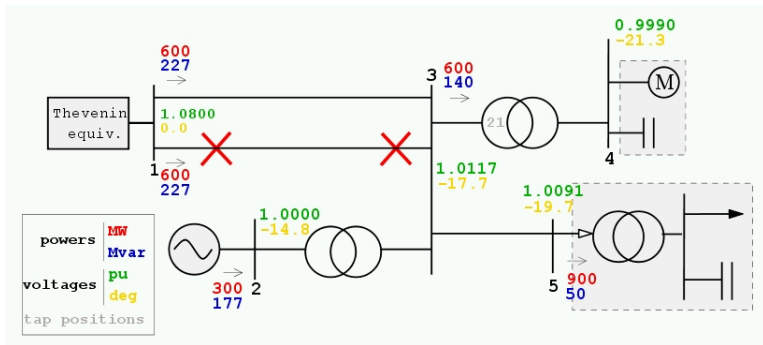


instability mechanism shown by PV curves



long-term instability \rightarrow slow system degradation \rightarrow instability of short-term dynamics (loss of synchronism) \rightarrow system collapse

Long-term voltage stability - example 4



50 % induction motor load

same disturbance

long-term instability → slow system degradation → instability of short-term dynamics (motor stalling, followed by loss of synchronism) → system collapse

