

# Nonlinear finite-element model to analyze a bolted assembly

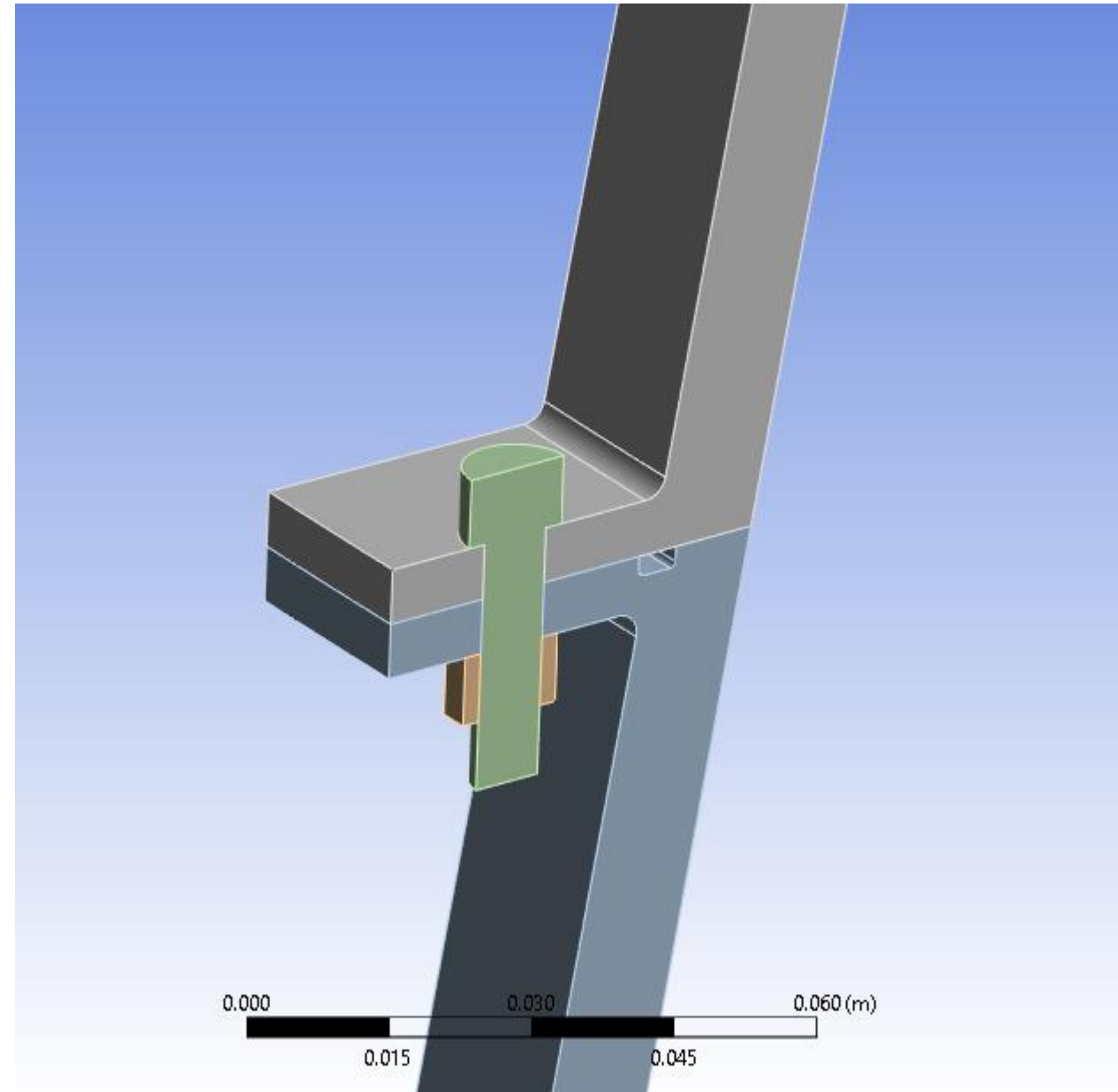
A study on the F1 Engine

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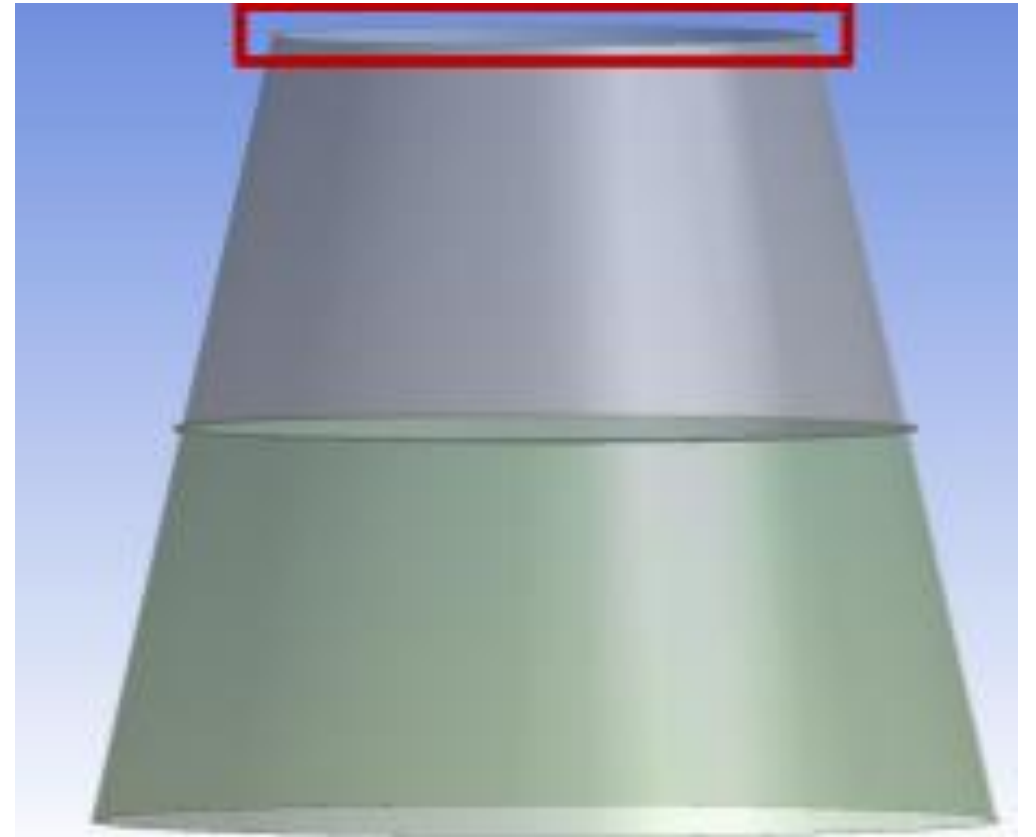
# Geometry

- The model considers only half of a bolt and nut.
- Axial symmetry can be used to find the results for the whole domain
  - Assume that all thermal and structural loads, and material properties are axially symmetric
- Parts:
  - Mid Nozzle
  - Lower Nozzle
  - Bolt
  - Nut



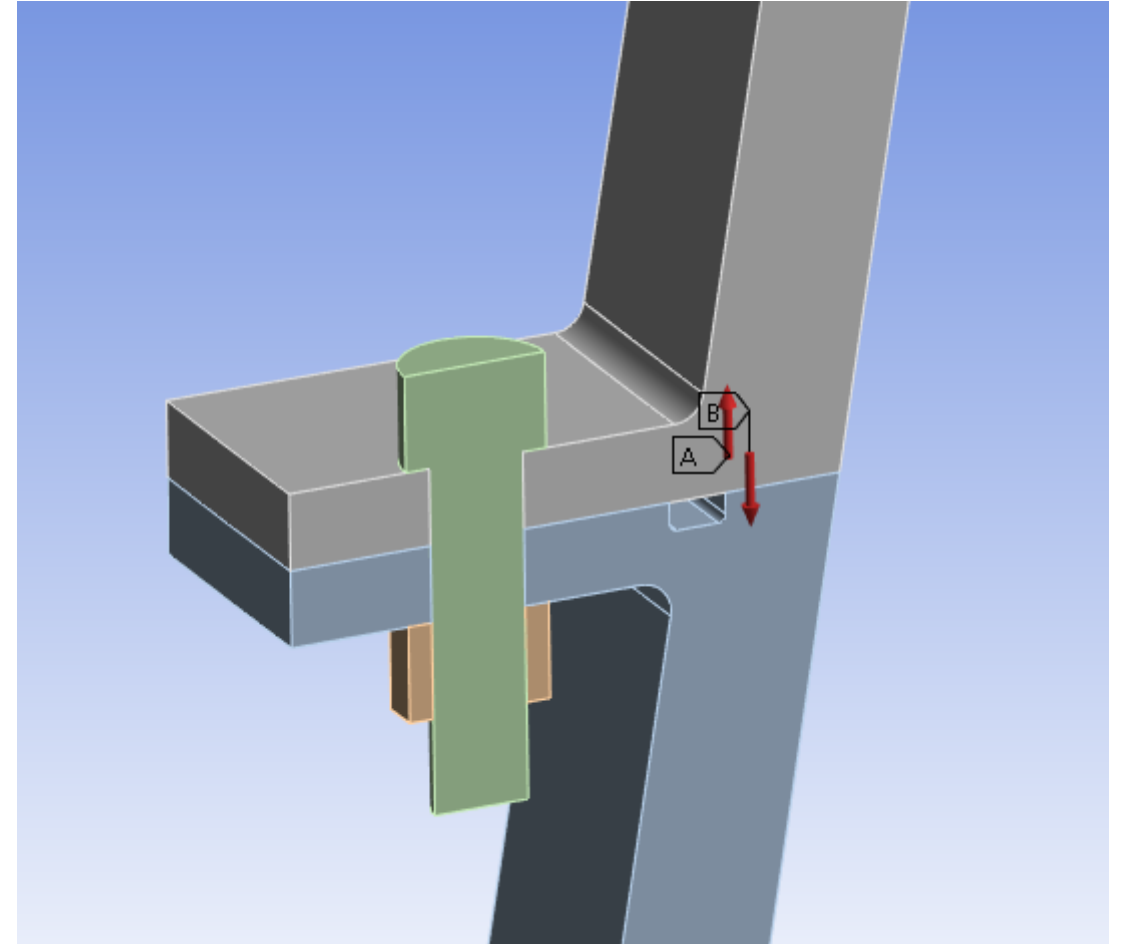
# Boundary conditions (1/2)

- Frictionless support on the top of the mid nozzle
  - This implies that there is not displacement and tangential traction, which approximates the connection to the upper nozzle, which is not considered in the model



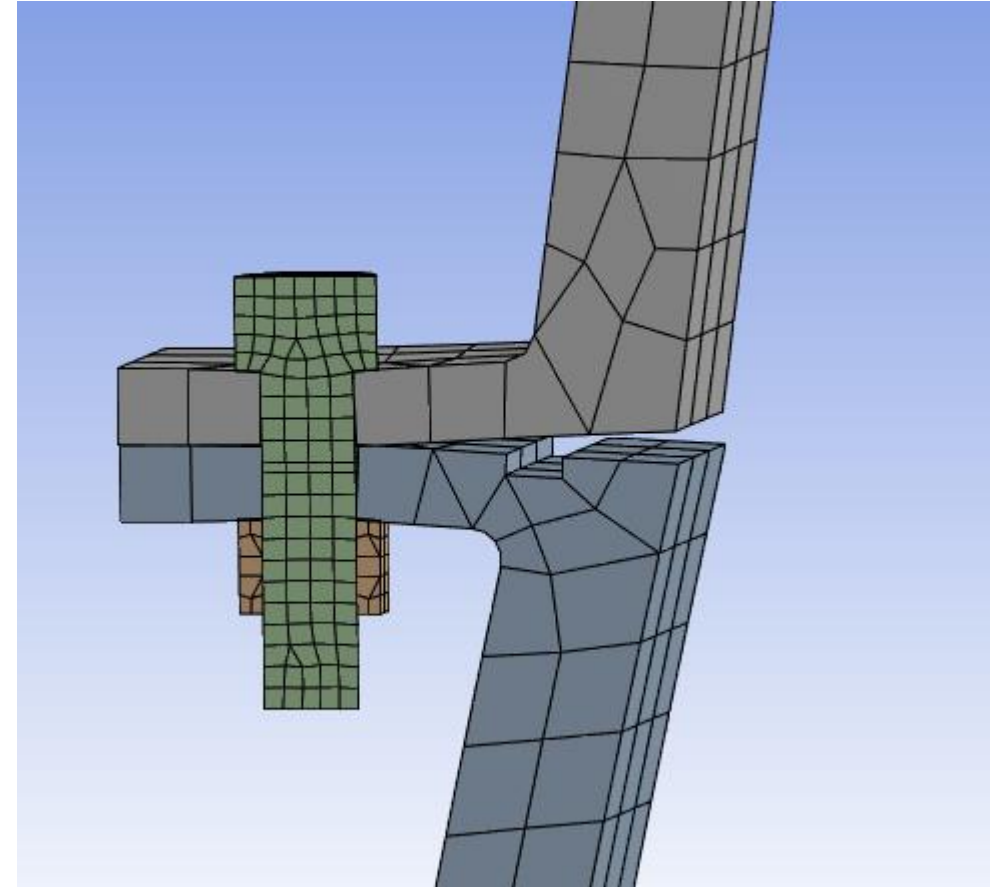
# Boundary conditions (2/3): Cooling channel pressure

- Calculated using 1D thermal analysis
- $F = 1000 \text{ lbf}$
- The coolant applies the force on both lower and upper nozzle



# Boundary condition (3/3): Pressure from the hot gas

- It acts on both the internal surface of the nozzle, but also on the surface that will be exposed after deformation due to the cooling channel pressure
- Need to set traction=0 to allow these surfaces to move during the simulation



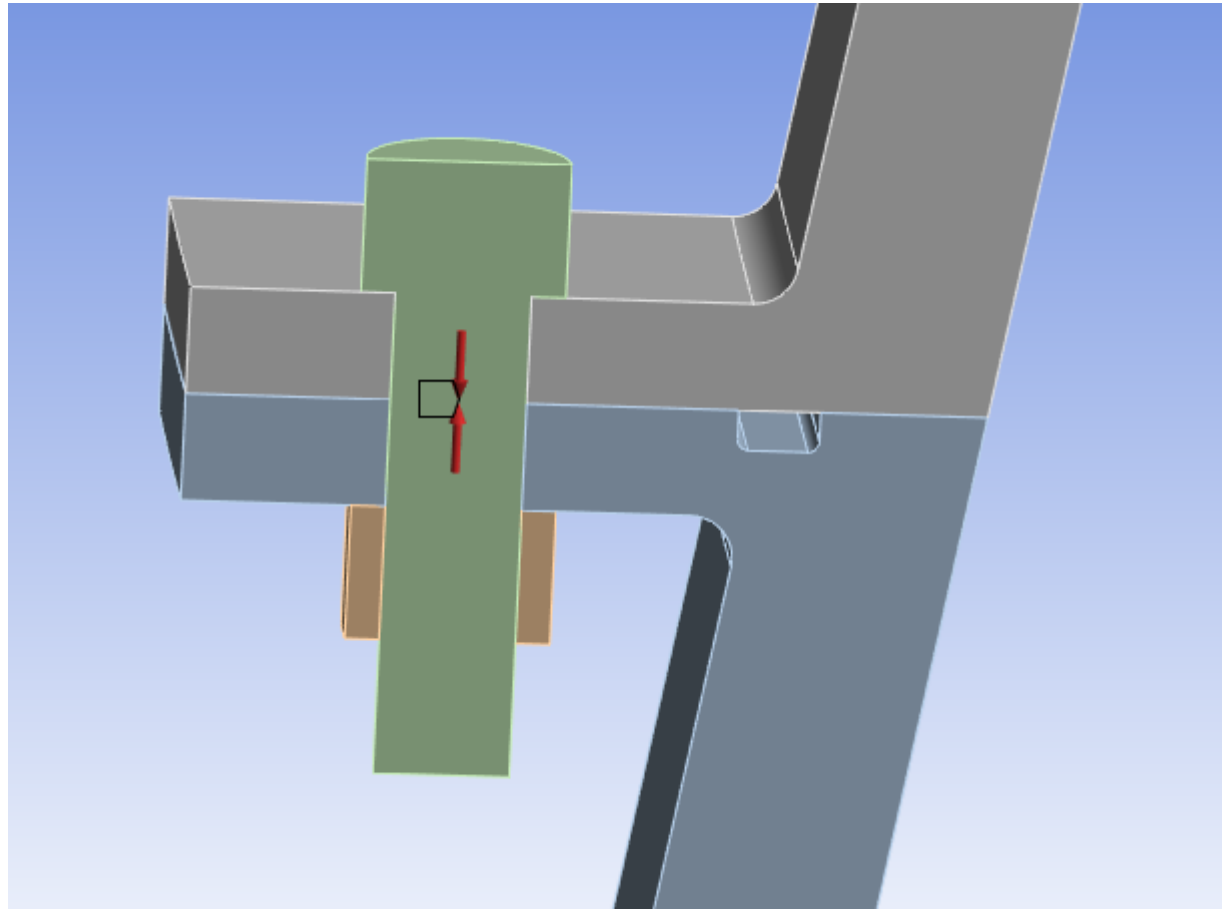
The deformation shown in this image is 2 times bigger for better visibility

# Boundary condition (4/4): Thermal load

- Body subject to hot gas temperature
- $T = 700\text{ F}$ 
  - This is the temperature at the wall on the gas side
  - It was found starting from the hot gas recovery temperature and the heat transfer coefficient (found with the Bartz correlation)

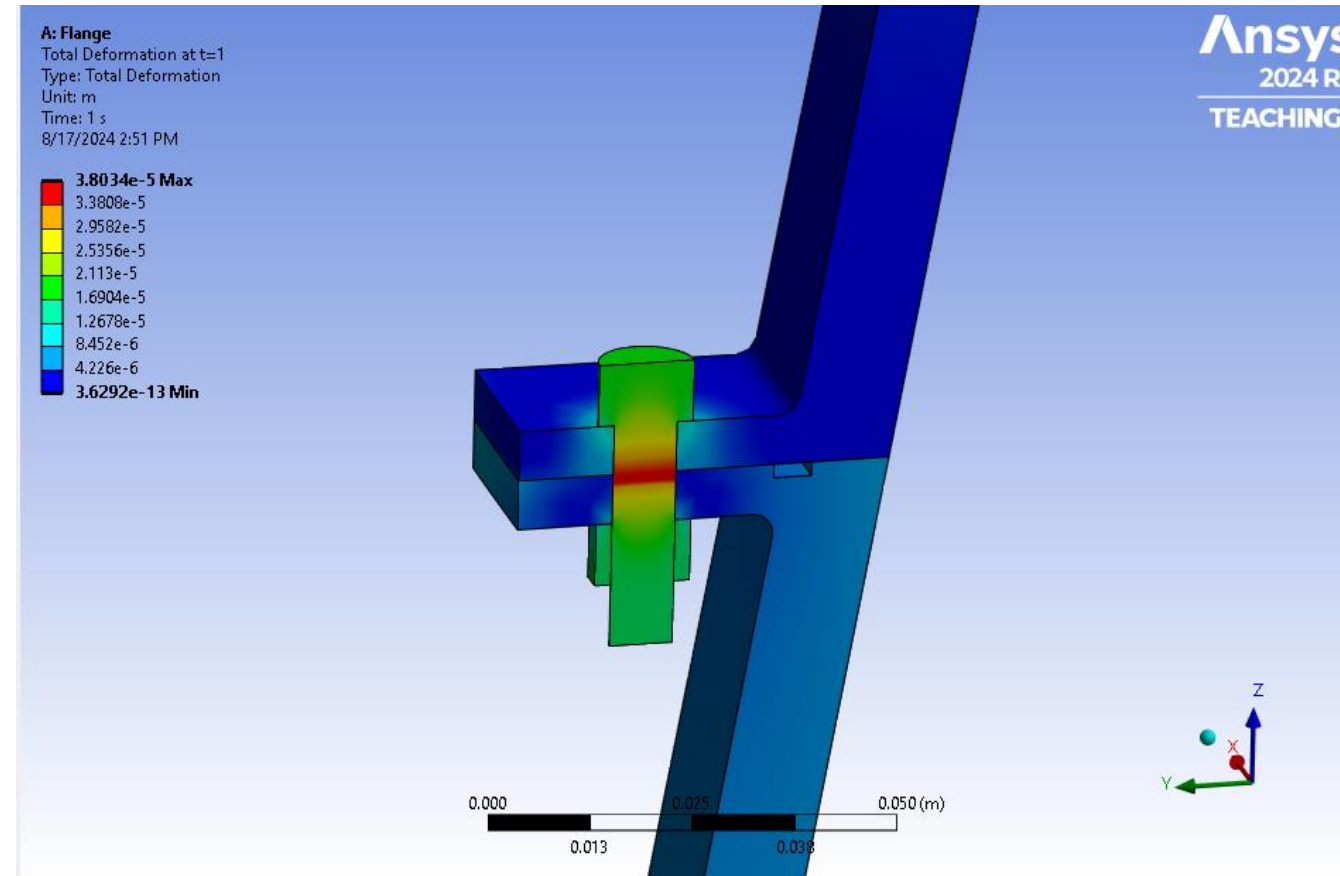
# Bolt preload

- 2320 lbf



# Deformation at $t=1$ (only bolt preload)

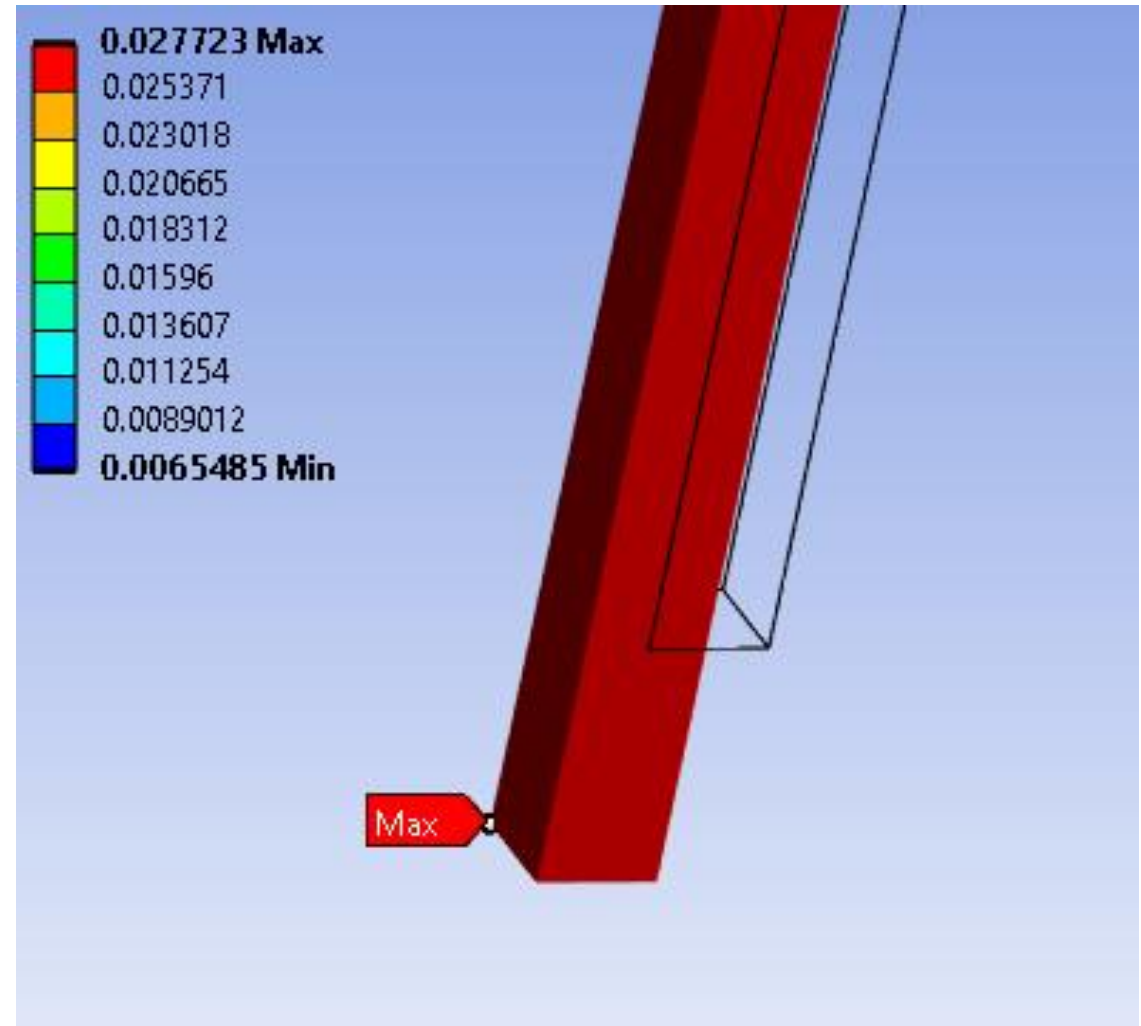
- Loads at  $t=1$ :
  - Bolt preload
- Nozzle doesn't have high deformation, which was expected
- The bolt pretension is visible





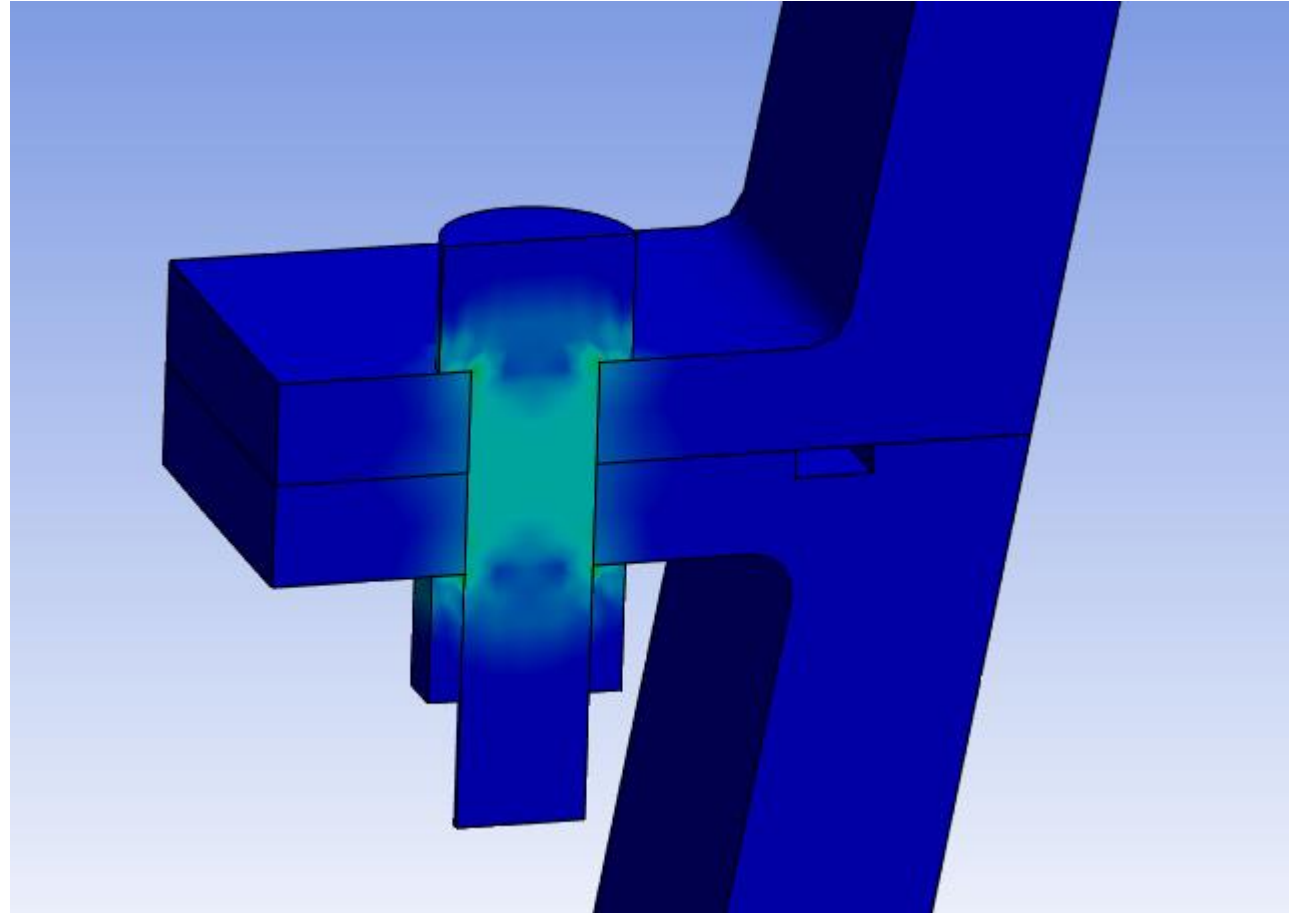
# Deformation at $t = 3$

- Additional Loads:
  - Thermal expansion due to hot gas
  - Coolant pressure
- The nozzle grows radially, and axially
- Total deformation is 0.0277 m (1.09 inches)
- The hoop stress at the nozzle exit (calculated using the normal stress) is 1672 psi < 30,000 psi, which is the yield strength of 300 stainless steel



# Equivalent stress at t=1 (Bolt pretension)

- Maximum stress in the bolt is:  $1.26 \times 10^5$  psi
- This is lower than the bolt capability which is  $1.60 \times 10^5$  psi (A-286 steel)



# Model validation

- Nozzle thermal expansion

$$DL = \alpha * DT * L = 1e-5[1/F] * (700\text{ F} - 30\text{ F}) * 160\text{ in} = 1.008\text{ in}$$

ANSYS predicted thermal expansion = 1.09 in

- Hoop stress

$$\text{Sigma} = P * r / t$$

$$P = 12.17\text{ psi}$$

$$r = 69.5\text{ in}$$

$$t = 0.5\text{ in}$$

$$\text{Sigma} = 1692\text{ psi}$$

ANSYS predicted hoop stress : 1672 psi