

Manipulator kinematics

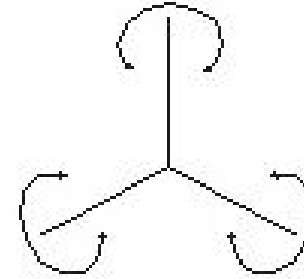
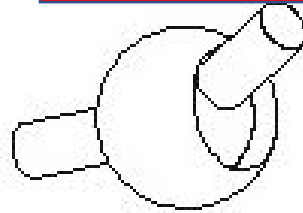
INTRODUCTION

- Kinematics is the **science of motion** that treats the subject **without regard to the forces** that cause it.
- The science of kinematics, studies the **position**, the **velocity**, the **acceleration**, and higher order derivatives of the position variables
- Hence, the study of the kinematics of manipulators refers to all **the geometrical and time-based properties of the motion**

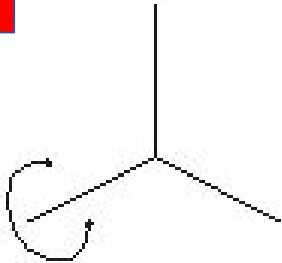
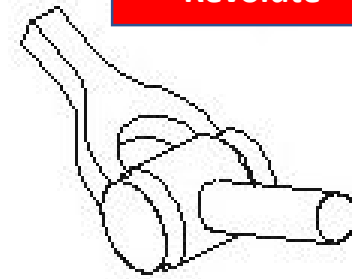
LINK DESCRIPTION

- A manipulator may be thought of as a set of **bodies connected** in a chain by **joints**.
- These bodies are called **links**.
- **Lower pair** is used to describe the connection between a pair of **bodies** when the relative motion is characterized by two surfaces sliding over one another

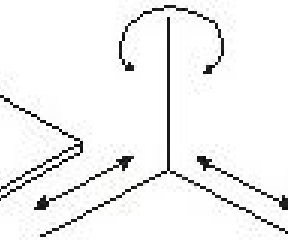
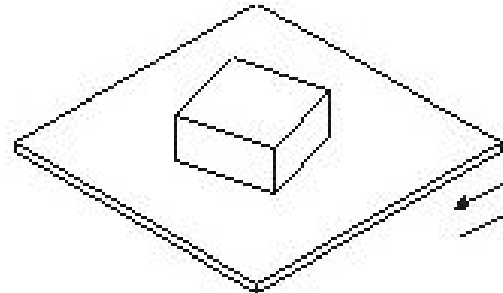
Spherical



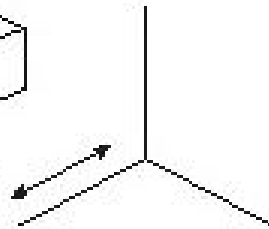
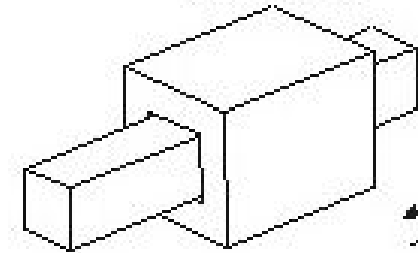
Revolute



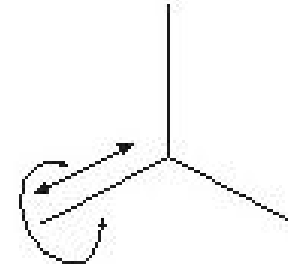
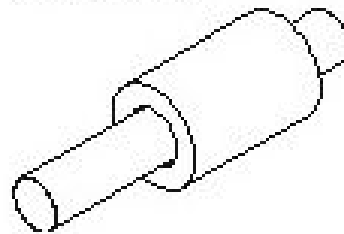
Planar



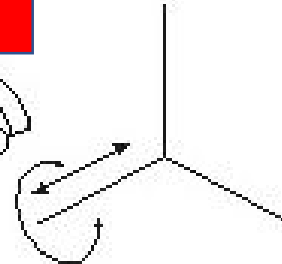
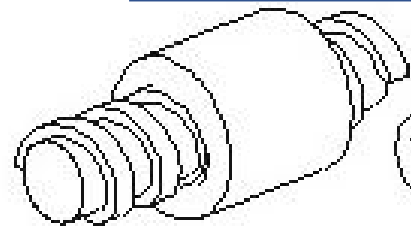
Prismatic



Cylindrical



Screw



The six possible lower-pair joints

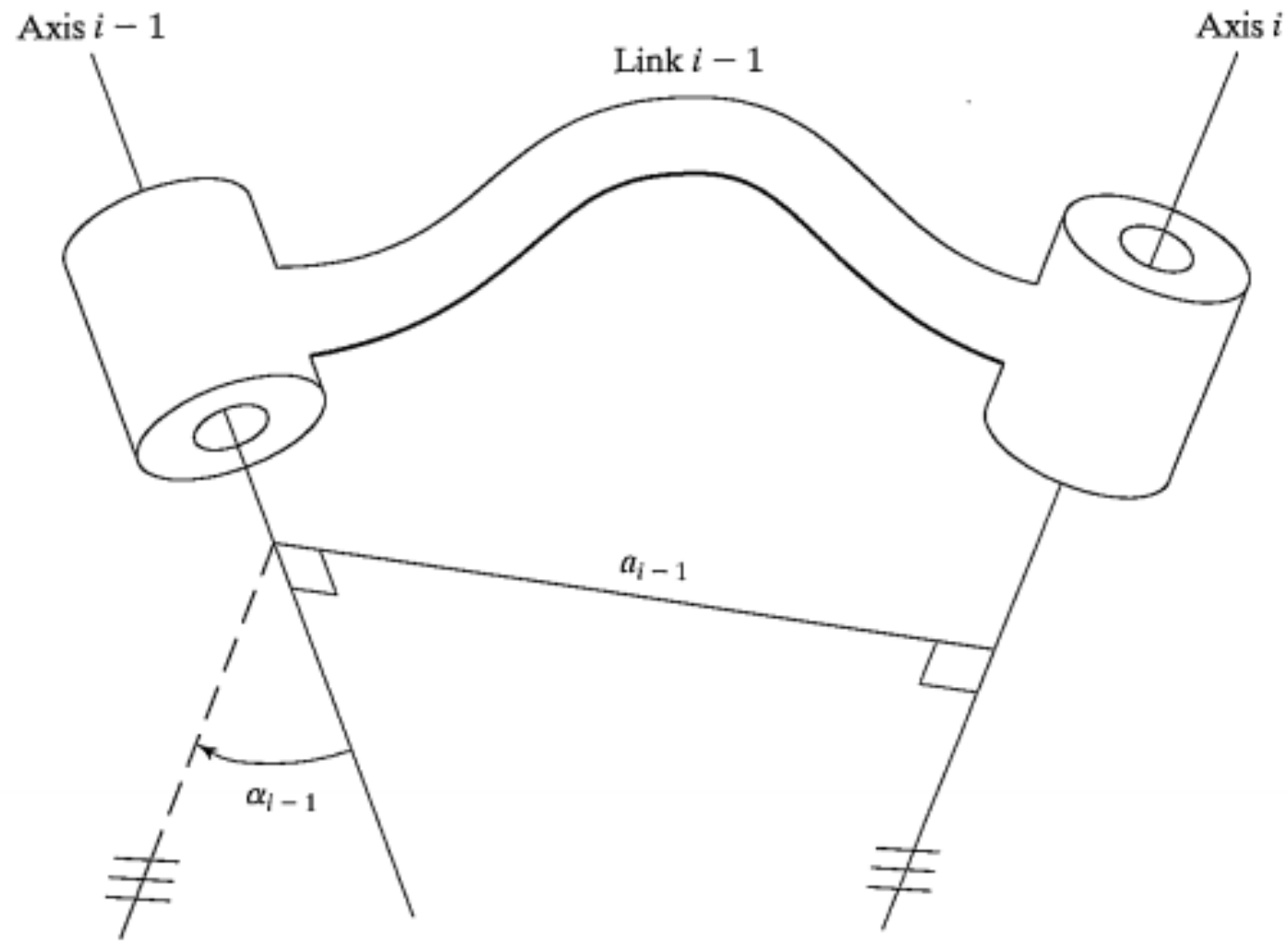
Typical link mechanical design attributes:

- The type of material used,
- The strength and stiffness of the link,
- The location and type of the joint bearings,
- The external shape,
- The weight and inertia, and more.

For obtaining kinematic equation

- *A link is considered only as a rigid body that defines the relationship between two neighboring joint axes of a manipulator.*

Link Description



The kinematic function of a link is to maintain a **fixed relationship** between the **two joint axes** it supports.

This relationship can be described with two parameters: the link length, **a** , and the link twist, **α** .

LINK-CONNECTION DESCRIPTION

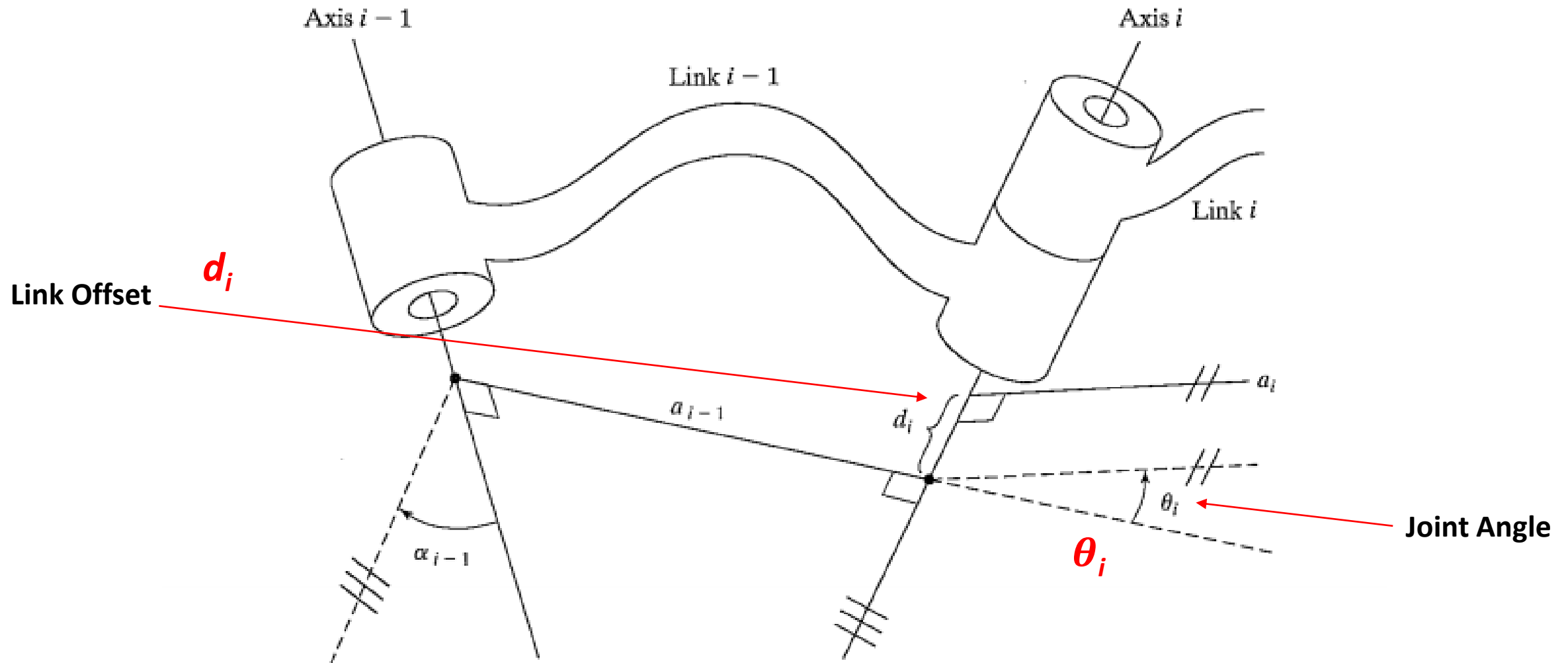


FIGURE 3.4: The link offset, d , and the joint angle, θ , are two parameters that may be used to describe the nature of the connection between neighboring links.

First and last links in the chain

- Link length, a_i and link twist α_i , depend on joint axes i and $i + 1$.
- a_1 through a_{n-1} , and α_1 to α_{n-1} are defined
- At the ends of the chain, assign zero to these quantities
- $a_0 = a_n = 0.0$ and $\alpha_0 = \alpha_n = 0$

Link parameters

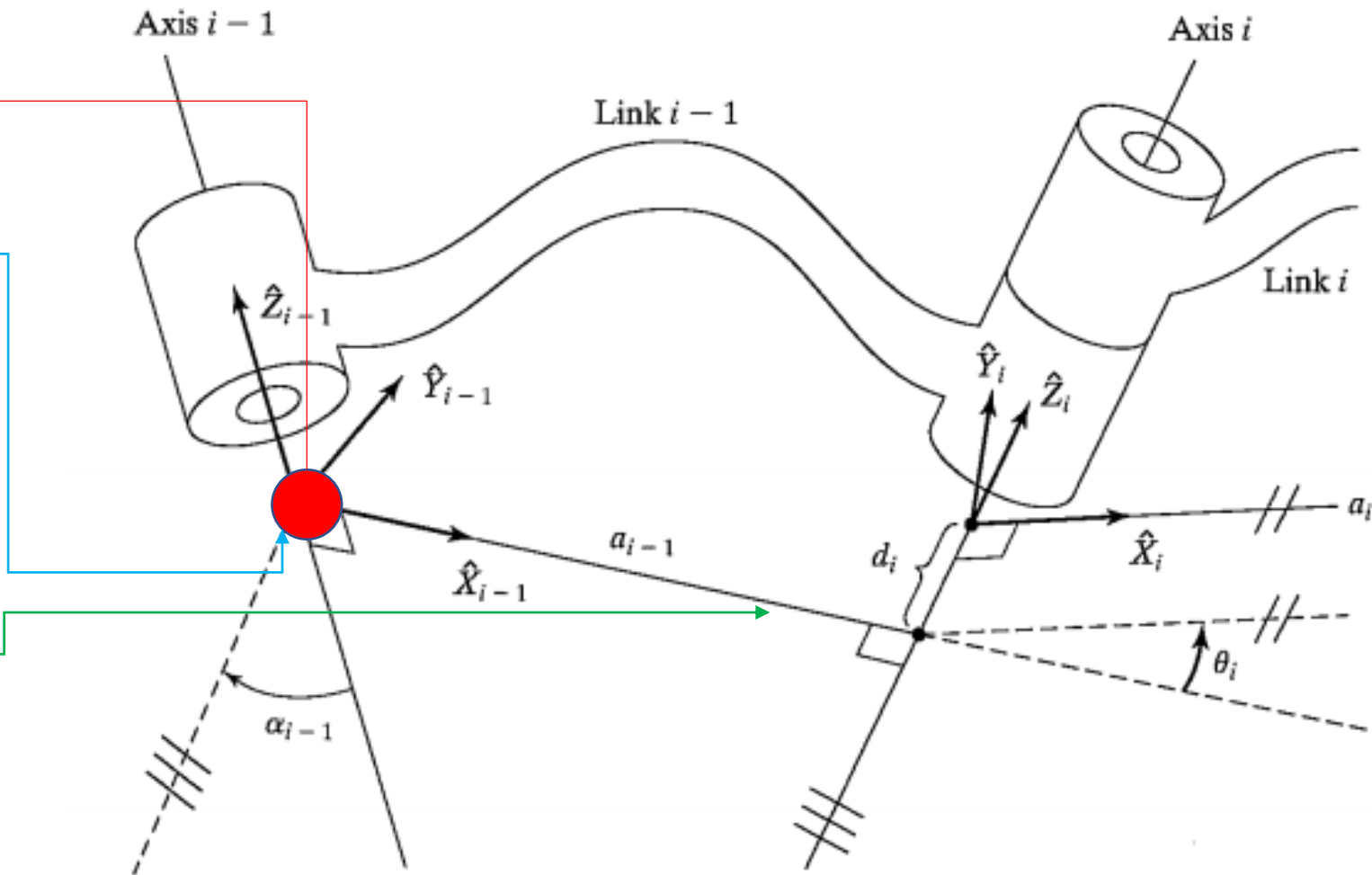
- Any robot can be described kinematically by giving the values of *four quantities* for each link
- Two describe the link itself, and two describe the link's connection to a neighboring link
- For a *revolute joint*, θ_i is called the *joint variable*, and the other three quantities would be fixed link parameters.
- For *prismatic joints*, d_i is the *joint variable*, and the other three quantities are fixed link parameters.
- The **definition** of mechanisms by means of these quantities is a convention usually called the **Denavit-Hartenberg** notation

CONVENTION FOR AFFIXING FRAMES TO LINKS

- *In order to describe the location of each link **relative to its neighbors**,*
- *we define a **frame** attached to **each link***
- *The link frames are named by number according to the link to which they are attached.*
- ***That is, frame {i} is attached rigidly to link i.***

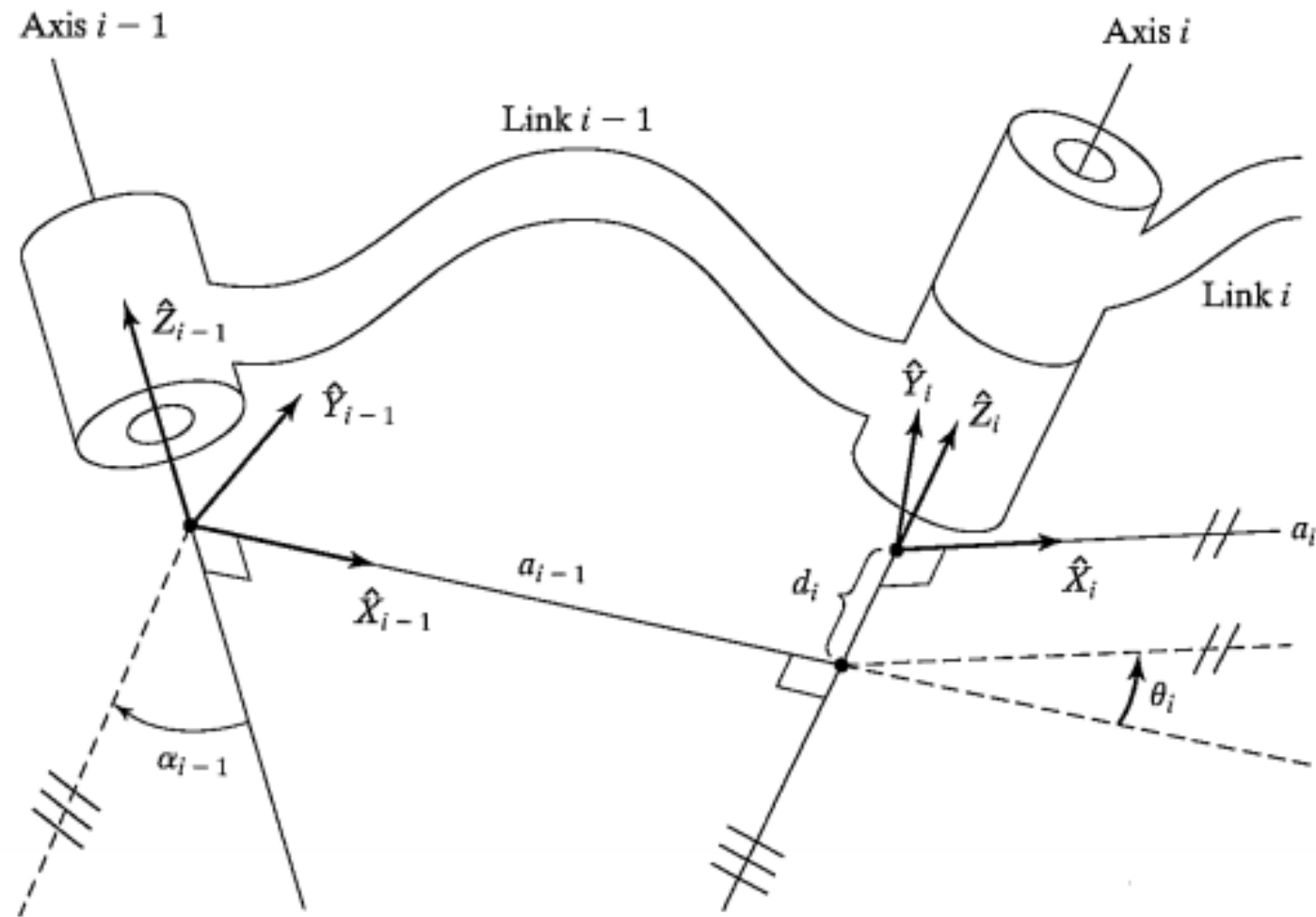
Intermediate links in the chain

- The Z-axis of frame $\{i\}$, called Z_i , is coincident with the joint axis X_i .
- The origin of frame $\{i\}$ is located where the perpendicular intersects the joint i axis.
- X_i points along a_i in the direction from joint i to joint $i + 1$.



Intermediate links in the chain

- We define α_i as being measured in the right-hand sense about \mathbf{X}_i
- \mathbf{Y}_i is formed by the right-hand rule to complete the *ith* frame.



Summary of the link parameters in terms of the link frames

- If the link frames have been attached to the links according to our convention, the following definitions of the link parameters are valid:

a_i = the distance from \hat{Z}_i to \hat{Z}_{i+1} measured along \hat{X}_i ;

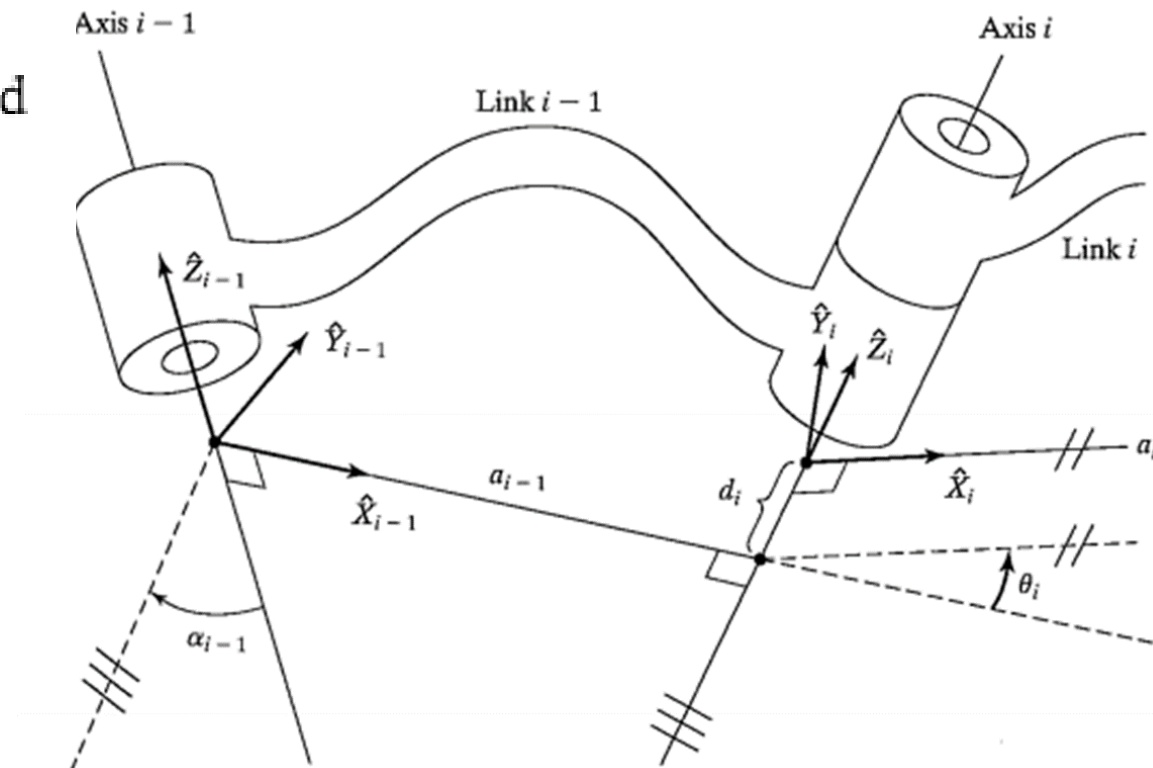
α_i = the angle from \hat{Z}_i to \hat{Z}_{i+1} measured about \hat{X}_i ;

d_i = the distance from \hat{X}_{i-1} to \hat{X}_i measured along \hat{Z}_i ; and

θ_i = the angle from \hat{X}_{i-1} to \hat{X}_i measured about \hat{Z}_i .

a, α = link Parameters

d, θ = Joint parameters



$a_i =$ the distance from \hat{Z}_i to \hat{Z}_{i+1} measured along \hat{X}_i ; }

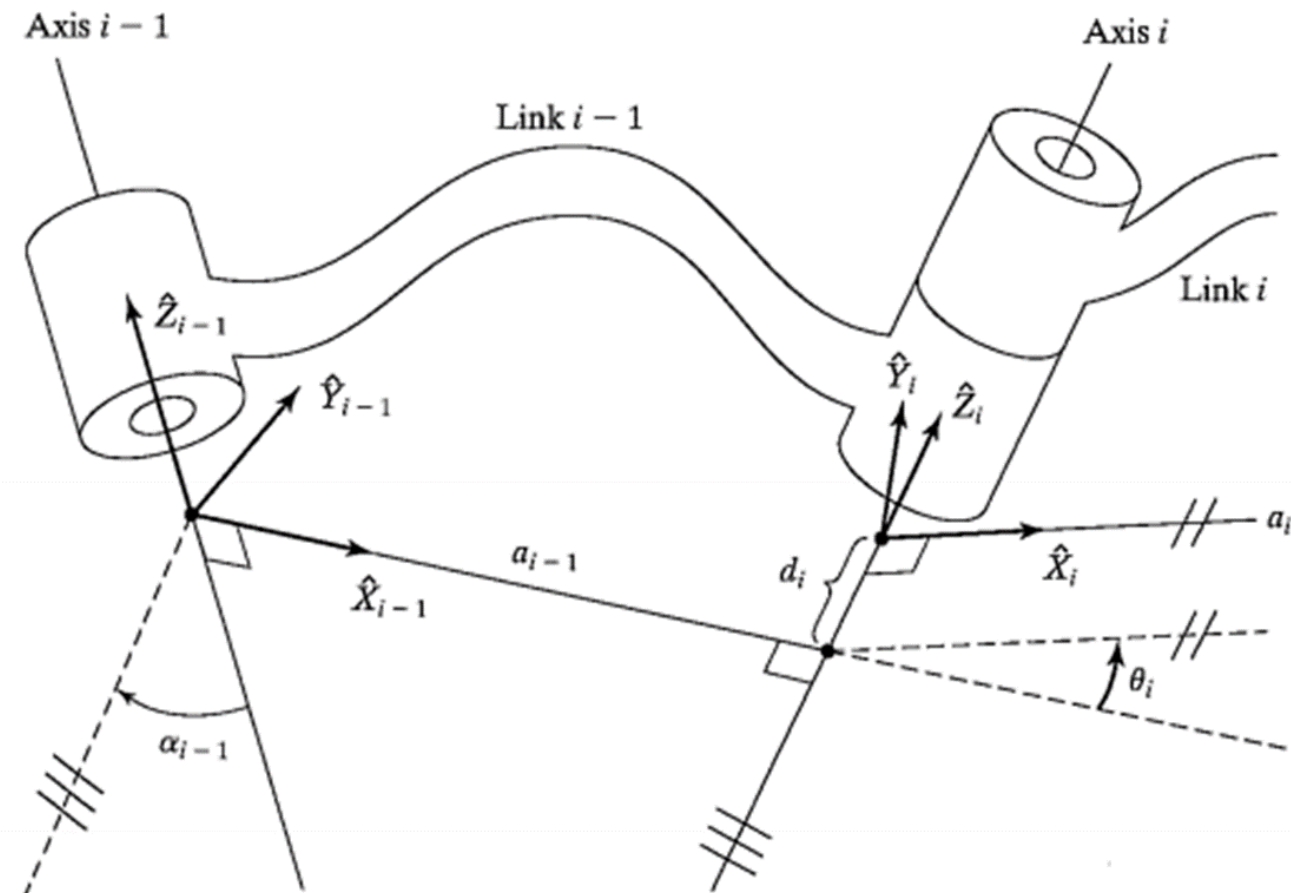
$\alpha_i =$ the angle from \hat{Z}_i to \hat{Z}_{i+1} measured about \hat{X}_i ; }

$d_i =$ the distance from \hat{X}_{i-1} to \hat{X}_i measured along \hat{Z}_i ; and }

$\theta_i =$ the angle from \hat{X}_{i-1} to \hat{X}_i measured about \hat{Z}_i .

Link

With next Link

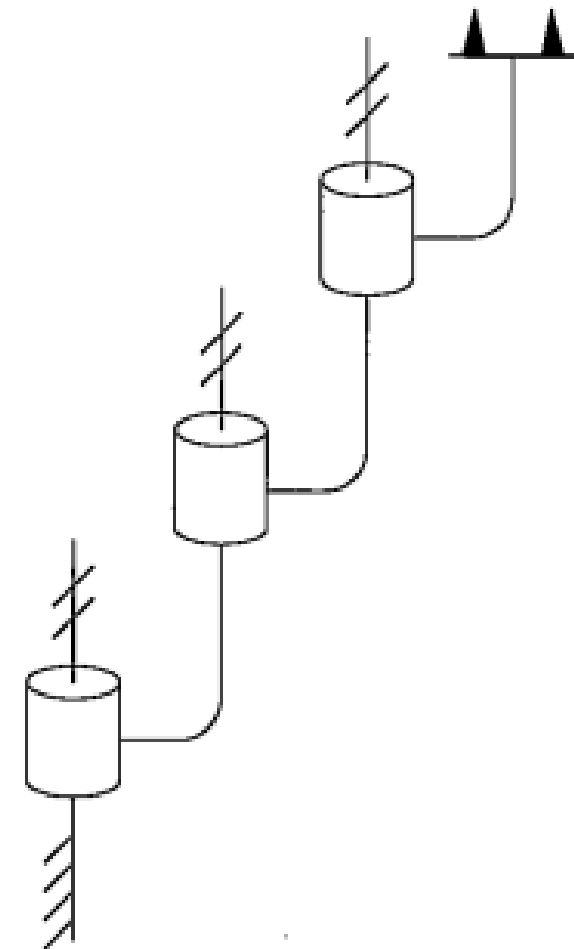
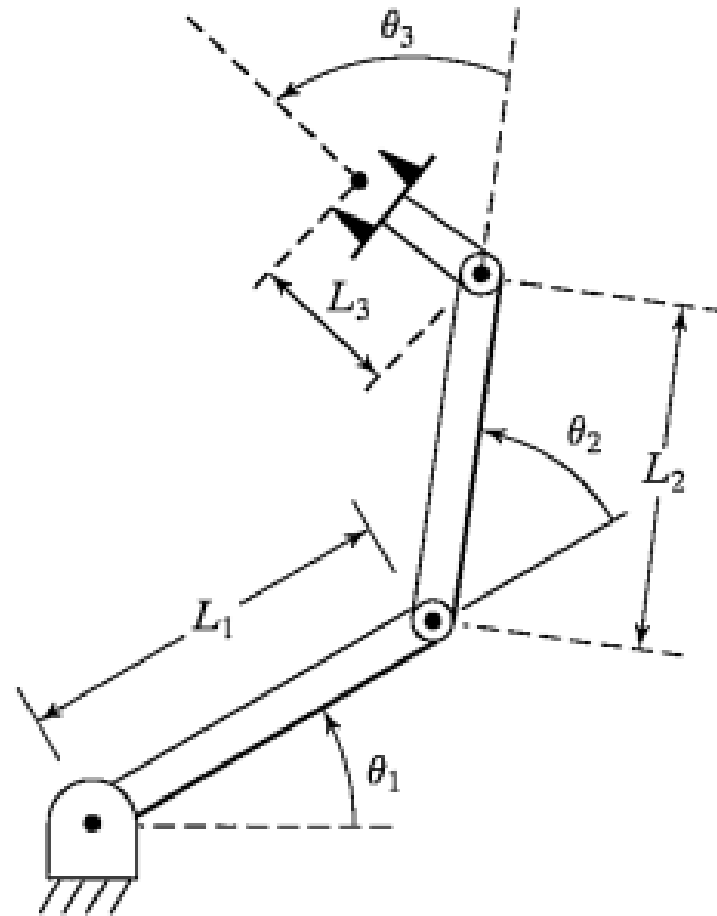


Summary of link-frame attachment procedure

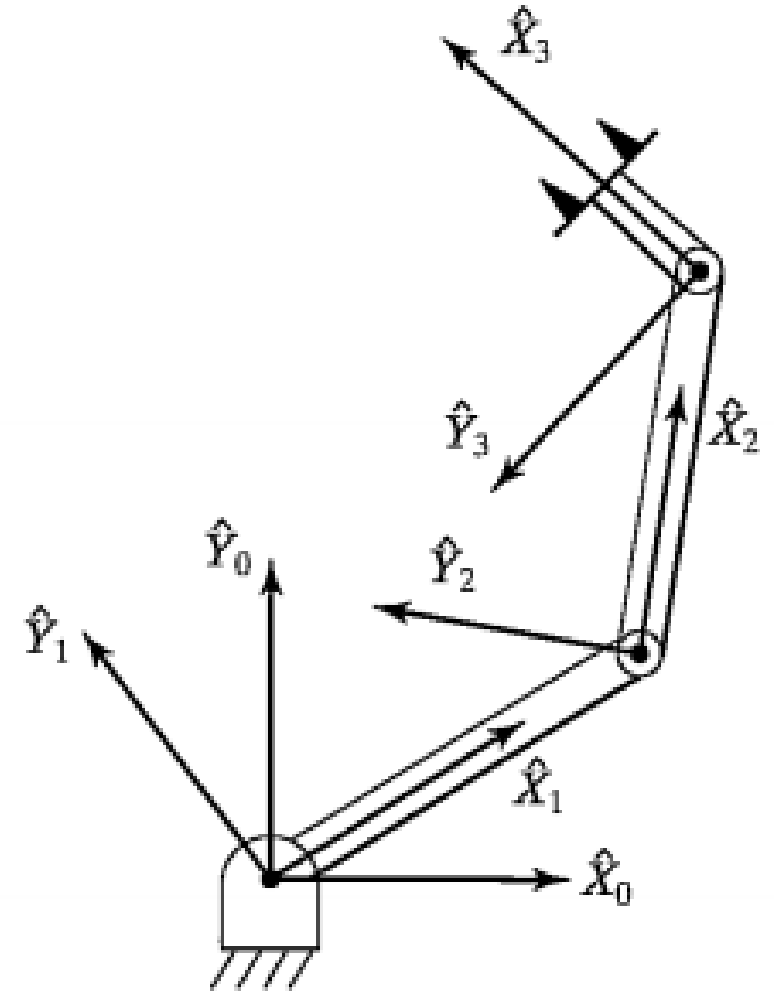
1. Identify the joint axes and imagine (or draw) infinite lines along them. For steps 2 through 5 below, consider two of these neighboring lines (at axes i and $i + 1$).
2. Identify the common perpendicular between them, or point of intersection. At the point of intersection, or at the point where the common perpendicular meets the i th axis, assign the link-frame origin.
3. Assign the \hat{Z}_i axis pointing along the i th joint axis.
4. Assign the \hat{X}_i axis pointing along the common perpendicular, or, if the axes intersect, assign \hat{X}_i to be normal to the plane containing the two axes.
5. Assign the \hat{Y}_i axis to complete a right-hand coordinate system.
6. Assign $\{0\}$ to match $\{1\}$ when the first joint variable is zero. For $\{N\}$, choose an origin location and \hat{X}_N direction freely, but generally so as to cause as many linkage parameters as possible to become zero.

- *Figure shows a three-link planar arm.*
- *all three joints are revolute, this manipulator is sometimes called an RRR (or 3R) mechanism.*

- *A three-link planar arm.*
- *On the right, the same manipulator by means of a schematic notation.*
- *Hash marks on the axes indicate that they are mutually parallel.*



- We start by defining the reference frame, frame $\{0\}$.
- It is fixed to the base and aligns with frame $\{1\}$ when the first joint variable (θ_1) is zero
- we position frame $\{0\}$ as shown in Fig. with **Z0** aligned with the joint-1 axis.



$a_i = \text{the distance from } \hat{Z}_i \text{ to } \hat{Z}_{i+1} \text{ measured along } \hat{X}_i;$
 $\alpha_i = \text{the angle from } \hat{Z}_i \text{ to } \hat{Z}_{i+1} \text{ measured about } \hat{X}_i;$
 $d_i = \text{the distance from } \hat{X}_{i-1} \text{ to } \hat{X}_i \text{ measured along } \hat{Z}_i;$ and
 $\theta_i = \text{the angle from } \hat{X}_{i-1} \text{ to } \hat{X}_i \text{ measured about } \hat{Z}_i.$

$i = i - 1$

i	α_{i-1}	a_{i-1}	d_i	θ_i
1	0	0	0	θ_1
2	0	L_1	0	θ_2
3	0	L_2	0	θ_3

$a_{i-1} = Z_{i-1} \text{ to } Z_i \mid X_{i-1}$
 $\alpha_{i-1} = Z_{i-1} \text{ to } Z_i \mid X_{i-1}$
 $d_i = X_{i-1} \text{ to } X_i \mid Z_i$
 $\theta_i = X_{i-1} \text{ to } X_i \mid Z_i$

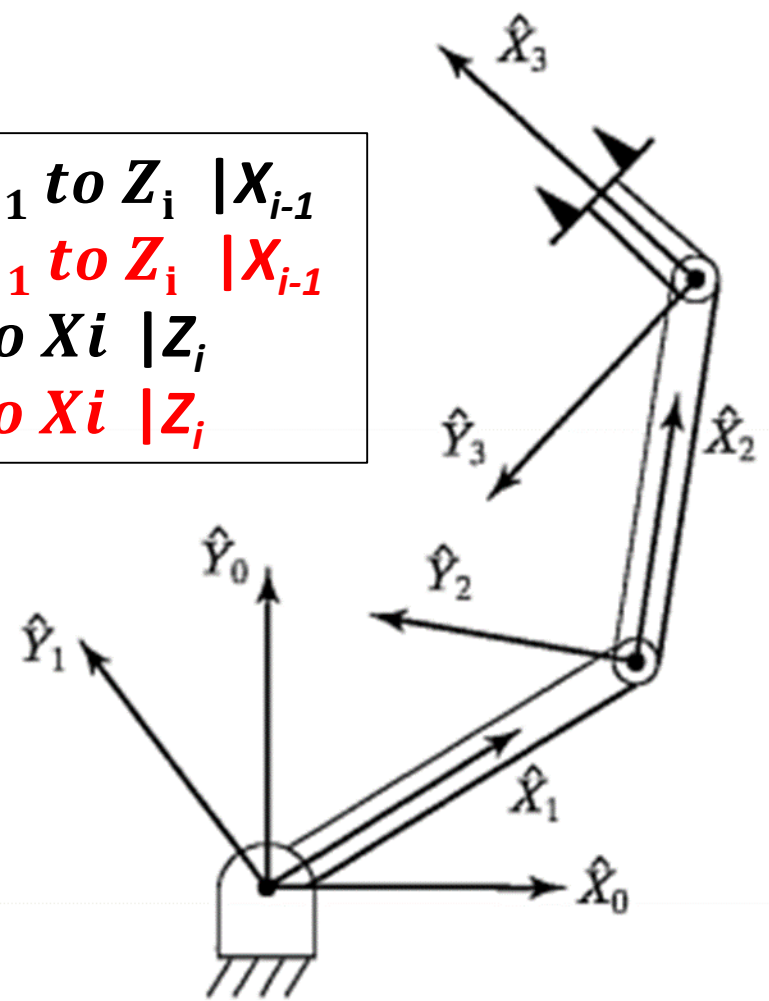
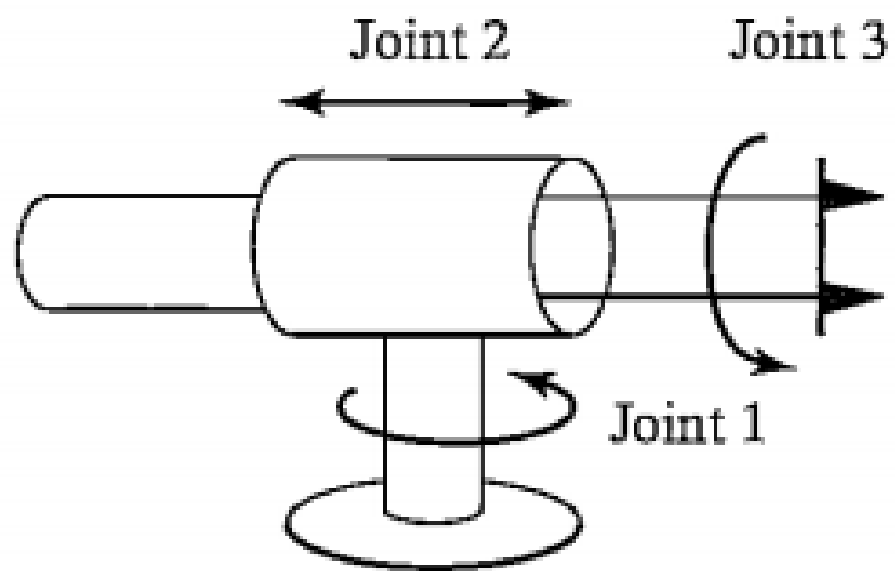
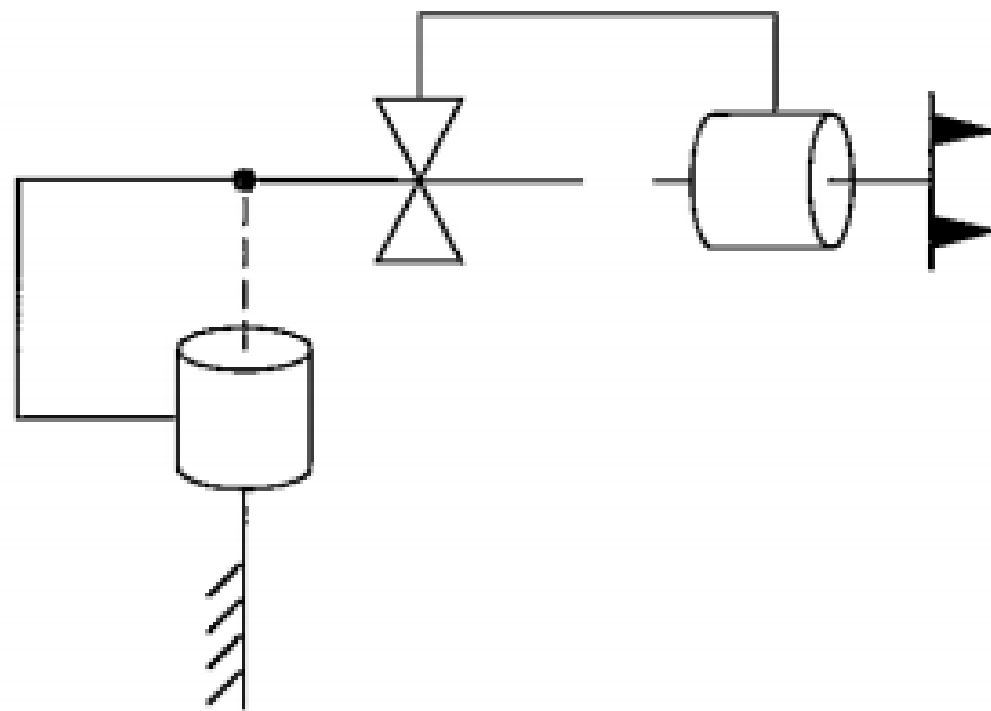


FIGURE 3.8: Link parameters of the three-link planar manipulator.

RPR mechanism



(a)



(b)

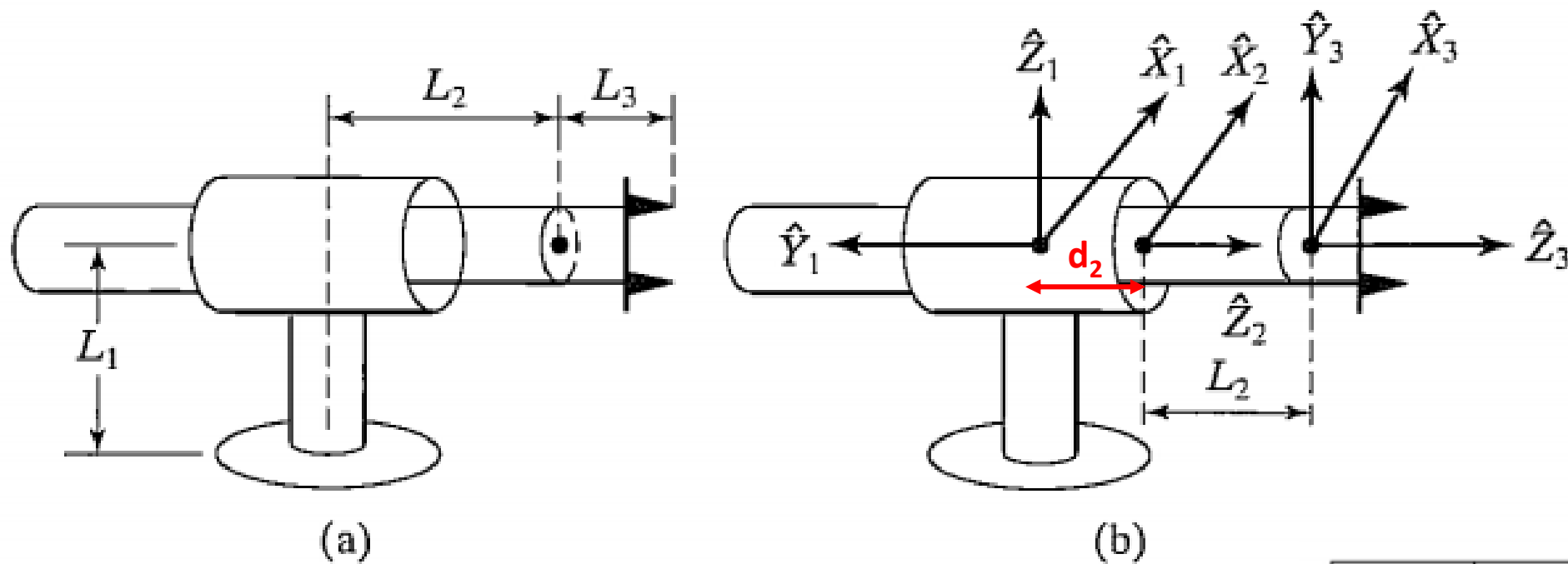


FIGURE 3.10: Link-frame assignments.

$$\begin{aligned}
 a_{i-1} &= Z_{i-1} \text{ to } Z_i \mid X_{i-1} \\
 \alpha_{i-1} &= Z_{i-1} \text{ to } Z_i \mid X_{i-1} \\
 d_i &= X_{i-1} \text{ to } X_i \mid Z_i \\
 \theta_i &= X_{i-1} \text{ to } X_i \mid Z_i
 \end{aligned}$$

i	α_{i-1}	a_{i-1}	d_i	θ_i
1	0	0	0	θ_1
2	90°	0	d_2	0
3	0	0	L_2	θ_3

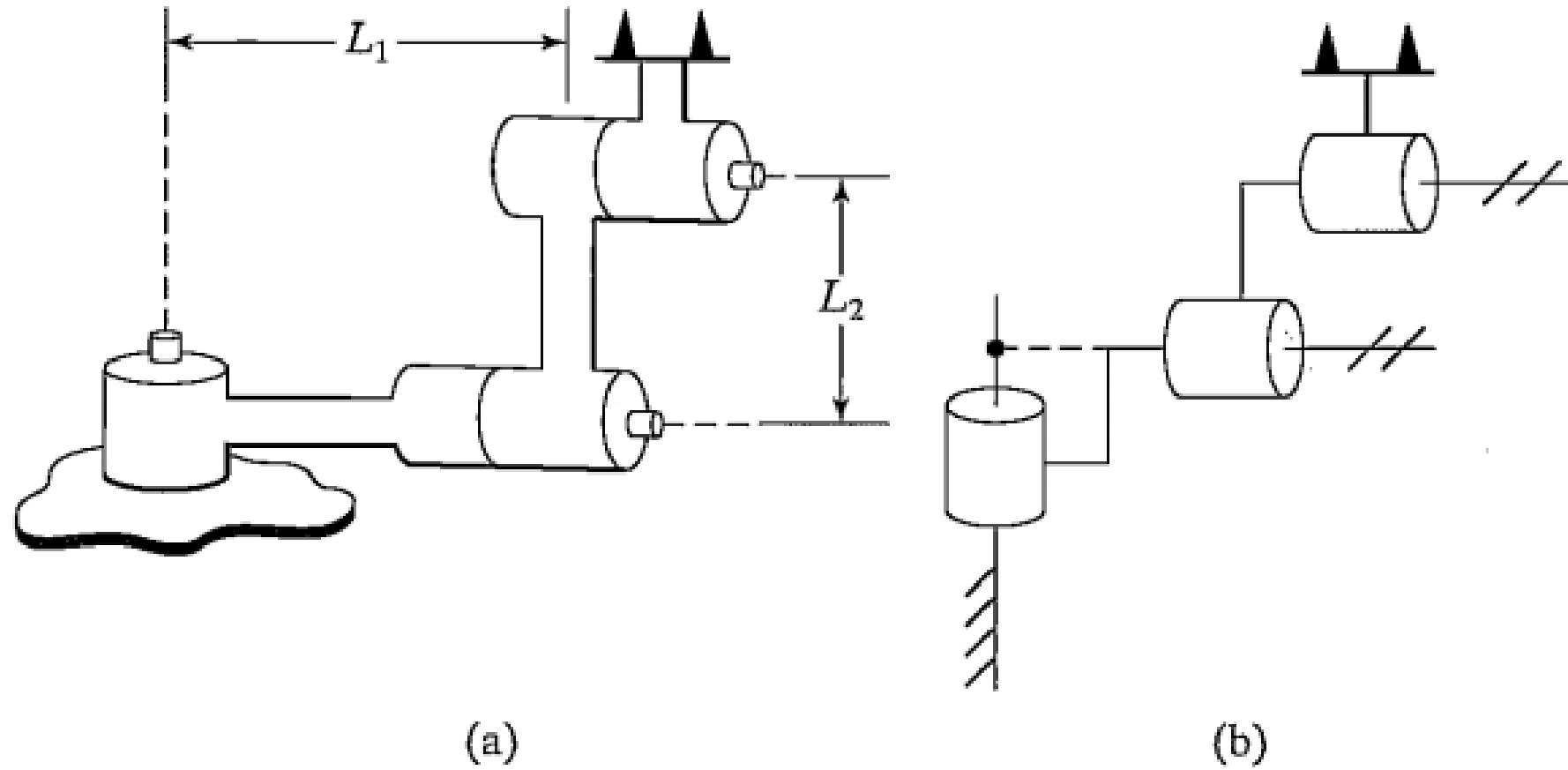
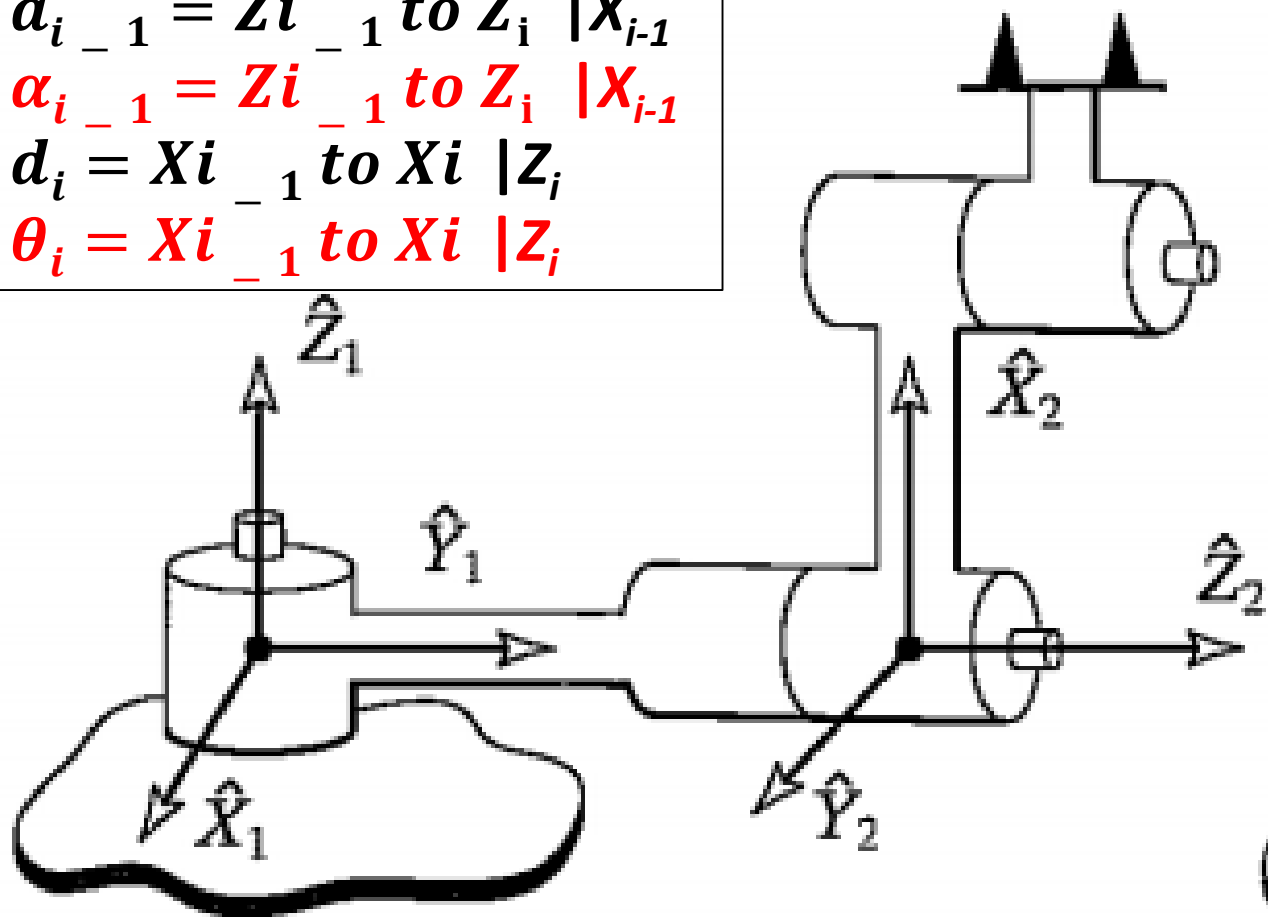


FIGURE 3.12: Three-link, nonplanar manipulator.

$$\begin{aligned}
 a_{i-1} &= Z_{i-1} \text{ to } Z_i \mid X_{i-1} \\
 \alpha_{i-1} &= Z_{i-1} \text{ to } Z_i \mid X_{i-1} \\
 d_i &= X_{i-1} \text{ to } X_i \mid Z_i \\
 \theta_i &= X_{i-1} \text{ to } X_i \mid Z_i
 \end{aligned}$$



$$a_1 = 0$$

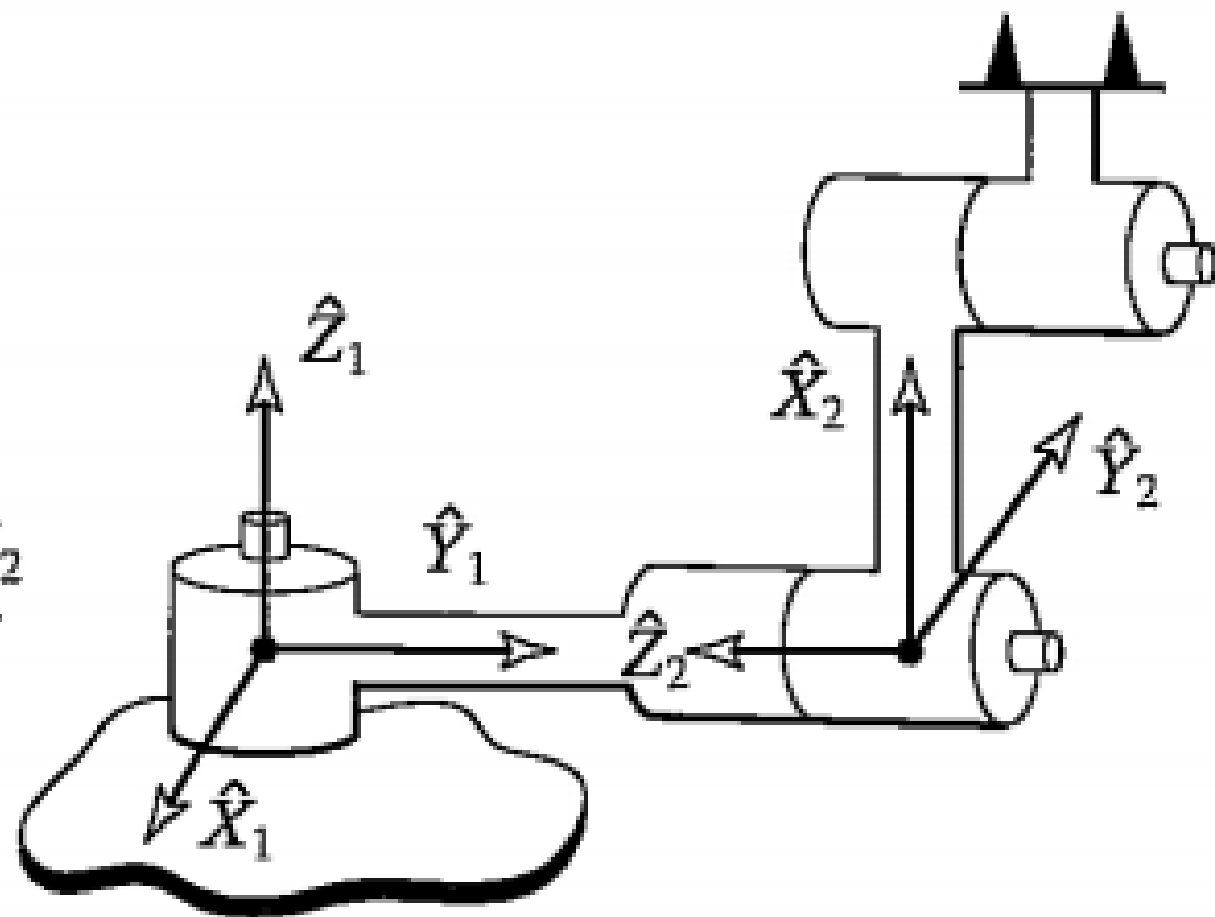
$$\alpha_1 = -90^\circ$$

$$d_1 = 0$$

$$a_2 = L_2$$

$$\alpha_2 = 0 \quad \theta_2 = -90^\circ$$

$$d_2 = L_1$$



$$a_1 = 0$$

$$\alpha_1 = 90^\circ$$

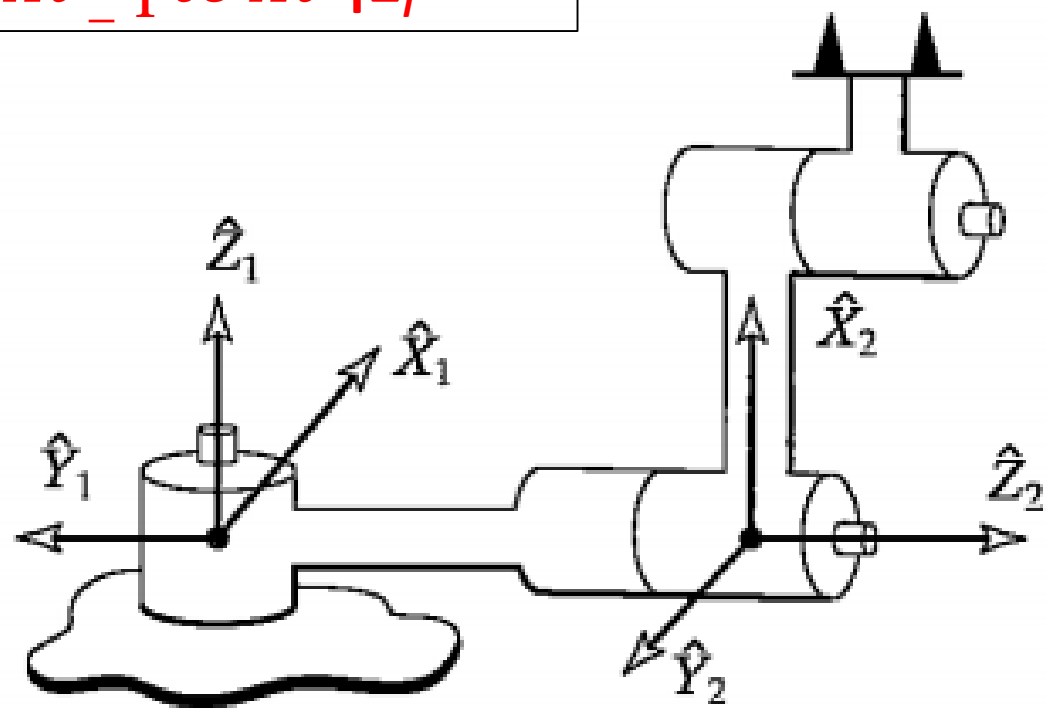
$$d_1 = 0$$

$$a_2 = L_2$$

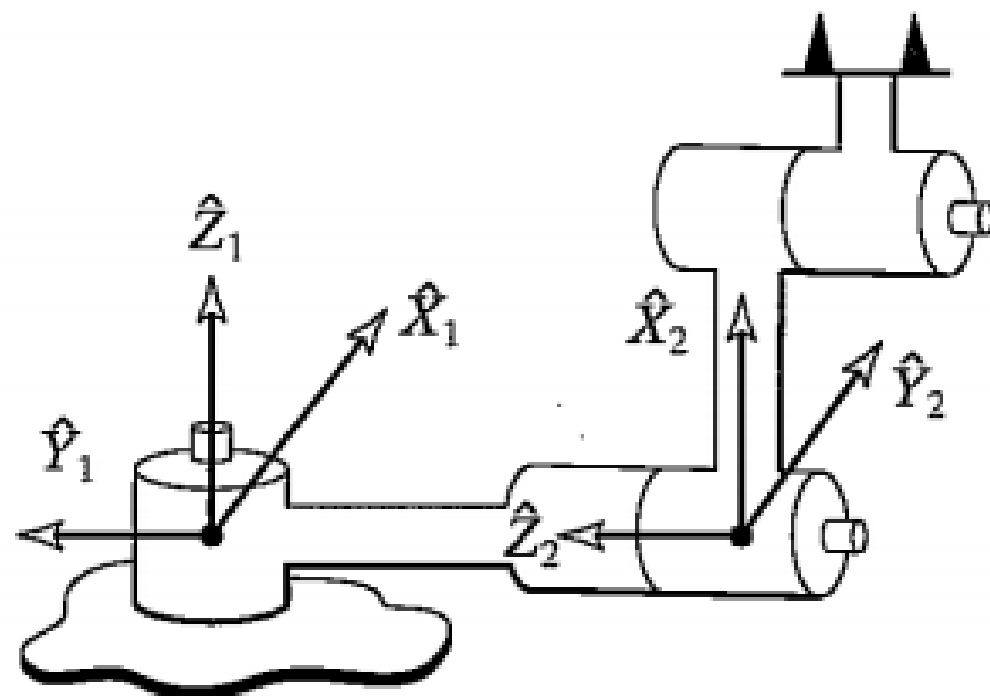
$$\alpha_2 = 0 \quad \theta_2 = 90^\circ$$

$$d_2 = -L_1$$

$$\begin{aligned}
 a_{i-1} &= Z_{i-1} \text{ to } Z_i \mid X_{i-1} \\
 \alpha_{i-1} &= Z_{i-1} \text{ to } Z_i \mid X_{i-1} \\
 d_i &= X_{i-1} \text{ to } X_i \mid Z_i \\
 \theta_i &= X_{i-1} \text{ to } X_i \mid Z_i
 \end{aligned}$$



$$\begin{aligned}
 a_1 &= 0 & a_2 &= L_2 \\
 \alpha_1 &= 90^\circ & \alpha_2 &= 0 & \theta_2 &= 90^\circ \\
 d_1 &= 0 & d_2 &= L_1
 \end{aligned}$$

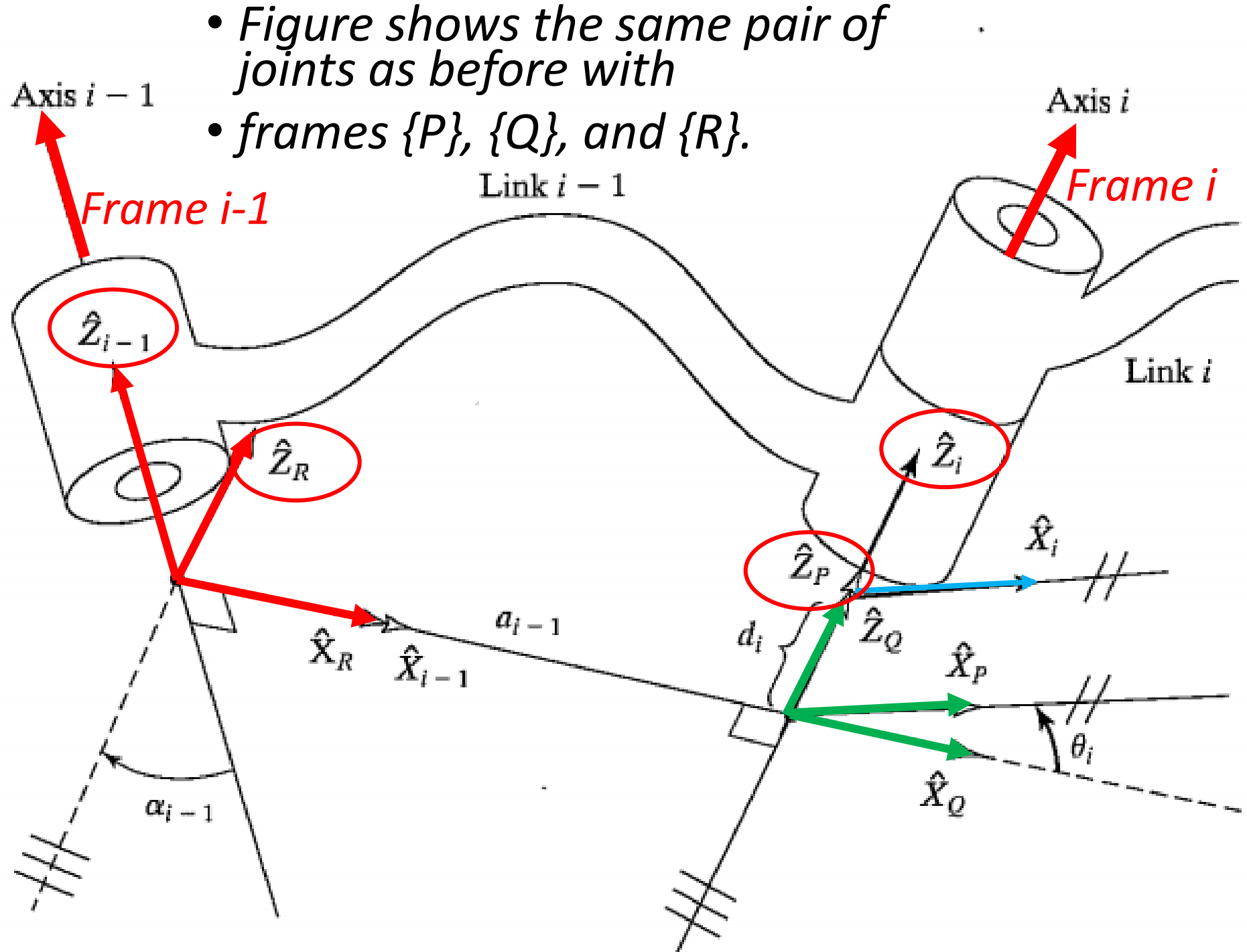


$$\begin{aligned}
 a_1 &= 0 & a_2 &= L_2 \\
 \alpha_1 &= -90^\circ & \alpha_2 &= 0 & \theta_2 &= -90^\circ \\
 d_1 &= 0 & d_2 &= -L_1
 \end{aligned}$$

Derivation of link transformations

- We wish to construct the **Transform** that defines frame $\{i\}$ relative to the frame $\{i - 1\}$.
- Function of the **four** link parameters.
- For any given robot, this transformation will be a function of **only one variable**, the other three parameters being fixed by mechanical design.
- In order to solve each of these subproblems, ${}^{i-1}_iT$ we will further break each subproblem **into four sub subproblems**.

- Frame $\{R\}$ differs from frame $\{i-1\}$ only by a rotation of α_{i-1}
- Frame $\{Q\}$ differs from $\{R\}$ by a translation a_{i-1}
- Frame $\{P\}$ differs from $\{Q\}$ by a rotation θ_i
- And frame $\{i\}$ differs from $\{P\}$ by a translation d_i .



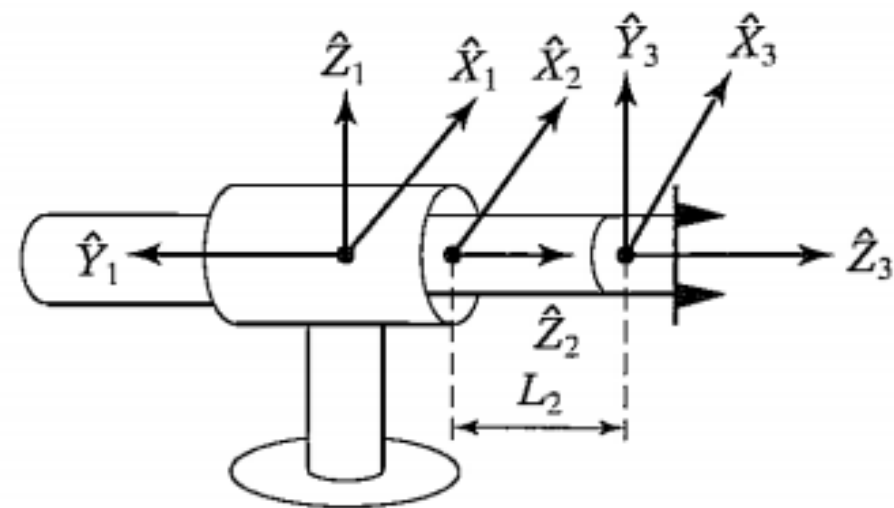
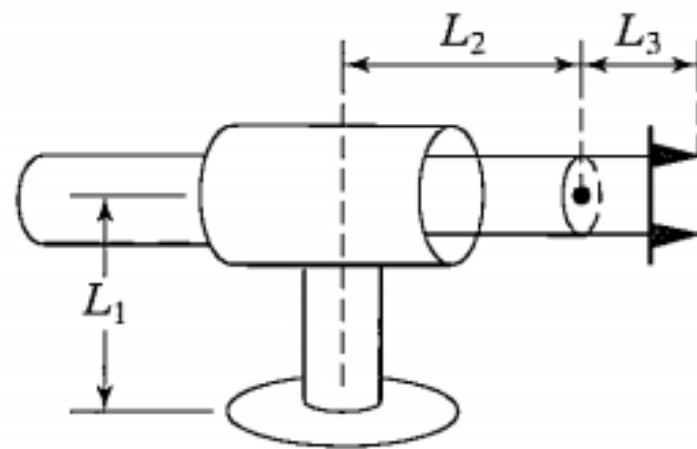
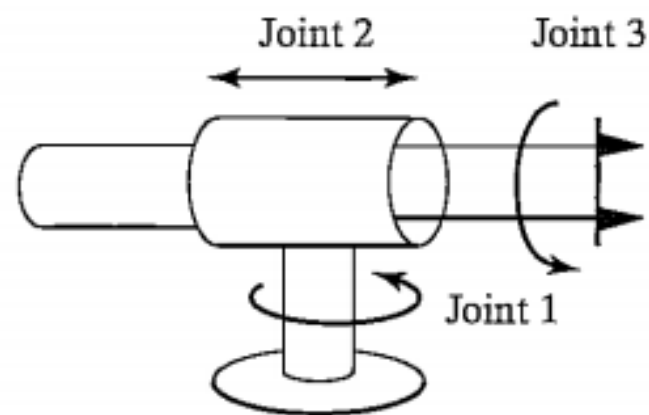
$${}^{i-1}\mathbf{P} = {}^{i-1}_R\mathbf{T} \mathbf{}^R_Q\mathbf{T} \mathbf{}^Q_P\mathbf{T} \mathbf{}^P_i\mathbf{T} \mathbf{}^i\mathbf{P}$$

$${}^{i-1}\mathbf{P} = {}^{i-1}_i\mathbf{T} \mathbf{}^i\mathbf{P}$$

$${}^{i-1}_i\mathbf{T} = {}^{i-1}_R\mathbf{T} \mathbf{}^R_Q\mathbf{T} \mathbf{}^Q_P\mathbf{T} \mathbf{}^P_i\mathbf{T}$$

$${}^{i-1}_i\mathbf{T} = R_X(\alpha_{i-1}) D_X(a_{i-1}) R_Z(\theta_i) D_Z(d_i)$$

$${}^{i-1}_i\mathbf{T} = \begin{bmatrix} c\theta_i & -s\theta_i & 0 & a_{i-1} \\ s\theta_i c\alpha_{i-1} & c\theta_i c\alpha_{i-1} & -s\alpha_{i-1} & -s\alpha_{i-1}d_i \\ s\theta_i s\alpha_{i-1} & c\theta_i s\alpha_{i-1} & c\alpha_{i-1} & c\alpha_{i-1}d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}.$$



(a)

i	α_{i-1}	a_{i-1}	d_i	θ_i
1	0	0	0	θ_1
2	90°	0	d_2	0
3	0	0	L_2	θ_3

$${}^{i-1}_i T = \begin{bmatrix} c\theta_i & -s\theta_i & 0 & a_{i-1} \\ s\theta_i c\alpha_{i-1} & c\theta_i c\alpha_{i-1} & -s\alpha_{i-1} & -s\alpha_{i-1} d_i \\ s\theta_i s\alpha_{i-1} & c\theta_i s\alpha_{i-1} & c\alpha_{i-1} & c\alpha_{i-1} d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0_1 T = \begin{bmatrix} c\theta_1 & -s\theta_1 & 0 & 0 \\ s\theta_1 & c\theta_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

$${}^1_2 T = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & -d_2 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

$${}^2_3 T = \begin{bmatrix} c\theta_3 & -s\theta_3 & 0 & 0 \\ s\theta_3 & c\theta_3 & 0 & 0 \\ 0 & 0 & 1 & l_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}.$$

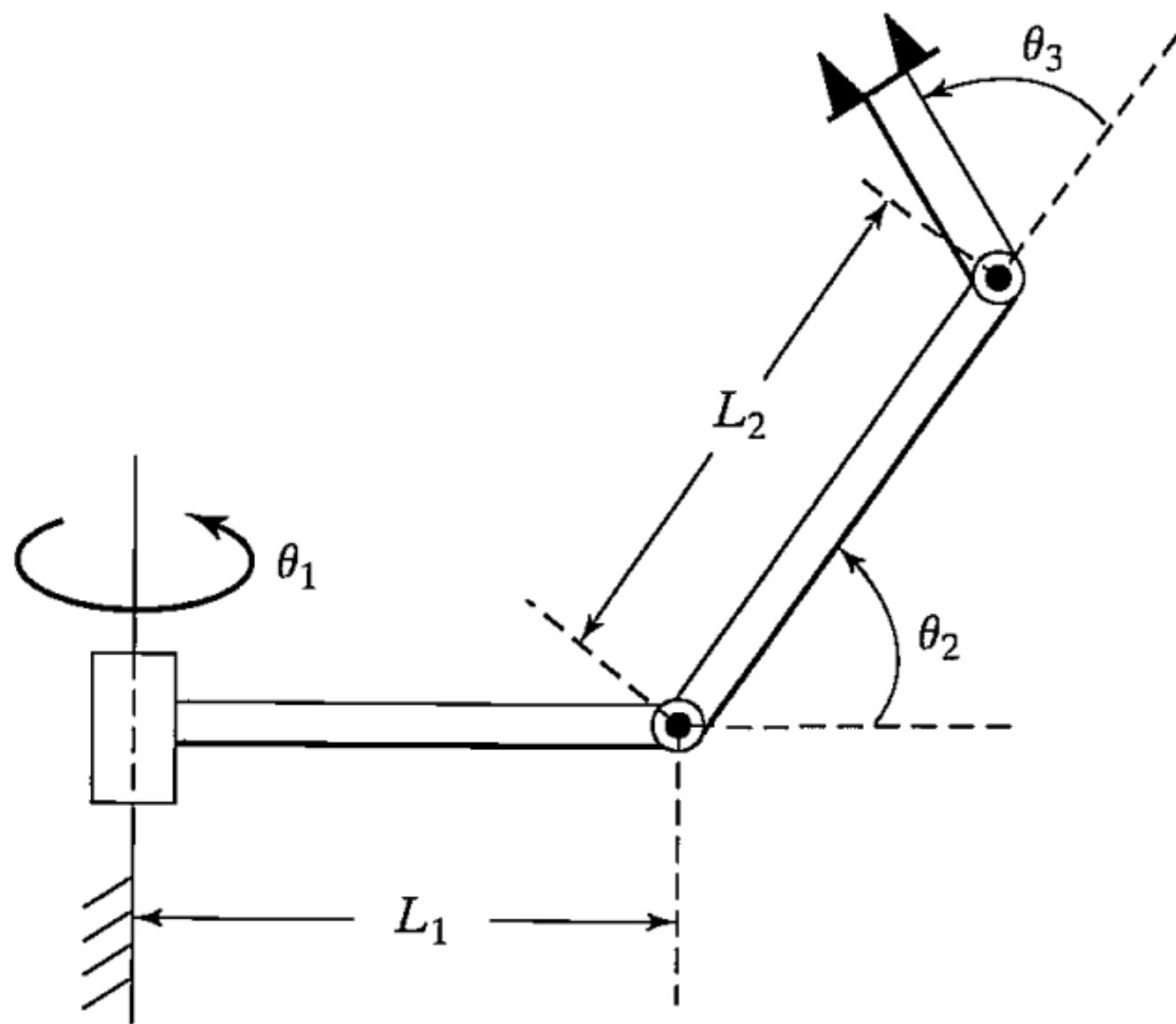
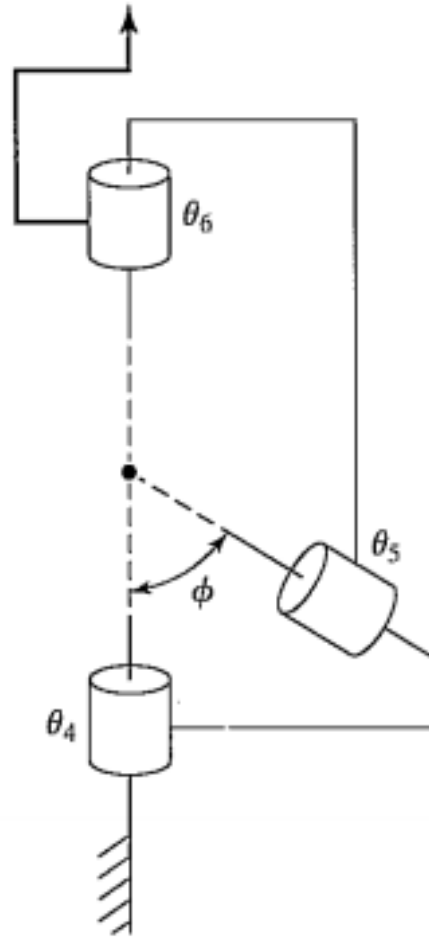
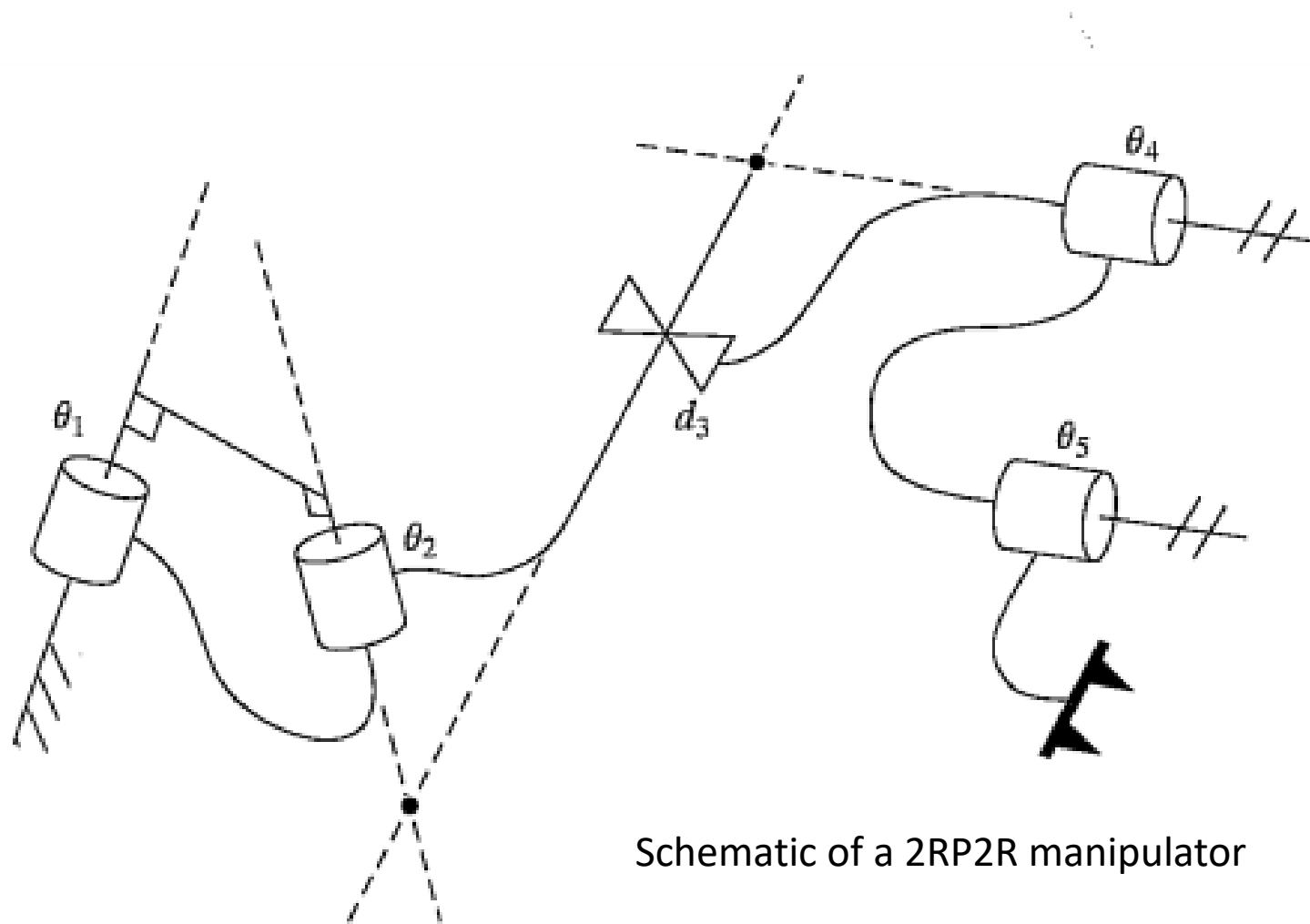


Figure shows the schematic of a wrist which has three intersecting axes that are not orthogonal. Assign link frames to this wrist, and give the link parameters.



Show the attachment of link frames for the 3-DOF manipulator shown schematically in Fig.



Schematic of a 2RP2R manipulator

Show the attachment of link frames for the 3-DOF manipulator shown schematically in Fig.

